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It should be noted that most of the pages are identifiable as having been processed by me.

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I put a lot of time into producing these files which is why you are met with this page when you open the file.

In order to generate this file, I need to scan the pages, split the double pages and remove any edge marks such as punch holes, clean up the pages, set the relevant pages to be all the same size and alignment. I then run Omnipage (OCR) to generate the searchable text and then generate the pdf file.

Hopefully after all that, I end up with a presentable file. If you find missing pages, pages in the wrong order, anything else wrong with the file or simply want to make a comment, please drop me a line (see above).

It is my hope that you find the file of use to you personally – I know that I would have liked to have found some of these files years ago – they would have saved me a lot of time !

Colin Hinson

In the village of Blunham, Bedfordshire.

Form 27 (Small)

**ROYAL AIR FORCE**

CHL

**SKETCH BOOK**

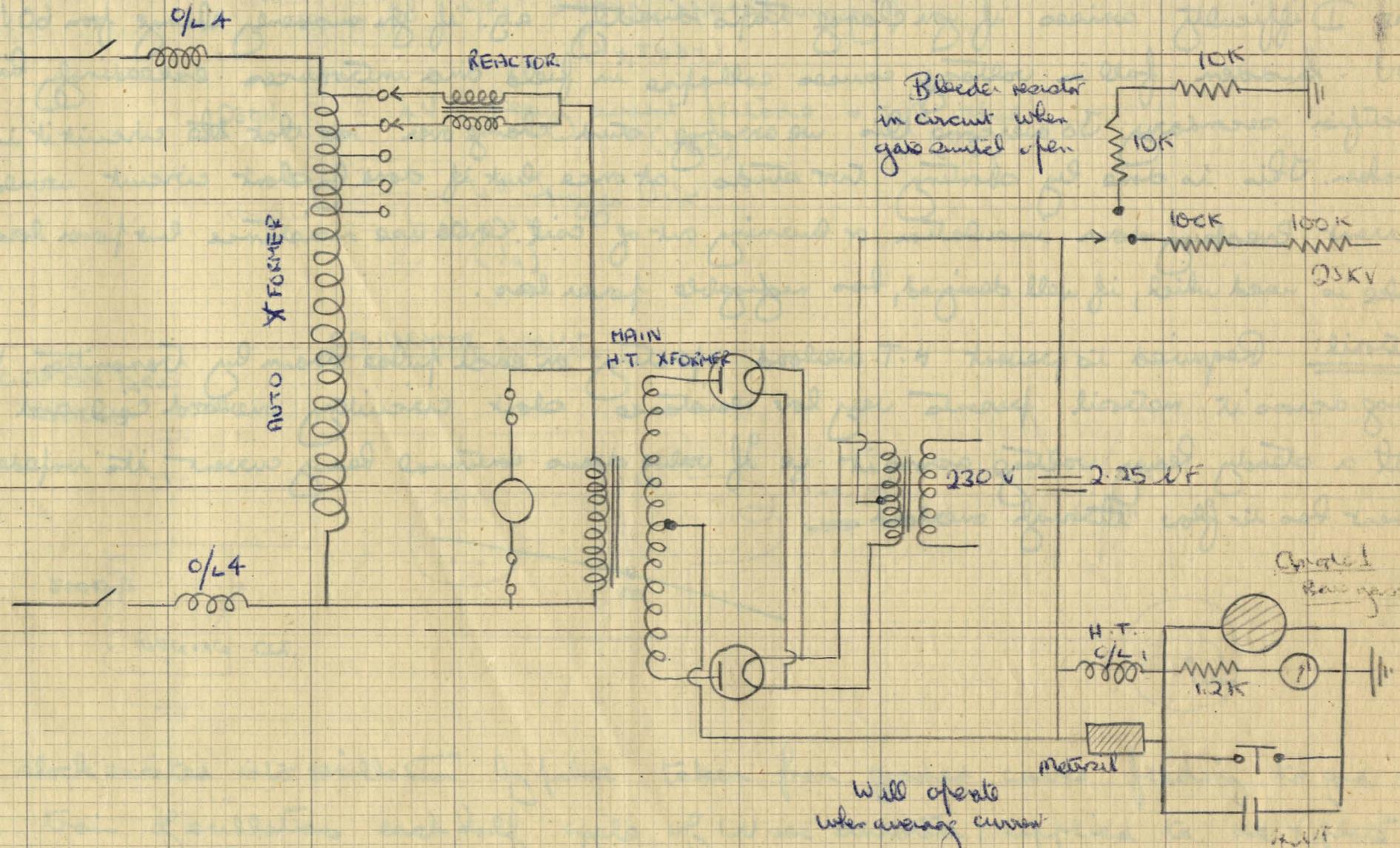
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(FOR USE OF THE AIRCRAFT APPRENTICES' TRAINING ESTABLISHMENTS,  
THE ROYAL AIR FORCE COLLEGE, AND THE OFFICERS'  
ENGINEERING COURSE, HENLOW.)

T. 3079.

CHL EXTRA NOTES

25KV POWER SUPPLY.



Bleeder resistor  
in circuit when  
gas switch open

Will operate  
when average current  
about .25mA

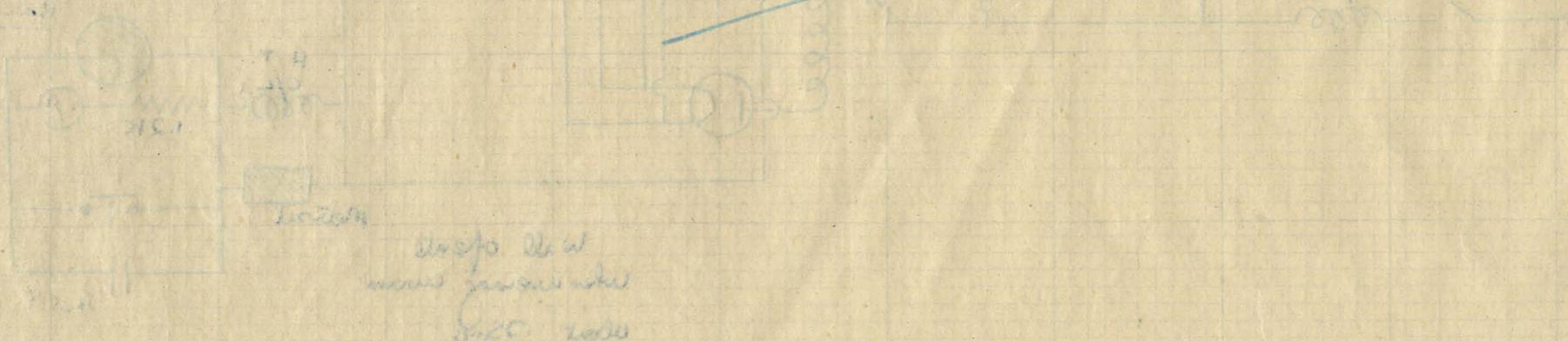
Control  
Gas gas tube

## 25KV Power Supply

Reactor: Auto transformer taps from 60-230 volts followed by second step up transformer PT 230-60V-300V

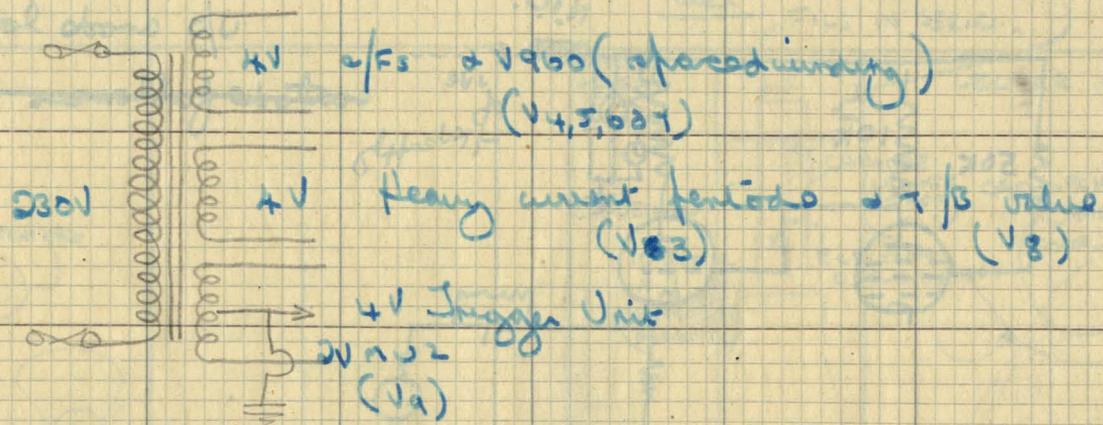
E.H.T. Difficulty arises if you change taps directly e.g. if you suddenly change from 60V-0 and then to 10V. Sudden fall in voltage causes collapse in field and introduces exceedingly high voltage in rectifier secondary. To overcome this we arrange stud change over so that the circuit it is never completely broken. This is done by shorting two studs at once, but if done by short circuit would create very high current breaking down insulation or burning out of coil. Could use resistance but power losses high so a choke is used which, if well designed, has negligible power loss.

Metroil: Required to prevent H.T. overload operating on each pulse drawn by transmitter. With a sudden swing across it metroil presents very low resistance short circuiting overload coil and preventing operation. With a steady heavy voltage across it i.e. if valve draws continual heavy current, its impedance is high and current has to flow through overload.

