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Colin Hinson
In the village of Blunham, Bedfordshire.

# TACAN (GROUND) <br> <br> TRANSPONDER AN/GRN-9D 

 <br> <br> TRANSPONDER AN/GRN-9D}

## GENERAL AND TECHNICAL INFORMATION

BY COMMAND OF THE DEFENCE COUNCIL

> T.Aunntt

Ministry of Defence

FOR USE IN THE
ROYAL AIR FORCE

Prepared by the Procurement Executive, Ministry of Defence

This 2nd Edition of AP 116C-0701-1A6A supersedes the original (1st) Edition. (The latter was originally NAVSHIPS $93881(A)$ ).

This publication refers to those models of the GRN-9D manufactured by ITT, and the associated special-to-type test equipment housed in the Power Supply Rack - OA1537/GRN-9A. A further model of the GRN-9D manufactured by the National Radio Company differs from the ITT version in that it has a non-temperature-controlled spectrum filter in the Control Duplexer C-2226A/GRN-9, (and other minor variations), and the original special-to-type test equipment has been superseded by the Test Monitor Control Rack, MM-TMC-212A. This publication has been amended to include details of these modifications, and later equipments.
between June 1973 and Jan 1977, further changes were introduced or are scheduled for general incorporation. These include (1) rationalization of individual drawer units for complete interchangeability between URN-3A and GRN-9D, and (2) incorporation of a non-temperature-controlled single-section dual-mode cavity in place of the previous twin-cavity spectrum filter in the Control Duplexer C-2226/GRN-9, and (3) phasing out of service of the Mechanical Keyer Sub-assembly in the Coder Indicator KY-382/GRN-9D, and its replacement by a solid-state Keyer Unit. These changes are dealt with in the new Section 8 to this work.

Where a fully updated equipment is being serviced, reference to Section 8 should be made. The new section is issued as Amendment List No.l. to the main publication.

## LIST OF ASSOCIATED PUBLICATIONS

```
AP 116C-0701-1B6B
AP 116C-0702-1A6A Series
AP 116C-0707-16
AP 116C-0709-1, 10
AP 116C-0712-16,10
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TACAN (Ground) Transponder AN/GRN-9D
TACAN (Ground) Test Monitor Control Group
TACAN (Surface) Aerial and Control System
TACAN Ground Systems Telatel

## LETHAL WARNING



HIGH VOLTAGE
HIGH VOLTAGE
high voltaces exist in this equipment ard due pricautions sholld be takfor. SEE ALSO SECTION 8, Chap 2, PáRA 22 Regardivg the updated transponder INDICATOR DRANER.

Title page<br>Amendment record sheet Preface Contents (this list)

SECTION 1 - GENERAL INFORMATIONParaPage
1-1 Introduction ..... 1-1
1-2 Functional Description ..... 1-1
a. Beacon Identification ..... 1-1
b. Distance Information ..... 1-1
c. Bearing Information ..... 1-2
(1) 15 Hz Amplitude Modulation ..... 1-2
(2) 15 Hz Reference Bursts ..... 1-2
(3) 135 Hz Amplitude Modulation ..... 1-2
(4) 135 Hz Reference Bursts ..... 1-2
1-3 Factory or Field Changes ..... 1-2
1-4 Quick Reference Data ..... 1-2
a. Nomenclature ..... 1-2
b. Contract Number ..... 1-2
c. Contractors ..... 1-2
d. Cognizant Naval Inspector ..... 1-2
e. Number of Packages Involved ..... 1-2
f. Total Cubic Contents ..... 1-2
g. Total Weight ..... 1-3
h. Radio Beacon Duty Cycle ..... 1-3
i. Characteristic of Radio Beacon Signals ..... 1-3
$\bar{j}$. High-Band and Low-Band Radio Beacon Frequency Allocation ..... 1-3
k. Frequency Stability ..... 1-4 ..... 1-4

1. Receiver Selectivity ..... 1-4
m. Receiver Bandwidth ..... 1-4
n. Triggering Level ..... 1-4
ㅇ. Receiver Echo Suppression ..... 1-4
p. Receiver Recovery Time ..... 1-4
q. Receiver Intermediate Frequency ..... 1-4
$\underline{r}$. Response Delay ..... 1-4
s. Interrogation Pulse Repetition Frequency (PRF) ..... 1-4
Traffic Capacity
Traffic Capacity ..... 1-4 ..... 1-4
느. Transmitter Pulse Count Limiting ..... 1-4
Crystal Frequencies ..... 1-4
$\stackrel{\rightharpoonup}{\mathrm{W}}$. Channel Frequency Separation ..... 1-4
X. Modulation ..... 1-4
y. Transmitter Identification ..... 1-5
$\underline{z}$. Transmitter Reference Pulses (For Bearing Information) ..... 1-5
aa. Squitter Rate ..... 1-5
$\overline{\mathrm{ab}}$. Transmitter Power Output ..... 1-5
ac. Transmitter R-F Duty Cycle ..... 1-5
ad. Pulse Spectrum ..... 1-5
ae. Power Input Requirements ..... 1-5
1-5 Equipment Lists ..... 1-5
a. Equipment Supplied ..... 1-5
b. Equipment and Publications Required but not Supplied ..... 1-5
Para

Page
1-5 c. Shipping Data ..... 1-5
d. Equipment Similarities ..... 1-5
(1) Receiver-Transmitter OA-3352/GRN-9D Similarities ..... 1-5
(2) Receiver-Transmitter 0A-3352/GRN-9D Differences ..... 1-5
(3) Power Supply Assembly OA-1537A/GRN-9D Similarities ..... 1-7
(4) Power Supply Assembly OA-1537A/GRN-9D Differences ..... 1-7
e. Electron Tube Complement ..... 1-7
SECTION 2 - INSTALLATION
2-1 Unpacking and Handling ... ... ... ... ... ... 2-1
a. General ..... 2-1
b. Typical Unpacking Procedure ..... 2-1
2-2 Power Requirements and Distribution ..... 2-1
2-3 Installation Layout ..... 2-1
2-4 Installation Requirements ..... 2-1
a. Cable Fabrication ..... 2-1
(1) Removing Armour ..... 2-1
(2) Stripping Insulation ..... 2-2
(3) Applying Terminal Lugs ..... 2-2
(4) Assembly of Cable RG-27/U ..... 2-4
(5) Assembly of Cable RG-18A/U ..... 2-4
(6) Assembly of Cable RG-10/U ..... 2-4
b. Layout and Installation of Cables ..... 2-4
(1) General ..... 2-4
(2) Cable Connections ..... 2-7
(a) Terminal Board Connections ..... 2-10a
(b) Power Cable Connections ..... 2-10a
(c) Coaxial Cable Connections ..... 2-10a
c. Electron Tube Installation ..... 2-10a
d. Built-in Test EQuipment Installation (Not MM-TMC-212A ..... 2-13
e. Built-in Test Equipment Installation (MM-TMC-212A) ..... 2-14
2-5 Inspection and Adjustments ..... 2-14
a. Initial Checks ..... 2-14
b. Preliminary Adjustment (Radio Set Unenergized) ..... 2-14
Initial Energizing ..... 2-14
d. Adjustment of Built-in Test Equipment ..... 2-17
(1) General ..... 2-17
(2) Original Test Equipment (Table 1-2) ..... 2-17
(3) Preliminary Setting of Front Panel Controls on Pulse Analyzer/Signal Generator TS-890A/URN-3 ..... 2-17
(4) Replacement Test Equipment (Table 1-2b) ..... 2-18
e. Adjustment of Power Supplies ..... 2-18b
(1) Low Voltage Power Supply PP-1766/URN ..... 2-18b
(2) Medium Voltage Power Supply PP-1765/URN ..... 2-19
f. Adjustment of Control Duplexer C-2226A/GRN-9 ..... 2-19
(1) Adjustment of Filament Voltage ..... 2-19
(2) Adjustment of Preselector Cavities ..... 2-20
(3) Adjustment of Transmission Line Filter ..... 2-20
g. Changing Crystals ..... 2-20
h. Adjustment of Frequency Multiplier Oscillator CV-1171/ GRN-9D ..... 2-25
(1) General ..... 2-25
(2) Tuning Carrier Frequency Generating Chain ..... 2-25
(3) Video Chassis Adjustments ..... 2-27

## SECTION 2 - INSTALLATION (Contd)



SECTION 3 - OPERATOR'S SECTION
3-1 Functional Operation ... ... ... ... ... ... ... 3-1
a. General ... ... ... ... ... ... ... ... 3-1
b. Capabilities ... ... ... ... ... ... ... 3-1
(1) Radio Beacon ... ... ... ... ... ... 3-1
(2) Radio Receiver R-824/URN ... ... ... ... 3-1
(3) Coder Indicator KY1382/GRN-9D ... ... ... ... 3-1
(4) Transmitter ... ... ... ... ... ... ... 3-2
(5) Control Circuits ... ... ... ... ... ... 3-2

3-2 Operating Procedures ... ... ... ... ... ... ... 3-2
a. General ... ... ... ... ... ... ... ... 3-2
b. Description of Controls ... ... ... ... ... 3-3
(1) Receiver-Transmitter OA-3352/GRN-9D ... ... ... 3-3
(2) Power Supply Assembly OA-1537/GRN-9A ... ... 3-10
c. Sequence of Operations ... ... ... ... ... ... 3-10
(1) Before Use ... ... ... ... ... ... ... 3-10
(2) During Use ... ... ... ... ... ... ... 3-16
(3) Standby Operation ... ... ... ... ... ... 3-18
(4) After Use ... ... ... ... ... ... ... 3-18
(5) Stopping the Equipment ... ... ... ... ... 3-18
d. Indicator Presentations ... ... ... ... ... 3-18

3-3 Summary of Operating Procedures ... ... ... ... ... 3-18
a. Starting Procedure ... ... ... ... ... ... 3-18
b. Tuning and Adjusting Procedure ... ... ... ... 3-20
c. Changing Frequencies ... ... ... ... ... ... 3-20
d. Changing Identification Call Code ... ... ... ... 3-21
e. Securing the Equipment ... ... ... ... ... ... 3-21
(1) Turning off Radio Beacon ... ... ... ... 3-21
(2) Shutting Down Radio Beacon ... ... ... ... 3-21

3-4 Emergency Operation ... ... ... ... ... ... ... 3-21
3-5 Test Procedures (For Test Equipment Only) ... ... ... 3-22
a. Original Test Equipment (Table 1-2) ... ... ... 3-22
b. Replacement Test Equipment (Table 1-2b) ... ... ... 3-22

3-6 Operator's Maintenance, Original Test Equipment (Table 1-2) Only 3-22
a. Operating Checks and Adjustments ... ... ... ... 3-22
(1) Preliminary Settings of Front Panel Controls on Pulse Analyzer-Signal Generator TS-890A/URN-3

3-22

## SECTION 4 - PRINCIPLES OF OPERATION (Contd)



SECTION 5 - TROUBLESHOOTING

| 5-1 | General |  |  |  | 5-1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5-2 | Test Equipment and Special Tools |  |  |  | 5-1 |
|  | a. Test Equipment |  |  |  | 5-1 |
|  | b. Special Tools |  |  |  | 5-1 |
| 5-3 | $\overline{\text { Overall }}$ Troubleshooting |  |  |  | 5-1 |
|  | a. Preliminary Check |  |  |  | 5-1 |
|  | b. Test Equipnent and Special Tools |  |  |  | 5-3 |
|  | c. Control Settings | . . |  |  | 5-3 |
|  | d. System Troubleshooting Chart |  |  |  | 5-3 |
| 5-4 | Functional Section Troubleshooting |  |  |  | 5-3 |
|  | a. Preliminary Check |  |  |  | 5-3 |
|  | $\underline{\text { b }}$. Test Equipment and Special Tools |  |  |  | 5-3 |
|  | c. Control Settings |  |  |  | 5-8 |



## SECTION 6 - REPAIR (Contd)

Para


SECTION 7 - PARTS LIST

| 7-1 | Introduction | ... ... ... | ... ... | . . . | 7-1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7-2 | List of Major Units |  | . - . | . . . | 7-1 |
| 7-3 | List of Major Units by | Colloquial Name | . $\cdot$. |  | 7-1 |
| 7-4 | Maintenance Parts List |  | -.. -.. | . $\cdot$ | 7-1 |
| 7-5 | List of Manufacturers | ... ... ... | ... ... |  | 7-1 |
| 7-6 | Notes |  | ... -. |  | 7-1 |

SECTION 8 - MODIFICATIONS
See Contents List, prelim page 21

LIST OF ILLUSTRATIONS

SECTION 1 - GENERAL INFORMATION
Fig
Page
1-1 Radio Beacon, Using Radio Set AN/GRN-9D and Antenna Group
AN/GRA-60 or AN/GRA-61 ... ... ... ... ... ...
1-2 Receiver-Transmitter Group OA-3352/GRN-9D, Overal1 View 1-7
1-3 Power Supply Assembly OA-1537A/GRN-9A, Overal1 View ... 1-8

## SECTION 2 - INSTALLATION

2-1 | Receiver-Transmitter Group or Power Supply Assembly, Typical |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Unpacking Diagram | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |

2-2 $\begin{array}{lllllll}\text { Receiver-Transmitter Group and Power Supply Assembly, Typical } \\ \text { Outline Drawing } & \ldots & \ldots & \ldots & \ldots & \ldots & \ldots\end{array} . .$.
2-3 Method of Attaching Terminal Lugs ... ... ... ... 2-4
2-4 Attaching Plug UG-154A/U to Cable RG-18/U, Assembly Details 2-5
2-5 Attaching Plug UG-943A/U to Cable RG-10/U, Assemb1y Details 2-6
2-6 Shore Radio Beacon Cable, Location Diagram ... ... 2-7
2-7 Amplifier Modulator AM-1701/URN, Front View with Klystron Access Door Open ... ... ... ... ... ... ... 2-11
2-8 Amplifier Modulator AM-1701/URN, Left Side View ... 2-12
2-9 Klystron Characteristics, Sample Calibration Curve ... 2-13
2-10 Klystron Installation Details ... ... ... ... 2-13
$\begin{array}{llll}\text { 2-11 } & \text { Built-in Test Equipment Interconnection Harness, Schematic } & \\ & \text { Diagram (Original Test Equipment, Table 1-2) ... ... } & 2-15\end{array}$

Page

| 2-11a | Sheet 1. Test Equipment Signal/Control Interconnections, |  |
| :---: | :---: | :---: |
|  | Replacement Test Equipment (Table 1-2b) | 2-16a |
| 2-12 | Low Voltage Power Supply PP-1766/URN, Right Side View | 2-18b |
| 2-13 | Medium Voltage Power Supply PP-1765/URN, Top View | 2-19 |
| 2-14 | Control Duplexer C-2226A/GRN-9, Left Side View | 2-20 |
| 2-15 | Transmission Line Filter Cavity, Tuning Curve | 2-24 |
| 2-16 | Control Duplexer C-2226A/GRN-9, Right Side View | 2-25 |
| 2-17 | Frequency Multiplier Oscillator CV-1171/GRN-9D, Top View | 2-26 |
| 2-18 | Frequency Multiplier Oscillator CV-1171/GRN-9D, R-F Chassis |  |
|  | Top View ... ... | 2-27 |
| 2-19 | Klystron Tuning Waveshapes, | 2-28 |
| 2-20 | Amplifier Modulator AM-1701/URN, Top Front View Showing |  |
|  | Double-Slug Tuner ... | 2-33 |
| 2-21 | Frequency Multiplier Oscillator, Adjustment of R1471 to |  |
|  | Correct for Pulse Droop in Reference Bursts | 2-34 |

## SECTION 3 - OPERATOR'S SECTION

3-1 Radio Receiver R-824/URN, Front Panel View ... ... 3-2
3-2 Coder Indicator KY-382/GRN-9D, Front Pane1 View ... ... 3-3

3-4 Amplifier Modulator AM-1701/URN, Front Panel View ... 3-5
3-5 Control Duplexer C-2226A/GRN-9, Front Panel View ... 3-5
3-6 Cabinet CY-3163/GRN-9D, Blower Compartment ... ... 3-10
3-7 Low Voltage Power Supply PP-1766/URN, Front Panel View 3-11
3-8 High Voltage Power Supply PP-1763/URN, Front Panel View 3-11
3-9 Medium Voltage Power Supply PP-1765/URN, Front Panel View 3-12
3-10 Cabinet CY-3164/GRN-9D, Blower Compartment ... ... 3-12
3-11 Coder Indicator Tone Wheel Assembly ... ... ... ... 3-16
3-12 Setting the Code ... ... ... ... ... ... ... 3-17
$\begin{array}{lccccccc}\text { 3-13 Test Equipment Front Panel Interconnection Diagram, Original } \\ \text { Test Equipment (Table 1-2) } & \ldots . . . . & \ldots & \ldots & . . . & 3-23\end{array}$
$\begin{array}{ll}\text { 3-13a Front Panel Interconnection for Receiver Selectivity Test, } \\ & \text { Replacement Test Equipment (Table 1-2b) Only ... ... 3-24 }\end{array}$
3-14 Pulse Analyzer-Signal Generator TS-89AA/URN-3, Front Panel
View ... ... ... ... ... ... ... ... ...

3-17 Power Meter-Pulse Counter TS-891/URN-3, Front Panel View 3-27
3-18 Transmitter Output R-F Envelope ... ... ... ... 3-28
3-19 Composite waveform. North and Auxiliary Reference Burst 3-29
3-20 Zero Distance Delay Measurement Waveforms ... ... ... 3-30
3-21 Coder Indicator Identification Keyer, Lubrication Points 3-36
3-22 North Reference Burst Waveform ... ... ... ... 3-30c
3-23 Identity Pulse Spacing, Waveform ... ... ... ... 3-30d
3-24 Equalizing Pulse Spacing, Waveform ... ... ... ... 3-30d
3-25 Radiated Antenna Pattern, Waveform Correct - In Phase ... 3-30j
3-26 Radiated Antenna Pattern, Waveform in Phase with Correct Pattern

3-30k
3-27 Radiated Antenna Pattern, Waveform Incorrect - $20 \%$ Phase Shift 3-30k
3-28 Radiated Antenna Pattern, Incorrect Pattern - $20 \%$ Phase Shift 3-30k

| Fig |  | Page |
| :---: | :---: | :---: |
| 4-1 | Radio Beacon Overall Functional Block Diagram | 4-2 |
| 4-2 | Development of Radio Beacon Radiation Pattern | 4-3 |
| 4-3 | Employment of North Reference Burst to Mark Bearing of |  |
|  | Aircraft Relative to Radio Beacon | 4-4 |
| 4-4 | Comparison of Bearing Information by Aircraft in Different |  |
|  | Geographical Positions Relative to Radio Beacon | 4-5 |
| 4-5 | Development of Composite Radiation Pattern | 4-7 |
| 4-6 | Compositing 15 Hz and 135 Hz Amplitude Modulation and Burst |  |
|  | Signal Elements into Bearing Information | 4-9 |
| 4-7 | Radio Set AN/GRN-9D, Simplified Block Diagram | 4-11 |
| 4-8 | Pulse-Sweep Generator SG-121A/URN-3, Simplified Functional |  |
|  | Block Diagram | 4-16 |
| 4-9 | Pulse Analyzer-Signal Generator TS-890A/URN-3, Simplified |  |
|  | Functional Block Diagram | 4-17 |
| 4-10 | Power Meter-Pulse Counter TS-891/URN-3, Simplified Functional |  |
|  | Block Diagram | 4-18 |
| 4-11 | Oscilloscope OS-54/URN-3, Simplified Functional Block Diagram | 4-19 |
| 4-12 | Switch-Test Adapter SA-420/URN-3, Simplified Block Diagram | 4-20 |
| 4-13 | Radio Receiver R-824/URN, Hybrid Balanced Mixer, Simplified |  |
|  | Schematic Diagram | 4-21 |
| 4-14 | Radio Receiver R-824/URN, Preamplifier, Simplified Schematic |  |
|  | Diagram | 4-22 |
| 4-15 | Radio Receiver R-824/URN, I-F Amplifier, Simplified Schematic |  |
|  | Diagram | 4-24 |
| 4-16 | Radio Receiver R-824/URN, Ferris Discriminator, Simplified |  |
|  | Schematic Diagram | 4-25 |
| 4-17 | Radio Receiver R-824/URN, Ferris Discriminator, Continuous- |  |
|  | Wave Response Curve | 4-26 |
| 4-18 | Radio Receiver R-824/URN, Video Amplifier, Simplified |  |
|  | Schematic Diagram | 4-27 |
| 4-19 | Radio Receiver R-824/URN, Coincidence Decoder, Simplfied |  |
|  | Schematic Diagram | 4-28 |
| 4-20 | Radio Receiver R-824/URN, One-Shot Multivibrator and Receiver |  |
|  | Output, Simplified Schematic Diagram | 4-29 |
| 4-21 | Radio Receiver R-824/URN, Blanking Gate Generator, Simplified |  |
|  | Schematic Diagram | 4-30 |
| 4-22 | Radio Receiver R-824/URN, Squitter Control Voltage Regulator, |  |
|  | Simplified Schematic Diagram | 4-30 |
| 4-23 | Coder-Indicator KY-382/GRN-9D, 135 Hz Reference Burst |  |
|  | Generator, Simplified Schematic Diagram | 4-32 |
| 4-24 | Coder-Indicator KY-382/GRN-9D, V609B Grid Voltage Curve During |  |
|  | Charge Time of C625 | 4-33 |
| 4-25 | Coder-Indicator KY-382/GRN-9D, Shaping Amplifier, Simplified |  |
|  | Schematic Diagram | 4-34 |
| 4-26 | Coder-Indicator KY-382/GRN-9D, Double Encoding Circuit, |  |
|  | Simplified Schematic Diagram | 4-35 |
| 4-27 | Coder-Indicator KY-382/GRN-9D, Output Amplifier, Simplified |  |
|  | Schematic Diagram | 4-36 |
| 4-28 | Coder-Indicator KY-382/GRN-9D, Control Function of Identity |  |
|  | Call Mechanical Keyer, Simplified Schematic Diagram | 4-37 |
| 4-29 | Coder-Indicator KY-382/GRN-9D, Keyed 1350 Hz Tone Generator, |  |
|  | Simplified Schematic Diagram ... ... ... | 4-38 |
| 4-30 | Coder-Indicator KY-382/GRN-9D, Development of Pulse Pairs on |  |
|  | Grid of V613B ... | 4-39 |

Fig
Page
$\begin{array}{ll}\text { 4-31 Coder-Indicator KY-382/GRN-9D, Priority Gate, Simplified } \\ & \text { Schematic Diagram ... ... ... ... ... ... ... }\end{array}$
4-32 Coder-Indicator KY-382/GRN-9D, Antenna Synchronization 1350 Hz
$\begin{array}{ll}\text { Oscillator, Simplified Schematic Diagram } & \text {... ... ... }\end{array}$ 4-41
4-33 Radio Set AN/GRN-9D, Transmitter Output Circuit, Simplified $\quad$ 4-43
4-34 Radio Set AN/GRN-9D, Transmitter Pulse Sequence ... ... 4-45
$\begin{array}{lll}\text { 4-35 Frequency Multiplier Oscillator CV-1171/GRN-9D, Shaped Pulse } \\ & \text { Generator, Simplified Schematic Diagram } & \text {... ... ... }\end{array}$
4-36 Frequency Multiplier Oscillator CV-1171/GRN-9D, Gate Pulse
4-37 Amplifier Modulator AM-1701/URN, Simplified Schematic Diagram 4-51
4-38 Control Duplexer C-2226A/GRN-9, Functional Schematic Diagram 4-54
4-39 $\begin{array}{lllllll}\text { Radio Receiver R-842/URN, Power Supply, Simplified Schematic } \\ \text { Diagram ... ... ... ... ... ... ... ... ... } & \text { 4-55 }\end{array}$
$\begin{array}{llll}\text { 4-40 Medium Voltage Power Supply PP-1765/URN, Voltage Regulator, } \\ & \text { Simplified Schematic Diagram } \quad . . \quad \text {... ... ... ... }\end{array}$
4-41 High Voltage Power Supply PP-1763/URN, Simplified Schematic Diagram
4-59

## SECTION 5 - TROUBLESHOOTING

5-1 Switch-Test Adapter SA-420/URN-3 ... ... ... ... 5-2

$\begin{array}{llllll}\text { 5-2a } & \text { Radio Beacon, Servicing Block Diagram (Replacement Test } \\ & \text { Equipment, Table 5-1a) } & \ldots & \ldots . & \ldots & \ldots\end{array} . .$.
5-3 Radio Receiver R-824/URN, Servicing Block Diagram ... ... 5-17
5-4 Radio Receiver R-824/URN, Signal Tracing Waveshapes ... 5-19

5-6 Radio Receiver R-824/URN, I-F Amplifier, Tube Socket Voltage and Resistance Diagram
5-7 Radio Receiver R-824/URN, Preamplifier and Mixer, Tube Socket Voltage and Resistance Diagram
5-26
5-27
5-8 Radio Receiver R-824/URN, Video Chassis, Tube Socket Voltage and Resistance Diagram5-28
5-9 Radio Receiver R-824/URN, Right Side View, Test Point Location 5-29
5-10 Coder-Indicator KY-382/GRN-9D, Servicing Block Diagram ... 5-37
5-11 Coder-Indicator KY-382/GRN-9D, Signal Tracing Waveshapes 5-39
$\begin{array}{ll}\text { 5-12 Coder-Indicator KY-382/GRN-9D, Power Supply Chassis, Tube } \\ & \text { Socket Voltage and Resistance Diagram ... ... ... ... 5-54 }\end{array}$
5-13 Coder-Indicator KY-382/GRN-9D, Video Chassis, Tube Socket Voltage and Resistance Diagram ... ... ... ... .. 5-55
5-14 Coder-Indicator KY-382/GRN-9D, Left Side View, Test Point Location
5-57
5-15 Radio Set, Transmitter, Servicing Block Diagram ... ... 5-63
5-16 Radio Set, Transmitter, Signal Tracing Waveshapes ... ... 5-65
5-17 Klystron Input Incident Test Setup ... ... ... ... 5-72
$\begin{array}{ll}\text { 5-18 Frequency Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, } \\ & \text { Tube Socket Voltage and Resistance Diagram ... ... ... 5-73 }\end{array}$
$\begin{array}{ll}\text { 5-19 Frequency Multiplier Oscillator CV-1171/GRN-9D, High or Low } \\ & \text { Band R-F Chassis, Tube Socket Voltage and Resistance Diagram 5-75 }\end{array}$

| Fig |  | Page |
| :---: | :---: | :---: |
| 5-20 | Amplifier-Modulator AM 1701/URN, Tube Socket Voltage and Resistance Diagram ... ... ... ... ... ... | 5-76 |
| 5-21 | Frequency Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, Bottom View, Test Point Location ... ... ... ... ... | 5-77 |
| 5-22 | Low Voltage Power Supply PP-1766/URN, Tube Socket Voltage and Resistance Diagram ... ... ... ... ... ... ... | 5-85 |
| 5-23 | Medium Voltage Power Supply PP-1765/URN, Tube Socket Voltage and Resistance Diagram | 5-87 |
| 5-24 | High Voltage Power Supply PP-1763/URN, Tube Socket Voltage and Resistance Diagram ... ... ... ... ... ... ... | 5-89 |
| 5-25 | Radio Set, Power Distribution and Control Circuits, Servicing |  |
|  | Block Diagram ... ... ... ... ... ... ... | 5-99 |

## SECTION 6 - REPAIR

| 6-1 | Low Voltage Power Supply PP-1766/URN, Right Side View | 6-2 |
| :---: | :---: | :---: |
| 6-2 | Medium Voltage Power Supply PP-1765/URN, Top View | 6-3 |
| 6-3 | Radio Receiver R-824/URN, Right Side View | 6-4 |
| 6-4 | Frequency Multiplier Oscillator CV-1171/GRN-9D, R-F Chassis, |  |
|  | Bottom View | 6-5 |
| 6-5 | Radio Receiver R-824/URN, Left Side View | 6-6 |
| 6-6 | Coder-Indicator KY-382/GRN-9D, Left Side View with Video |  |
|  | Chassis Lowered | 6-7 |
| 6-7 | Coder-Indicator KY-382/GRN-9D, Right Side View | 6-8 |
| 6-8 | Overall System Delay Measurement Waveforms | 6-10 |
| 6-9 | Frequency Multiplier Oscillator CV-1171/GRN-9D, Video Chassis, |  |
|  | Bottom View | 6-11 |
| 6-10 | Medium Voltage Power Supply PP-1765/URN, Right Side View | 6-13 |
| 6-11 | High Voltage Power Supply PP-1763/URN, Left Side View | 6-14 |
| 6-12 | Crystal Detector for Use in Preamplifier Alignment | 6-14 |
| 6-13 | Test Circuit For Alignment of Preamplifier | 6-15 |
| 6-14 | Receiver Response Characteristics | 6-18 |
| 6-15 | Radio Set AN/GRN-9D, Primary Power Distribution, Schematic |  |
|  | Diagram | 6-19 |
| 6-15a | Sheet 1. Radio Set AN/GRN-9D, Primary Power Distribution, |  |
|  | Schematic Diagram (Replacement Test Equipment, Table 5-1a) | 6-19a |
| 6-16 | Control Duplexer C-2226A/GRN-9, Schematic Diagram | 6-25 |
| 6-16a | Control Duplexer C-2226A/GRN-9, Schematic Diagram (Replacement Test Equipment, Table 5-la) ... | 6-25a |
| 6-17 | Radio Receiver R-824/URN, Schematic Diagram | 6-27 |
| 6-18 | Frequency Multiplier Oscillator CV-ll7l/GRN-9D, Video Chassis, |  |
|  | Schematic Diagram | 6-31 |
| 6-19 | Frequency Multiplier Oscillator CV-1171/GRN-9D, Low and High |  |
|  | Band R-F Chassis, Schematic Diagram | 6-33 |
| 6-20 | Amplifier-Modulator AM-1701/URN, Schematic Diagram | 6-35 |
| 6-21 | Coder-Indicator KY-382/GRN-9D, Video Chassis, Schematic |  |
|  | Diagram | 6-37 |
| 6-22 | Coder-Indicator KY-382/GRN-9D, Power Supply, Schematic Diagram | 6-39 |
| 6-23 | Coder-Indicator KY-382/GRN-9D, Video Frame, Schematic Diagram | 6-41 |
| 6-24 | Low Voltage Power Supply PP-1766/URN, Schematic Diagram | 6-43 |
| 6-24a | Low Voltage Power Supply PP-1766/URN, Schematic Diagram (Replacement Test Equipment, Table 5-la) ... ... | 6-43a |



## SECTION 6 - REPAIR (Contd)

| Fig |  |  |  | Page |
| :--- | :--- | :--- | :--- | :--- |
| 6-63 | Low Voltage Power Supply PP-1766/URN, Top View | $\ldots$ | $\ldots$ | $6-110$ |
| $6-64$ | Low Voltage Power Supply PP-1766/URN, Rear View | $\ldots$ | $\ldots$ | $6-111$ |
| 6-65 | Medium Voltage Power Supply PP-1765/URN, Overall View | $\ldots$ | $6-112$ |  |
| 6-66 | Medium Voltage Power Supply PP-1765/URN, Left Side View |  | $6-113$ |  |
| 6-67 | High Voltage Power Supply PP-1763/URN, Overall View | $\ldots$ | $6-114$ |  |
| $6-68$ | High Voltage Power Supply PP-1763/URN, Top View | $\ldots$ | $\ldots$ | $6-115$ |

## LIST OF TABLES

## SECTION 1-GENERAL INFORMATION

Table

| 1-1 | Radio Set AN/GRN-9D, Equipmen | Supplied |  | 1-6 |
| :---: | :---: | :---: | :---: | :---: |
| 1-2 | Radio Set AN/GRN-9D, Equipment | and Publications | Required but |  |
|  | not Supplied |  |  | 1-9 |
| 1-2a | Radio Set AN/GRN-9D, Equipment | and Publications | Required but |  |
|  | not Supplied (AN/GRA-34) |  |  | 1-10a |
| 1-2b | Radio Set AN/GRN-9D, Equipment | and Publications | Required but |  |
|  | not Supplied (MM-TMC-212A) |  |  | 1-10b |
| 1-3 | Radio Set AN/GRN-9D, Shipping | ata |  | 1-10c |
| 1-4 | Radio Set AN/GRN-9D, Elec |  | Diode | 1-11 |

## SECTION 2 - INSTALLATION

2-1 Initial Control Settings Prior to Energizing ... ... 2-2
2-2 Wiring List of Interconnecting Cables for Shore Radio Beacon Radio Set AN/GRN-9D

2-8
2-3 Electron Tube Installation ... ... ... ... ... 2-11
2-4 Function Switch Position for Testing ... ... ... ... 2-17
2-5 Channel Crystal Frequencies and Preselector Micrometer Cavity Head Settings
$2-21$

SECTION 3-OPERATOR'S SECTION


SECTION 4 - PRINCIPLES OF OPERATION
4-1 Function Switch Positions for Testing ... ... ... 4-15


SECTION 6 - REPAIR
6-1 Preamplifier Alignment Voltage Chart ... ... ... ... 6-15
6-2 Radio Receiver, I-F Amplifier Voltage Chart ... ... ... 6-17

SECTION 7 - PARTS LIST

| 7-1 | Radio Set AN/GRN-9D, List of Major Units |  | 7-3 |
| :---: | :---: | :---: | :---: |
| 7-2 | Radio Set AN/GRN-9D, List of Major Units by | Colloquial Name | 7-4 |
| 7-3 | Radio Set AN/GRN-9D, Maintenance Parts List |  | 7-5 |
| 7-4 | Radio Set AN/GRN-9D, List of Manufacturers | ... ... ... | 7-149 |

CHAPTER 1 - MODIFICATIONS, ELECTRICAL DESCRIPTION

## Para.

## Page

| Control Duplexer (Mod strike-off No.3) |  | 1 |
| :---: | :---: | :---: |
| Low Voltage Power Supply (Mod strike-off No.3) |  | 1 |
| Amplifier Modulator (Mod strike-off No.3) |  | 2 |
| High Voltage Power Supply (Mod strike-off No.3) |  | 2 |
| Control Duplexer (Mod strike-off No.4) |  | 3 |
| Maintenance and Repressurizing |  | 6 |
| Procedure Where a Small Residual Pressure Exists |  | 6 |
| Procedure "A" Where no Discernible Pressure Exists |  | 6 |
| Procedure "B" where no Discernible Pressure Exists |  | 7 |
| Pressure Cannot be Maintained |  | 7 |
| Frequency Multiplier Oscillator (Mod strike-off No.3) |  |  |
| Coder Indicator (Mod strike-off No.4) |  |  |
| Transmitter-Receiver Cabinet (Mod strike-off No.3) |  |  |
| Setting up Identification Code |  | 9 |
| Coder Indicator (Mod strike-off No.2) |  | 12 |
| High Voltage Power Supply (Mod strike-off No.5) |  | 12 |
| Freq. Mult. Osc. - Osc. Sub. Assy. HB/LB (Mod strike-o | off No.3) | 13 |
| Amplifier Modulator (Mod strike-off No.4) |  | 13 |

## CHAPTER 1 - ILLUSTRATIONS

Fig.


## SECTION 8 - MODIFICATIONS (cont'd)

## CHAPTER 2-ELECTRONIC KEYER UNIT (INTRODUCED BY MOD A6364)

## Para.

1 Introduction ... ... ... ... ... ... ... 1
5 Circuit Description ... ... ... ... ... ... ... 2
6
17
18

| Reading | . . | . . | . | . | . . . | . . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reset | . . | . . | . . . | . . . | . . | . . |
| Enter |  | . . . | -•• | -•• | -•• | -•• |
| Setting up the code | . . . | . . . | -•• | -•• | . . . | . . |
| Speed Adjustment . | . . . | . . | ... | ... | ... | . . |2

- 

3

## CHAPTER 2 - ILLUSTRATIONS

Fig. Page
1 Electronic Keyer Unit ... ... ... ... ... ... ... 1
2 Timing Diagram for Entry of " 1 " at $t=0$ (after reset) ... 5
3 Clock Timing Diagram ... ... ... ... ... ... ... 6
4 Control Display Board ... ... ... ... ... ... ... 7
5 Logic Board ... ... ... ... ... ... ... ... 8
6 Keyer Unit Assembly ... ... ... ... ... ... ... 9
7 Keyer Unit Circuit ... ... ... ... ... ... ... 11

## MODIFICATIONS SUMMARY

(completely revised)

These modifications are included in Section 8. The information given in Section 8 supplements and updates earlier sections of this book during the period of transition, when transponders in various states of modification may exist together. Modifications with no electrical significance are omitted here but can be found in the topic 2 publication.

| Mod <br> No. | Leaflet No. | $\begin{gathered} \text { Strike-off } \\ \text { No. } \end{gathered}$ | Brief Description | ```Unit or Sub-unit affected.``` |
| :---: | :---: | :---: | :---: | :---: |
| A3375 | B9 | 3 | E.H.T. Protection Monitor point. | HV Power Supply |
| A3825 | B11 | 3 | $\begin{aligned} & \text { GRN-9D/URN-3A } \\ & \text { Interchangeability. } \\ & \text { Fitting of R.F. Cable. } \end{aligned}$ | Amp-Mod drawer |
| A4295 | B15 | 3 | TMC/Non-TMC switch S 1109. | Control Duplexer |
| A4299 | B16 | 3 | TMC/Non-TMC switch S 1602 | LV Power Supply |
| A3831 | B22 | 2 | GRN-9D/URN-3A <br> Interchangeability | Coder-Indicator |
| A4838 A4837 | B25) | 4 | New cavity <br> (High or Low-band) | Control Duplexer |
| A4620 | B28 | 3 | $\begin{aligned} & \text { Protection resistor } \\ & \text { R1475 } \end{aligned}$ | Freq.Mult.Osc. |
| A6364 | B31 | 4 | Electronic Keyer Unit | Coder-Indicator |
| A6368 | B32 | 4 | Installation of VORTAC switching cables. | Cabinet, Receiver CY-3163/GRN-9D |
| A6726 | B33 | 5 | Resistor R1919 Increased rating | HV Power Supply |
| A7031 | B34 | 3 | Change of valve types | Freq.Mult.Osc. Osc. Sub. Assy. HB / LB |
| B0790 | B35 | 4 | Klystron filament supply resistor. | Amp-Mod drawer |



Figure 1-1. Radio Beacon, Using Radio Set AN/GRN-9D and Antenna Group AN/GRA-60 or AN/GRA-61

## SECTION 1

## GENERAL INFORMATION

## 1-1 INTRODUCTION.

This technical manual provides the general description, theory of operation, and instructions for the installation, operation, and maintenance of Radio Set AN/GRN-9D (see figure 1-1 and table 1-1) constituting a portion of the shorebased installation of a tactical air communication and navigation (TACAN) system.

## 1-2. FUNCTIONAL DESCRIPTION

Radio Set AN/GRN-9D is a shore-based radio set intended for use with Antenna Group AN/GRA-60 or AN/GRA-61. The radio set and the antenna group together function as a radio beacon that provides navigational information for aircraft within a $200-\mathrm{mile}$ radius of the radio beacon. The radio beacon is part of TACAN. Each beacon installation consists of a re-ceiver-transmitter group, a power supply assembly, and an antenna group.

The signals transmitted by the radio beacon provide aircraft equipped with Radio Set AN/ARN-2ł with the distance and bearing information needed to determine their positions.

The AN/ARN-21 transmitter in the aircraft requests distance information by sending out interrogation signals with a repetition pattern peculiar to that transmitter. Reception of these distance interrogations at the radio beacon causes the transmission of a series of replies having the same pattern. The aircraft receives these replies along with other replies emitted by the beacon in response to interrogations from other aircraft. The AN/ARN-21 then picks out its own reply by comparing the reply pulse patterns with that of its own transmitter. Distance is determined by measuring the total time elapsed between the initial transmission of the distance interrogation pulse pair and receipt of the corresponding radio beacon reply pulse pair, and translating this time into miles.

The radio beacon transmits bearing information by rotating a lobed antenna radiation pattern through 360 degrees and then transmitting omni-directional bursts of reference pulse pairs at the instant that the antenna radiation pattern is in certain reference positions. The aircraft obtains its bearing by noting the position of the antenna pattern, as determined by the relative signal strength at the time of the reference burst.

Each of the information elements supplied by the radio beacon is analyzed briefly in the following paragraphs.
a. BEACON IDENTIFICATION.--Every 37.5 seconds, the radio beacon transmits its identifying call in International Morse Code; this enables the aircraft to determine the radio beacon with which it is in contact. The identification signal originates as a $1350-\mathrm{cps}$ tone signal and is then converted into a series of coded pulses that are inserted into the radio beacon output pulse train. These pulses are received by the airborne radio set and converted back into a coded $1350-\mathrm{cps}$ tone signal that is audible to the pilot. Because it is essential that the average output pulse rate of the radio beacon be maintained during transmission of all signal elements, the identification signal is transmitted at the rate of 2700 pulse pairs per second. Each cycle of the 1350 -cps tone signal initiates a pair of pulses spaced 100 microseconds apart. Each pulse of these pairs is then further encoded into pulse pairs having 12-microsecond spacing between pulses. A mechanical keying device in the radio beacon keys the identification tone pulses in and out of the output pulse train. For each dot, the identification tone pulses are transmitted for 0.125 second; for each dash, the identification pulses are transmitted for 0.375 second. During transmission of these dots and dashes, the transmission of distance information is interrupted, but the reception of distance information by the aircraft is not adversely affected. Bearing reference bursts, which are transmitted 135 times per second as a short group of coded pulses, interrupt ihe identification tone pulses in the output pulse train; because of their short duration however, they do not interrupt the audible sig. nal received by the pilot.
b. DISTANCE INFORMATION.-Distance information originates in the aircraft as a series of randomly spaced pulse pairs. These pulse pairs are transmitted by the aircraft and are called the distance interrogation signal. Because the pulse pairs of this signal are randomly spaced, the distance interrogation signal from each aircraft will be different. The radio beacon receives distance interrogation signals from up to 100 aircraft and, after a delay of 50 microseconds, transmits all of these interrogation signals as part of the r-f output pulse train. The distance measuring circuits in each aircraft are capable of extracting from the series of pulses received those reply pulses that have the same random spacing as the pulses in the distance interrogation signal it transmitted. The time interval between transmission of interrogation pulses and reception of reply pulses is measured. After subtracting the 50 -microsecond delay inserted by the radio beacon, the time required for the radio signals to travel from the aircraft to the radio beacon and back again is converted into distance (nautical miles). Distance information appears as a direct-reading meter indication to the pilot.

## GENERAL INFORMATION

c. BEARING INFORMATION. - The bearing information supplied by the radio beacon is originated in the antenna system of the radio beacon. Bearing information consists of four components, each of which is described in this section and more thoroughly described in Section 4.
(1) 15-CPS AMPLITUDE MODULATION. -The $r-f$ output of the transmitter portion of the radio beacon consists of a series of pulse pairs that have an average repetition rate of 3600 pulse pairs per second. The amplitude of these pulses is constant at the output of the transmitter. Therefore, the average carrier level of the $r$-f signal fed to the central array of the antenna is constant. A parasitic element is mounted on a rotatable cylinder that has the central array at its center of rotation. By rotating the parasitic element about the central array at the rate of 15 rps , the signal is modulated in amplitude at the rate of 15 cps . The phase of the $15-\mathrm{cps}$ amplitudemodulation signal, with respect to reference burst received by each aircraft, depends on the bearing of the aircraft relative to the beacon.
(2) 15-CPS REFERENCE BURSTS. - A burst of 12 pulse pairs spaced 30 microseconds apart is transmitted 15 times per second. This pulse group is known as the 15 -cps reference burst or north reference burst. It serves as a timing point from which the phase of the $15-\mathrm{cps}$ amplitude-modulation of the output pulse train may be measured by the airborne radio set. The $15-\mathrm{cps}$ modulation and $15-\mathrm{rps}$ reference burst provide sufficient information to determine the bearing of an aircraft relative to the radio beacon within a 40 -degree sector. The timing of the $15-\mathrm{cps}$ reference burst is determined by trigger pulses initiated by the antenna. When the main lobe of the $15-$ cps modulation signal is directed due east, a $15-\mathrm{cps}$ reference burst is transmitted.
(3) 135-CPS AMPLITUDE MODULATION. Nine parasitic elements are mounted on a rotatable cylinder that has the central array at its center of rotation. As this cylinder is rotated about the central array, the amplitude of the $\mathrm{r}-\mathrm{f}$ signal is modulated at a rate of 135 cps . The cylinder containing the $135-\mathrm{cps}$ modulating element rotates as a unit with the cylinder containing the $15-\mathrm{cps}$ modulating element. Therefore, the phase of the $15-\mathrm{cps}$ modulation and the phase of the $135-\mathrm{cps}$ modulation are locked relative to each other. The phase of the $135-\mathrm{cps}$ signal with respect to the $135-\mathrm{cps}$ reference burst received by an aircraft is dependent on the bearing of the aircraft relative to the beacon.
(4) 135-CPS REFERENCE BURSTS. - A burst of six pulse pairs spaced 24 microseconds apart is transmitted 120 times per second. This pulse group is known as the 135-cps reference burst or auxiliary reference burst. One $135-\mathrm{cps}$ reference burst occurs for each 40 degrees of antenna cylinder rotation except for that 40 -degree point which coincides with the transmission of the $15-\mathrm{cps}$ reference burst. Therefore, eight 135-cps reference bursts are transmitted for each rotation of the antenna cylinder. The $135-\mathrm{cps}$ reference bursts serve as a timing point from which the airborne radio set measures the
phase of the $135-\mathrm{cps}$ amplitude modulation of the received signal. After the bearing of the aircraft has been determined to be within a certain 40 -degree sector by means of the $15-\mathrm{cps}$ modulation and $15-\mathrm{cps}$ reference bursts, the $135-\mathrm{cps}$ modulation and $135-\mathrm{cps}$ reference bursts provide sufficient information to localize the bearing of the aircraft to within plus or $\pm 1$ degree.

## 1-3. FACTORY OR FIELD CHANGES.

All units of the AN/GRN-9D are supplied, on initial delivery, without factory or field changes.

## 1-4. QUICK REFERENCE DATA.

a. NOMENCLATURE. - The official nomenclature for units of Radio Set AN/GRN-9D is as follows:
(1) Receiver-Transmitter OA-3352/GRN-9D contains the following units:
(a) Coder-Indicator KY-382/GRN-9D
(b) Radio Receiver R-824/URN
c. CONTRACTORS. - (i) ITT Federal Laboratories formerly ITT Federal Division, a division of International Telephone and Telegraph Corporation, New Jersey and (ii) National Company Incorporated Melrose, Mass. For the purpose of this manual, the models of the individual manufacturers will be designated ITT and National respectively.
(d) Amplifier-Modulator AM-1701 URN
(e) Frequency Multiplier-Oscillator CV-

## 1171/GRN-9D

(f) Cabinet CY-3163/GRN-9D
(2) Power Supply Assembly OA-1537A/GRN-9A contains the following units:
(a) Low Voltage Power Supply PP-1766 URN
(b) Medium Voltage Power Supply PP-1765 URN
(c) High Voltage Power Supply PP-1763 URN
(d) Cabinet CY-3164 GRN-9D
b. CONTRACT NUMBER. - The contract number is NObsr 81170, dated 26 April 1960.
c. CONTRACTOR. - ITT Federal Laboratories, formerly 1TT Federal Division, a division of International Telephone and Corporation. Clifton, New Jersey is the contractor.
d. COGNIZANT NAVAL INSPECTOR. - The cognizant Naval Inspector is: Inspector of Naval Material, Newark, New Jersey.
e. NUMBER OF PACKAGES INVOLVED. -

Eighteen packages are involved, including equipment spares.

## f. TOTAL CUBIC CONTENTS.

(1) Crated: approximately 460 cubic feet. including equipment spares.
(2) Uncrated: approximately 250 cubic feet, not including equipment spares.

## g. TOTAL WEIGHT.

(1) Crated: approximately 6500 pounds, including equipment spares.
(2) Uncrated: approximately 4000 pounds, not including equipment spares.
h. RADIO BEACON DUTY CYCLE. -The term duty cycle is expressed here as percentage of actual transmitting time per second.
(1) The useful signal pulse-pair contents, per second of operation of the radio beacon, is variable, consisting of:
(a) 180 north reference burst pulse pairs per second (12 pulse pairs occurring 15 times per second).
(b) 720 auxiliary ( 135 cps ) reference burst pulse pairs per second ( 6 pulse pairs occurring 120 times per second).
(c) Identify tone pulses occurring at a rate of 2700 pulse pairs per second when keyed. The actual number of code pulse pairs present depends, however, on the particular code assigned to the radio beacon.
(d) Distance measuring interrogation pulse pairs, the number of which depends on the number of aircraft inter rogating the radio beacon at any particular time. The maximum, for 100 aircraft interrogating the beacon simultaneously, is 2700 pulse pairs per second.
(2) To sustain the sine-wave modulation envelope of the transmitted r-f energy, it is necessary to mantain the total number of pulse pairs transmitted during each second constant. The radio beacon maintains a constant duty cycle by introducing noise pulses into the signal train in a number sufficient to bring the total number of pulse pairs in the sirnal pulse train to 3600 pulse pairs per second. The noise pulses thus introduced into the signal are referred to as squitter. Obviously. since the burst pulse pairs occur at a constant rate, and the identification code pulse pairs also occur at a constant rate. the number of squitter pulses in the signal train varies inversely with the number of aircraft interrogating the radio beacon at any given time. Thus, the number of squitter pulses is maximum when no aircraft is interrogating the beacon, and is minimum when the maximum number of 100 aircraft are inter rogating the radio beacon at any one time. When the number of aircraft interrogating the radio beacon exceeds 100 (that is, when the total number of distance measuring interrogation pulse pairs exceeds the 2700 for which time is available), the excess number of pulse pairs is suppressed.