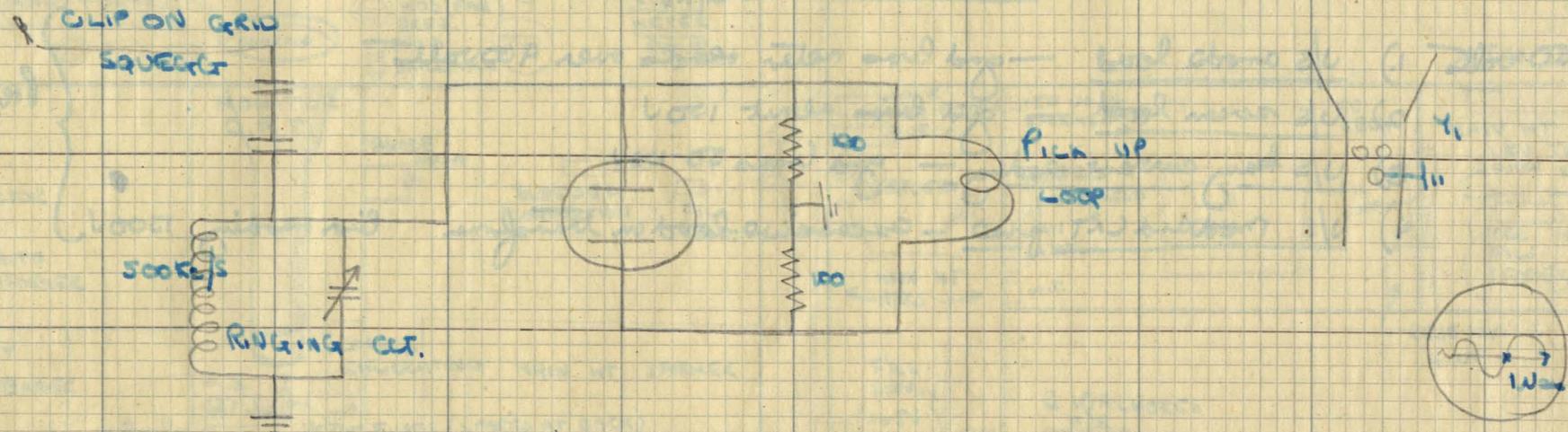


steps down  
main transformer  
25KV 2000

MODULATOR TRANSFORMER



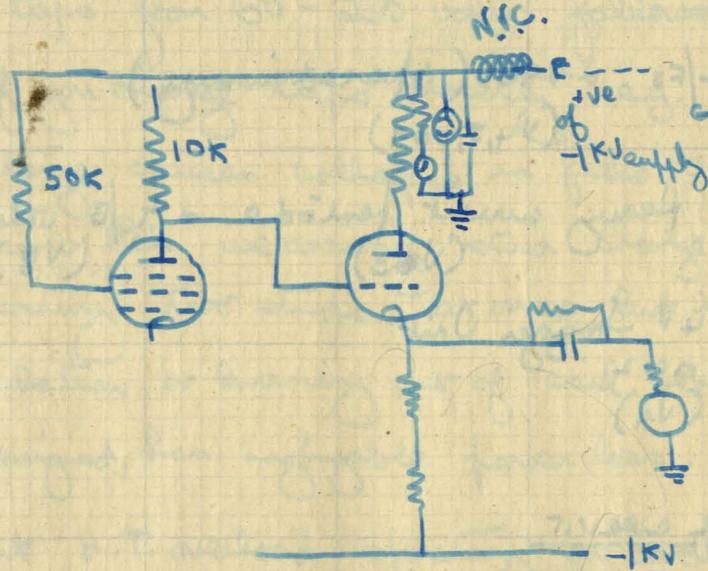
CALIBRATOR CIRCUIT



500kfs ckt. shock excited into oscillation by pulse taken from graded cable feeding to grid squeaker. Gives damped train of oscillations each half cycle of 100µs duration. Applied to one Y plate by connecting wander lead to CRT in place of normal loop connection. A piece of paper can now be calibrated.

Faults

Heavy current periods



1/3 anode load - ~~constant diameter~~

~~control follows~~ remains constant

Normal bias 650-850 volts

- 1) 1/3 anode load - grid bias meter reads over 900 volts
- 2) 1/3 screen load - grid bias about 150V
- 3) 1/3 beam current reading - grid bias 50-100V
- 4) 1/3 mod and CRT fuse - excessive load on transformer bias reading 1300V

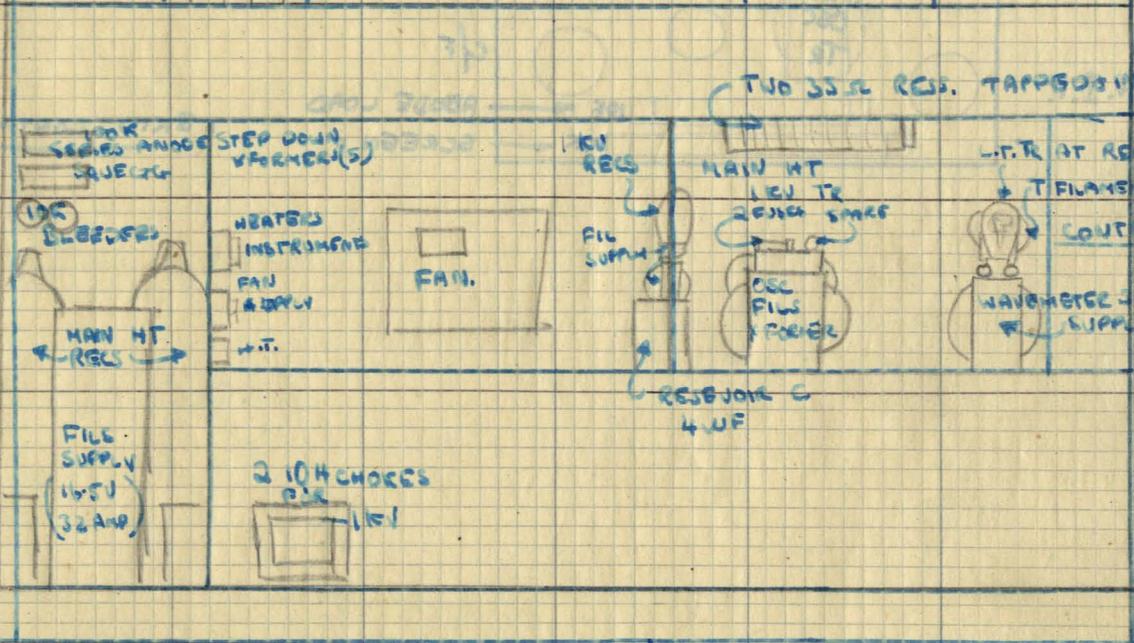
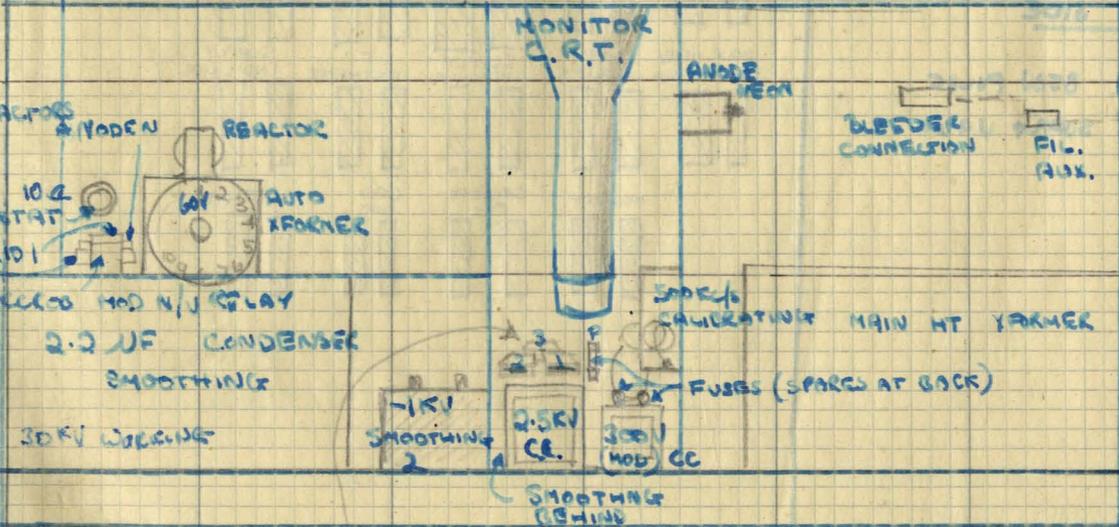
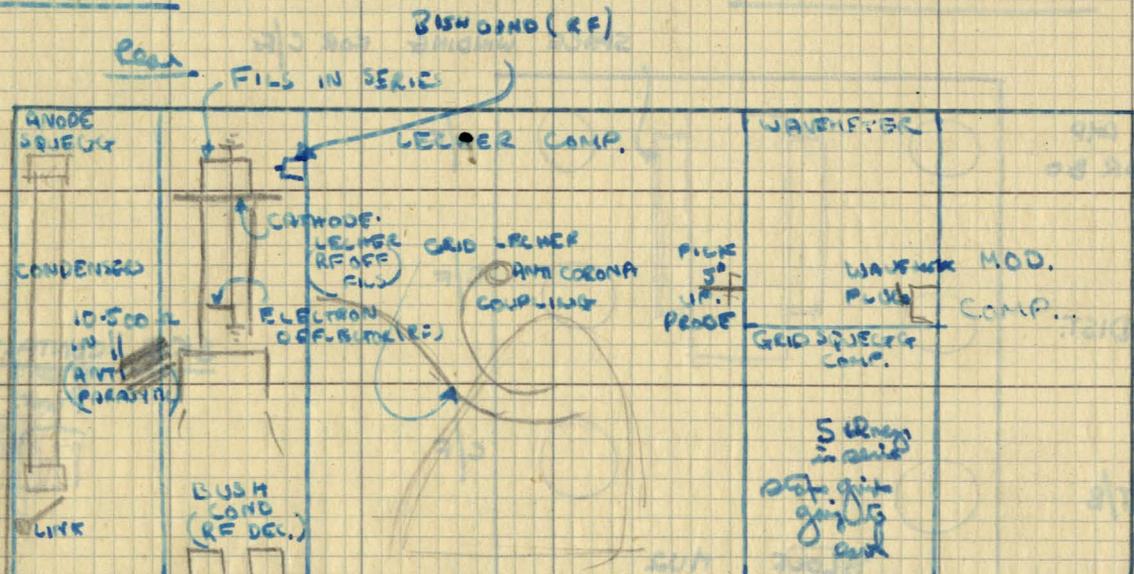
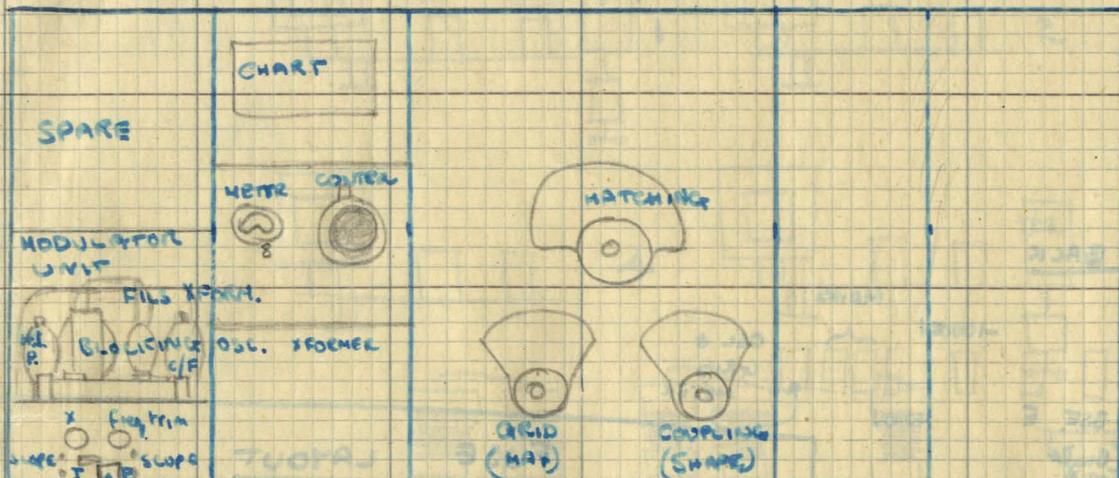
Prevent mod HV coil operating