## i. CHARACTERISTIC OF RADIC BEACON SIGNALS.

(1) All signals transmitted by the radio beacon are characterized by the fact that they consist of pulse pairs, with 12 -microsecond spacing between the two pulses of the pair. The number of pulse pairs per second and the spacings between pulse pairs (the spacing between the leading edge of the first pulse of one pair and the leading edge of the first pulse of the next pair) depend on the particular signal element and are characteristic of that particular signal element. However, it is the spacing of 12 mic coseconds between the pulses of a pair that provides the AN/ARN21 of the aircraft with the means for distinguishing between the signal pulses from the radio beacon and other pulses present on the received radio frequency.
(2) The characteristics of the signal elements as transmitted by the radio beacon are as follows:
(a) NORTH REFERENCE BURST. -The north reference burst consists of 12 pulse pairs. There is 12 -microsecond spacing between pulses of a pair and a 30 -microsecond spacing between pulse pairs, occurring 15 times per second.
(b) AUXILIARY REFERENCE BURST. -The auxiliary reference burst consists of six pulse pairs. There is 12 -microsecond spacing between pulses of a pair and 24 microseconds between pulse pairs occurring 120 times per second at the rate of 135 cps .
(c) IDENTIFICATION CODE. - The identification code consists of a train of 2700 pulse pairs per second. There is 12 -microsecond spacing between pulses of a pair occurring at $1350-\mathrm{cps}$ doublepulsed rate ( 100 microseconds between double-pulsed pairs), keyed by a coding wheel built into the beacon. The tone pulses are synchronized to the reference bursts.
(d) DISTANCE MEASURING INTERROGA-

TIONS. - The distance measuring interrogations consist of pulse pairs with 12 -microsecond spacing between pulses of the pair; spacing between pulse pairs depending on the pulse-repetition rate peculiar to the interrogating aircraft.
(e) SQUITTER PULSES. - Squitter pulses consist of pulse pairs with 12 -microsecond spacing between pulses of the pair. The number of pulst pairs per second depends on the number of interrogations being received by the beacon. with a mimmum spacing of 40 microseconds between puise pairs.

## j. HIGH-BAND AND LOW EAND RADIO BEACON FREQUENCY ALLOCATION.

(1) The radio beacon operates in the frequenc: range between 962 and 1213 mc . This frequency range is divided into two transmitting bands and one receiving band as follows:
(a) The band between 962 and 1024 mc (low band) is used for transmission from the radio beacon.
(b) The band between 1025 and 1150 mc (low and high band) is used for reception by the radio beacon.
(c) The band between 1151 and 1213 mc (high band) is also used for transmission from the radio beacon.
(2) In any one radio beacon, the receiver and transmitter operate at frequencies 63 mc apart; thus, a beacon transmitting at 962 mc receives at 1025 mc . Similarly, a beacon transmitting at 1024 megacycles receives at 1087 megacycles, and a transmitter operating at 1151 megacycles receives at 1088 mc . Finally, a transmitter operating at 1213 mc receives at 1150 mc . These frequencies serve to illustrate how the end frequencies for each band are used and show how the total frequency range of the radio beacon is divided into low band and high band. Thus:
(a) A radio beacon operating in the low band transmits at a frequency between 962 and 1024 mc and receives at a frequency 63 mc above the transmitter frequency. This receiver frequency falls in the band of 1025 and 1087 mc .
(b) Similarly, a radio beacon transmitting in the high band between 1151 and 1213 mc receives at a frequency 63 mc below the transmitter frequency. In this case, the receiver frequency falls in the band between 1088 and 1150 mc .
(3) Radio beacons are provided to operate either in the high band or in the low band, depending on the antenna used. The high-band and the low-band antennas differ in size, but are otherwise basically similar.

## k. FREQUENCY STABILITY.

(1) Transmitter frequency stability is $\pm 25 \mathrm{kc}$ (over the operating range).
(2) Receiver frequency stability is $\pm 50 \mathrm{kc}$ (over the operating range).

1. RECEIVER SELECTIVITY. - The receiver rejects properly coded interrogations on adjacent channels 80 db above the threshold level of a properly coded interrogation in the pass band. Signals arriving at intermediate frequency are suppressed 80 db . All other spurious responses within the 960 - to $1215-\mathrm{mc}$ band are suppressed 75 db . Low-pass filters are provided for the suppression of radar interference from 1650 to $10,500 \mathrm{mc}$. The suppression will be at least 60 db .
m. RECEIVER BANDWIDTH. - The receiver bandwidth is such that the triggering level does not deteriorate by more than 3 db when its total frequency drift is added directly to an incoming frequency drift of $\pm 70 \mathrm{kc}$.
n. TRIGGERING LEVEL. - Receiver triggering level (triggering level is the sensitivity level of the receiver at which a signal will cause the transmitter to fire 60 percent of the time in the absence of refer-
ence and identity pulses) is properly coded interrogation 125 db below 1 watt measured at the input connector on the receiver chassis; it is sufficient to trigger the transmitter under a condition of no load. A properly coded interrogation 124 db below 1 watt measured at the same point is sufficient to trigger the transmitter under a condition of full load. The total number of pulses out of the receiver is $2700 \pm 90$ pulses for conditions of normal loading or for a 50 percent overload.
o. RECEIVER ECHO SUPPRESSION. -Properly spaced pulse pairs do not trigger the transmitter more than 20 percent of the time for any signal 70 db below 1 watt or stronger if the amplitude of the second pulse of the pair is at least 25 db below the amplitude of the first pulse.
p. RECEIVER RECOVERY TIME. -After the second pulse of a correctly coded interrogation which results in decoding, the receiver becomes deactivated. Provisions are made for adjusting the dead time which follows decoding from 20 to 65 microseconds.

## q. RECEIVER INTERMEDIATE FREQUENCY. -

 The receiver intermediate frequency is 63 mc .r. RESPONSE DELAY. -The radio beacon response delay is $50 \pm 0.25$ microseconds measured from the leading edge of the second incoming pulse to the leading edge of the second reply pulse measured at a standard signal strength of 50 db above threshold.
s. INTERROGATION PULSE REPETITION FREQUENCY (PRF). -The average prf of the pulse pairs which this equipment receives shall be 24 cps from each of 95 interrogating sources. In addition, the equipment receives interrogations at a prf of 150 cps from each of five other sources. The equipment shall be considered to be operating at full load when receiving interrogations from both prf sources simultaneously. Under full load conditions and in absence of identification keying, the transmitter shall reply to at least 78 percent of the interrogation.
t. TRAFFIC CAPACITY. - The maximum traffic capacity is 100 aircraft.
u. TRANSMITTER PULSE COUNT LIMITING.From zero to full load, pulse count limiting is effective to maintain the average number of transmitter pulses constant to within $\pm 2.5$ percent of its nominal value.
v. CRYSTAL FREQUENCIES. -The equipment is adjustable to any one of 126 crystal controlled frequencies in the range listed in paragraph 1-4j.
w. CHANNEL FREQUENCY SEPARATION. There is a channel frequency separation of 63 mc between nominal interrogation frequency and nominal reply frequency for all operating channels. There is a channel frequency spacing of 1 mc .
x. MODULATION. -The modulation depth in the horizon for each modulation frequency is $21 \pm 9$ percent at the respective frequency bands. The modulation
frequencies produced by the antenna are 15 cps and 135 cps (the ninth harmonic of 15 cps ). The horizontal antenna pattern is a scalloped cardioid. Pulse type transmission at a rate of 3600 pulse pairs per second (includes reference groups and distance replies).
y. TRANSMITTER IDENTIFICATION.--Identification is provided by switching the transmitter from pulse pairs of random spacing to pulse pairs which occur at a fixed frequency rate of 1350 cps during the keydown position. The first pulse of the identity occurs $740 \pm 50$ microseconds after the first pulse of each auxiliary reference group.

## z. TRANSMITTER REFERENCE PULSES (FOR BEAR-

 ING INFORMATION).-A total of 120 code groups are transmitted at a rate of 135 cps . Each code group consists of six pulse pairs spaced 24 microseconds apart. Fifteen code groups per second are transmitted at a rate of 15 cps . Each of these code groups consist of 12 pulse pairs spaced 30 microseconds apart.aa.SQUITTER RATE. -Squitter rate is the rate of random firing of the transmitter in the absence of interrogations. The total number of pulses out of the receiver is $2700 \pm 90$ for normal operation.
ab.TRANSMITTER POWER OUTPUT.- The power output of the transmitter is 7 kw minimum.
ac.TRANSMITTER R-F DUTY CYCLE.-Under normal operation at 3600 pulse pairs per second, the transmitter r-f duty cycle is $\pm 2.5$ percent.
ad.PULSE SPECTRUM.--The energy level contained in an 0.5 -megacycle bandwidth, centered about a frequency $\pm 0.8 \mathrm{mc}$ fiom the nominal frequency, is 60 db below the energy level contained in an $0.5-\mathrm{mc}$ bandwidth centered about the nominal frequency. The energy level contained in an $0.5-\mathrm{mc}$ bandwidth centered about a frequency $\pm 2.0 \mathrm{mc}$ from the nominal frequency is more than 65 db below the energy level contained in an $0.5-\mathrm{mc}$ bandwidth centered about the nominal frequency.
ae. POWER INPUT REQUIREMENTS. - All incoming primaty power is brought to the input terminals of ReceiverTransmitter OA-3352/GRN-9D and is used either within the receiver-transmitter group or redistributed to Power Supply Assembly OA-1537/GRN-9A, associated antenna group, and the convenience outlets on each of these units.

The receiver-transmitter group and the power supply assembly (less convenience outlets) have a 208 -volt, 4 -wire, 3 -phase, $60-\mathrm{cps}, 6.8 \mathrm{kw}, 7.2 \mathrm{kva}$ power consumption with an 0.9 power facton and a maximum current of 25 amperes per phase.

## 1-5. EQUIPMENT LISTS

## a. EQUIPMENT SUPPLIED.

The major components of the radio set are contained in two main groups, the receiver-transmitter group and the power
supply assembly. The complete equipment supplied by the manufacturer is listed in table 1-1, and illustrated in figures 1-2 and 1-3.

## NOTE

Space is provided in the power supply assembly of the radio set for the test equipment listed in table 1-2 Switch-Test Adapter SA-420/URN-3 is mounted external to the radio set. The test equipment, referred to as built-in test equipment, is to be installed by the using activity after delivery of the beacon power supply assembly from the manufacturer.

## b. EQUIPMENT AND PUBLICATIONS REQUIRED BUT

 NOT SUPPLIED.--Additional equipment required for the operation of the radio set, but not supplied by the manufacturer under this contract, is listed in table 1-2.c. SHIPPING DATA.--The dimensions, volumes, and weights of the equipment, packed and ready for shipment, are listed in table 1-3.
d. EQUIPMENT SIMILARITIES.--The Radio Set AN/GRN9D, produced by the National Co. Inc., is similar to both the AN/GRN-9A and AN/GRN-9D manufactured by ITT Federal Laboratories. There are, however, certain differences between the models; mainly in the transmitter output power, the type of antenna group used, the primary power supply requirements and the power distribution circuits. Where differences occur between the ITT and National models, reference is made to them in the text, schematics and wiring diagrams.
(1) RECEIVER-TRANSMITTER OA-3352/GRN-9D SIMILARITIES.-The radio receiver and the amplifier-modulator in the AN/GRN-9D are identical to those in the AN/GRN. 9A.
(2) RECEIVER-TRANSMITTER OA-3352/GRN-9D DIFFERENCES
(a) The coder-indicator in AN/GRN-9D is similar to that in the AN/GRN-9A, except that the magnetic variation unit, the METER SELECTOR switch, the ANTENNA POSITION SELECTOR switch, and the SET TO MAGNETIC VARIATION dial, have been deleted. Also, the identification tone keyer assembly, has been slightly modified. The wiring of the unit has been changed to incorporate these modifications.
(b) The differences which occur between the various models of Control Duplexer are:

1. ITT Federal Laboratories - The Control Duplexer in the AN/ $\overline{\mathrm{GRN}}$-9D is similar to that in AN/GRN-9A with the following exceptions. The high-and low-band filters in AN/GRN9D are of the sealed, gas-filled, temperature-stabilized type. The desiccant chamber and flexible tubing have been deleted. Temperature stability of the filters in the AN/GRN-9D is achieved by use of a thermostatically-controlled heating element housed in the filter assembly. A CAVITY HEATER ON lamp is provided on the front panel and indicates the operation of the heater element.
2. National Co. Inc. - The filters of the AN/GRN9D Control Duplexer of this model are not temperature-stabilized although they are sealed and, as with the AN/GRN-9A (ITT), a desiccant chamber has been incorporated.

TABLE 1-1. RADIO SET AN/GRN-9D, EQUIPMENP SUPPLIED

| $\begin{gathered} \text { QTY } \\ \text { PER } \\ \text { EQUIP. } \end{gathered}$ | $\begin{gathered} \text { QTY } \\ \text { PER } \\ \text { GROUP } \end{gathered}$ | NOMENCLATURE |  | OVERALL DIMENSIONS ${ }^{1}$ |  |  | VOLUME ${ }^{1}$ | WEIGHT ${ }^{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | NAME | DESIGNATION | HEIGHT | WIDTH | DEPTH |  |  |
| 1 |  | ReceiverTransmitter | OA-3352/GRN-9D | 72 | 25 | 34-1/8 | 35.5 | 1126 |
|  | 1 | Coder-Indicator | KY-382/GRN-9D |  |  |  |  |  |
|  | 1 | Radio Receiver | R-824/URN |  |  |  |  |  |
|  | 1 | Control- <br> Duplexer | C-2226A/GRN-9 |  |  |  |  |  |
|  | 1 | AmplifierModulator | AM-1701/URN |  |  |  |  |  |
|  | 1 | Frequency MultiplierOscillator | CV-1171/GRN-9D |  |  |  |  |  |
|  | 1 | Cabinet | CY-3163/GRN-9D |  |  |  |  |  |
| 1 |  | Power Supply Assembly | OA-1537A/GRN-9A | 72 | 25 | 34-1/8 | 35.5 | 986 |
|  | 1 | High Voltage <br> Power Supply | PP-1763/URN |  |  |  |  |  |
|  | 1 | Medium Voltage Power Supply | PP-1765/URN |  |  |  |  |  |
|  | 1 | Low Voltage Power Supply | PP-1766/URN |  |  |  |  |  |
|  | 1 | Cabinet | CY-3164/GRN-9D |  |  |  |  |  |
|  | 1 | Test Equipment Cable Harness |  |  |  |  |  |  |
| 2 |  | Technical Manual | NAVSHIPS $93881(\mathrm{~A})$ |  |  |  |  |  |
| 1 |  | Performance Standards Sheet | NAVSHIPS 93881.32 |  |  |  |  |  |
| 1 |  | Maintenance Standards | NAVSHIPS 93881.42 |  |  |  |  |  |

${ }^{1}$ Dimensions in inches, volume in cubic feet, and weight in pounds, unless otherwise stated.
3. The wiring of the units has been adjusted to suit the various differences.
(c) The frequency multiplier-oscillator in the AN/GRN-9D is similar to that in the AN/GRN-9A with the following exceptions:

1. Additional $\mathbf{r}$-f shielding is incorporated in order to reduce the radiation of superfluous r-f energy.
2. The crystal oven assemblies used in the high-band and low-band $r$ - f chassis have been slightly modified. The adjustable coil provided in the AN/GRN-9A crystal oven assembly has been deleted.
3. The wiring of this unit has been changed to incorporate these modifications.
(d) The cabinet in the AN/GRN-9D is similar to that in the AN/GRN-9A except that relay 1902 and


Figure 1-2. Receiver-Transmitter OA-3352/GRN-9D, Overall View
terminal board TB906 have been deleted, and the wiring has been extensively changed to incorporate the modifications in the receiver-transmitter group.
(3) POWER SUPPLY ASSEMBLY OA-1537A/ GRN-9D SIMILARITIES. - The high voltage power supply, the medium voltage power supply, and the low voltage power supply in the AN/GRN-9D are identical to their counterparts in the AN/GRN-9A.
(4) POWER SUPPLY ASSEMBLY OA-1537A/ GRN-9D DIF FERENCES. - The cabinet in the AN/GRN-

9D is similar to that in the AN/GRN-9A except that the AN/GRN-9D cabinet has a switch to reduce the high voltage applied to the klystron during the performance of aging the klystron. The wiring of the AN/ GRN-9D cabinet has been changed to reflect this modification.
e. ELECTRON TUBE COMPLEMENT. -The full complement of electron tubes used in the equipment is broken down in table 1-4 to show the number of each type used in each of the component units and also the total number of each type used in the equipment.


Figure 1-3. Power Supply Assembly OA-1537/GRN-9A, Overall View

TABLE 1-2. RADIO SET AN/GRN-9D, EQUIPMENT AND PUBLICATIONS REQUIRED BUT NOT SUPPLIED

|  | NOMENCLATURE |  | REQUIREDUSE | REQUIRED <br> CHARACTERISTICS |
| :---: | :---: | :---: | :---: | :---: |
|  | NAME | DESIGNATION |  |  |
| 1 | Power Meter-Pulse Counter | TS-891/URN-3 | Performs power measurements, counts radio beacon squitter output pulses, and determines reply rate. Also checks receiver sensitivity. | Provides variable d-c source used to bias a diode in switch-test adapter and provides facilities for counting pulses. |
| 1 | Switch-Test Adapter | SA-420/URN-3 | Performs power measurements. | Provides means of transferring radio beacon transmitter output power from antenna to dummy load and supplies detected signal to test equipment. |
|  | Technical Manual | $\begin{aligned} & \text { NAVSHIPS } \\ & 92809 \end{aligned}$ |  |  |
| 1 | Oscilloscope | OS-54/URN-3 | Measures signal waveform amplitude and pulse width. | Provides timing markers and calibrating voltage to permit accurate measurements. |
|  | Technical Manual | NA VSHIPS 92778 |  |  |
| 1 | Pulse AnalyzerSignal Generator | $\begin{gathered} \text { TS-890A/URN-3 } \\ \text { or } \\ \text { TS-890B/URN-3 } \end{gathered}$ | Tests operation of radio beacon and analyzes radio beacon output signal. | Provides r-f carrier source and calibrated receiver for spectrum analysis of a signal. |
|  | Technical Manual | NAVSHIPS $93231$ |  |  |
| 1 | Pulse Sweep Generator | SG-121A/URN-3 | Simulates pulse output of one or more airborne Radio Sets AN/ -ARN-21. | Provides facilities for generating pulsed pairs at controlled variable rate. |
|  | Technical Manual | NAVSHIPS $92745$ |  |  |

TABLE 1-2. RADIO SET AN/GRN-9D. EQUIPMENT AND PUBLICATIONS REQUIRED BUT NOT SUPPLIED (cont)

| $\begin{gathered} \text { QTY } \\ \text { PER } \\ \text { EQUIP. } \end{gathered}$ | NOMENCLATURE |  | REQUIREDUSE | REQUIRED <br> CHARACTERISTICS |
| :---: | :---: | :---: | :---: | :---: |
|  | NAME | DESIGNATION |  |  |
| 1 | Antenna Group <br> Technical Manual | AN/GRA-60 <br> or AN/GRA-61 <br> or equivalent | Transmits r-I output signal of radio set. receive distance interrogation signals from aircraft, and modulates radio beacon r-f output. Provides facilities for transmitting $\mathrm{r}-\mathrm{f}$ output of the radio set, modulating radio set $\mathbf{r}$-f output so that envelope of $\mathrm{r}-\mathrm{f}$ signal is modulated in a mplitude at 15cps and $135-\mathrm{cps}$ rates, generating trigger pulses that time generation by radio set of bearing reference pulse groups, and receiving distance interrogation signals from aircraft equipped with AN/ARN-21 or equivalent. | Frequency range transmission: 962 to 1024 mc (low-band operation) or 1151 to 1213 mc (highband operation) <br> Frequency range reception: 1025 to 1087 mc (low-band operation) or 1088 to 1150 mc (highband operation) <br> Vswr: not more than 2 to 1 over the specified transmission band <br> R-f power: 20-kw peak power with a duty cycle of 2 percent <br> Antenna impedance: 50 ohms <br> Polarization: vertical <br> Horizontal pattern: scalloped cardioid rotated at 15 cps ( 900 rpm ) <br> Vertical pattern: maximum carrier energy is radiated above a plane perpendicular to axis of antenna |


| TABLE 1-2a. RADIO SET AN/GRN-9D. EQUIPMENT AND PUBLICATIONS REQUIRED BUT NOT SUPPLIED (AN/GRA-34) |  |  |
| :---: | :---: | :---: |
| Qty per Equip. | NOMENCLATURE | EQUIPMENT CHARACTERISTICS |
| 1 | Antenna Transfer Switching Unit SA-544/GRA-34 <br> Technical Manual: <br> NAVSHIPS 93121(A) | In response to alarm or proper diallingsignals, provides automatic switching of either of the TACAN transmitters r.f. output to one antenna group input; also provides a facility for manual switching. The unit incorporates dummy load facilities to permit maintenance tests to be performed on either or both transmitters under load conditions. The chassis also provides for manual switching of the antenna azimuth leads from either of the two transmitters. The unit incorporates, and supplants the SA-420/ URN-3 Switch Test Adapter listed in TABLE 1-2. |
| 1 | Radio Set Transfer Control C2233/GRA-34 <br> Technical Manual: NAVSHIPS 93121(A) | Provides for manual and automatic control, alarm indication, telephone facilities and simulation testing; also provides power for the entire transfer control chassis. |
| 2 | Radio Frequency Monitor MX-2229/GRA-34 <br> Technical Manual: NAVSHIPS 92975(A) | Provides a continuous and complete check of all TACAN functions and provides an alarm signal, after a suitable delay, in the event of system malfunction. |
| 1 | Electrical Equipment Cabinet CY-2200/GRA-34 <br> Technical Manual: <br> NAVSHIPS $93121(A)$ | The four above-mentioned major components plus a fan are housed in this cabinet which provides interconnections between the components and facilities for interconnection to related units. |
| 1 | Remote Switching Control C2234/GRA-34 <br> Technical Manual: <br> NAVSHIPS 93121 (A) | This unit contains alarm indicators, a standard navy telephone for communication with the local station and a telephone dial which effects the same functions as the telephone dial of the Radio Set Transfer Control Unit at the local station. |


|  | TABLE 1-2b. RADIO SET AN/GRN-9D: EQUIPMENT AND FUBLICATIONS REQUIRED BUT NOT SUPPLIED (MM-TMC-212A) (This equipment supersedes that listed in TABLES 1-2 and 1-2a) |  |
| :---: | :---: | :---: |
| Qty Per Equip. | NOMENCLATURE | EQUIPMENT CHARACTERISTICS |
| 1 | TACAN Transfer and Switching Unit MM-1602 <br> Technical Manual: <br> AP 116C-0702-1D6D | In response to an external command, the unit provides automatic transfer of TACAN beacons between antenna and dummy load and between beacon and test equipment. The unit also provides facilities for sampling the transmitter output signals and injection of interrogation signals. Manual switching is also provided in the event of automatic transfer failure. |
| 1 | Spectrum Analyzer/Test Generator MM-705 <br> Technical Manual: <br> AP 116C-0702-1H6H | The unit tests the operation of the radio beacon and analyzes the radio beacon output. <br> The spectrum analyzer section provides the facility to measure the transmitted energy in each of six bands adjacent to the transponder transmitting frequency, as well as the onchannel energy. <br> The test generator section provides (a) a suitable signal to use for aligning the IF stages of the beacon receiver and (b) the r.f. energy. (at beacon receiver frequency) for testing and maintenance purposes. |
| 1 | Oscilloscope MM-504 <br> Technical Manuals: <br> AP 116C-0702-1J6J <br> AP 116C-0702-1K6K | This unit enables inspection and measurement of of the amplitudes and pulse-widths of all signals associated with the GRN-9D and its associated test equipment. |
| 1 | Power Meter - Pulse Counter Marker Generator MM-109 | This unit enables the following functions to be performed by the MM-TMC-212A. <br> (a) Power Meter - measures the peak r.f. power output of the GRN-9D and its test equipment in the frequency range 960 to 1215 MHz . The unit is used in conjunction with the Transfer and Switching Unit which, in this instance of its use, provides the necessary facilities for sampling the transmitter output signal and the interrogation signals. |
|  | Technical Manual: AP 116C-0702-1G6G | (b) Pulse Counter - measures the average repetition rates of all the pulse sources in the GRN-9D and its test equipment. <br> (c) Marker Generator - provides precision time marker pulses for modulating the $Y$ and 2 axis of the MM-504 Oscilloscope. The markers are used for measurements of pulse width, pulse spacing, time intervals and frequencies |


| TABLE 1-2b. RADIO SET AN/GRN-9D. EQUIPMENT AND PUBLICATIONS REQUIRED BUT NOT SUPPLIED (MM-TMC-212A) (cont) (This equipment supersedes that listed in TABLES $1-2$ and $1-2 a$ ) |  |  |
| :---: | :---: | :---: |
| Qty Per Equip. | NOMENCLATURE | EQUIPMENT CHARACTERISTICS |
| 1 | Transfer and State Transmission Unit (TELOTEL) and associated logic interface. <br> Technical Manual:* <br> AP 116C-0702-1L6L <br> *Note. This manual also contains details of the central information centre. | On receiving an alarm signal (confirmed by both Transponder Monitors) of a parameter failure, the unit sends a command signal to the Transfer and Switching Unit thereby initiating a transfer of beacons between antenna and dummy load. The unit is also capable of accepting specific failure data from the monitors and other nonelectronic parts of the system (e.g. frequency converter) and transmitting an indication of such a failure to a remote indicator. <br> Facilities are provided whereby the unit can automatically call a central station remote from the installation and pass such failure data as it has received. |
| 2 | TACAN Transponder Monitor MM-209 <br> Technical Manuals: <br> AP 116C-0702-1E6E <br> AP 116C-0702-1F6F | These units automatically provide, every 4 seconds, a detailed analysis of 13 TACAN transponder parameters and in the event of a failure of any one of them will register, after a preset time delay, an alarm indication. The particular parameter malfunction is retained as a memory indication. The units are interconnected such that a failure must be registered by both units before an alarm condition is signalled. |
| 1 | Electrical Equipment Cabinet MM-TMC-212A <br> Technical Manuals: <br> AP 116́C-0702-1A6A <br> AP $116 \mathrm{C}-0702-1 \mathrm{~B} 6 \mathrm{~B}$ <br> AP $116 \mathrm{C}-0702-1 \mathrm{C} 6 \mathrm{C}$ | The seven above-mentioned major components plus two ventilation fans are housed in this cabinet, which provides interconnections between the components and facilities for interconnection to related units. <br> The technical manuals listed cover the following aspects of the Electrical Equipment Cabinet and its associated units: <br> (a) 1A6A - Installation Instructions <br> (b) $1 B 6 B$ - Overall servicing manual <br> (c) 1C6C - Beacon Performance testing. |

TABLE 1-3. RADIO SET AN GRN-9D, SHIPPING DATA

| BOX NO. $^{2}$ | NOMENCLATURE |  | OVERALL DIMENSIONS $^{1}$ |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  | NAME | DESIGNATION | HEIGHT | WIDTH | DEPTH |  | WEIGHT |
|  | Receiver-Transmitter | OA-3352 GRN-9D | 90 | 44 | 46 | 105 | 1935 |
|  | Power Supplv <br> Assembly | OA-1537A GRN -9A | 90 | 44 | 46 | 105 | 1655 |
|  | Tube. Klvstron | SAL-89 | 30 | 20 | 20 | 7 | 78 |
|  | Equipment Spares |  |  |  |  |  |  |

${ }^{1}$ Dimensions in inches, volume in cubic feet, and weight in pounds. unless otherwise stated.