*[Faint, mostly illegible handwritten notes at the bottom of the page, possibly describing the effects of the faults or the state of the equipment.]*

# LAYOUT DIAGRAMS

T3079 - 3101



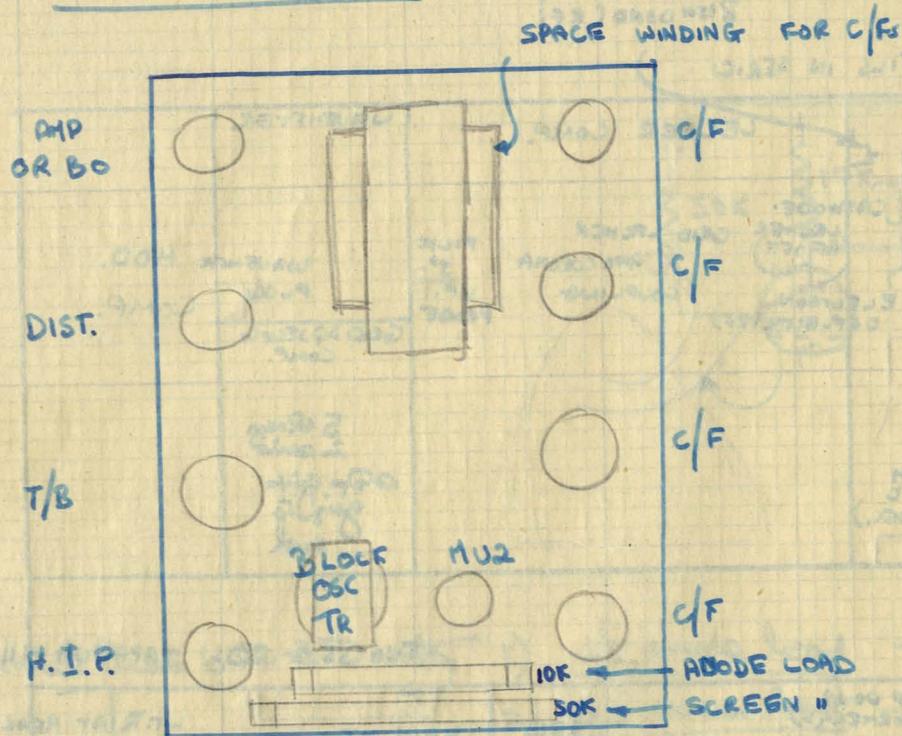
mods CRT fuse also  
fuse file to mod. unit

- PLUGS
1. BRILL & FOCUS
  2. MAIN IN & 300V OUT TO MOD. UNIT.
  3. 2.5KV SUPPLY TO MON. & 4V TO FIL. HEATERS

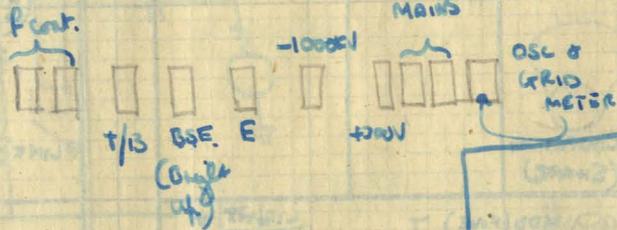
- NETS
- 1) MAINS - across supply
  - 2) EHT - 2ndy auto x forma
  - 3) Filo - 2ndy fil x forma
  - 4) Grid Bias - 2ndy grid supply (10V)
  - 5) anode I - anode VERT
  - 6) grid - 1KV (anode C/I)

- 1) Row nets
- 2) Waveform - after T02 + GSWK

# MODULATOR LAYOUT



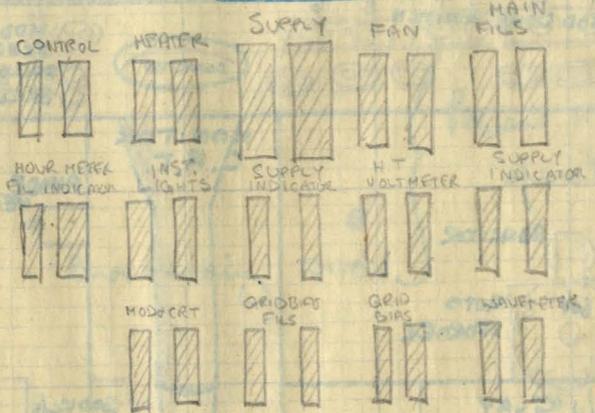
SKID CONTACTS BACK



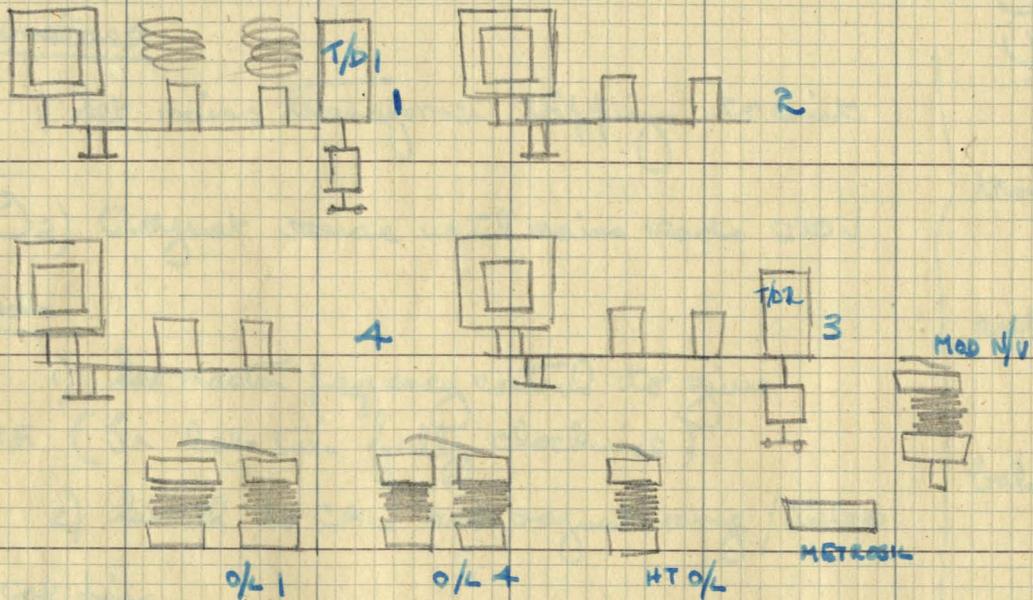
SKID CONTACTS SIDE

-  85V PULSE
-  SUPPLY VARIO

# FUSE LAYOUT



CONTRACTOR LAYOUT



## R 3202 Setting up Procedure.

### H/R Timebase

General 1) Set mains transformer tapping to suit local supply  
2) Adjust variac until mains reads 230V

### Horizontal deflection

1) Set master frequency control to give required P.R.F. (5x lab turn fully clockwise)  
2) Switch to CAL and adjust range/lines

control for 1st cal fit

3) Switch off and remove top cap of second

P.P.A.

4) Switch on set and adjust velocity for trace length of 3"

trace length of 3"

5) Switch off and replace top cap

6) " on and adjust horiz balance

control for trace length of 6"

7) Linearity trace with lining and velocity controls.

### Vertical deflection

1) Adjust vertical shift control until trace reads DCR level.

2) Remove beam lead and adjust cal amp control for 1st cal fit.

3) Replace beam lead and adjust vertical balance for 2nd cal fit.

4) Adjust CRT intensity control for operator convenience

5) Adjust primary signal limiter for trace of ground ray.

6) Adjust T<sub>2</sub> phase until ground ray on 3rd cal fit.



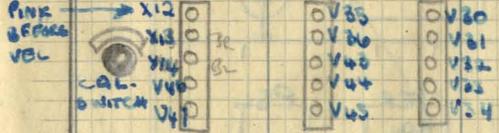
LAYOUT

RECEIVER

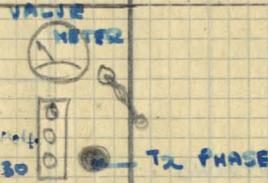
RECEIVER TUNING



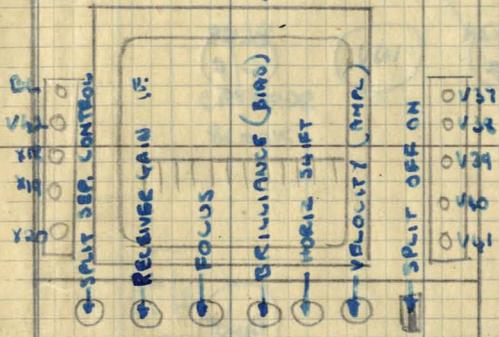
CAL. PHASE & PPI (TOP CAP GRIDS) PPI LIM.



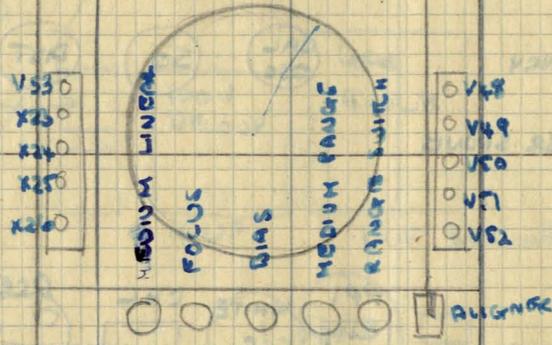
CONTROL UNIT



H/R (TOP CAP ANODES)

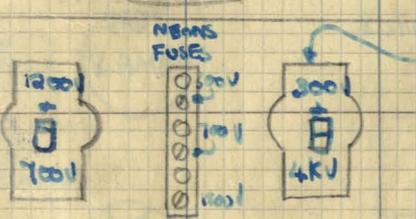


P.P.I.



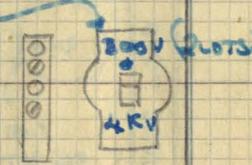
ALIGNER

MAIN



300V (FUSED) RECEIVER SCREEN SUPPLY TANG T/B VALVE CAL. PHASE PPI LIM

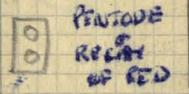
2 300V (FUSED) CONTROL UNIT FOCUS COIL PPI T/B CHAIN



VARING 200V MAINS

PPI

POWER UNIT



POWER UNIT

50V for RELAYS

200V: X AMPS  
100V:

Scope points

X.23.



CATHODE FLIP FLOP (PPI)

X.24.



"BRIGHT UP" CATHODE YELLOW C/F (PPI)

X.25

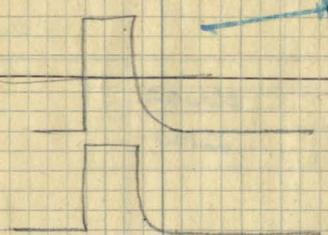


'PROBETAL' ANODES OF T/B GEN (PPI)

X.26

CAL-OR-FIGS ON CRT GRID. (PPI)

X.12.



TO CALL PINK INPUT "USUAL" (H/R) PINK INPUT AFTER 'VEL' (H/R)

BLOCKS OF CALS {X.13} GROW {X.14} GROW

X.19.



F/D ANODE OF 1ST PARA AMP.

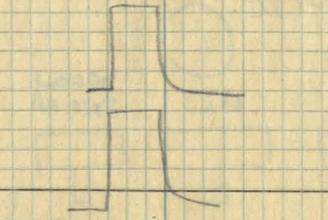
X.18

SIGS OR CALS

CRT GRID (H/R)

X.20

X.29



RED PULSE CATHODE C/F (H/R)

X.30

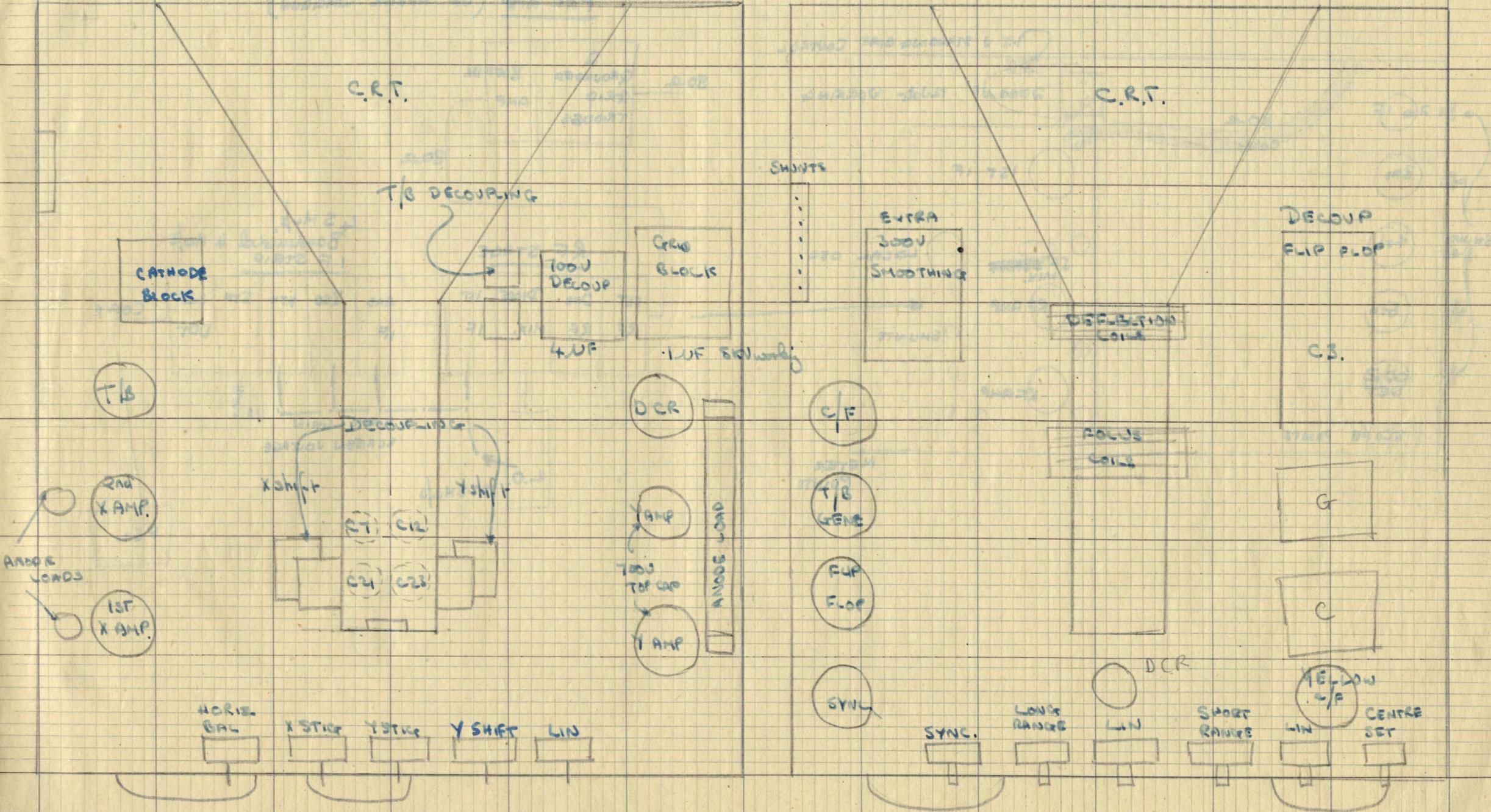
GREEN PULSE GREEN C/F (H/R)