${ }^{2}$ Box numiers have not been assigned.
Issued June 73

TABLE 1-4. RADIO SET AN/GRN-9D, ELECTRON TUBE AND GERMANIUM DIODE COMPLEMENT

|  | NUMBER OF TUBES AND GERMANIUM DIODES OF TYPES INDICATED |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| UNIT | \|r | $\stackrel{\sim}{\sim}$ | R | $\left\lvert\, \begin{aligned} & \infty \\ & \mathbf{N} \\ & \underset{Z}{Z} \end{aligned}\right.$ | $\left\|\begin{array}{l} \infty \\ 0 \\ \underset{\sim}{z} \\ \end{array}\right\|$ | $\left\|\begin{array}{l}  \\ \underset{\sim}{4} \\ \underset{\sim}{0} \\ \underset{N}{2} \end{array}\right\|$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 3 \\ & 0 \\ & \text { 落 } \end{aligned}$ | $\left\|\begin{array}{c} 9 \\ \substack{9 \\ 4 \\ \infty} \end{array}\right\|$ | $\left\|\right\|$ | $\left\lvert\, \begin{aligned} & 3 \\ & \underset{X}{*} \\ & \underset{心}{*} \end{aligned}\right.$ | $\left\|\begin{array}{l} 4 \\ \underset{n}{2} \\ \hline \mathbf{c} \end{array}\right\|$ | $\left\|\begin{array}{l} 4 \\ 3 \\ 2 \\ 6 \\ \underset{\sim}{4} \\ \underset{\sim}{4} \end{array}\right\|$ |  | $\left\|\begin{array}{c} \infty \\ \underset{\infty}{\infty} \\ \underset{\infty}{2} \end{array}\right\|$ | $\underset{\infty}{\infty}$ | $\left\|\begin{array}{l} 4 \\ 3 \\ 3 \\ 8 \\ 80 \end{array}\right\|$ | $\left\lvert\, \begin{aligned} & 3 \\ & 0 \\ & 0 \\ & 4 \\ & d \\ & 0 \\ & \vec{~} \\ & 0 \\ & 0 \end{aligned}\right.$ | $\left\|\begin{array}{l} 0 \\ \hline 0 \\ 8 \end{array}\right\|$ |  |  |  | $\left\lvert\, \begin{aligned} & 4 \\ & \underset{\sim}{4} \\ & \infty \\ & \sim \end{aligned}\right.$ | 3 3 3 3 3 0 0 0 0 0 |  | \|e: |  | $\left\|\begin{array}{l} \mathbb{4} \\ B \\ 0 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{array}\right\|$ | \|o이 | TOTAL |
| Radio Receiver R-824/URN | 2 |  |  | 5 |  |  | 1 |  | 1 | 1 |  | 3 |  |  |  |  | 8 | 3 |  | 2 | 3 |  | 1 | 1 |  |  | 2 |  | 33 |
| Coder-Indicator KY-382/GRN-9D |  |  | 6 |  |  |  | 1 | 1 |  | 1 |  | 7 |  |  |  |  |  | 5 | 3 |  |  |  |  | 1 |  |  | 1 |  | 26 |
| AmplifierModulator AM-1701/URN |  |  |  |  | 2 |  |  |  |  |  |  |  | 1 |  |  | 1 | 1 |  | 1 |  |  |  |  |  |  |  |  |  | 6 |
| Frequency MultiplierOscillator CV-1171/GRN9D |  | 2 | 2 |  |  | 6 |  |  | 2 |  | 1 |  |  |  |  |  | 2 | 2 | 4 |  |  | 1 |  |  | 5 |  |  |  | 27 |
| Low Voltage Power Supply PP-1766/URN |  |  |  |  |  |  | 3 |  |  |  |  | 2 |  | 3 |  | 2 |  |  |  |  |  |  |  |  |  |  |  |  | 10 |
| Medium Voltage Power Supply PP-1765/URN |  |  |  |  |  |  |  |  |  |  |  | 1 |  | 5 | 2 |  |  |  |  |  |  |  |  |  |  | 5 |  |  | 13 |
| High Voltage Power Supply PP-1763/URN |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 | - 6 |
| Total Number of Each Type | 2 | 21 | 8 | 5 | 2 | 6 | 5 | 1 | 3 | 2 | 1 | 13 | 1 | 8 | 2 | 3 | 11 | 10 | 8 | 2 | 3 | 1 | 1 | 2 | 5 | 5 | 3 | 6 | 121 |

${ }^{1}$ Crystal detector assembly E1152, one of which is supplied with each radio set, contains one 1 N 25 diode.


Figure 2-1. Receiver-Transmitter Group or Power Supply
Assembly, Typical Unpacking Diagram

## SECTION 2

## INSTALLATION

## 2-1. UNPACKING AND HANDLING.

a. GENERAL. -The components and accessories of Radio Set AN/GRN-9D are packed in several crates. For a list of crates and packages constituting the complement of a radio set, refer to table 1-3. Before unpacking the equipment, determine the exact location for each major component; then bring the crate containing the component to the immediate vicinity of the location selected for it. Unpack the equipment, one component at a time, in the order in which the major components are to be installed.
b. TYPICAL UNPACKING PROCEDURE. - A typical component unpacking diagram is shown in figure 2-1. Unpack the equipment in accordance with the procedure outlined in the following steps:

Step 1. Use nail puller to remove all nails.
Step 2. Remove outer layer of waterproof paper.
Step 3. Remove all straps.
Step 4. Remove top and sides of wooden crate.
Step 5. Tear off inner layer of waterproof paper.
Step 6. Check humidity indicator for presence of moisture.

## CAUTION

If humidity indicators show that moisture has penetrated to equipment, examine equipment carefully for signs of corrosion or fungus.

Step 7. Remove desiccant.
Step 8. Remove corrugated pads.
Step 9. Remove front blocking strip.
Step 10. Install two eyebolts and attach tackle to support weight.


#### Abstract

Note The consolidating parts box, which is included in shipment of radio beacon, contains two eyebolts that are used when lifting re-ceiver-transmitter group and power supplytest set group. The consolidating parts box also contains electron tubes to be installed in these groups, as well as cable connectors, etc.


Step 11. Loosen turnbuckle.

Step 12. Remove clamp and blocks.
Step 13. Lift cabinet off platform by means of eyebolts.

Receiver-Transmitter OA-3352/GRN-9D and Power Supply Assembly OA-1537A/GRN-9A are now uncrated and ready for installation. Before connecting cables or applying power, make certain that the front-panel controls are set to the positions shown in table 2-1.

## 2-2. POWER REQUIREMENTS AND DISTRIBUTION.

The overall primary power distribution for the radio set is shown in figure 6-15. All incoming primary power is brought to the input terminals of the receiver-transmitter group, the associated antenna group, and the convenience outlets on each of these units.

The power requirements for the receiver-transmitter group and the power supply assembly are 208 volts, 4 wire, 3 phase, $60 \mathrm{cps}, 6.8 \mathrm{kw}, 7.2 \mathrm{kva}$, with an 0.9 -power factor and a maximum current of 25 amperes per phase.

The power requirements for the convenience outlets are 120 volts, 1 phase, $60 \mathrm{cps}, 15$ amperes maximum, and 1.8 kva maximum obtained either from a 208 -volt, 4 -wire, 3 -phase, $60-\mathrm{cps}$ source or from an auxiliary 120 -volt, 1 -phase, 60 -cps source.

## 2-3. INSTALLATION LAYOUT.

The receiver-transmitter group and power supply assembly should be placed as close together as practical (but a minimum of 15 inches apart) so as to be accessible for operation and maintenance. The maximum permissible distance between the cabinets is 5 feet. Figure $\mathbf{2 - 2}$ shows the placement of the components of a radio set for a typical installation and the dimensional data and mounting details.

## 2-4. INSTALLATION REQUIREMENTS.

a. CABLE FABRICATION. - For the multiconductor cables, a terminal lug-type connection is satisfactory. This connection is applicable to all cables shown except those with RG-18A/U and RG-10/U designations.
(1) REMOVING ARMOR. - The method of removing the armor is as follows:

Step 1. Form cable as it is to be run into stuffing tube; carefully estimate where cable should come

TABLE 2-1. INITIAL CONTROL SETTINGS PRIOR TO ENERGIZING

| NAME OR <br> PANEL MARKING | REFERENCE <br> SYMBOL | LOCATION | INITIAL <br> POSITION |
| :--- | :---: | :--- | :--- |
| EMERGENCY SWITCH | S901 | Front panel of receiver-transmitter <br> group blower compartment | OFF (arrow pointing <br> left or right) |
| MASTER SWITCH | S1101 | Panel of control-duplexer | OFF |
| CODER-INDICATOR | S601 | Panel of coder-indicator | OFF |
| Receiver ON-OFF | S502 | Panel of radio receiver | OFF |
| ANTENNA CONTROL | S1102 | Panel of control-duplexer | OFF |
| FIL ON | S1108 | Panel of control-duplexer | OFF |
| LV | S1601 | Panel of low voltage power supply | OFF |
| MV | S1801 | Panel of medium voltage power supply | OFF |
| HV | S1902 | Panel of high voltage power supply | OFF |
| BATTLE SHORT | S1107 | Panel of control-duplexer | NOR |
| HIGH VOLTAGE | S1006 | Power supply assembly | BREAK IN |

through tube. Mark this position with piece of friction tape.

Step 2. Cut armor with either a diagonal cutter or an armor stripper. If using diagonal cutter, be careful not to cut through insulation.

Step 3. Cut either in front of tape marker or within it. By cutting just in front of marker, cut can be closely observed. Frayed edges of armor can then be trimmed away. When cutting within tape marker, tape serves to hold frayed edges down, but care must be used to avoid cutting insulation.

## CAUTION

Do not cut insulation when cutting armor, to prevent frayed armor edges from penetrating cable and causing grounding.
(2) STRIPPING INSULATION. -After armor has been removed, start to remove the insulation approximately $1 / 2$ inch from where armor terminates. The following procedure is recommended in stripping insulation:

Step 1. Place one end of cable in vise or have another man hold cable.

Step 2. Put a bend in cable and carefully ring insulation, taking care to cut only insulating jacket and not into insulation of individual conductors.

Step 3. With knife blade at an angle, start cutting a strip lengthwise, approximately $1 / 2$ inch wide and
long enough to allow side cutters to get grip on insulation.

Step 4. Pull down on cut with side cutters; this action will form a $1 / 2$-inch strip. After stripping approximately 4 inches, remainder of strip can usually be removed by hand.
(3) APPLYING TERMINAL LUGS. - Remove just enough insulation so that the stripped conductor fits lug exactly. Always use lug large enough to fit over all strands of conductor. All lugs used must be soldered; however, solderless-type lugs may also be used to provide good mechanical and electrical connection by crimping before soldering (figure 2-3). A solder lug, type 20-14 (SNSN G17-L-14325) or equivalent, is connected to the cable conductors as follows:

## Note

Cables used in this installation have a waterproofing compound (silicone grease) which fills all voids even in individual conductors. This grease makes the soldering of terminal lugs very difficult. Individual strands must be cleaned with Decalene (deca-hydronapthalene).

Step 1. Slip lug over inner conductor and heat with soldering iron.

Step 2. As lug becomes warm, force it under insulation so that when it cools off it has added support of insulation (B, figure 2-3).


Figure 2-2. Receiver-Transmitter Group and Power Supply Assembly, Typical Outline Drawing

A. SOLDERLESS TYPE


Figure 2-3. Method of Attaching Terminal Lugs

Step 3. Make sure that inner conductor is well bonded and secured to solder lug.
(4) ASSEMBLY OF CABLE RG-27/U. - Cable RG-27/U is connected between the receiver-transmitter group and power supply assembly. This cable has a standard lug-type termination, fastened by a nut to special standoff insulator binding posts E903 and E1001. Six inches of the armor should be removed from each end before the cable is inserted in the stuffing tubes.

The shielding at each end of the cable should be grounded. The two layers of shielding should be soldered together and then connected to the ground terminals on terminal board TB1002 in the power supply-test assembly entrance box and on binding post E999 in the receiver-transmitter cable entrance box.

## CAUTION

At least 4 inches of the thin layer of conducting rubber over the inner insulation must be removed; otherwise the high voltage will cause a breakdown. If the inner insulation is cut even slightly during preparation, the high voltage will eventually cause a breakdown.
(5) ASSEMBLY OF CABLE RG-18A/U. -Cable RG-18A/U is connected between the antenna and the receiver-transmitter group. An r-f cable connector, UG-154A/U connects one end of this cable through adapter UG-216B/U to receiver-transmitter group jack J1155. Plug UG-1041-A/U connects the other end of this cable to antenna jack J3302, type $427 \mathrm{~B} / \mathrm{U}$. Figure 2-4 provides complete instructions for assembly of a connector UG-154A/U to cable RG-18A/U.

## Note

Before mating connector UG-154A/U into adapter, coat face of dielectric with dielectric compound ANA Specification AN-D-128.
(6) ASSEMBLY OF CABLE RG-10/U. - Cable RG-10/U is connected between the antenna and the receiver-transmitter groups. The r-f cable connectors UG-943A/U for the $135-\mathrm{cps}$ and 15 -cps reference pulse cables connect both ends of these cables to the equipment. Figure 2-5 provides complete instructions for this connector.

## b. LAYOUT AND INSTALLATION OF CABLES.

(1) GENERAL. -After all cables have been prepared as described in paragraph 2-4a, they should be laid out and routed in accordance with a plan applicable to the specific installation. Since cable layout and routing details vary from installation to installation, layout details have been omitted in this manual. The general plan shown in figure 2-6 for a shore-based radio beacon should be adapted to fit specific requirements. Cables may be routed in trenches, ducts, or overhead cable racks. The objectives are to limit total cable lengths to the maximum lengths specified above, to bring cable terminations to within connecting distance of the components involved, and to secure cable runs with clamps or other suitable means, so as to prevent damage due to cable movements.

The cables intended for connection to the receivertransmitter group and to the power supply assembly are brought into the equipment through cutouts provided in the cable entrance box. Cover plates are secured by means of hex bolts. The cutouts are intended to provide cable entrance to the interior of the box. To place the interconnecting cables into the equipment and to prepare for making the connections, proceed as follows:

Step 1. Open amplifier-modulator and frequency multiplier-oscillator drawers of receiver-transmitter group and high-voltage power supply unit just above transformer and blower compartment of power supply assembly, as far as they will go.

## WARNING

Unless cabinet has been bolted in place, it may topple over if too many drawers are opened at one time.

Step 2. Remove screws securing sides of cabinet to frame, and lift off sides of cabinet.

Step 3. In receiver-transmitter group only, release four knurled thumbscrews securing lower portion of ventilating duct inside cabinet. Push down on that section of duct to disengage it from retaining clamps, and move it aside to gain access to front of terminal boards in cable entrance box.

ARMOR NUT WASNER NO 3
BULGE SHIELO ERAID
WASHER NO 2
FAN ARMOR WASHER NO 2


STI:P 5. Slide clamp against fanned out braid. Splitfingers on clamp should extend towards end of cable.

STI:P 6. Push spanner nut No. I back to bulging armor, allowing approximately 2 inches for spanner wrench. Insert prepared end of cable into plug body.

STI:P 7. Apply a small amount of dielectric compound to spanner nut threads and gasket. Serew spamer nut No. 1 tightly into Body using wrench TL-323/(I) Siide gasket and washer No. 2 into body. Screw spamer No. 2 tight against washer No. 2. Push armor and washer No. 3 into body by smoothing bulge in armor. Screw up armor nut tightly securing armor. Tap end of dielectric with hammer to allow braid andarmor to set properly. Cut diclectric of cable thush with forward edge of coupling ring. Do not nick centre conduttor. Remove dielectric with saspliers. Cut centre conductor $1 / 2$ inch from dielectric. Round off centre cenductor with file. Using a file, cut a chamfer $1 / 16$ "deep by 45 into the dielectric immediately surrounding the centre conductor. This will enable any excessive fength of the associated female mating pin to be accommodated.

CAUTION Make sure no filings are left on dielectric.
Figure 2-4. Attaching Plug UG-154A/U to Cable RG-18/U, Assembly Details


CLAMP NUT GASKET | OUTER |
| :--- |
| CONOUCTOR |
| 8RAIO |

|  |  |
| :---: | :---: |
| ERAN CLAMP |  |

STEP 3. Pull braid forward and taper to a point. Slide braid clamp over braid and against jacket so that jacket fits snugly against internal shoulder of clamp.

|  | STEP 4. Cut off braid $1 / 4$ inch from braid clamp. Do not damage |
| :---: | :---: | dielectric.



STEP 5. Unbraid ends of outer conductor and fan straight back onto tapered portion of clamp. Trim braid flush with flange portion of braid clamp so that no strands extend beyond outside diameter of flange. Braid strands should not cross each other. Cut off dielectric surface and square $1 / 16$ inch from point where braid bends back over clamp. This dimension is critical. Be careful not to nick, bend, or otherwise damage the inner conductor. Cut off inner conductor $5 / 32$ inch from end of dielectric.

Figure 2-5. Attaching Plug UG-943A/U to Cable RG-10/U, Assembly Details


Figure 2-6. Shore Radio Beacon Cable, Location Diagram

Step 4. Use hex wrench to remove bolts securing cover plate over cutout selected to provide cable entrance. Remove cover plate. Fit cover plates with stuffing tubes, as required.

Step 5. Feed cables into stuffing tubes and then into equipment through cutout, guiding cables so that terminals appear inside cabinet frame near front of cable entrance box terminal boards. Fan out individual cables and leads as required for making connections to individual terminal boards. Restore cover plates.

## CAUTION

Be careful not to damage any of the cables or components while doing work inside the cabinet.