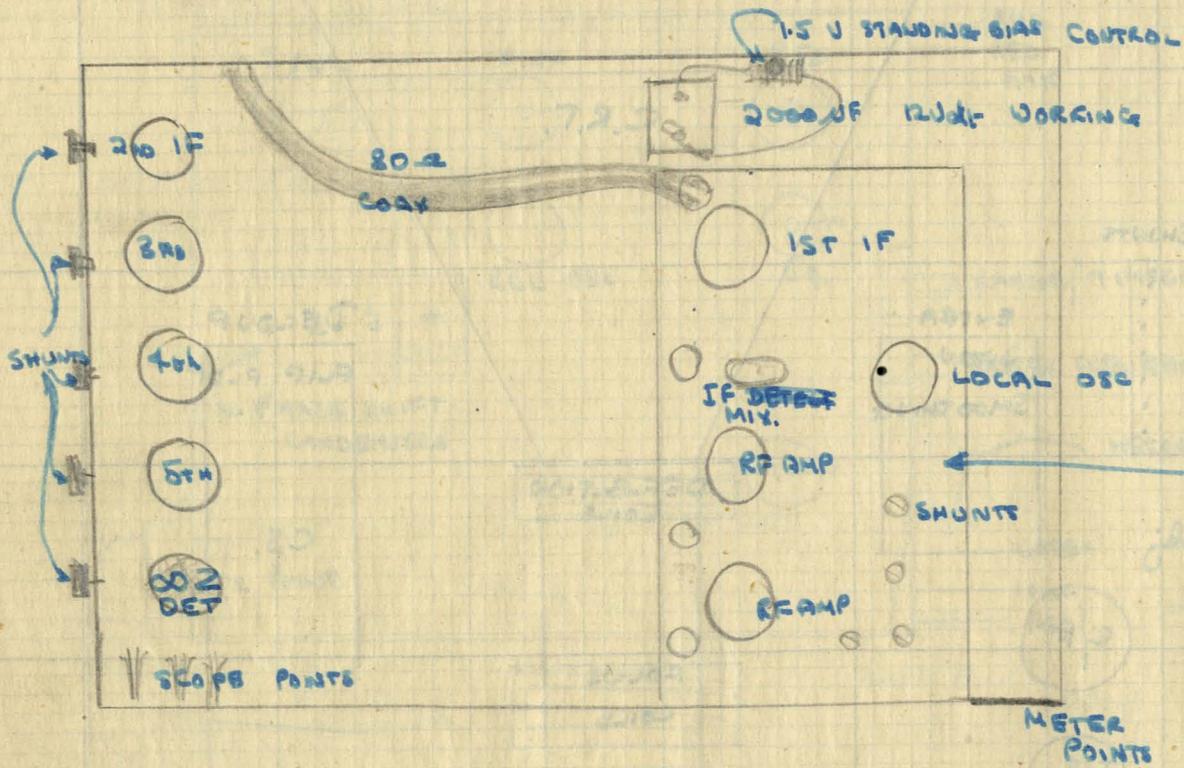
TIMEBASE LAYOUTS

H/R TIMEBASE

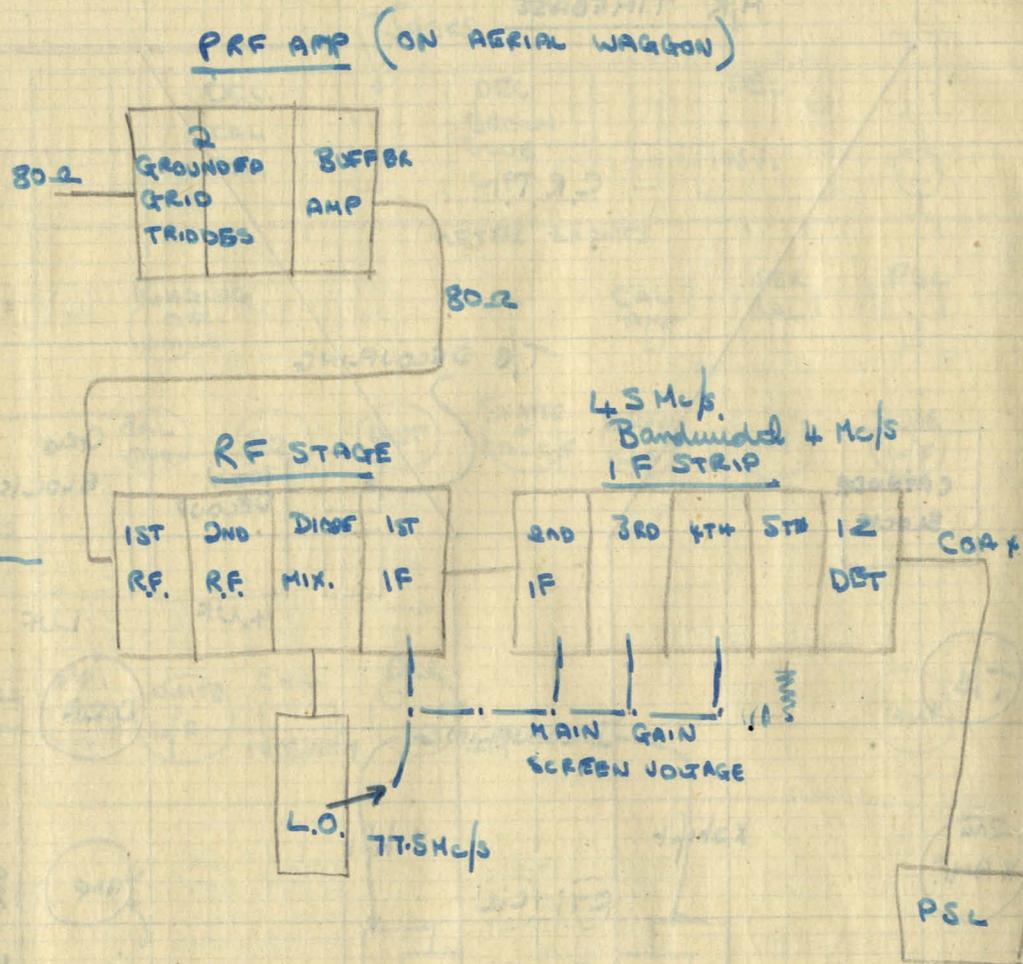
P.P.I. LAYOUT



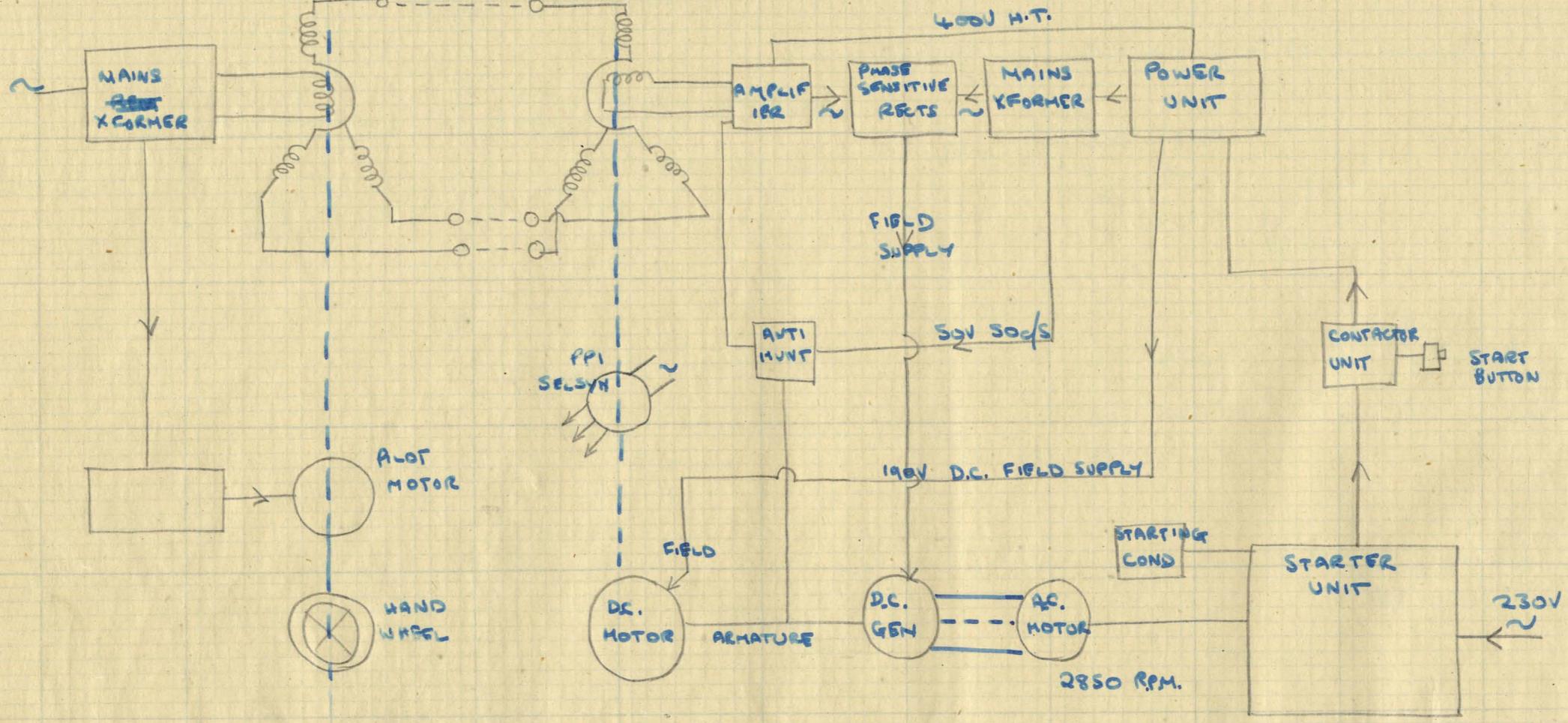
RECEIVER LAYOUT



BLOCK DIAGRAM



BLOCK DIAGRAM 5TH TURNING GEAR T.3.

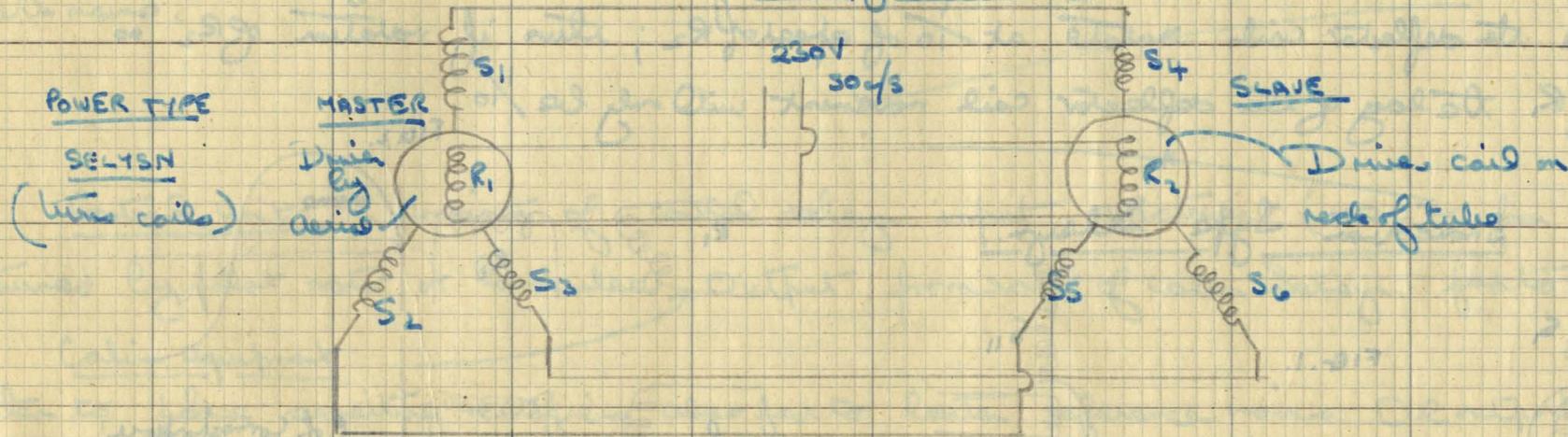


CONTROL UNIT                      CABIN EQUIPMENT

Requirements

- 1) Continuous rotation either direction of 1 to 6 R.P.M. — done by Ward Leonard system.
- 2) Provision for Remote control i.e. from control unit to aerial — Done by servo relays.
- 3) Direct indication of a sector on P.P.I. — Done by special commutator.
- 4) Facilities for P.P.I. indication of aerial position — done by power relays.
- 5) Control of two aerial coils from one point.
- 6) Automatic holding to any fixed bearing.

Servos Motors



POWER TYPE

SELYSN

(line coils)

MASTER

Driven by aerial

SLAVE

Driver coil on neck of tube

aerial  
Relay

No lag  
10%  
100 feet

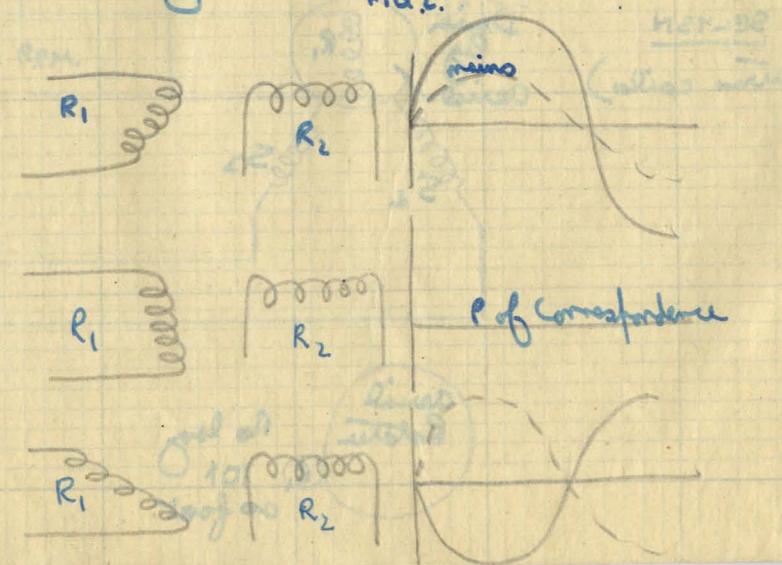
Coil  
Relay  
ground

CRT  
1% lag

Power Type Delays      output Mechanical

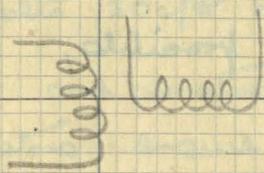
When a PPI is used for determination of bearing the scan (trace) must be aligned with the rotation of the aerial. When a magnetic tube is used this can be achieved by moving the deflector coils round the neck of the tube. Mechanical means of obtaining this motion from the aerial rotation are impracticable. Therefore an electrical method known as the delay motor is used. Assume 230V applied to  $R_1$  &  $R_2$  and  $R_1$  being rotated by the aerial system is in a vertical position. Maximum EMF induced into  $S_1$  and max. EMF in the slave system across  $S_4$ . Since  $R_2$  is an electro magnet it will be pulled into line with  $S_4$ , thus slave is always aligned with master and so coils on neck of CRT are driven in synchronism with aerial rotation same principle applies to every other pos. of  $R_1$ . In order to reduce the slight lag which is bound to be produced in the coils  $R_1$  is caused to rotate 10x for one revolution of the aerial, at the other end the deflector coils rotate at  $\frac{1}{10}$  of speed of  $R_2$ ; thus if rotation of  $R_2$  is lagging by 1% on rotation of  $R_1$  the lag of the deflector coil movement will only be  $\frac{1}{10}$

Indication Type Delays

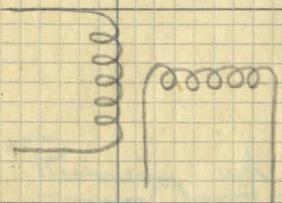


Aerial      Cabin

Sensor      Indication Type Relay      output Electrical



Prim. of correspondence



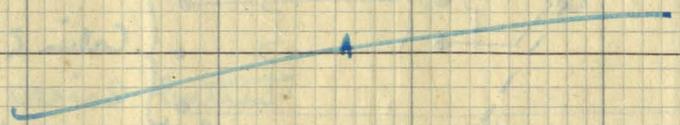
variable tap.