(2) CABLE CONNECTIONS. - Detailed interconnection information for the radio set is given in table 2-2. Most of the connections are made to terminal boards with screw-type terminals. An r-f coaxial cable RG-18A/U, fitted with plug UG-154A/U on the transmitter end and plug UG-1041A/U on the antenna end, is connected between a coaxial connector

TABLE 2-2. WIRING LIST OF INTERCONNECTING CABLES FOR SHORE RADIO BEACON RADIO SET AN/GRN-9D

| WIRE <br> NO. | FUNCTION | VOLTS | AMPS | CONDUCTOR <br> SIZE (CM) | COLOR <br> CODE | FROM | TO |
| :---: | :---: | :---: | :---: | :---: | :--- | :--- | :--- | :--- |
| INCOMING CABLES TO RECEIVER-TRANSMITTER OA-3352/GRN-9D |  |  |  |  |  |  |  |
| (FHFH-23: 35 -foot maximum) |  |  |  |  |  |  |  |

CABLES BETWEEN RECEIVER-TRANSMITTER OA-3352/GRN-9D AND POWER SUPPLY ASSEMBLY OA-1537A/GRN-9A
(MSCA-30: 5 -foot maximum distance between units; 35 -foot maximum cabling)

| 1 | 12-kv ground | Gnd |  | 1779 | Blk | TB1004(1) | TB903(1) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 1 -minute delay circuit | 120 | 0.05 | . 1779 | W | TB1003(1) | TB908(19) |
| 3 | 1 -minute delay coil | 120 |  | 1779 | R | TB1004(12) | TB908(17) |
| 4 | 5 -minute delay coil | 120 |  | 1779 | Gn | TB1004(14) | TB908(14) |
| 5 | Remote ready indicator |  |  | 1779 | 0 | TB1004(12) | TB907(13) |
| 6 | Control circuit neutral | 120 | 0.94 | 1779 | Blu | TB1003(12) | TB907(3) |
| 7 | Chassis ground | Gnd |  | 1779 | W-Blk | TB1002(12) | E999(9) |
| 8 | Spare |  |  | 1779 | R-Blk |  |  |
| 9 | Interlock circuit | 120 | 0.32 | 1779 | Gn-Blk | TB1003(15) | TB907(7) |
| 10 | Spare |  |  | 1779 | O-Blk |  |  |
| 11 | Cabinet blower B1001. phase A | 208 | 3.1 | 1779 | Blu-Blk | TB1001(18) | TB908(8) |
| 12 | Interlock circuit | 120 | 0.48 | 1779 | Blk-W | TB1003(17) | TB907(10) |
| 13 | Spare |  |  | 1779 | R-W |  |  |
| 14 | Spare |  |  | 1779 | Gn-W |  |  |
| 15 | Cabinet air switch circuit | 120 | 0.29 | 1779 | Blu-W | TB1003(20) | TB907(12) |
| 16 | High-voltage interlock | 120 |  | 1779 | Blk-R | TB1002(6) | TB908 (15) |
| 17 | Spare |  |  | 1779 | W-R |  |  |
| 18 | Spare |  |  | 1779 | O-R |  |  |
| 19 | Automatic overload circuit | 120 | 0.3 | 1779 | Blu-R | TB1003(10) | TB907(4) |
| 20 | Spare |  |  | 1779 | R-Gn |  |  |
| 21 | Spare |  |  | 1779 | O-Gn |  |  |
| 22 | Control circuit | 120 | 0.94 | 1779 | Blk-W-R | TB1003(14) | TB907(5) |
| 23 | Interlock circuit | 120 | 0.63 | 1779 | W-Blk-R | TB1003(18) | TB907(9) |
| 24 | Cabinet blower B1001, phase B | 208 | 3.1 | 1779 | R-Blk-W | TB1001(17) | TB908(7) |
| 25 | Spare |  |  | 1779 | Gn-Blk-W |  |  |
| 26 | Spare |  |  | 1779 | O-Blk-W |  |  |
| 27 | Spare |  |  | 1779 | Blu-Blk-W |  |  |
| 28 | Spare |  |  | 1779 | Blk-R-Gn |  |  |
| 29 | Cabinet blower B1001, phase C | 208 | 3.1 | 1779 | W-R-Gn | TB1001(20) | TB908(10) |
| 30 | High-voltage indicator circuit | 120 | 0.15 | 1779 | R-Blk-Gn | TB1003(7) | TB908(18) |

TABLE 2-2. WIRING LIST OF INTERCONNECTING CABLES FOR SHORE RADIO BEACON RADIO SET AN/GRN-9D (contd)

| $\begin{aligned} & \text { WIRE } \\ & \text { NO. } \end{aligned}$ | FUNCTION | VOLTS | AMPS | $\begin{gathered} \text { CONDUCTOR } \\ \text { SIZE (CM) } \end{gathered}$ | $\begin{gathered} \text { COLOR } \\ \text { CODE } \end{gathered}$ | FROM | TO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CABLES BETWEEN RECEIVER-TRANSMITTER OA-3352/GRN-9D AND POWER SUPPLY ASSEMBLY OA-1537A/GRN-9A <br> (MSCA-10: 5 -foot maximum distance between units; 35 -foot maximum cabling) |  |  |  |  |  |  |  |
| 1 | +250-volt ground | Gnd | 0.46 | 1779 | Blk | TB1004(17) | E999(2) |
| 2 | +1000 -volt regulated from medium voltage power supply | +1000 | 0.41 | 1779 | W | E1011 | E907 |
| 3 | Spare |  |  | 1779 | R |  |  |
| 4 | +250 -volt regulated from low voltage | +250 | 0.36 | 1779 | Gn | TB1004(18) | TB903(11) |
| 5 | +1000-volt ground | Gnd | 0.41 | 1779 | 0 | TB1004(8) | E999(3) |
| 6 | +1000 -volt regulated from medium voltage power supply | +1000 | 0.41 | 1779 | Blu | E1011 | E907 |
| 7 | +100-volt ground | Gnd | 0.41 | 1779 | W-Blk | TB1004(8) | E999(3) |
| 8 | Spare |  |  | 1779 | R-Blk |  |  |
| 9 | Spare |  |  | 1779 | Gn-Blk |  |  |
| 10 | Spare |  |  | 1779 | O-Blk |  |  |
| MSCA-7: 5-foot maximum distance between units; 35 -foot maximum cabling) |  |  |  |  |  |  |  |
| 1 | Spare |  |  | 1779 | BIk |  |  |
| 2 | -375-volt regulated | -375 | 0.14 | 1779 | W | TB1004(11) | TB903(12) |
|  | from low voltage |  |  |  |  |  |  |
| 3 | -375-volt ground | Gnd | 0.12 | 1779 | R | TB1004(13) | E999(3) |
| 4 | Spare |  |  | 1779 | Gn |  |  |
| 5 | Spare |  |  | 1779 | 0 |  |  |
| 6 | Spare |  |  | 1779 | Blu |  |  |
| 7 | Spare |  |  | 1779 | W-Blk |  |  |
| (FSGA-4: 5 -foot maximum distance between units; 35 -foot maximum cabling) |  |  |  |  |  |  |  |
| 1 | 12-kv plate transprimary T1001, phase A | 208 | 8.3 | 4497 | Blk | TB1001(12) | TB901(2) |
| 2 | 12-kv plate transprimary T1001, phase | 208 | 8.3 | 4497 | W | TB1001(11) | TB901(3) |
|  |  |  |  |  |  |  |  |
| 3 | 12-kv plate transprimary T1001, phase C | 208 | 8.3 | 4497 | R | TB1001(14) | TB901(4) |
| 4 | Plate trans-neutral | 208 | 8 | 4497 | G | TB1002(5) | TB904(13) |
| 1 | Cabinet convenience outlets | 117 | 15 | 4497 | Blk | TB1001(9) | TB904(9) |
| 2 | Cabinet convenience outlets | 117 | 15 | 4497 | W | TB1001(10) | TB904(10) |
| 3 | Cabinet convenience outlets | 117 | 15 | 4497 | R | TB1001(8) | TB904(4) |
| 4 | Cabinet convenience outlets | 117 | 15 | 4497 | G | TB1001(7) | TB904(6) |

TABLE 2-2. WIRING LIST OF INTERCONNECTING CABLES FOR SHORE RADIO BEACON RADIO SET AN/GRN-9D (cont)

| WIRE NO. | FUNCTION | VOLTS | AMPS | $\begin{aligned} & \text { CONDUCTOR } \\ & \text { SIZE (CM) } \end{aligned}$ | COLOR CODE | FROM | TO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 120 | 10 | 4497 | Blk | TB1002(15) | TB901(8) |
| 2 | Test set input, 1- | 120 | 3.4 | 4497 | W | TB1002(14) | TB902(1) |
| 3 | phase, phase C ${ }_{\text {Test set input, 1- }}$ | 120. | 3.4 | 4497 | R | TB1002(13) | TB902 (3) |
| 4 | phase, phase A Test set input, 1phase, phase B | 120 | 3.4 | 4497 | G | TB1002(16) | TB902 (2) |
| 1 | Regulated filament | 120 | 4.6 | 4497 | Blk | TB1002(10) | TB904(19) |
| 2 | bus <br> Low and medium voltage P1 trans- | 120 | 3.4 | 4497 | W | TB1002(3) | TB904(14) |
| $\begin{aligned} & 3 \\ & 4 \end{aligned}$ | Spare <br> Filament bus neutral | 120 | 4.5 | $\begin{aligned} & 4497 \\ & 4497 \end{aligned}$ | $\begin{aligned} & R \\ & G \end{aligned}$ | TB1002(8) | TB904(20) |
| (TTHFWA-1-1/2: 5-foot maximum distance between units; 35-foot maximum cabling) |  |  |  |  |  |  |  |
| 1 | Sound powered trlephone | 60 micro- | $\begin{aligned} & 100 \\ & \text { micro- } \end{aligned}$ | 704 |  | TB903(8) | TB1004(19) |
| 2 | Sound powered telephone | $\begin{gathered} 60 \\ \text { micro- } \end{gathered}$ | $\begin{aligned} & 100 \\ & \text { micro- } \end{aligned}$ | 704 | W | TB903(10) | TB1004(20) |
| 3 | Spare |  |  | 704 | R |  |  |
| (RG-27/U: 5-foot maximum distance between units; 35-foot maximum cabling) |  |  |  |  |  |  |  |
| 1 | 12-kv high voltage output | 12 kv | 300 ma |  |  | E903 | E1001 |

CABLES BETWEEN RECEIVER - TRANSMITTER OA - 3352/GRN-9D
AND TEST MONITOR CONTROL RACK TYPE MM - TMC - 212A

| $\begin{aligned} & \text { WIRE } \\ & \text { NO } \end{aligned}$ | FUNCTION | DESIGNATION | COLOR CODE | FROM | TO (TMC) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | Keyer Output to TMC | $\begin{aligned} & \text { CABLE DOO2247-14-(5) } \\ & \text { RG } 188 / \mathrm{U} \end{aligned}$ | WHT / CENTRE SHORT SHIELD LONG SHIELD | $\begin{aligned} & \text { TB903 (5) } \\ & \text { TB903 (3) } \\ & \text { TB903 (4) } \end{aligned}$ | TB8-7 (TB8-9) |
| 2. | Pre - Trig | CABLE DOO2247-8-(7) RG 223/U | CENTRE <br> SHIELD <br> EXT. SHIELD | $\begin{aligned} & \text { TB903 (6) } \\ & \text { TB903 (4) } \\ & \text { E999 } \end{aligned}$ | J1 (J2) |
| 3. | High Voltage Interlock to TMC | CABLE DOO2247-11-(17) (Min elec. DEF-10 No. 2C).* | $\begin{aligned} & \text { WHT } \\ & \text { BLK } \end{aligned}$ | TB907 (11) TB907 (14) | TB3-4 IN (6) TB3-5 OUT (7) |
| 4. | Mis - set cables to TMC | CABLE DOO2247-18-(10) <br> (Min elec. DEF-10 <br> No. 2C).* <br> *Nato Stock No. 6145-99-910-0004 | $\begin{aligned} & \text { WHT } \\ & \text { BLK } \end{aligned}$ | $\begin{aligned} & \text { TB907 (19) } \\ & \text { TB907 (13) } \end{aligned}$ | $\begin{aligned} & \text { TB5-8 (10) } \\ & \text { TB5-7 (9) } \end{aligned}$ |
|  | NOTE: Suffixes shown in brackets in the 'DESIGNATION' and 'TO (TMC)' columms refer to alternative beacon in dual-operation installations. |  |  |  |  |

Paragraph

on the antenna and a connector on the front panel of Control-Duplexer C-2226A/GRN-9. Two r-f coaxial cables RG-10/U, fitted with plug UG-943A/U at each end, are connected between the cable entrance box on the receiver-transmitter group cabinet and the antenna base. High-voltage power cable RG-27/U is connected between binding posts in the transmitterreceiver group and power supply assembly cable entrance boxes. To make the connections outlined above. proceed as follows:

## CAUTION

Three-phase power connections are made to tilters FL901, FL902, and FL903. Before connecting power, check the phase rotation of the line, so that after connection the antenna spin motor and the cooling blowers of the receiver-transmitter and power supplytest set groups rotate in the proper directions. The correct direction of rotation is indicated on an instruction plate on the spin motor.
(a) TERMINAL BOARD CONNECTIONS. Connect the terminal lugs on the cables brought into the cable entrance boxes in accordance with procedures of paragraph 2-4a (3) to the terminals on the cable entrance box terminal boards in the receivertransmitter group and power supply assembly. Similarly. connect the cable leads to the terminal boards on the other equipment components. For further details, refer to table 2-2.
(b) POWER CABLE CONNECTIONS. - Connect one end of high-voltage power cable RG-27/U to binding post E903 in the receiver-transmitter group cable entrance box. Connect the cable armor to ground at terminal 12 on binding post E999.

## CAUTION

Make sure that the areas around binding posts E903 and E1001 are cleared of all other cable leads.
(c) COAXIAL CABLE CONNECTIONS. -R-f cable $\mathrm{RG}-18 \mathrm{~A} / \mathrm{U}$ is fitted with plug UG-1041A/U at the antenna end. and a plug UG-154A/U at the equipment end. Conneet one end to jack J3302 on the (shore) antenna pedestal. Connect the other end of the cable to
plug P1169, a UG-216B/U, right-angle fitting. Connect the fitting to KF OUTPUT jack J1155 on the front panel of the control-duplexer in the receiver-transmitter group. For further details, refer to table 2-2.

The two r-f cables RG-10/U have been fitted with plugs UG-943A/U at each end. One cable brings the $15-\mathrm{cps}$ reference trigger and the other, the $135-\mathrm{cps}$ reference trigger, to the receiver-transmitter group. Connect one of the cables between jack J904 on top of the receiver-transmitter group cable entrance box and J3303 on the antenna pedestal. This is the $15-\mathrm{cps}$ reference trigger connection. Connect the other cable between jack J903 on top of the receiver-transmitter group cable entrance box and jack J3304 on the antenna pedestal. This is the 135 -cps reference trigger connection.
c. ELECTRON TUBE INSTALLATION. -The electron tubes listed in table 2-3 should be installed after the receiver-transmitter group and power supply-test group have been fastened in place.

The klystron V1304 should be installed in accordance with the procedure outlined below (figures 2-7 and 2-8).

Note.
For those beacors incorporating the Test Monitor Control Rack MM - TMC - 212A, the main $R F$ and pulser plate cables from the antenna to the beacon are routed via the TMC rack

TABLE 2-3. ELECTRON TUBE INSTALLATION

| TUBE TYPE | UNIT | REFERENCE SYMBOL |
| :--- | :--- | :--- |
| 836 | Medium voltage Power supply <br> 8020 <br> Klystron SAL-89 voltage power supply <br> Amplifier modulator | V1801 and V1802 <br> V1901 through V1906 <br> V1304 |



Figure 2-7. Amplifier Modulator AM-1701/URN, Front View with Klystron Access Door Open

Step 1. Before installing klystron, preset spacings of cavity rings to approximate required distance determined by assigned frequency. The spacing of cavity tuning rings is determined by special tuning chart provided with each klystron. A typical chart is shown in figure 2-9.

## CAUTION

Do not use sample chart, figure 2-9 for presetting cavity ring spacing. Instead, use chart supplied with particular klystron being installed.


Figure 2.8. Amplifier-Modulator AM-1701/URN, Left Side View

## Note

As shown in figure 2-9, the chart contains three curves, one for each of the three klystron cavities; these are klystron INPUT, MIDDLE, and OUTPUT cavities.

Step 2. Determine channel at which radio beacon is to operate and appropriate transmitter frequency. Using chart provided with klystron, determine spacing required for each of the three cavities. To determine spacing from calibration curve, use transmitter frequency as ordinate of curve; spacing (in thousandths of an inch) between inside surfaces of flanges is abscissa of curve.

Step 3. Using caliper micrometer, gauge spacing between cavity rings and adjust. Use adjusting wrench provided for this purpose. It is very
important that flanges be moved parallel to each other while being tuned. Turn each adjusting nut by not more than one full turn before ad justing other nuts on flange by same amount. Repeat as necessary until
required setting is obtained.

## CAUTION

Some klystrons are shipped with flexible filament leads unattached. When attaching leads to terminals, take care not to crack filament rod seals (figure 2-10).

Step 4. Check that cup shield provided with klystron is over filament terminals. Remove two back screws but not two screws that face front when klystron is in amplifier-modulator. (The back screws are not accessible for removal when tube is installed).



Figure 2-9. Klystron Characteristics, Sample Calibration Curve

Step 5. Pull amplifier-modulator out to fully extended position and be sure that the slides lock unit in this position. Open access door and hinged shield that covers klystron filament terminals.

Step 6. Loosen the four cradle bolts and tilt cradle forward, pushing band up and to rear of compartment. Loosen bolt holding cradle to chassis and push it completely to right.

Step 7. Place klystron into compartment, cathode end first. Position anode end on two anode supports and allow other end to rest on cradle.

Step 8. Insert and tighten the four bolts in anode plate. Secure grounding strap to anode.

Step 9. Position cradle directly under raised ring on input cavity and tighten band around klystron.

Step 10. Tighten bolt holding cradle to chassis; then tighten the four bolts on cradle.

Step 11. Attach r-f input and output cables.

## CAUTION

Make sure, when attaching r-f output cable to klystron, that equal torque is maintained on the two pin wrenches (figure 2-10); this ensures that torque required to tighten connector is not applied to r-f out put terminal. The bend in cable should be maintained so that transverse force is not applied to terminal.

Step 12. Remove cup shield from filament end of klystron and attach flexible leads to terminals at insulating bushing at back of compartment. Make sure to connect lead from heatercathode terminal (marked HK) to outer conductor of coaxial connector. Connect other heater terminal to inner conductor.

Step 13. Attach flexible grid lead to solid terminal on cathode end of klystron SAL-89.

## d. BUILT-IN TEST EQUIPMENT INSTALLATION

 (Not MM - TMC - 212A).-The power supply assembly is shipped with-out the built-in test equipment installed (figure 1-3). At the time of installation, the blank panel covering the upper half of the power supply assembly is removed, and the built-in test equipment is installed in its place.

The physical arrangement of the built-in test equipment in the power supply assembly cabinet is

A. removal of cup shielo


Figure 2-10. Klystron Installation Details
shown in figure 2-2. The test equipment interconnecting harness, shown schematically in figure 2-11, is added to the power supply assembly when the builtin test equipment is installed. Figure 3-13 shows the front panel connections needed to perform the standard tests listed in paragraph 2-5d. These connections are temporary, and are removed when testing is complete. The test equipment provided includes the following:
(1) Pulse-Sweep Generator SG-121A/URN-3 (Technical Manual NAVSHIPS 92745).
(2) Pulse Analyzer-Signal Generator TS-890A/ URN-3 (Technical Mantal NAVSHIPS 93231).
(3) Power Meter-Pulse Counter TS-891/URN-3 (Technical Manual NAVSHIPS 92809).
(4) Switch-Test Adapter SA-420/UṘN-3 (Technical Manual NAVSHIPS 92809).
(5) Oscilloscope OS-54/URN-3 (Technical Manual NAVSHIPS 92778).
e. BUILTT-IN TEST EQUIPMENT INSTALLATION (MM-TMC-212A). - The MM-TMC-212A has been designed to replace the built-in test equipment described in para $2-4 \mathrm{~d}$ and completely replaces the AN/GRA34 Control Monitor Group. Minor modifications to the AN/GRN-9D are necessary in order to incorporate the TMC-212A and these are described in AP 116C-0702-1A6A which also includes complete installation details of the TMC-212A. The schematic and wiring diagrams in this manual incorporate the changes resulting from the introduction of the TMC-212A and a block diagram of the equipment is shown in Fig 2-11a whilst Fig 3-13a shows the front panel connections required to perform certain standard tests described in pargraph 3-6a(12). The TMC-212A rack comprises the following pieces of test equipment whose functions are briefly described in TABLE 1-2b.
(1) Transfer and Switching Unit MM-1602 Technical Manual: AP 116C-0702-1D6D.
(2) Spectrum Analyzer/Test Generator MM-705

Technical Manual: AP 116C-0702-1H6H
(3) Oscilloscope MM-504

Technical Manuals: AP 116C-0702-1J6J
AP 116C-0702-1K6K
(4) Power Meter - Pulse Counter - Marker Generator MM-109
Technical Manual: AP 116C-0702-1G6G
(5) Transfer and State Transmission Unit (TELOTEL)
Technical Manual: AP 116C-0702-1L6L
(6) Two. Transponder Monitors MM-209

Technical Manuals: AP 116C-0702-1E6E
AP 116C-0702-1F6F

## 2-5. INSPECTION AND ADJUSTMENTS.

Note
Details regarding the setting up of the TACAN beacon using MM-TMC-212A can be found in Paragraph 3-6a(12).
a. INITIAL CHECKS. - After the equipment has been installed and interconnected, and before proceeding with the initial adjustments outlined in paragraph 2-5b, proceed as follows:
(1) Check that all connections have been properly made.
(2) Check fuses, pilot lamps, and other removable items to be sure they are properly installed.
(3) Inspect cables, drawers, and panel-mounted components, particularly meters, to make sure that nothing was damaged during installation.
(4) Make certain that all panel screws are tight, so that interlocks function properly.
(5) Restore equipment cabinets to normal operating condition as follows:
(a) Replace the section of ventilating duct removed $\overline{f o r}$ connection of cables to cable entrance box terminal boards.
(b) Restore sides of each cabinet.
(c) Close equipment drawer units that were opened for interconnection of incoming cables.

## Note

Safety interlock switches along equipment frames are held in closed position when drawers are fully closed and open when drawers are opened.
(6) Initially set switches listed in table 2-1 in positions indicated.

## b. PRELIMINARY ADJUSTMENT (RADIO SET

 UNENERGIZED). - The equipment is shipped with a crystal in place in the frequency multiplier-oscillator. This crystal should not be replaced unless it is necessary to change the channel. If the channel frequency is changed, the equipment must be retuned (paragraph 2-5g).c. INITIAL ENERGIZING. - Proceed as follows when energizing the radio beacon equipment. consisting of the radio set and associated antenna group. for the first time:

## WARNING

Operation of this equipment involves use of high voltages which are dangerous to life. Operating personnel must at all times observe all safety regulations. Do not change tubes
or make adjustments inside the amplifier-modulator or high-voltage power supply chassis while high voltage power supply is on. Do not depend upon safety interlock switches for protection. Under certain conditions, dangerous potentials may exist in the circuit with power controls set OFF because of charges retained by capacitors. To avoid shock and severe burns, always discharge and ground circuits before touching them. Never service or adjust the equipment without the presence or the assistance of another person capable of rendering first aid immediately.

## CAUTION

Before energizing the equipment for the first time, set the controls in the initial positions listed in table 2-1.

Step 1. Turn EMERGENCY SWITCH S901, on bottom panel of receivertransmitter group cabinet, right to ON (arrow pointing up or down). Check that OVEN lamp DS1403 and NORMAL lamp DS1402, on panel of frequency multiplier oscillator, are on.

## Note

When crystal oven has reached proper operating temperature, NORMAL lamp will go out.
Thereafter NORMAL lamp goes on and off as oven thermostat turns heater on and off to maintain oven temperature.

Step 2. Turn MASTER SWITCH Sllol on panel of control-duplexer to STANDBY. Check that blue MAIN POWER ON lamp DSIl02 on control-duplexer goes on. Check that amber AIR SWITCH OPEN lamps DS1303 (on amplifier modulator panel). DS901 (on panel of blower compartment of receiver-transmitter cabinet), and DS1001 (on power supplytest set group bottom panel) are not on. When on, these lamps indicate that blowers operating air switches are not working properly.

## CAUTION

If amber lamps are on, blowers may be rotating in wrong direction. Shut off equipment immediately and check wiring for possible phase reversal by comparing equipment wiring and interconnection with schematic and wiring diagrams in Section 6. Operating equipment while blowers rotate in wrong direction may cause serious damage because of overheating.

Step 2a. Remove the klystron access panel from the front of the Amplifier Modulator drawer, see figure 2-7.

Step 2 b . Using a true rms reading voltmeter, HP3400A (6625-00-727-4706) or equivalent, measure the klystron filament voltage between terminals $H$ and $H K$ on the klystron. The voltage should be between 4.1 V and 4.3 V rms.

## Note

Do not measure between the resistor clamps or between the Rl 390 resistor board flying leads.

Step 2c. If the filament voltage is within range, proceed to step 21.

Step 2d. If the filament voltage is low, the klystron or filament transformer may be faulty and should be investigated.

Step 2e. If the filament voltage is high, turn MASTER SWITCH Sllol to OFF.

Step 2f. Obtain R1390 Resistor Set for the Amplifier Modulator, see Table 7-3. Select a mid-range value resistor from the resistor set and fit it into the clips on the R 1390 resistor board.

Step 2g. Turn MASTER SWITCH Sllol to STANDBY and wait for 5 minutes.

Step 2h. Repeat step 2b.
Step 2i. If the filament voltage is out of range, turn MASTER SWITCH Sllol to OFF.

Step 2j. (a) If the voltage is low, fit a higher value resistor.
(b) If the voltage is high, fit a lower value resistor.

Step $2 k$. Repeat steps $2 g$ to $2 j$ until the voltage is within range.

Step 21. Allow the equipment to remain in STANDBY for a further 15 minutes and then check that the filament voltage is within range. If not, repeat steps $2 i$ to $2 k$.

Step 3. Snap switch S 502 on radio receiver panel, to $O N$. Check that white POWER ON lamp DS501 on radio receiver is on.

Step 4. Snap CODER-INDICATOR switch S 601 on coder-indicator panel to ON. Check that white POWER ON lamp DS601 on panel of coder-indicator is on.

## Note

Check that all switches on antenna control unit are at $O N$. These switches are intended for use during servicing, and are normally left at $0 N$.

Step 5. Snap ANTENNA CONTROL switch Sllo2 on control-duplexer panel, to ON. Check that white ANTENNA CONTROL lamp DS 1103 on controlduplexer panel, is on. Check that antenna is rotating in proper direction; correct direction of rotation is indicated on instruction plate on antenna spin motor.

## CAUTION

If both antenna and ventilating blowers in equipment cabinets are rotating in wrong direction(air switches fail to operate), interchange power input leads to FL908 and FL909 in rear of receivertransmitter group cable entrance box. If only antenna is rotating in wrong direction, stop equipment
and reconnect antenna spin motor by interchanging wires installed on terminals 3 and 5 of test board TB3394 in antenna pedestal. If blowers alone are rotating in wrong direction (air switches fail to operate) check wiring from power input to terminal boards on blowers for possible reversal of phase. Check that ANTENNA CONTROL lamp DS602 on coder-indicator panel is on constantly; blinking of this lamp indicates trouble in antenna or antenna control circuits.

Step 6. Set FIL ON switch Sll08 on control-duplexer panel to ON. Check that FIL ON lamp DSllol on controlduplexer, FIL lamp DS1301 on amplifiermodulator, FILAMENT lamp DS 1401 on frequency multiplier-oscillator go on. Check that blue LV-MV READY lamp DS 1605 on low voltage power supply goes on after a l-minute time delay.

Step 7. Read SUPPLY VOLTS meter M1101 on control-duplexer. If reading is 120 V ac, proceed to next step. If reading is not 120 V ac, open controlduplexer drawer, loosen locking screw on ADJUST FOR 120 V knob (on left side of control-duplexer drawer), and adjust for reading of 120 V ac on SUPPLY VOLTS meter.

## Note

Use SUPPLY VOLTS meter to check
control line voltage by holding
spring-return REG FIL BUS-LINE
switch Sllo6 at LINE. Line voltage,
as read on meter should be $120 \pm 12 \mathrm{~V}$.

Step 8. Turn MASTER SWITCH S 1101 to OFF and then immediately to ON. Check that there is a 1 - minute delay before blue LV-MV READY lamp DS 1605 on the panel of the low-voltage power supply goes on.

Step 9. When blue LV-MV READY lamp goes on, snap LV switch S1601 on low voltage power supply panel, to $0 N$. Check that red LV lamp DS 1602 and green -375 V lamp DS 1601 on pane 1 of low


Fig. 2-11. Built-in Test Equipment Interconnection Harness, Schematic Diagram
voltage power supply are on. The green lamp indicates that low voltage power supply is delivering dc power to the other transmitter units of radio beacon.

Step 10. Check, and if necessary adjust, low voltage power supply output voltages. (Refer to paragraph 2-5e(1) for adjustment procedure.)

Step 11. Snap MV switch S1801, on medium voltage power supply panel to ON. Check that red +1000V lamp DS1801 on panel of medium voltage power supply is on. Check that amber MV OVERLOAD lamp DS 1803 on medium voltage power supply panel does not go on. Check that lamp DS1802 inside the power supply unit is on. To make this check, open power supply drawer unit and temporarily lock interlock switch on cabinet frame behind panel.

## WARNING

Dangerous voltages are present when lamp DS1802 is on.

Step 12. Check, and if necessary adjust, medium voltage power supply output voltage.

## CAUTION

When starting radio set for the first time, or when starting a radio set containing a klystron that has not been in use for 3 months or more, age klystron (paragraph 2-5k) before applying full power to it.

Step 13. Turn MASTER SWITCH to OFF and then immediately to ON. Check that there is a 5-minute delay before blue HV READY lamp DS1902 on high voltage power supply panel goes on.


TACAN (GROUND) TEST-MONTTOR-CONTROL GROUP MM-TMC-212A.

Step 14. When HV READY lamp DS 1902 goes on, set HV switch S1902 to ON. Check that red HV lamp DS1901, on high voltage power supply panel is on. Check that amber HV OVERLOAD lamp DS1903 on high voltage power supply panel is not on. Check that HV SUPPLY meter M1302 on amplifier-modulator panel reads approximately 12,000 volts.

Step 15. Check that ANTENNA SPEED ERROR meter reads in green portion of its scale; a reading in red portion of meter scale is an indication of trouble in antenna control circuits.

## Note

Under normal operating conditions, the radio set is turned off and on by means of MASTER SWITCH on controlduplexer. All off-on switches, except those on built-in test equipment, are left in the on position. When MASTER SWITCH is turned to ON, the radio set will be energized with proper time delays applied to various power supplies. Whenever a radio set is being energized for the first time, or whenever tuning or troubleshooting operations are being performed on the radio set, it is best to perform the initial energizing procedure step by step.

## d. ADJUSTMENT OF BUILT-IN TEST EQUIPMENT.

(1) GENERAL. -Internal adjustments to test equipment (before use) are given in the individual manuals supplied with the test equipment.

The units are interconnected internally through a cable harness and a built-in switching system permits rapid connection for standard test procedures.
(2) ORIGINAL TEST EQUIPMENT (TABLE 1-2).The switching system for this equipment includes two fourposition function switches located on the front panels of the Oscilloscope OS-54/URN-3 and Power Meter - Pulse Counter TS-891/URN-3, and a two-position coaxial r.f. switch located in the Switch Test Adapter SA-420/URN-3. If the front panel connections of Figure 3-13 are made it is only necessary to ammipulate the front panel controls to make the checks as listed. Note that the two function switches should be in the same position specified in TABLE 2-4 for any one of the tests.

## Note

With the function switches in position 4, GENERAL TESTING, all internal inter-unit connections, except power connections, are effectively disconnected and the test equipments are operated as individual units. For checks and adjustments not listed in the table, set the function switches to position 4.

TABLE 2-4. FUNCTION SWITCH POSITION FOR TESTING

| SWITCH <br> POSITION | PANEL <br> NAME | TEST |
| :---: | :--- | :--- |$|$| OPERATING |
| :--- |
| 2 |
| 3 |

(3) PRELIMINARY SETTING OF FRONT PANEL CONTROLS ON PULSE ANALYZER-SIGNAL GENERATOR TS-890A/URN-3.-Before making any tests with the Pulse Analyzer/Signal Generator, set the POWER switch to ON (see fig 3-14), allow equipment to warm up for 10 minutes, and proceed as follows:

Step 1. Set INTERROGATE switch to OFF.
Step 2. Set INPUT ATTEN SELECTOR switch to maximum attenuation.

Step 3. Set BAND SHIFT switch to 0.
Step 4. Set MODULATION SELECTOR switch to CW.
Step 5. Set CHANNEL SELECTOR switch to applicable channel.

## Note

If a built-in crystal oscillator is to be used as the frequency generating source, omit Steps 6, 7 and 8.
Step 6. Set MAIN TUNING control to applicable channel.
Step 7. Set the OSCILLATOR SELECTOR switch to VFO CALIBRATE.

Step 8. Adjust VFO CALIBRATE control until zero beat is heard in a telephone headset plugged into the VFO CALIBRATE jack.

Step 9. Set OSCILLATOR SELECTOR switch to either REF OSC, for crystal control or VFO depending on which oscillator is to be used as the generating source.

Step 10. Adjust ZERO SET control for 0 reading on OUTPUT LEVEL INDICATOR.

Step 11. Set INTERROGATE switch to ON. Note
Before proceding with the next step, energize the Pulse Sweep Generator and allow it to warm up for at least two minutes.
Step 12. Adjust POWER SET control on TS-890A/ URN-3 and PULSE AMPLITUDE control on SG-121A/ URN-3 for mid-scale (100) reading on OUTPUT LEVEL INDICATOR. Retune CHANNEL control slightly and recheck setting of POWER SET control for mid-scale reading on OUTPUT LEVEL INDICATOR.

Step 13. Set MODULATOR SELECTION switch to PULSE.

## Note

The TS-890A/URN-3 is now read for special tests. Upon completion of the tests, shut down the eçuipment by turning INTERROGATE and POWER switches to OFF.
(4) REPLACEMENT TEST EQUIPMENT (TABLE 1-2b).

Note
Due to an inherent characteristic in the Pulse Counter (part of the MM-109), the counter normally returns to '00001' and only returns to ' 00000 ' when reset by the CTR/RESET switch on the front panel of the unit.
Step 1. Turn the MM-TMC-212A on by turning the POWER ON switches of each unit to ON.

Step 2. Observe XPONDER ON ANT light on MM1602 Transfer and Switching Unit. Number -1 indicator should be lit; if not, select position -1 on the ANTENNA XFER SEL switch to achieve this state.

Step 3. On the Spectrum Analyzer/Test Oenerator MM-705:-
a. Switch FUNCTION switch to RF PEAK PWR position.
b. Switch TEST METER to -12.6 V position, and note meter indication. Meter reading should be approximately mid-scale.
c. Repeat Step b. for $+12 \cdot 6,+25 \cdot 2$ and +75 TEST METER positions. All readings should be approximately mid-scale.
d. Switch FUNCTION switch to RF AVG PWR position and repeat Steps b. and c.
e. Set ATtENUATOR to 0 .
f. Place FUNCTION switch in PWR METER ZERO SET position and adjust SET ZERO control to position AVERAGE POWER meter indication over the ZERO SET position.
g. Switch FUNCTION switch to the IF SIG GEN position and repeat Steps b. and $c$.
h. Set IF SIG GEN FREQ control to approximately mid-range.
i. Adjust IF SIG GEN LEVEL control (increase or decrease) until POWER SET is obtained on the AVERAGE POWER meter. Note whether, or not, POWER SET can be obtained.
j. Switch FUNCTION switch to RF. SIG GEN position and repeat Steps $b$. and $c$.
k. Switch RF SIG GEN MODE switch to OFF and adjust SET ZERO control for ZERO SET reading on the AVERAGE POWER meter.
1.• Switch RF SIG GEN MODE switch to the CW position.
m. Switch RF SIG GEN FREQ SEL switch to ON CHAN position.
n. Adjust RF.SIG GEN PWR SET control for POWER SET reading on the AVERAGE POWER meter. Note whether, or not, POWER SET reading can be obtained.
o. Repeat Step n. for RF SIG GEN ${ }^{\mathbf{+}}+\mathbf{2 0 0},+900$, -200 and -900 kHz FREQ SEL positions.
p. Switch RF SIG GEN MODE switch to PULSE position.
q. Switch RF SIG GEN FREQ SEL switch to ON CHAN position.
r. Switch MODULATOR PULSE SPACING switch to VAR and set variable control to mid-range.
s. Set PRR variable control to 10 and PRR switch to X 400 .
t. Observe linear detector output with the Oscilloscope MM-504, using the procedure for the normal transponder test set-up. (Refer to the receiver sensitivity tests in Paragraph 3-6a(12)).
u. Adjust the RF SIG CEN AMPL ADJ control and oscilloscope controls until a $2 \cdot 0 \mathrm{~V}$ Gaussian pulse pair is observed on the oscilloscope. The spacing between the pulses of the pulse pair should be either $12 \pm 3 \mu \mathrm{sec}$ or $36 \pm 3 \mu \mathrm{sec}$; depending on the setting of the PULSE SPACING switch mounted internally on the Modulator Unit and normally set to the $12 \mu \mathrm{sec}$ position.
v. Measure the pulse repetition rate on the oscilloscope (the spacing between pulse pairs). The spacing should be $250 \pm 25 \mu \mathrm{sec}$.
w. Switch MODULATOR PRR switch to X40 and repeat Step $v$. except that the spacing between pulse pairs should be $2.5 \pm 0.25 \mathrm{~ms}$.
x. Switch MODULATOR PRR switch to X 4 and repeat Step $v$. except that the spacing between pulse pairs should be $25 \pm 2.5 \mathrm{~ms}$.
y. Switch FUNCTION switch to PWR METER ZERO SET and adjust the ZERO SET control to cause the AVERAGE POWER meter to indicate ZERO SET.
z. Switch the FUNCTION switch to SA and repeat Steps b. and c.
aa. Switch SPECTRUM ANALYZER BAND SHIFT switch to 0.
ab'. Adjust the NOISE SET control for NOISE
SET reading on the AVERAGE POWER meter. Note whether or not NOISE SET indication is obtained.
ac. Repeat Step ab. for SPECTRUM ANALYZER
BAND SHIFT positions $+0.8,+1.0,+2.0,-0.8$, -1.0 and -2.0 MHz .

Step 4. On the Oscilloscope MM-504:
a. Set the B TRIG SOURCE switch to AC-
b. Set the HORIZ DISPLAY switch to A.
c. Set the combined TIME/CM AND DELAY TIME switch to $5 \mu \mathrm{sec}$.
d. Set the MODE switch to CH 1 and CH 1 INPUT switch to AC.
e. Set the CH 1 VOLTS/CM switch to 2.

On the Power Meter - Pulse Counter - Marker Generator MM-109, set the FUNCTION switch to GEN TEST and the COUNTER/MARKER SELECT switch to MARKERS 10. Connect a patch cable from the MARKER OUTPUT socket to $C H 1$ INPUT socket on the Oscilloscope. Adjust the oscilloscope controls for a suitable picture of the markers which should be displayed on the CRT.
f. Set the MODE switch to CH 2 and CH 2 INPUT switch to AC. Set the CH 2 VOLTS/CM switch to 2 and change the patch cable from the INPUT of CH 1 to that of CH 2. The markers now displayed are routed via channel 2.
g. Set the HORIZ DISPLAY switch to A INTEN BY $B$, adjust $B$ TRIGGER LEVEL (red knob) and note that the intensity of the displayed markers varies. Disconnect the patch cable.

Step 5. On the MM-109:
a. Set the COUNTER/MARKER SELECT switch to SELF CHK.
b. Set the TIME INTERVAL switch to MANUAL and GATE OPEN/CLOSED switch to OPEN.
c. Set the FUNCTION switch to GEN TEST. The unit will begin to 'count'.
d. Set the TIME INTERVAL GATE switch to CLOSED. The counting action will stop.
e. Press the CTR/RESET switch and observe that the counter digits return to ' 0 '. Switch the GATE switch to OPEN and the counting action will restart.

Step 6. On the MM-109:
a. Set the COUNTER INPUT COARSE switch to $1 \cdot 0$ and FINE control fully counter-clockwise.
b. Press the ZERO SET switch and whilst pressed, zero the meter by adjusting the SET ZERO control.
c. Set the FREQ STD switch to INT and connect the patch cable between the FREQ STD output socket and that of COUNTER INPUT.
d. Press the COUNTER INPUT READ switch and adjust the FINE control until the meter indicates in the green area. Disconnect the patch cable.

## e. ADJUSTMENT OF POWER SUPPLIES.

## (1) LOW VOLTAGE POWER SUPPLY PP-1766/ URN.

Step 1. Turn meter selector switch S1402, under D. C. SUPPLY VOLTAGE meter M1402 on frequency multiplier-oscillator panel, to -375 V and +250 V .

Check whether these voltages are within tolerance, or whether they require adjustment; permissible tolerance for each voltage is $\pm 10$ volts.

## Note

When drawer unit is opened, the interlock switch located on cabinet frame behind panel will open and disconnect power to power supply unit. Operate this switch manually before making adjustments by pushing interlock pin gently to side and pulling it out until it catches. Ordinarily, the power supply assembly will be located near enough to the receiver-transmitter group so that meter M1402 on frequency multiplier-oscillator panel may be observed while making the adjustments of low voltage power supply. If this is not possible however, the adjustment adjustment must be made by two technicians. The sound-powered telephone (outlets provided on front of units) may be used for communication between the two groups, if necessary.

Step 2. The low voltage power supply adjustment potentiometers R1623 ( +250 V ) and R1663 (-375V) are located inside drawer unit on side of chassis (figure 2-12) and are marked with voltages which they control. To make the adjustments, open drawer unit, loosen hex nut which locks potentiometer shaft in adjusted position, manually operate interlock and, using screwdriver, adjust potentiometer until proper volt-


Figure 2-12. Low Voltage Power Supply PP-1766/URN, Right Side View


Figure 2-13. Medium Voltage Power Supply PP-1765/URN, Top View
age reading is obtained on D. C. SUPPLY VOLTAGE meter on frequency multiplier-oscillator panel. Tighten the hex nut to secure potentiometer in adjusted position. Be careful not to change potentiometer setting while tightening locknut. After all adjustments have been made, close drawer unit. The interlock will be released automatically.

## (2) MEDIUM VOLTAGE POWER SUPPLY PP1765/URN.

Step 1. Turn meter selector switch S1402, under D. C. SUPPLY VOLTAGE meter M1402 on panel of frequency multiplier-oscillator, to +1000 V . Note which voltages are out of tolerance and will require adjustment; permissible tolerance is $\pm 20$ volts.

Step 2. Medium voltage power supply adjustment potentiometer R1842 +1000 V is located inside power supply drawer unit on top of chassis (figure 2-13) and
is marked with the voltage it controls. To make the adjustments, open drawer unit, loosen hex nut which locks potentiometer shaft in adjusted position, manually operate interlock switch (see notes preceding step 2 of paragraph $2-5 e(1)$ ), and, using screwdriver, adjust potentiometer until proper voltage reading is obtained on D. C. SUPPLY VOLTAGE meter located on frequency multiplier-oscillator panel. Tighten hex nut to secure potentiometer in adjusted position. Be careful not to change potentiometer setting while tightening nut. After both adjustments have been made, close drawer unit.

## f. ADJUSTMENT OF CONTROL-DUPLEXER.

(1) ADJUSTMENT OF FILAMENT VOLTAGE. The regulated filament voltage should be adjusted to exactly 120 volts. To perform this adjustment, proceed as follows:

Step 1. Open control-duplexer drawer unit.


Step 2. Locate ADJUST FOR 120V knob on left side toward rear of control-duplexer. (See figure 2-14.)

Step 3. Loosen locking screw under ADJUST FOR 120V knob.

Step 4. Turn ADJUST FOR 120 V knob until 120 volts is read on D. C. SUPPLY VOLTS meter M1101.

Step 5. Tighten locking screw.
(2) ADJUSTMENT OF PRESELECTOR CAVITIES. Open the control-duplexer drawer to gain access to cavity heads of preselector Z1153. Adjust micrometer heads according to data listed for the particular operating channel in table 2-5.
(3) ADJUSTMENT OF TRANSMISSION LINE FILTER. - The transmission line filter is adjusted in conjunction with the tuning of the klystron output stage. When tuning the cavities for the first time, or when tuning the radio set to a new channel, the cavities should be preset to the approximate adjustment according to the tuning curves shown in figure 2-15. The transmission line filter is illustrated in figure 2-16.

## CAUTION

Do not use the sample chart in figure 2-15 for presetting the cavities. Use the chart supplied with the particular transmission line filter that is installed in the controlduplexer.

For touch-up tuning or when changing to an adjacent channel, it is not necessary to preset the cavities according to the tuning curves. All that is necessary is a slight adjustment for maximum output signal at the ANTENNA INCIDENT jack on the control-duplexer front panel. There is an interaction between the tuning of the klystron, double-slug tuner Z1303, and transmission line filter Z1156. Therefore, if an adjustment is made on any one of these units, the adjustment of the others must be checked. Refer to the tuning procedure of the transmitter output stages for a step-by-step method of tuning the transmission line filter and associated circuits.
g. CHANGING CRYSTALS. - It may be necessary to change the channel frequencies used by the radio beacon. There are 126 crystal frequencies available for use. Refer to table 2-5 for a list of channel numbers and corresponding crystal frequencies.

To change crystals, open the front panel tuning access door on the frequency multiplier-oscillator and insert a crystal oven assembly containing the crystal of the desired frequency in the crystal oven socket (figure 3-3). For channels 1 to 63, the low-band r-f chassis is used with the crystal oven assembly plugged into socket XY1501. For channels 64 and 126, the highband r-f chassis is used with the crystal oven assembly plugged into socket XY1502.

After changing crystals, retune the frequency multiplier-oscillator and output circuits as instructed.

TABLE 2-5. CHANNEL CRYSTAL FREQU ENCIES AND PRESE LECTOR MICROMETER CAVITY HEAD SETTTINGS

| CHANNEL NO. | CRYSTAL FREQUENCIES (mc) | RECEIVER FREQUENCY (mc) | TRANSMITTER FREQUENCY (mc) | MICROMETER CAVITY HEAD SETTING (mils) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 40.083333 | 1025 | 962 | 087 |
| 2 | 40.125000 | 1026 | 963 | 090 |
| 3 | 40.166667 | 1027 | 964 | 093 |
| 4 | 40.208333 | 1028 | 965 | 096 |
| 5 | 40.250000 | 1029 | 966 | 099 |
| 6 | 40.291667 | 1030 | 967 | 102 |
| 7 | 40.333333 | 1031 | 968 | 105 |
| 8 | 40.375000 | 1032 | 969 | 108 |
| 9 | 40.416667 | 1033 | 970 | 111 |
| 10 | 40.458333 | 1034 | 971 | 114 |
| 11 | 40.500000 | 1035 | 972 | 117 |
| 12 | 40.541667 | 1036 | 973 | 120 |
| 13 | 40.583333 | 1037 | 974 | 123 |
| 14 | 40.625000 | 1038 | 875 | 126 |
| 15 | 40.666667 | 1039 | 976 | 129 |
| 16 | 40.708333 | 1040 | 977 | 132 |
| 17 | 40.750000 | 1041 | 978 | 135 |
| 18 | 40.791667 | 1042 | 979 | 138 |
| 19 | 40.833333 | 1043 | 980 | 141 |
| 20 | 40.875000 | 1044 | 981 | 144 |
| 21 | 40.916667 | 1045 | 982 | 147 |
| 22 | 40.958333 | 1046 | 983 | 150 |
| 23 | 41.000000 | 1047 | 984 | 153 |
| 24 | 41.041667 | 1048 | 985 | 156 |
| 25 | 41.083333 | 1049 | 986 | 159 |
| 26 | 41.125000 | 1050 | 987 | 162 |
| 27 | 41.166667 | 105 I | 988 | 164 |
| 28 | 41.208333 | 1052 | 989 | 167 |
| 29 | 41.250000 | 1053 | 990 | 170 |
| 30 | 41. 291667 | 1054 | 991 | 173 |
| 31 | 41.333333 | 1055 | 992 | 176 |
| 32 | 41.375000 | 1056 | 993 | 179 |
| 33 | 41.416667 | 1057 | 994 | 182 |
| 34 | 41.458333 | 1058 | 995 | 185 |
| 35 | 41.500000 | 1059 | 996 | 188 |
| 36 | 41.541667 | 1060 | 907 | 190 |
| 37 | 41.583333 | 1061 | 398 | 194 |
| 38 | 41.625000 | 1062 | 999 | 197 |

TABLE 2-5. CHANNEL CRYSTAL FREQUENCIES AND PRESELECTOR MICROMETER CAVITY HEAD SETTINGS (cont)

| CHANNEL NO. | CRYSTAL FREQUEiJCIES (mc) | $\begin{aligned} & \text { RECEIVER } \\ & \text { FREQUENCY } \\ & \text { (mc) } \end{aligned}$ | TRANSMITTER FREQUENCY (mc) | MICROMETER CAVITY HEAD SETTING (mils) |
| :---: | :---: | :---: | :---: | :---: |
| 39 | 41.666667 | 1063 | 1000 | 199 |
| 40 | 41.708333 | 1064 | 1001 | 202 |
| 41 | 41.750000 | 1065 | 1002 | 205 |
| 42 | 41.791667 | 1066 | 1003 | 209 |
| 43 | 41.833333 | 1067 | 1004 | 211 |
| 44 | 41.875000 | 1068 | 1005 | 214 |
| 45 | 41.916667 | 1069 | 1006 | 218 |
| 46 | 41.958333 | 1070 | 1007 | 220 |
| 47 | 42.000000 | 1071 | 1008 | 223 |
| 48 | 42.041667 | 1072 | 1009 | 226 |
| 49 | 42.083333 | 1073 | 1010 | 229 |
| 50 | 42.125000 | 1074 | 1011 | 232 |
| 51 | 42.166667 | 1075 | 1012 | 235 |
| 52 | 42. 208333 | 1076 | 1013 | 238 |
| 53 | 42.250000 | 1077 | 1014 | 241 |
| 54 | 42.291667 | 1078 | 1015 | 244 |
| 55 | 42.333333 | 1079 | 1016 | 247 |
| 56 | 42.375000 | 1080 | 1017 | 251 |
| 57 | 42.416667 | 1081 | 1018 | 254 |
| 58 | 42.458333 | 1082 | 1019 | 257 |
| 59 | 42.500000 | 1083 | 1020 | 259 |
| 60 | 42.541667 | 1084 | 1021 | 262 |
| 61 | 42.583333 | 1085 | 1022 | 265 |
| 62 | 42.625000 | 1086 | 1023 | 268 |
| 63 | 42.666667 | 1087 | 1024 | 271 |
| 64 | 47.958333 | 1088 | 1151 | 274 |
| 65 | 48.000000 | 1089 | 1152 | 277 |
| 66 | 48.041667 | 1090 | 1153 | 279 |
| 67 | 48.083333 | 1091 | 1154 | 282 |
| 68 | 48.125000 | 1092 | 1155 | 285 |
| 69 | 48.166667 | 1093 | 1156 | 288 |
| 70 | 48.208333 | 1094 | 1157 | 291 |
| 71 | 48.250000 | 1095 | 1158 | 294 |
| 72 | 48.291667 | 1096 | 1159 | 296 |
| 73 | 48.333333 | 1097 | 1160 | 299 |
| 74 | 48.375000 | 1098 | 1161 | 302 |
| 75 | 48.416667 | 1099 | 1162 | 305 |
| 76 | 48.458333 | 1100 | 1163 | 307 |

TABLE 2-5. CHANNEL CRYSTAL FREQUENCIES AND PRESELECTOR MICROMETER CAVITY HEAD SETTINGS (cont)

| CHANNEL NO. | $\begin{gathered} \text { CRYSTAL } \\ \text { FREQUENCIES } \\ (\mathrm{mc}) \end{gathered}$ | $\begin{aligned} & \text { RECEIVER } \\ & \text { FREQUENCY } \\ & \text { (mc) } \end{aligned}$ | TRANSMITT ER FREQUENCY (mc) | MICROMETER CAVITY HEAD SETTING (mils) |
| :---: | :---: | :---: | :---: | :---: |
| 77 | 48.500000 | 1101 | 1164 | 310 |
| 78 | 48.541667 | 1102 | 1165 | 312 |
| 79 | 48.583333 | 1103 | 1166 | 315 |
| 80 | 48.625000 | 1104 | 1167 | 318 |
| 81 | 48.666667 | 1105 | 1168 | 320 |
| 82 | 48.708333 | 1106 | 1169 | 323 |
| 83 | 48.750000 | 1107 | 1170 | 325 |
| 84 | 48.791667 | 1108 | 1171 | 328 |
| 85 | 48.833333 | 1109 | 1172 | 331 |
| 86 | 48.875000 | 1110 | 1173 | 333 |
| 87 | 48.916667 | 1111 | 1174 | 336 |
| 88 | 48.958333 | 1112 | 1175 | 338 |
| 89 | 49.000000 | 1113 | 1176 | 341 |
| 90 | 49.041667 | 1114 | 1177 | 343 |
| 91 | 49.083333 | 1115 | 1178 | 346 |
| 92 | 49.125000 | 1116 | 1179 | 349 |
| 93 | 49.166667 | 1117 | 1180 | 351 |
| 94 | 49.208333 | 1118 | 1181 | 354 |
| 95 | 49.250000 | 1.19 | 1182 | 356 |
| 96 | 49.291667 | 1120 | 1183 | 359 |
| 97 | 49.333333 | 1121 | 1184 | 361 |
| 98 | 49.375000 | 1122 | 1185 | 364 |
| 99 | 49.416667 | 1123 | 1186 | 367 |
| 100 | 49.458333 | 1124 | 1187 | 369 |
| 101 | 49.500000 | 1125 | 1188 | 372 |
| 102 | 49.541667 | 1126 | 1189 | 374 |
| 103 | 49.583333 | 1127 | 1190 | 377 |
| 104 | 49.625000 | 1128 | 1191 | 379 |
| 105 | 49.666667 | 1129 | 1192 | 382 |
| 106 | 49.708333 | 1130 | 1193 | 385 |
| 107 | 49.750000 | 1131 | 1194 | 38? |
| 108 | 49.791667 | 1132 | 1195 | 390 |
| 109 | 49.833333 | 1133 | 1196 | 392 |
| 110 | 49.875000 | 1134 | 1197 | 395 |
| 111 | 49.916667 | 1135 | 1198 | 397 |
| 112 | 49.958333 | 1136 | 1199 | 400 |
| 113 | 50.000000 | 1137 | 1200 | 403 |
| 114 | 50.041666 | 1138 | 1201 | 405 |

TABLE 2-5. CHANNEL CRYSTAL FREQUENCIES AND PRESELECTOR MICROMETER CAVITY HEAD SETTINGS (cont)

| CHANNEL <br> NO. | CRYSTAL <br> FREQUENCIES <br> (mc) | RECEIVER <br> FREQUENCY <br> (mc) | TRANSMITTER <br> FREQUENCY <br> (mc) | MICROMETER <br> CAVITY HEAD <br> SETTING <br> (mils) |
| :---: | :---: | :---: | :---: | :---: |
| 115 | 50.083333 | 1139 | 1202 | 407 |
| 116 | 50.125000 | 1140 | 1203 | 410 |
| 117 | 50.166667 | 1141 | 1204 | 412 |
| 118 | 50.208333 | 1142 | 1305 | 415 |
| 119 | 50.250000 | 1143 | 1206 | 417 |
| 120 | 50.291667 | 1144 | 1207 | 419 |
| 121 | 50.333333 | 1145 | 1208 | 422 |
| 122 | 50.375000 | 1146 | 1209 | 424 |
| 123 | 50.416667 | 1147 | 1210 | 427 |
| 124 | 50.458333 | 1148 | 1212 | 429 |
| 125 | 50.500000 | 1149 | 1213 | 432 |
| 126 | 50.541667 | 1150 |  | 435 |



Figure 2-15. Transmission Lme Filter Cavity, Tuning Curve


Figure 2-16. Control-Duplexer C-2226A/GRN-9, Right Side View (There are slight differences between the models of the various manufacturers).