Fig 1 If we pass an AC current through  $R_1$ , EMF will be

induced into  $S_1, S_2 \rightarrow S_3$  and current will be established in  $S_{11}, S_{12}$  and  $S_{13}$ . Thus the field set up by  $R_1$  will be reproduced in the calin relay.  $R_2$  is a search coil and according to its tap, will react to tap of  $R_1$  will pick up voltage which after amplification and rectification are used used to control the turning motor.

Fig 2 Shows how the output of  $R_2$  will vary with direction of the

turning of  $R_1$  from the pos. of correspondence. Output from calin will either be directly in phase or  $180^\circ$  out of phase with mains.



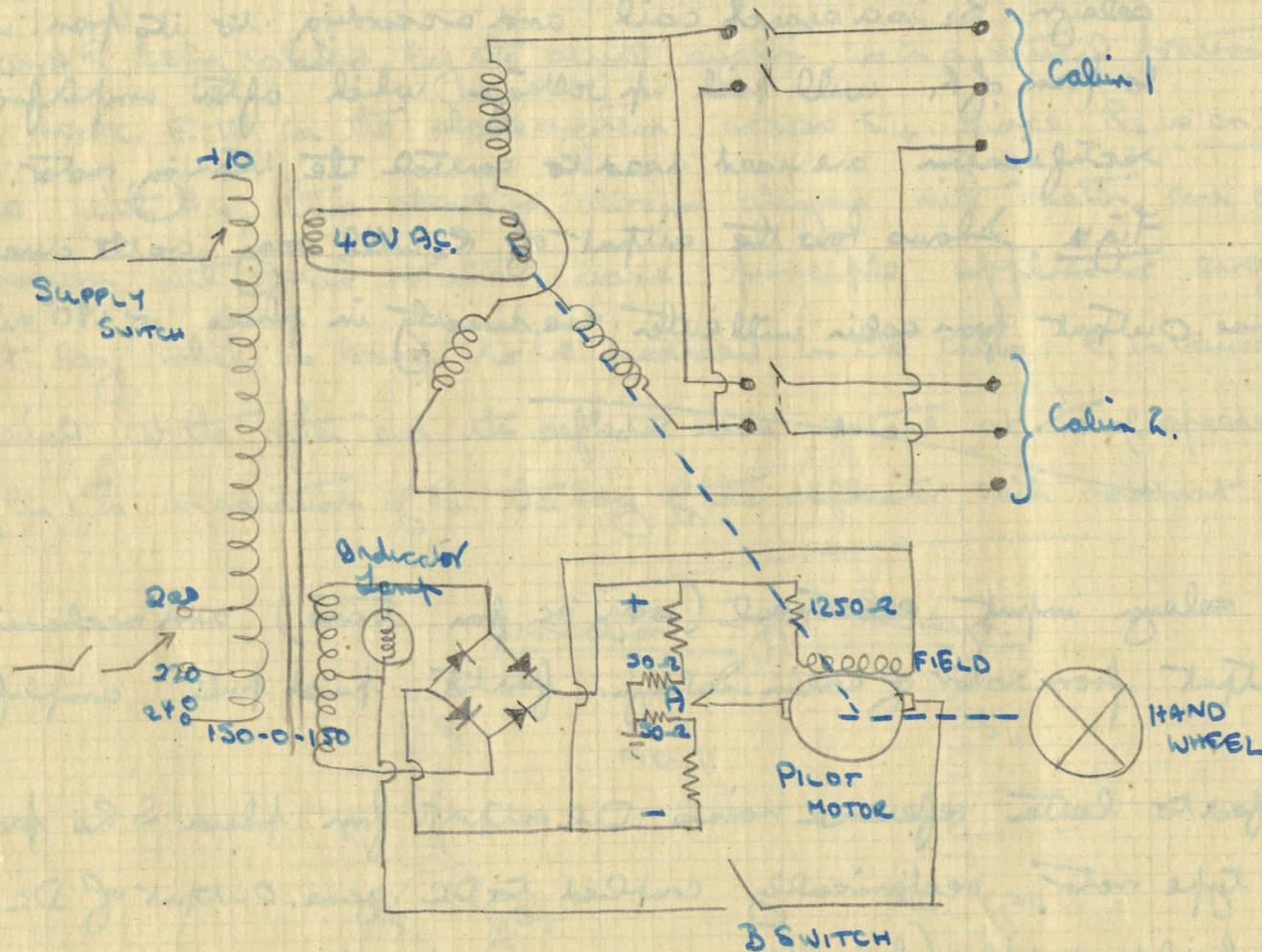
Control Unit consists of control relay input electrical (40V AC for trans.) and mechanical (rotor turned by pilot motor or handwheel). Output from rotor of calin relay. fed to push pull amplifier and

Calin equipment

then to phase sensitive rectifier also fed to latter reference mains DC output from these S Rs provides field supply to DC gene. AC induction type motor mechanically coupled to DC gene. Output of DC gene dependant upon polarity and magnitude of field supply (from phase sens. recs.) provides a variable current for

"Work" motor. Work motor has permanent field supply hence speed and direction of rotation governed by armature supply. "Work" motor turns aerial P.P.L relay and cabin rotor into form of correspondence. Contactor unit safety device enabling mechanic to leave aerial cabin before rotation possible,

Control Unit



Control Unit Contains a relay which is used to control position of cabin. The rotor supplied with 40 volts 50 c/s rotated either manually by hand or automatically by pilot motor. Powered motor small DC machine, obtains field and armature supply from rectifier, armature current variable in direction and magnitude by 'A' control. 50 ohm resistors ensure aerial commences turning at a 2 R.P.M. Automatic turning and hand wheel control interlocked when hand wheel control engaged. Banned open circuits.

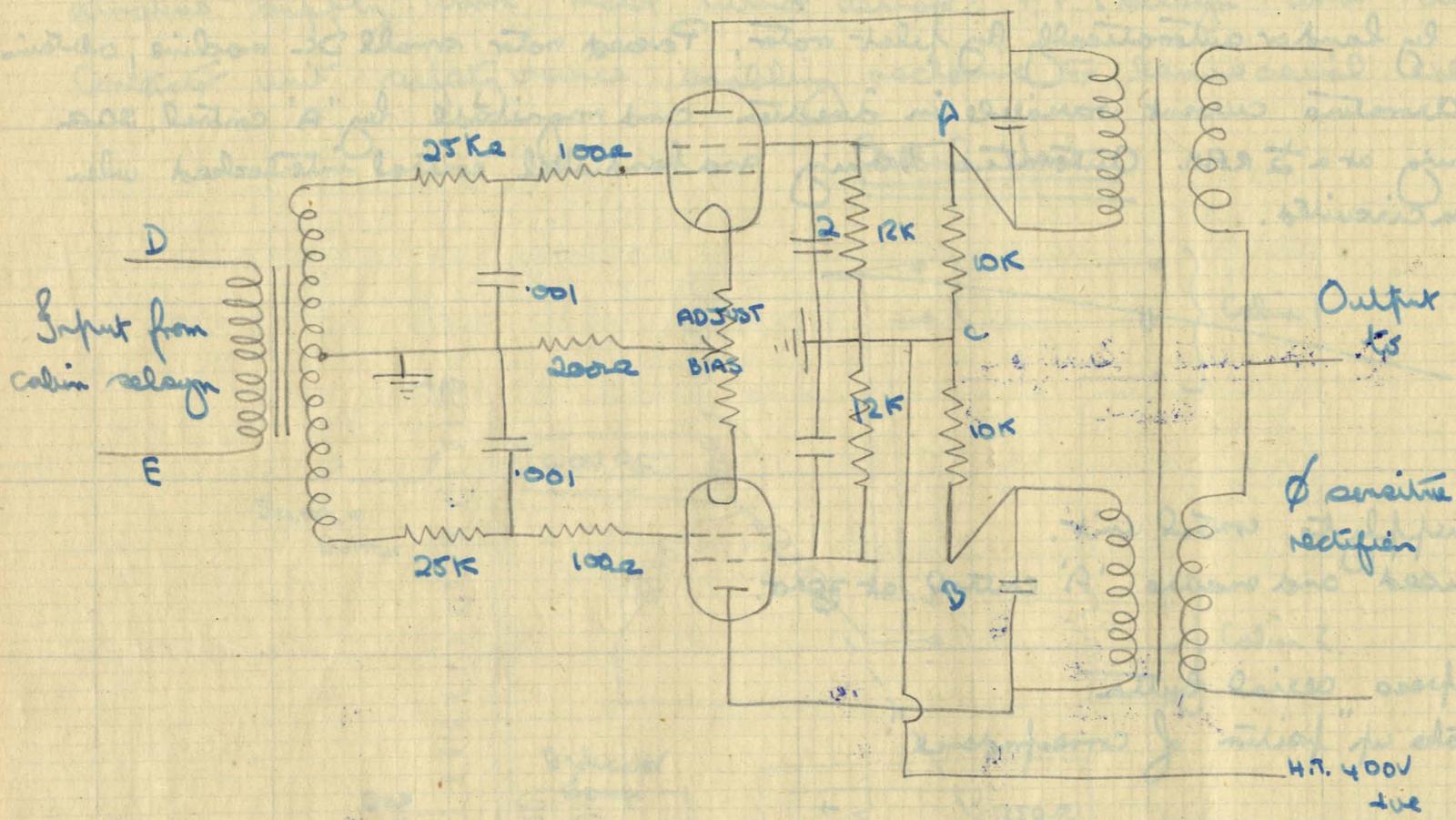
### Running up procedure

- 1) Switch on mains supply to control unit.
- 2) Select cabin to be used and ensure 'A' control at zero.
- 3) Start up A.C. motor.
- 4) Close cabin door and press aerial button.
- 5) Wait for cabin to take up "position of correspondence".
- ~~6) Run~~