## h. ADJUSTMENT OF FREQUENCY MULTIPLIEROSCILLATOR CV-1171/GRN-9D.

(1) GENERAL.-If the desired output frequency falls between 962 and 1024 mc , the low-band r-f chassis is used, power plug P1504 is connected to jack J1510, the receiver local oscillator signal plug P1514 on cable W1502 is connected to jack J1505, and plug P1513 on cable W1501 is connected to output jack J1506. If the desired output frequency falls between 1151 and 1213 mc , the high-band r-f chassis is used, power plug P1504 is connected to jack J1509, the receiver local oscillator signal plug P1514 is connected to jack J1502, and plug P1513 is connected to the output jack J1503 (figure 2-17).

## (2) TUNING CARRIER FREQUENCY GENERATING CHAIN.

## Note

With switch S1401 set at TRIPLER and AMPL., TUNING meter MI401 will show a reading, even though these stages are untuned. However, as the associated cavities are tuned through resonance, a definite peak will occur in the meter reading.

Step 1. Insert crystal oven containing crystal of desired frequency into crystal oven socket on frequency multiplieroscillator r-f chassis. When crystal oven is installed, both OVEN
and NORMAL lamps on frequency oscillator-multiplier front panel will go on. Wait until crystal oven reaches operating temperature (indicated when NORMAL lamp goes off) before proceeding with tuning. NORMAL lamp will turn on and off occasionally as crystal oven temperature cycles through its normal operating temperature range.

Step 2. Set switch S1401 to OSC, and adjust oscillator tuning coil L1 502 (high band) or L1513 (low band) for maximum reading on TUNING meter M1401 (figures 2-17 and 2-18)

Step 3. Set switch S1401 to 1ST DOUBLER and adjust first doubler tuning coil L1 503 (high band) or L1514 (low band for maximum reading on TUNING meter M1401.

Step 4. Set switch S1401 to 2ND DOUBLER and adjust second doubler tuning coil L1 509 (high band) or L1519 (low band) for maximum reading on TUNING meter M1401.

Step 5. Set switch S1401 to 3RD DOUBLER and adjust third doubler tuning capacitors C1519 and C1522 (high band) or capacitors C1536 and C1537 (low band) for maximum reading on TUNING meter M1401.

Step 6. Set METER SELECTOR switch S501, located on front panel of radio receiver, to CR201 and adjust tuning screw on tripler cavity Z1501 (high band) or Z1504 (low band)(figure 2-18) for maximum reading on TEST METER M501. If reading on TEST METER M501 exceeds midscale ( 50 microamperes), open frequency multiplier-oscillator drawer and adjust receiver local oscillator output jack J1 502 (high band) or J1505 (low band) by moving assembly in or out until TEST METER M501 reading is below midscale.


Figure 2-17. Frequency Multiplier-Oscillator CV-1171/GRN-9D, Top View


Figure 2-18. Frequency Multiplier-Oscillator CV-1171/GRN-9D, R-F Chassis, Top View

Step 7. Repeat step 6 until maximum reading, which is below midscale, is obtained on TEST METER M501; then, adjust receiver local oscillator jack J1502 (high band) or J1505 (low band) to set TEST METER M501 reading between 0.6 and 1.0 ma (between 30 and 50 microamperes on meter scale) with METER SELECTOR switch S501 set to CR201 and CR202.

Step 8. Set switch S1401 to AMPL. and adjust tuning screw on first amplifier cavity Z1502 (high band) or Z1505 (low band) for maximum reading on TUNING meter M1401.

Step 9. Recheck current through crystals CR201 and CR202 as described in step 7.

Step 10. Set switch S1401 to INCID. -KLYSTRON INPUT and adjust tuning screw on second amplifier cavity Z 1503 (high band) or Z1506 (low band) for maximum reading on TUNING meter M1401.

Step 11. Connect vertical input of Oscilloscope OS-54/URN-3 or equivalent to KLYSTRON INPUT-

INCIDENT jack J1409, and peak the tuning adjustments of first and second $r$ - $f$ amplifiers described in three steps 8,9 , and 10 to obtain maximum pulse amplitude on oscilloscope screen.

## Note

Since both the first and second amplifiers are pulsed, TUNING meter readings for these stages are rather broad. More definite indication of proper tuning is obtained by observing a rectified sample of output pulse on oscilloscope.

Step 12. When observing signal at KLYSTRON IN-PUT-INCIDENT jack, test lead to oscilloscope should be terminated in a 50 - to 70 -ohm resistance to prevent distortion of pulse. Pulse should appear as shown in waveform $b$ of figure 2-19.
(3) VIDEO CHASSIS ADJUSTMENTS. -Adjustable components in the frequency multiplier-oscillator video chassis are preset at the factory. Under normal conditions it is not necessary to check these adjust-


## o. WAVEFORM OBTAINED AT KLYSTRON INPUT INCIDENT JACK JI409


b. WAVEFORM AT KLYSTRON OUTPUT INCIDENT JACK JII57

Figure 2-19. Klystron Tuning Waveshapes
ments at the time of installation. Detailed instructions on video chassis adjustments are included in Section 6.
i. ADJUSTMENT OF RADIO RECEIVER R-824/ URN. -The radio receiver should be adjusted after OFF-ON switch 5502 on the radio receiver panel has been set to ON, and after POWER ON lamp DS501 on the receiver panel has been on for 10 minutes.
(1) POWER CHECKS.

Step 1. Set METER SELECTOR switch S501, located on front panel of radio receiver (figure 3-1) to $\mathrm{B}+200$ VFS; meter reading should be 150 volts.

## Note

200 VFS means 200 volts full-scale deflection; therefore, a meter reading of 75 represents 150 volts.

Step 2. If meter reading is not 150 volts, adjust potentiometer R 507 (figure $6-3$ ) to obtain a reading of 150 volts.

Step 3. Set METER SELECTOR switch to C - 200 VFS; meter reading should be $-105 \pm 5$ volts.

## Note

-200 VFS represents -200 volts full-scale deflection; therefore, a meter reading of 52.5 represents -105 volts.
(2) SQUITTER CONTROL VOLTAGE CHECK.

Step 1. Turn METER SELECTOR switch S501 on radio receiver panel first to CR201 and then to CR202. In each case, meter reading should be about 1 ma (half-scale deflection).

Step 2. Turn METER SELECTOR switch to SQUITTER CONTROL - 10 VFS; meter reading should be about 5 volts (half-scale deflection) when the local oscillator is normal; that is, when 1 -ma reading is obtained for either CR201 or CR202 on METER SELECTOR switch.

Step 3. Disconnect local oscillator input at jack J201; meter reading should be no less than 4 volts. Reconnect local oscillator input at jack J201.
(3) SQUITTER RATE ADJUSTMENT.

Step 1. Turn FUNCTION SWITCH on power meterpulse counter to position 2, RECEIVER SENSITIVITY. (See figure 3-17.)

Step 2. Set COUNTER SELECTOR switch on power meter-pulse counter to SQUITTER.

Step 3. Set RANGE SWITCH on power meter-pulse counter to X10.

Step 4. Squitter rate, as read on PULSE COUNT METER, should be $2700 \pm 90$ pulses per second.

Step 5. If reading obtained in step 4 is not $2700 \pm 90$ pulses per second, carefully adjust PULSE COUNT CONTROL potentiometer R 427 , located on the video chassis on the left side of the radio receiver drawer unit, until reading of $2700 \pm 90$ pulses per second is obtained on PULSE COUNT METER.
j. ADJUSTMENT OF CODER-INDICATOR KY-382/GRN-9D.
(1) ADJUSTMENT OF 1350-CPS IDENTIFICATION TONE OSCILLATOR. - To adjust the 1350-cps identification tone oscillator (figures 6-6 and 6-7), proceed as follows:

Step 1. Turn on coder-indicator by turning CODER-INDICATOR ON-OFF switch S 601 on coder-indicator panel to ON, and BATTLE SHORT switch on control-duplexer to INTLK SHORTED.

Step 2. Turn on antenna by turning ANTENNA CONTROL switch Sll02 on control-duplexer panel to $O N$.

Step 3. Connect coaxial cable from TEST OUTPUT jack on coder-indicator to VERT SIG INPUT jack on oscilloscope.

Step 4. Connect coaxial test lead from SYNC OUTPUT jack on coderindicator to EXT TRIG INPUT jack on oscilloscope.

Step 5. Open coder-indicator drawer and lower video chassis.

Step 6. Set switch S603,located on top of video chassis, to CONTINUOUS TONE.

Step 7. Lock in signal on oscilloscope with sweep speed set to 4000 microseconds per inch.

Step 8. Auxiliary reference bursts will apear as heavy pulses with tone pulse groups appearing as faint pulses, evenly spaced between auxiliary reference bursts (waveform 24E, figure 5-11). Count number of tone pulse groups which occur between auxiliary reference bursts. If 1350-cps identification tone oscillator is properly adjusted, nine tone pulse groups will appear between auxiliary reference bursts.

Step 9. If necessary, adjust coil L603 on coder-indicator video chassis until nine tone pulse groups appear between auxiliary reference bursts.

Step 10. Set oscilloscope sweep speed to 100 microseconds per inch and lock in two identification pulse pairs on oscilloscope screen.

Step 11. Adjust potentiometer R798 on coder-indicator video chassis until spacing between leading edges of first pulses in each pulse-pair is $100 \pm 10$ microseconds.
(2) ADJUSTMENT OF NORTH AND AUXILIARY REFERENCE BURSTS. -To adjust the north and auxiliary reference bursts (figures 6-6 and 6-7), proceed as follows:

Step 1. Perform steps 1 through 5 of paragraph 2-5j(1).

Step 2. Remove plug $P 906$ from jack J603 on coder-indicator video chassis.

Step 3. Lock in signal on oscilloscope with sweep speed set to 110 microseconds per inch. North reference burst will appear on oscilloscope screen as series of pulse pairs. When radio set is operating properly, north reference burst consists of $12 \pm 1$ pulse pairs (waveform 24A, figure 5-11).

Step 4. Locate potentiometer R675 on coder-indicator video chassis. Loosen shaft locking nut and adjust to obtain 12 pulse pairs on oscilloscope screen.

## Note

Turning shaft clockwise decreases the number of pulse pairs. Turning shaft counter-clockwise increases number of pulse pairs.

While observing north reference burst on oscilloscope, turn shaft of potentiometer R675 clockwise to obtain 11 pulse pairs; then turn shaft counterclockwise to obtain 13 pulse pairs. The correct setting of potentiometer R 675 is midway between settings which provide 11 and 13 pulse pairs. After potentiometer R 675 is set correctly, carefully tighten locking screw.

Step 5. Check spacing between leading edge of first pulse and leading edge of twenty-third pulse; this spacing should be $330 \pm 5$ microseconds (3 inches on oscilloscope screen with sweep speed set at 110 microseconds per inch). If spacing is incorrect, adjust coil L601 on coderindicator video chassis to obtain correct spacing.

Step 6. Replace plug p906 in jack J603 and remove plug P905 from jack J604.

Step 7. Lock in auxiliary reference burst with sweep speed set to 40 microseconds per inch. When radio set is operating properly, auxiliary reference burst should consist of $6 \pm 1$ pulse pairs.

Step 8. Locate potentiometer R672 on coder-indicator video chassis. Loosen shaft locking nut and adjust potentiometer R 672 while observing auxiliary reference burst on oscilloscope. Turn shaft clockwise until five pulse pairs are obtained; then turn shaft counterclockwise until seven pulse pairs are obtained.

The correct setting for potentiometer R672 is midway between settings which give five and seven pulse pairs.

Step 9. Check spacing between leading edge of first pulse and leading edge of eleventh pulse; this spacing should be $120 \pm 2$ microseconds ( 3 inches on oscilloscope with sweep speed set to 40 microseconds per inch). If spacing is incorrect, adjust coil L602 on coderindicator chassis to obtain correct spacing. After completing this step, north and auxiliary bursts are properly adjusted. Replace plug $P 905$ in jack J604 and close coder-indicator drawer.
(3) SETTING IDENTIFICATION CALL CODE. - For tactical reasons it may be necessary to change the identification call code. Whenever a new code is to be assigned to the radio beacon, reset the code as follows:

## Note

If the radio beacon must provide bearing and distance information to aircraft during the time taken to set up the code, turn BATTLE SHORT switch on control-duplexer to INTLK SHORTED. The radio beacon will continue to transmit a signal normal in every way except for the absence of the identification call tone. After setting the code, turn BATTLE SHORT switch to NOR (normal operating). Shut off equipment if supplying bearing and distance information is not necessary.

Step 1. Loosen the four captive screws holding coder-indicator in place and slide drawer forward. The code wheel and coder switch will be exposed on right side of drawer (figure 6-7).

Step 2. Turn off coder switch S605 located below and to right of the center of the keying wheel.

Step 3. Remove hub nut from keying wheel shaft by rotating hub nut counterclockwise.

## CAUTION

Be sure to lift keying switch 6607 cam during removal of keying wheel, to prevent damaging cam.

Step 4. To remove keying wheel, pull it forward by handles provided.

Step 5. Starting with segment indicated by START CODE arrow and going in clockwise direction, set back first three segments before starting first code character.

Step 6. Set up first character of code, using one segment pulled out for each dot, three segments pulled out for each dash, and one segment set in for space between dots and dashes (figure 3-12).

Step 7. Continuing in clockwise direction, set three segments in, to provide one full space between characters.

Step 8. Set up remaining characters of code following procedure outlined in steps 6 and 7 .

Step 9. Replace keying wheel and restore coder-indicator drawer to operating position by reversing procedure outlined in steps 1 to 4.
k. AGING THE KLYSTRON. - To age the klystron, proceed as follows (figures 2-7 and 2-8):

## Note

A new klystron, or one that has not been energized within three months or more must be aged according to the following procedure before being used. When installing a klystron, or making more than a minor change in output frequency, the three cavities of the klystron should be pretuned mechanically to the approximate operating frequency by reference to the individual tuning chart provided with each klystron. This should be done while the klystron is out of the equipment to permit access to the
three adjusting nuts on each cavity. Refer to paragraph $2-4 \mathrm{c}$ for this tuning procedure. Before aging a new klystron, check the filament voltage and, if necessary, adjust to be within the range 4.1 V to 4.3 V , see para. $2-5 \mathrm{c}$.

Step 1. Set HV switch S1902 on high voltage power supply to OFF.

Step 2. Disconnect r-f drive at input BNC jack on klystron.

Step 3. Turn MASTER SWITCH S 1101 on control-duplexer to OFF.

Step 4. Set BREAK IN-OPERATE switch Sl006 behind power supply blower compartment front panel to BREAK-IN.

Step 5. Reduce grid drive voltage to zero by turning CODER-INDICATOR switch to OFF and potentiometer R1470 located on the frequency multiplieroscillator video chassis, completely counterclockwise (figure 2-17).

## WARN ING

Make sure that HV switch S1902 on high voltage power supply is off and that high voltage is discharged.

Step 6. Connect multimeter (AN/PSM4 or equivalent)across klystron grid to cathode (figure 2-8). Set multimeter to appropriate range to read approximately 125 V dc negative on grid with reference to cathode.

Step 7. Turn MASTER SWITCH to ON.
Step 8. Reading from klystron grid to cathode should be -125 V dc. If not, adjust potentiometer R1382 on bias supply chassis of amplifier modulator (figure 2-8) for -125 V .

Step 9. Turn MASTER SWITCH to OFF and remove multimeter.

Step 10. Turn MASTER SWITCH to ON and operate klystron filament for 15 minutes.

Step 11. Set HV switch S1902 on high voltage power supply to ON. Allow a 15 -minute warmup period before proceeding.

Step 12. Set CODER-INDICATOR switch to ON and adjust potentiometer R1470 until 10 ma of beam current is indicated on BEAM CURRENT meter M1301, located on front panel of amplifier-modulator. Allow a 15 -minute period before proceeding.

Step 13. Every 5 minutes, for 15 minutes, advance potentiometer R1470 clockwise to provide incremental increase of 10 ma until 50 ma of beam current is reached. Operate at 50 ma beam current for 5 minutes.

Step 14. Set HV switch to OFF, turn potentiometer R1470 completely counterclockwise, and turn MASTER SWITCH to OFF.

Step 15. Set BREAK IN-OPERATE switch S1006 behind power supply blower compartment front panel to OPERATE.

Step 16. Turn MASTER SWITCH to ON.
Step 17. Set HV switch to ON and turn potentiometer R1470 clockwise until 60 ma of beam (HV) current is reached.

Step 18 . Every 5 minutes during a 15 -minute period, advance potentiometer R1470 clockwise to provide incremental increase of 10 ma until 90 ma is reached. Operate at 90 ma beam current for 5 minutes.

Step 19. Set MASTER SWITCH and HV switch to OFF and discharge high voltage.

Step 20. Reconnect r-f drive at input BNC jack on klystron.
Step 21. Klystron SAL-89 is now properly aged; check setting of potentiometer R1420 as follows:
a. Set HV switch and CODER-INDICATOR switch to OFF.
b. Connect multimeter (AN/PSM-4 or equivalent) across potentiometer R1425 in frequency multiplier-oscillator video chassis.
c. Set MASTER SWITCH to ON and adjust potentiometer R1420 to obtain reading of 8 volts dc.

1. TRANSMITTER OUTPUT CIRCUIT TUNING
ADJUSTMENT.

## (1) GENERAL INSTRUCTIONS.

(a) When installing a klystron, or making more than a minor change in output frequency, mechanically pretune the Issued June 73
three cavities of the klystron to the approximate operating frequency. This should be done while the klystron is out of the equipinent, to permit access to the three adjusting nuts on each cavity. To tune the three cavities, proceed as follows:

Step 1. Refer to special klystron chart provided with klystron; this chart shows a curve for each of the three cavities: INPUT, MIDDLE, and OUTPUT. (A typical klystron chart is shown in figure $2-9$ for explanatory purposes only.) Transmitter frequency is represented in horizontal scale of the curve; spacing in thousandths of an inch between inside surface of flanges is represented in vertical scale of the curve.

Step 2. Choose proper transmitter frequency and record proper spacing for each cavity.

Step 3. Check, and if necessary, readjust each cavity to settings recorded, making use of wrench provided and an inside vernier caliper. Flanges must be kept parallel to each other; this is accomplished by not turning any one nut more than a full turn before turning the other nuts the same amount.
(b) If klystron is being energized for the first time, or has not been energized during the past 3 months, age it according to procedure outlined in paragraph $2-5 \mathrm{k}$.
(c) To perform several of the steps listed in tuning procedure (paragraph 2-51(2)), detect the r-f carrier signal and observe detected pulse on oscilloscope. To preserve pulse shape, terminate coaxial test lead from oscilloscope to test jacks on radio set in low impedance at oscilloscope end. To provide this termination, connect BNC T-connector UG-274/U to oscilloscope end of test lead, and connect a BNC 50 -ohm termination MX-554/U to T-connector. (If MX-544/U termination is not available, connect $1 / 2$-watt, 50 - to 70 -ohm resistor across side jack of T-connector.) This termination must be used when observing signal at KLYSTRON INPUT 1NCIDENT and REFLECTED jacks on frequency multiplier-oscillator front panel, and at KLYSTRON OUTPUT INCIDENT and REFLECTED jacks and ANTENNA INCIDENT and REFLECTED jacks on the control duplexer front panel.
(d) Before tuning transinitter output circuits, tune carrier frequency generating chain in frequency multiplier-oscillator drawer (paragraph 2-5h).
(e) When tuning the radio set for first time or when making a large change in output frequency, preset resonant cavities of transmission line filter according to tuning curves shown in figure 2-15. Rotate tuning disc (figure 2-16) fully counterclockwise and then clockwise by the number of turns specified on tuning curves. When tuning the radio set to an adjacent channel or making slight change in tuning, it is not necessary to preset the transmission line filter cavities.
(f) The proper tuning procedure for klystron SAL-89 includes three basic steps which if performed, prevent damage of the klystron output connector from
high transmission line voltage and r-f arcing. To perform these three steps, proceed as follows:

Step 1. Create matched r-f transmission line while operating reduced klystron power levels (steps 1 through 19 of paragraph 2-51(2)).

Step 2. Apply rated klystron output power to this matched load by tuning klystron to deliver maximum power at rated operating voltage (steps 20 through 25, paragraph 2-51(2)).

## CAUTION

(ITT Models only)
The transmission filter cavities must be allowed to reach operating temperature before any attempt is made to retune the klystron. Operating temperature has been reached when the OVEN lamp DS1105 on front panel of the control-duplexer begins to flash.

Step 3. Without retuning klystron output cavity, adjust double slug tuner, filter cavities, klystron input and middle cavity for best shape and spectrum with rated antenna power (step 26, paragraph 2-51(2)).
(2) TUNING ADJUSTMENTS. - To perform the tuning adjustments, proceed as follows:

## Note

Refer to paragraph 2-5l(1) before proceeding.
Step 1. Reduce grid drive to zero by turning potentiometers R1470 and R1471. located on the frequency multiplier-oscillator video chassis, completely counterclockwise (figure 2-17).

## WARNING

Make sure HV switch S1902 on high voltage power supply is off and that high voltage is discharged.

Step 2. Connect multimeter (AN/PSM-4 or equivalent) across klystron grid and cathode connections (figure 2-8). Set multimeter to appropriate range to read approximately 125 volts de negative on grid with reference to cathode.

Step 3. Turn MASTER SWITCH S1101 to ON.
Step 4. Reading from klystron grid to cathode sinould be -125 -volt dc; if not. adjust potentiometer R1382 on bias supply chassis of amplifier-modulator. (figure 2-8) for -125 volts.

Step 5. Turn MASTER SWITCH to OFF and remove multimeter.

Step 6. Set HV switch S1902 and CODER-INDICATOR switch S601 to OFF and connect multimeter (AN PSM-4 or equivalent) across potentiometer R1425 on frequency multiplier-oscillator video chassis. Turn MASTER SWITCH S1 101 to ON.

Step 7. Adjust potentiometer R1420 to obtain reading of 8 volts de on multimeter and remove multimeter.

Step 8. Set HV switch S1902 and CODER-INDICATOR switch 6601 to $O N$ and check shaped pulse on oscilloscope.

Step 9: Turn MASTER SWITCH S1 101 to OFF and remove multimeter.

Step 10. Turn MASTER SWITCH S1101 to ON.
Step 11. Adjust potentiometer R1470 (figure 2-17) to set beam current, as indicated by BEAM CURRENT meter M1301, to 30 ma . Set HV switch S 1902 to OFF

Step 12. Connect oscilloscope input to SHAPED PULSE jack J1405 on fr squency multiplier-oscillator front panel. Connect oscilloscope sync jack to VIDEO IN jack J1404 on frequency multiplier-oscillator front panel. Adjust oscilloscope sweep and position controls to position klystron grid drive pulse peaks on. two easily remembered graticule lines.