### Running down Procedure

- 1) Turn A control to zero
- 2) Trip AC motor
- 3) Switch off control unit

# PUSH PULL AMPLIFIER

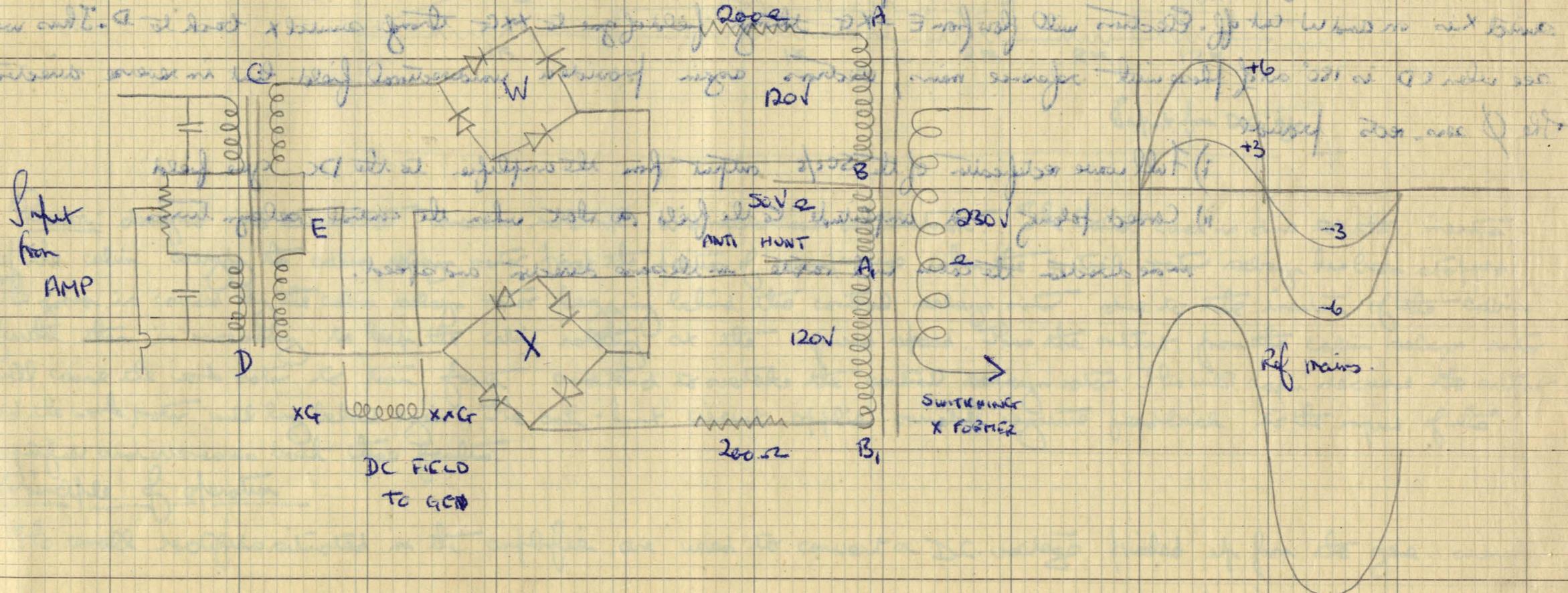


- Handwritten notes and a list of components:
- (1) 25K
  - (2) 100Ω
  - (3) .001
  - (4) 20K
  - (5) 10K
  - (6) HT. 400V 400
  - (7) 20K
  - (8) 10K
  - (9) .001
  - (10) 25K
  - (11) 100Ω
  - (12) .001
  - (13) 20K
  - (14) 10K
  - (15) .001

# Amplifier

Purpose: to drive into grid input the Amplifier just as required as it is done  
 a grid-formal push-pull amp. (class A), required to supply necessary space to field of grid after  
 rectification. Since the input for detection is alternating at 50 c/sec the amp. has been specially  
 designed to give maximum efficiency at this frequency, other higher frequencies may be picked up in the circuit  
 lines but are attenuated only field input circuit. Bias is adjustable, so that balance may be obtained  
 indicated when zero potential difference between A & B. (3 volts across each resistor)  
 200  $\Omega$  resistor across safe is applied to values

## Sensitive Rectifiers

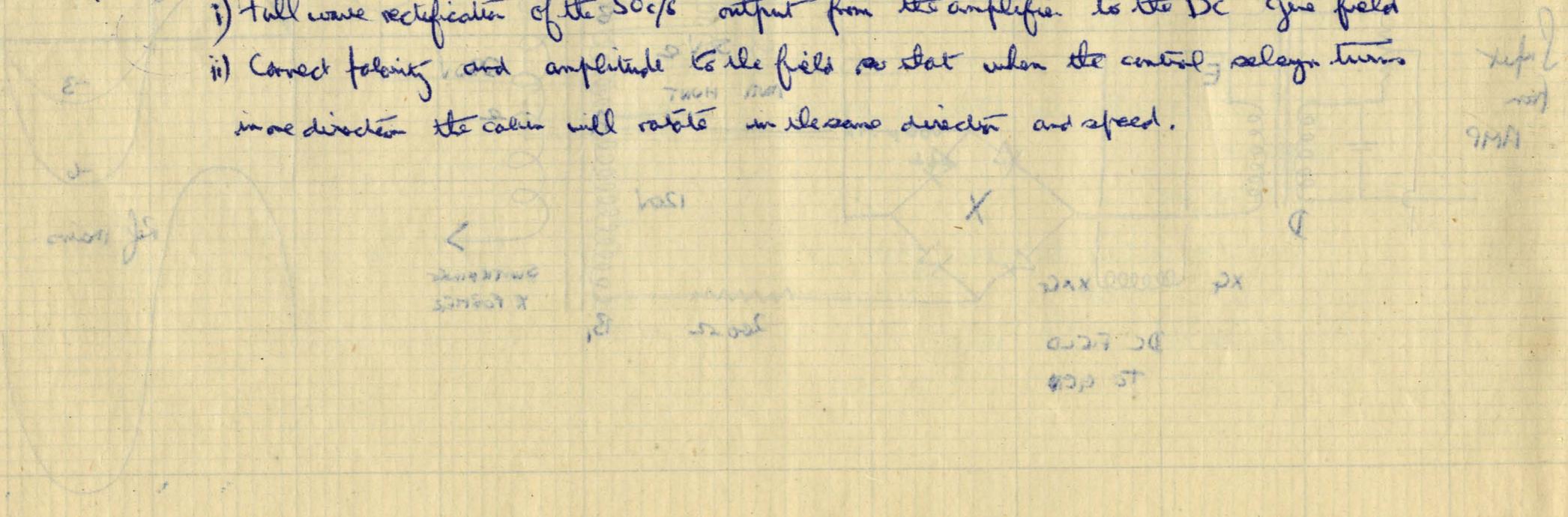


Points C & D can be considered as a pair of switching contacts and the circuit through them made and broken by application of a suitable potential across A & B, providing that the latter is always in excess of the voltage to be switched across C & D. Voltage across ED in phase with the voltage across AB, A<sub>1</sub>B<sub>1</sub>. When A is positive with respect to B, switch X cut on and W cut off. C positive with respect to D. electrons flow from D through switch X to XXG, through field of gene to X generator and back to E. On the next half cycle A will be -ve and B, positive, and C will be negative D positive.

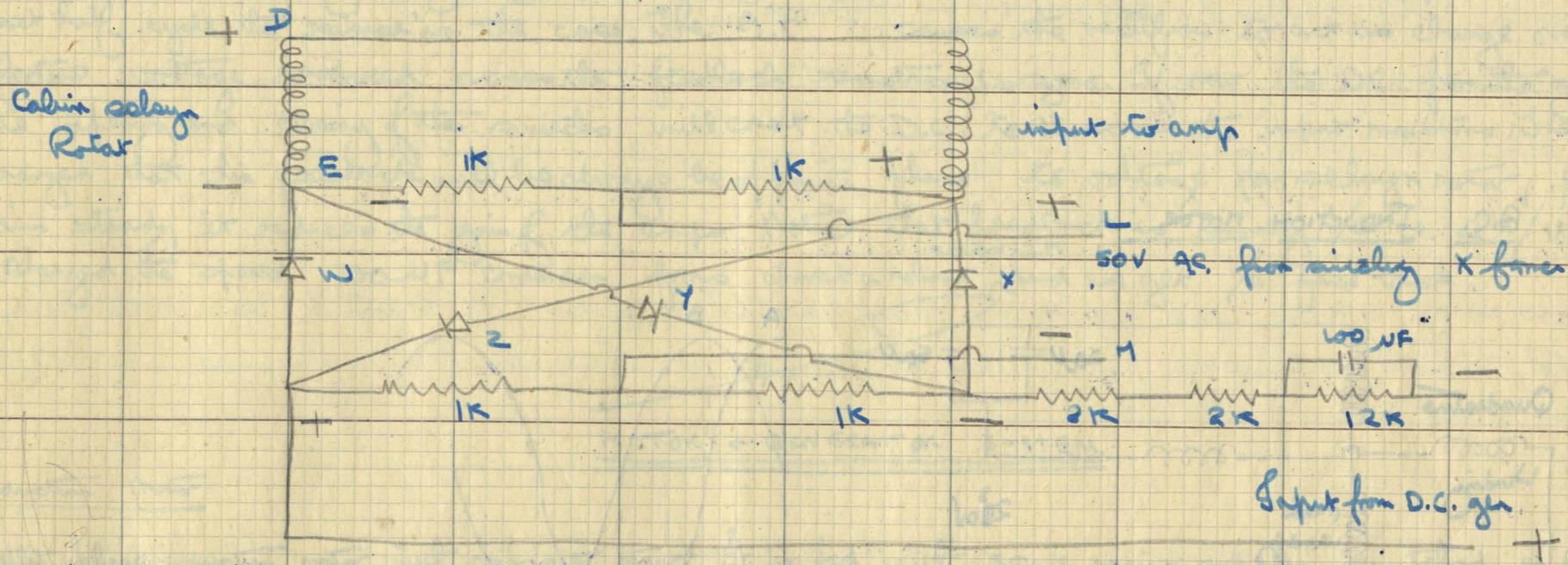
Switch W cut on and switch X cut off. electrons will flow from C through switch W to XXG through field of gene to XG and back to E. Thus as long as CD is in phase with AB and A<sub>1</sub>B<sub>1</sub>, electrons will flow from XXG to XG providing DC. gene. and a uni directional field. However, when CD is out of phase with AB and A<sub>1</sub>B<sub>1</sub>, with A +ve and B, negative, C -ve and D +ve switch X is on and W cut off. Electrons will flow from E - XG through field of gene to XXG through switch X back to D. Thus we see when CD is 180° out of phase with reference mains, electrons again provide a unidirectional field but in reverse direction.

The  $\phi$  sens. rect provide

- i) Full wave rectification of the 50c/s output from the amplifier to the DC gene field
- ii) Correct polarity and amplitude to the field so that when the control, relay turns in one direction the cabin will rotate in the same direction and speed.



## ANTI HUNT CIRCUIT

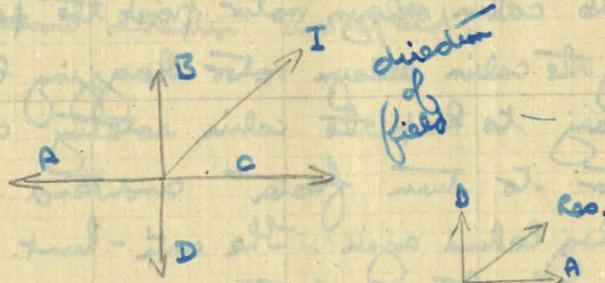
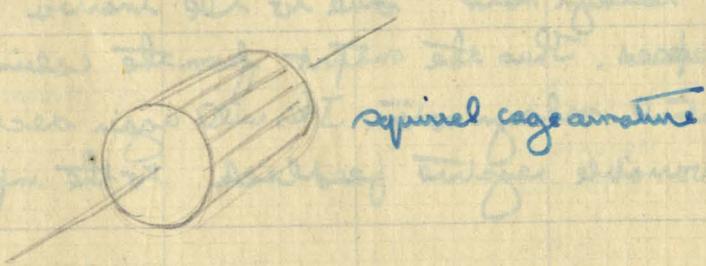
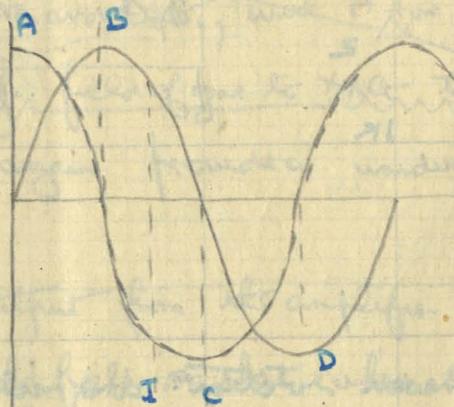
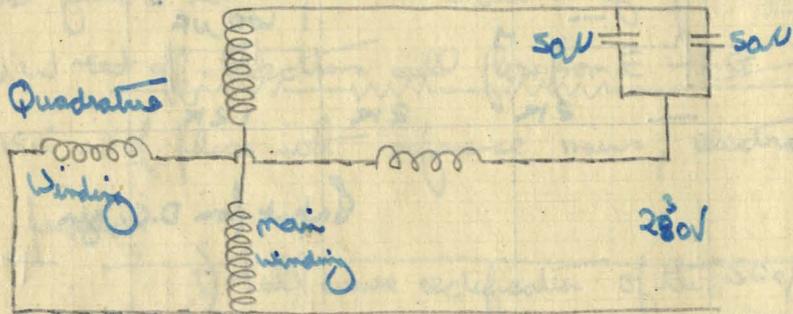


Reason: designed to eliminate uneven rotation and mechanical oscillation. The latter case is due to the inertia of the cabin carrying the cabin relay motor past the position of commutators when the control rotor relay has been stopped. The former is caused by the cabin relay rotor lagging behind the control relay motor due to the inertia of the cabin. Hence it is necessary to keep the cabin rotating at the required speed. Thus the output from the cabin relay rotor will cause the work motor to turn faster and tend to overtake the control relay rotor. This will again decrease the output and the work motor will lag behind again. The anti-hunt circuit applies variable negative feedback to the input of the amplifier and overcomes both these faults.

### Principle of operation

The small rectifiers situated in the amplifier are used to convert a D.C. voltage picked up from the gear armature

A.C. INDUCTION MOTOR



Principle of operation

into A.C. which is used to damp out natural oscillations of the circuit and to make recovery from a change of speed approximately aperiodic. During  $\frac{1}{2}$  cycle of A.C. 1 pr. of rectifiers is conducting and the other pair is open circuit. On the next half cycle the reverse is the case. The A.C.  $\therefore$  causes the rectifiers to act as change over switches, but the effective voltage produced across the feedback resistors is zero. If now the D.C. from the generator is applied the alternate opening and closing of the switches will convert the D.C. to A.C. across the input resistors. The frequency is so averaged that this feedback will be always in opposite phase to voltage from relay motor, providing the D.C. remains steady it reduces the gain of the amp. Notice that feedback is normally  $\frac{1}{4}$  i.e.  $2K/18K$ , If however we suddenly changed the speed 100  $\mu F$  condenser forms almost a short <sup>at 12K</sup> and we get  $\frac{1}{3}$  feedback.

### MOTOR & GENERATOR SYSTEM.

#### A.C. Induction Motor

This is a split phase induction motor with capacity start. It is fed with 50 c/s mains supply switched on by starter unit. It remains at constant running speed whenever the valve is switched on and drives the armature of the D.C. generator.

Action:— condenser in series with quadrature winding causes current through it to lead on main winding by  $90^\circ$ . At point A current through main winding zero, current in quadrature winding maximum. Field I in direction of arrow. Similarly for points B, C, D and E. Thus the field rotates 1 complete revolution for each cycle of the A.C. Field rotates at 3,000 r.p.m. (since mains 50 c/s). If a shorted coil is placed in the field it has an EMF induced into it and will rotate and try to catch up with the main field (squirrel cage type conductors). Note the speed of conductors cannot be the same as speed of the field, otherwise no EMF induced in conductors and speed will fall off. Good efficiency to get within 50-150 rpm. Two condensers chosen are in || i.e. 100  $\mu F$  for starting to overcome the inertia of the rotor, switched in series 25  $\mu F$  for running by the start run switch which also makes the A.C. supply to motor.

Slipping clutch

Adjustment

- 1) Run gear up until friction of cone is obtained
- 2) Connect meter capable of reading 50 amps across fuse connections
- 3) Free axial handle out of cone and adjust clutch nuts until it slips at 26.7 amps.

D.C. Generator

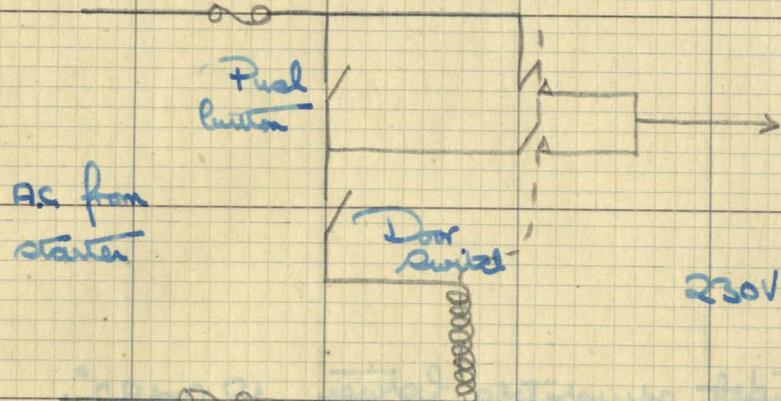
This has a separately excited field fed by the phase sensitive rectifier. The armature, being mechanically coupled to the A.C. motor rotates continuously it provides no D.C. output until the field is energized. The output of this gene depends on the output of the field current.

Main turning motor:

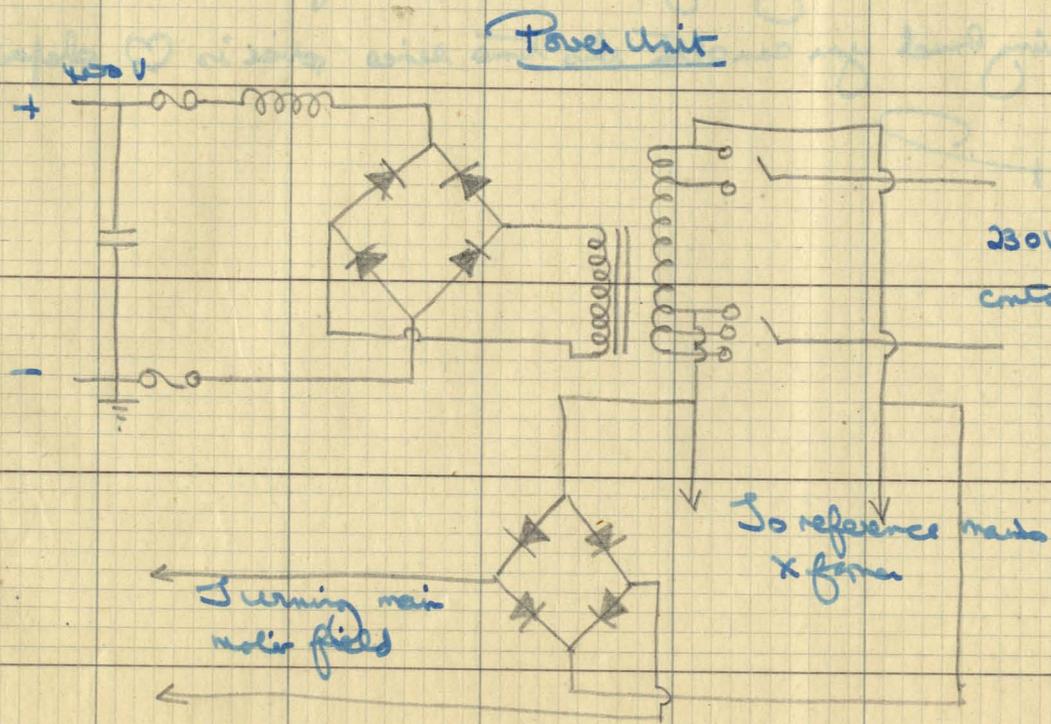
This is a D.C. motor fed from the D.C. gene output. It turns the calin and calin relay. Its field is separately excited which is continuously supplied so that the direction of rotation depends upon the polarity of the armature input.



Contactor Cct.



Power unit Xformer  
Reference mains  
L.T. Xformer.

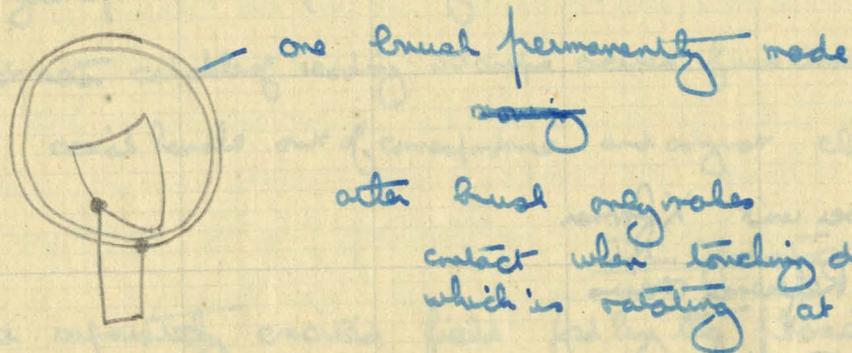


230V for  
contactor unit

3rd reference mains  
Xformer

Turning main  
motor field

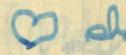
# Stroke Commutator



one brush permanently made

after brush only makes contact when touching disc which is rotating at axial speed.

This enables an indication of any desired sector to be seen width adjustable between 10 and 90°.

Disc rotates at axial speed two brushes feed D.C. to two conducting rings, output is from one fixed and one movable brush. N.B. Output only when brush touches disc. by moving brush you can alter this time since disc is  shaped.