Step 13. Connect oscilloscope to KLYSTRON INPUT INCIDENT jack J1409. Tune output cavity of the frequency multiplier-oscillator for maximum pulse amplitude at time of klystron grid drive pulse peaks by matching klystron input reflected pulse peaks to graticule lines selected in step 12.

Step 14. Connect oscilloscope to KLYSTRON INPUT REFLECTED jack J1408. Tune input cavity of klystron for minimum reflected signal at time of klystron grid drive pulse peaks.

Step 15. Repeat steps 13 and 14 until there is no further improvement, and the best symmetry about the peak of the klystron incident pulses is attained.

## Note

To preserve the waveshape of the detected r-f pulse monitored at the center cavity of the klystron, klystron output, and antema jacks. comect a $10-\mathrm{d})$ pad between the jack to be monitored and crystal detector E1152. The crystal detector 1 s stored withm the control-duplexer drawer.

Step 16. Connect oscilloscope through crystal detector E1152 to klystron center cavity fack, Adjust center cavity for maximum output without pulse flattening or loss of symmetry.

Step 17. Connect oscilloscope through crystal detector E1152 to KLYSTRON OUTPUT INCIDENT jack J1157 and adjust output cavity of klystron and double slug tuner (figure 2-20) for maximum output without pulse flattening or loss of symmetry.

Step 18. Connect oscilloscope through crystal detector E1152 to KLYSTRON OUTPUT REFLECTED jack J1152 and tune first filter cavity for minimum at peak of pulse. The first filter cavity is on the left as


Figure 2-20. Amplifier Modulator AM-1701/URN, Top Front view Showing Double-Slug Tuner
seen when facing right side of fully opened controlduplexer drawer (figure 2-16).

Step 19. Leave oscilloscope connected as in step 11 and tune second filter cavity for minimum reflected signal.

Step 20. Set HV switch S1902 to ON.

Step 21. Connect oscilloscope through crystal detector E1152 to KLYSTRON OUTPUT INCIDENT jack J1157. Adjust potentiometer R1470 for maximum pulse amplitude possible without limiting. A limited shaped pulse is shown in figure 2-21.

Step 22. Detune center cavity of klystron toward high frequency side until klystron output incident pulse amplitude is halved.

Step 23. Alternately adjust the input cavity of klystron and output cavity of frequency multiplieroscillator for maximum output.

Step 24. Alternately adjust klystron output cavity and double-slug tuner for maximum pulse amplitude without pulse flattening or loss of symmetry. Adjust klystron center cavity for maximum pulse amplitude without flattening or loss of symmetry.

Step 25. Connect oscilloscope through crystal detector E1152 to ANTENNA OUTPUT INCIDENT jack J1157. Make minor adjustments in klystron center and output cavities and double-slug tuner for best pulse shape for spectrum.

## CAUTION

After this adjustment, the output cavity of the klystron must not be retuned.

Step 26. Connect oscilloscope through crystal detector E1152 to ANTENNA INCIDENT jack J1154. Tune first and second filter cavities and make minor adjustments in double-slug tuner and in klystron input and center cavities while viewing antenna incident signal for specified power and for best pulse shape for spectrum. Further pulse shape improvement can frequently be obtained by repeating step 21.

Step 27. With oscilloscope connected as directed in step 26, look at the auxiliary reference burst on oscilloscope screen. Check that amplitude of pulses remains constant throughout reference burst. If reference burst appears as shown in waveform $c$ of figure 2-21, no further adjustment is necessary. If reference burst appears as shown in either waveform a or b of figure 2-21, adjust potentiometer R1471 on frequency multiplier-oscillator video chassis (figure 2-17) to obtain a constant amplitude for all pulses in reference burst, as shown in waveform. Adjustment of potentiometer R1470, as described in step 17, and the adjustment of potentiometer R1471 are interde-
(a)

(b)

(c)


Figure 2-21. Frequency Multiplier-Oscillator, Adjustment of R1471 to Correct for Pulse Droop in Reference Bursts
pendent. If it is necessary to adjust potentiometer R1471 to minimize droop, recheck readjustment of potentiometer R1470 by observing a single pulse on oscilloscope and touching up adjustment of potentiometer R1470 to obtain maximum pulse amplitude possible without limiting.
m. RADIO BEACON PERFORMANCE CHECKS. After the equipment has been checked, aligned, and adjusted as described in the preceding paragraphs, make the overall radio beacon performance checks described in paragraphs 3-6a(1) through 3-6a(11) of Section 3. Use the built-in test equipment for these checks. If all the requirements given for these checks are met, the radio beacon may be assumed to be in proper operating condition, and it is ready to be turned over to operating personnel.

## Note

Detailed procedures for checking the performance of the radio beacon are also covered in the Performance Standards Handbook, NAVSHIPS 93881. 32, furnished with the equipment.

## 2-6. PREPARATION FOR RESHIPMENT.

To prepare the equipment for reshipment, reverse the order of the procedure fow installing the klystron and unpacking the equipment. Determine whether the shipment is domestic or overseas and pack accordingly. Mark the carton containing the technical manuals: TECHNICAL MANUALS INSIDE.

# SECTION 3 OPERATOR'S SECTION 

## 3-1. FUNCTIONAL OPERATION.

a. GENERAL. - Radio beacons installed at shore stations employ Radio Set AN/GRN-9D, and the associated antenna groups and accessories. The radio beacon installation consists of, a receiver-transmitter group (figure 1-2), a power supply assembly (figure 1-3), and an antenna group. The major units of radio beacon are identified in table 1-1 and shown in figure 1-1.

The signals transmitted by these radio beacons provide aircraft equipped with Radio Set AN/ARN-21 with the distance and bearing information needed to determine their positions.

The AN/ARN-21 transmitter in the aircraft requests distance information by sending out interrogation signals with a repetition pattern peculiar to that transmitter. Reception of these distance interrogations at the radio beacon causes the transmission of a series of replies having the same pattern. The aircraft receives these replies along with other replies emitted by the beacon in response to interrogations from other aircraft. The AN/ARN-21 then picks out its' own reply by comparing the reply pulse patterns with that of its own transmitter. Distance is determined by measuring the total time elapsed between the initial transmission of the distance interrogation pulse pair and receipt of the corresponding radio beacon reply pulse pair, and translating this time into miles.

The radio beacon transmits bearing information by rotating a lobed antenna radiation pattern through 360 degrees, and then transmitting omnidirectional bursts of reference pulse pairs at the instant that the antenna radiation pattern is in certain reference positions. The aircraft obtains its bearing by noting the position of the antenna pattern, as determined by the relative signal strength at the time of the reference burst. A more detailed description of the operation of the radio beacon is given in Section 4.

## b. CAPABILITIES AND LIMITATIONS.

(1) RADIO BEACON. - The radio beacon transmits on one of 126 channel frequencies one mc apart, in the ranges between 962 and 1024 mc and between 1151 and 1213 mc . It receives on one of 126 channel frequencies one mc apart, in the ranges between 1025 and 1150 mc .

The radio beacon can provide individual distancemeasuring service to 100 interrogating aircraft simultaneously. The repetition frequency of the average distance interrogation pulse which the radio beacon receives is 24 cps , from as many as 95
interrogating aircraft. When receiving from 100 aircraft simultaneously, the radio beacon is operating at full load. The number of pulse pairs that the beacon transmits per second is 3600 . Of these, 2700 are either random-noise pulses or replies to distance interrogations, and the remaining nine hundred are the reference burst pulses used to provide bearing information. Once every 37.5 seconds, the inter rogation-reply and random-noise pulses are interrupted for the transmission of identificationtone pulses.

Peak power emitted from the AN/GRN-9D is 7.5 kw . Maximum range of the radio beacon is 200 miles for distance information. Bearing information may be received beyond 200 miles depending on the altitude of the aircraft. Aircraft flying in the cone of silence, approximately 55 degrees in any direction from the vertical extension of the antenna axis, will receive distance replies but not bearing information.

The 126 pairs of frequencies to which the radio beacon can be tuned fall into two groups of 63 pairs each. Since one of these groups requires a high-band antenna and the other a low-band antenna, operation of any given beacon is limited to one group of 63 channels.
(2) RADIO RECEIVER R-824/URN. -Radio Receiver R-824/URN (figure 3-1) receives and decodes pulse pairs in the frequency range of 1025 to 1087 mc when the low-band antenna is used, and 1088 to 1150 mc when the high-band antenna is used.

The radio receiver converts the received distance interrogation pulse pairs, along with random noise pulses, into an intermediate frequency of 63 mc , and amplifies and demodulates these signals. It also produces, by means of a coincidence-type decoding circuit, a single pulse for each pulse pair (interrogation or noise).
(3) CODER-INDICATOR KY-382/GRN-9D. -Coder-Indicator KY-382/GRN-9D (figure 3-2) receives distance information and noise pulses from the radio receiver. It also receives 15 -cps trigger pulses and $135-\mathrm{cps}$ trigger pulses from the reference pulse-generator in the antenna. The 15 -cps trigger, the 135 -cps trigger, and the pulses from the radio receiver are coded and mixed in proper sequence by the coder-indicator into pulses that are applied to the frequency multiplier-oscillator of the transmitter. To prevent the transponder from responding to its own transmitted output, the coder-indicator blanks the radio receiver while a pulse pair is being transmitted. The coder-indicator also generates an identification call signal which is applied to the frequency multiplier-oscillator.


Figure 3-1. Radio Receiver R-824/URN, Front Panel View
(Models fitted for TMC have a 10 dB COUPLER socket).
(4) TRANSMITTER. - The radio transmitter includes the frequency multiplier-oscillator (figure $3-3$ ), the amplifier-modulator (figure 3-4), and the duplexer in the control-duplexer (figure 3-5), and produces shaped r-f pulses spaced at proper time intervals, which are radiated from the antenna. It is capable of transmitting on any one of 126 channels in the frequency ranges of 962 to 1024 mc and 1151 to 1213 mc . The primary function of the duplexer is to permit simultaneous reception and transmission over a common antenna without interference. The receiver and transmitter carrier frequencies are always 63 mc apart.
(5) CONTROL CIRCUITS. - The control circuits of the radio beacon make it possible to automatically energize the units of the beacon in proper sequence so that no unit will be overloaded or damaged due to improper warmup. These circuits provide overload protection; the overload protective relays shut the
system down for 3 seronds if an overload occurs, and then automatically re-energize it. They will do this a total of three times during a continued overload and then will shut down the system until the cause of the overload is removed, after which the overload circuits must be manually reset. Other circuits put the automatic overload circuit into operation if a power phase or a high-voltage rectifier tube fails.

## 3-2. OPERATING PROCEDURES.

a. GENERAL. - The radio beacon is started, monitored, and stopped by controls located on the front panels of the receiver-transmitter and the power supply assembly cabinets. With the exception of EMERGENCY SWITCH S901 on the bottom panel of the receiver-transmitter group, all controls for starting the radio beacon are on the front panels of the individual units. Meters and lamps on the units indicate the stages completed in energizing the radio


Figure 3-2. Coder-Indicator KY-382/GRN-9D, Front Panel View
beacon, but it is not necessary for the operator to consult them during normal operation of the equipment. Because the various units of the radio beacon should be energized in proper sequence, relay circuits are provided which prevent the turning on of any unit prematurely.
b. DESCRIPTION OF CONTROLS. -Radio Set AN/GRN-9D consists of two main groups, ReceiverTransmitter OA-3352/GRN-9D, and Power Supply Assembly OA-1537A/GRN-9A.
(1) RECEIVER-TRANSMITTER OA-3352/ GRN-9D. -The receiver-transmitter group includes the following drawer units which are housed in Cabinet CY-3163/GRN-9D:
(a) Radio Receiver R-824/URN (figure 3-1).
(b) Coder-Indicator KY-382/GRN-9D
(figure 3-2).
(c) Frequency Multiplier-Oscillator CV-1171/GRN-9D (figure 3-3).
(d) Amplifier-Modulator AM-1701/URN (figure 3-4).
(e) Control-Duplexer C-2226A/GRN-9
(figure 3-5).
A description of each control and indicator in the receiver-transmitter group is presented in table 3-1. The controls and indicators are listed according to their physical location on the individual drawer units and their location on the cabinet (figure 3-6). Illustrations which will aid in the location of the controls and indicators are listed in the table.


Figure 3-3. Frequency Multiplier-Oscillator CV-1171/GRN-9D, Front Panel View


Figure 3-4. Amplifier-Modulator AM-1701/URN. Front Panel View


Figure 3-5. Control-Duplexer C-2226A/GRN-9, Front Panel View

TABLE 3-1. RECEIVER-TRANSMITTER GROUP OA-3352/GRN-9D, CONTROLS AND INDICATORS

| NAME OR PANEL MARKING | REFERENCE SYMBOL | TYPE | FUNCTION |
| :---: | :---: | :---: | :---: |
| RADIO RECEIVER R-824/URN <br> (figure 3-1) |  |  |  |
| TEST METER | M501 | D-c ammeter, scale, 0 to 100 microamperes | Indicates voltage present in selected receiver circuit when associated METER SELECTOR switch is set to desired position. |
| METER SELECTOR | S501 | 6 -position rotary switch | Selects signal to be fed to TEST METER meter. Function of each position is as follows: <br> OFF: Meter disconnected from receiver circuits. <br> CR201: Feeds current from crystal diode CR201 to meter. CR202: Feeds current from crystal diode CR202 to meter. B+200VFS: Feeds current from +150 voltage regulator VR503 to meter. <br> C-200 VFS: Feeds current from voltage regulator VR503 to meter. <br> SQUITTER CONTROL-10 VFS: <br> Feeds current from squitter control voltage regulator to meter. |
| ON-OFF | S502 | Toggle switch | Control for energizing or deenergizing receiver. |
| POWER | F501 and F502 | Blown fuse indicating fuse holders | Fuse cap goes on, indicating corresponding primary power fuse has blown. |
| POWER ON | DS501 | White lamp | Goes on to indicate that primary power is applied to receiver power supply. |

CODER-INDICATOR KY-382 GRN-9D
(figure 3-2)

| ANTENNA SPEED <br> ERROR | M601 | D-c meter with 3 scaled <br> arcs: red, green. and red | Indicates error voltage present <br> in the speed control. |
| :--- | :--- | :--- | :--- |
| ANTENNA CONTROL | DS602 | Amber lamp | Indicates status of antenna and <br> antenna control circuits. <br> Intermittent illumination <br> indicates malfunction. |
| POWER ON | DS601 | White lamp | Goes on to indicate that prinary <br> power is applied to coder- <br> indicator power supply. |
| CODER INDICATOR | S601 | Toggle switch | Control for energizing or de- <br> energizing coder-indicator. |
| POWER | F601 and F602 | Blown-fuse indicating <br> fuse holders | Fuse cap goes on indicating corresponding <br> primary power fuse has blown. |

TABLE 3-1. RECEIVER-TRANSMITTER GROUP OA-3352/GRN-9D, CONTROLS AND INDICATORS (cont)

| NAME OR | REFERENCE |  |  |
| :---: | :---: | :---: | :---: |
| PANEL MARKING | SYMBOL | TYPE | FUNCTION |

FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
(figure 3-3)

| OVEN | F1402 and F1403 | Blown-fuse indicating fuse holders | Fuse cap goes on, indicating corresponding crystal oven power fuse has blown. |
| :---: | :---: | :---: | :---: |
| FILAMENT | F1401 | Blown-fuse indicating fuse holder | Fuse cap goes on, indicating filament power fuse has blown. |
| TUNING | M1401 | D-c ammeter, scaled at 0 to 100 microamperes | Tuning indicator. Indicates level of signal from selected circuit when associated meter selector switch is set to desired position. |
| Meter Selector | S1401 | 9-position rotary switch | Selects signal to be fed to TUNING meter. Function of each position is as follows: OFF - Meter disconnected from frequency multiplier-oscillator circuits. <br> OSC. .. Feeds crystal oscillator V1501A or V1507A grid current to meter. <br> 1ST DOUBLER - Feeds signal from first doubler V1501B or V1507B to meter. <br> 2ND DOUBLER - Feeds signal from second doubler V1502 or V1508 to meter. <br> 3RD DOUBLER - Feeds signal from third doubler V1503 or V1509 to meter. <br> TRIPLER - Feeds signal from tripler V1504 or V1510 to meter. <br> AMPL. - Feeds signal from first amplifier V1505 or V1511 to meter. <br> KLYSTRON INPUT REFL. <br> Feeds sample of klystron reflected signal to meter. KLYSTRON INPUT INCID. Feeds sample of klystron incident signal to meter. |
| D. C. SUPPLY VOLTAGE | M1402 | D-c voltmeter, scaled at 0 volt center, 1 kilovolt at both ends | Indicates dc supplied by either low voltage power supply or medium voltage power supply when associated meter selector switch is set to desired position. |
| Meter Selector | S1402 | 5-position rotary switch | Selects voltage to be fed to D. C. SUPPLY VOLTAGE meter. <br> Function of each position is as follows: <br> OFF - Meter disconnected from circuit. <br> -375V - Feeds - 375 -volt d-c output of low voltage power supply to meter. |

TABLE 3-2. POWER SUPPLY ASSEMBLY OA-15374A/GRN-9A, CONTROLS AND INDICATORS

| NAME OR <br> PANEL MARKING | REFERENCE <br> SYMBOL |  | FUNCTION |
| :--- | :--- | :--- | :--- |$|$| TYPE |
| :--- |

## AMPLIFIER MODULATOR AM-1701/URN

(figure 3-4)

| FIL | F1302 | Blown-fuse indicating <br> fuse holder | Fuse cap goes on to indicate that <br> fuse F1302 has blown. |
| :--- | :--- | :--- | :--- |
| AIR SW OPEN | DS1303 | Neon lamp | Goes on to indicate that klystron <br> is not receiving sufficient cooling <br> air. |
| BEAM CURRENT | M1301 | D-c ammeter, scaled <br> at 0 to 200 milliamperes | Indicates amplitude of klystron <br> V1304 beam current. |
| H.V. SUPPLY | M1302 | D-c voltmeter, scaled <br> at 0 to 15 kilovolts | Indicates amplitude of voltage <br> supplied by high voltage power <br> supply. |
| FIL ON | DS1301 | White lanıp | Goes on to indicate presence of <br> filament voltages. |

CONTROL-DUPLEXER C-2226A/GRN-9
(figure 3-5)

| LINE-REG FIL BUS | S1106 | Toggle switch | Selects voltage to be fed to <br> SUPPLY VOLTS meter. <br> Function of each position is as <br> follows: <br> LINE - Feeds 120-volt ac (line <br> voltage unregulated) to meter. <br> REG FIL BUS - Feeds 120-volt <br> as (regulated) to meter. |
| :--- | :--- | :--- | :--- |
| BATTLE SHORT | S1107 | M1101 | A-position rotary switch <br> at 0 to I 50 volts |
| SUPPLY VOLTS | Provides means of shorting interlocks. |  |  |

TABLE 3-1. RECEIVER-TRANSMITTER GROUP OA-3352/GRN-9D, CONTROLS AND INDICATORS (cont)

| NAME OR <br> PANEL MARKING | REFERENCE <br> SYMBOL |  | FYPE |
| :--- | :--- | :--- | :--- |



Figure 3-6. Cabinet CY-3163/GRN-9D, Blower Compartment
(2) POWER SUPPLY ASSEMBLY OA-1537/ GRN-9A. - The power supply assembly includes the following drawer units, housed in Cabinet CY-3164/ GRN-9D.
(a) Low Voltage Power Supply PP-1766/ URN (figure 3-7).
(b) High Voltage Power Supply PP-1763/ URN (figure 3-8).
(c) Medium Voltage Power Supply PP-1765/URN (figure 3-9).

A description of each control and indicator in the power supply assembly is presented in table 3-2. The controls and indicators are listed according to their physical location on the individual power supplies listed above and to their location on the cabinet (figure 3-10). Illustrations which will aid in the location of the controls and indicators are listed in the table.

The power supply assembly cabinet also houses built-in test equipment. For a description of the controls and indicators provided on the built-in test equipment, refer to the manuals specified in table 1-2.

## c. SEQUENCE OF OPERATIONS.

(1) BEFORE USE. - After the equipment has been installed, interconnected, and adjusted as specified in Section 2, and before proceeding with the initial starting procedure outlined in paragraph 3-2 c (1) (a), proceed as follows:

Step 1. Check that the fuses, pilot lamps, and crystal oven assembly are properly installed.

Step 2. Check that all drawer units are fully closed and that all panel screws are tight, so that the interlocks function properly.

Step 3. Check that BATTLE SHORT switch, located on control-duplexer panel, is set to NOR.
(a) INITIAL STARTING. - Under certain conditions, it may be necessary for the operator to start the radio beacon after all switches have been turned off. To do this, proceed as follows:

Step 1. Place all switches on the controlduplexer to OFF (figure 3-5).

Step 2. Turn the switches on the antenna control unit to ON.


Figure 3-7. Low Voltage Power Supply PP-1766/URN, Front Panel View


Figure 3-8. High Voltage Power Supply PP-1763/URN, Front Panel View


Figure 3-9. Medium Voltage Power Supply PP-1765/URN, Front Panel View


Figure 3-10. Cabinet CY-3164/GRN-9D, Blower Compartment

TABLE 3-2. POWER SUPPLY ASSEMBLY OA-1537A/GRN-9A, CONTROLS AND INDICATORS

| NAME OR <br> PANEL MARKING | REFERENCE SYMBOL | TYPE | FUNCTION |
| :---: | :---: | :---: | :---: |
| LOW VOLTAGE POWER SUPPLY PP-1766/URN (figure 3-7) |  |  |  |
| FIL | F1601 and F1602 | Blown-fuse indicating fuse holders | Fuse cap goes on to indicate that corresponding fuse has blown. |
| PLATE | F1603 and F1604 | Blown-fuse indicating fuse holders | Fuse cap gues on to indicate that corresponding fuse has blown. |
| LV | DS1603 | Red lamp | Goes on to indicate that low voltage power supply is energized. |
| -375V | DS1601 | Green lamp | Goes on to indicate availability of -375-volt dc. |
| LV-MV READY | DS1605 | Blue lamp | Goes on to indicate that status of power control circuits enables power supply to be energized. |
| LV | S1601 | Toggle switch | Control for energizing or deenergizing low voltage power supply. |

HIGH VOLTAGE POWER SUPPLY PP-1763/URN
(figure 3-8)

| HV RECT <br> FILAMENT | F1901 | Blown-fuse indicating <br> fuse holder | Fuse cap goes on to indicate <br> that fuse F1901 has blown. |
| :--- | :--- | :--- | :--- |
| HV PLATE HOURS | M1901 | Electric time totalizing <br> meter | Indicates total number of hours <br> that plate circuits have been <br> energized. |
| FiLAMENT HOURS | M1902 | Electric time totalizing <br> meter. | Indicates total number of hours <br> that filament circuits have been <br> energized. |
| HV | S1902 | Toggle switch | Control for energizing or de- <br> energizing high voltage power <br> supply. |
| HV OVERLOAD | DS1903 | Neon lamp | Goes on to indicate presence of <br> overload condition (existence of <br> trouble) in power supply. |
| HV READY | DS1902 | Blue lamp | Goes on to indicate that status of <br> power control circuits enables <br> power supply to be energized. |
| HV | DS1901 | Red lamp | Goes on to indicate availability <br> of -12-kilovolt dc. |

MEDIUM VOLTAGE POWER SUPPLY PP-1765/URN
(figure 3-9)

| PLATE | F1801 | Blown-fuse indicating <br> fuse holders | Fuse cap goes on to indicate that <br> corresponding fuse has blown. |
| :--- | :--- | :--- | :--- |
| FIL | F1802 and F1803 | Blown-fuse indicating <br> fuse holders | Fuse cap goes on to indicate that <br> corresponding fuse has blown. |

TABLE 3-2. POWER SUPPLY ASSEMBLY OA-1537A/GRN-9A, CONTROLS AND INDICATORS (cont)

| NAME OR <br> PANEL MARKING | $\begin{aligned} & \text { REFERENCE } \\ & \text { SYMBOL } \end{aligned}$ | TYPE | FUNCTION |
| :---: | :---: | :---: | :---: |
| OVERLOAD RESET | S1802 | Toggle switch | Provides capability for manually restoring power supply to energized state after cause of the overload condition has been removed. |
| MV | S1801 | Toggle switch | Control for energizing or deenergizing high voltage power supply. |
| MV OVERLOAD | DS1803 | Neon lamp | Goes on to indicate presence of overload condition in the power supply. |
| $+700 \mathrm{~V}-+1000 \mathrm{~V}$ | DS1801 | Red lamp | Goes on to indicate availability of +1000 -volt dc. |
| CABINET CY-3164/GRN-9D <br> (figure 3-10) |  |  |  |
| AIR SWITCH OPEN | DS1001 | Neon lamp | Goes on to indicate that cabinet is not receiving sufficient cooling air. |
| BATTLE SHORT ON | DS1002 | Red lamp | Goes on to indicate that BATTLE SHORT switch, on controlduplexer, is set to BATTLE SHORTED. |
| HV PLATE 15A | F1001 to F1005 | Blown-fuse indicating fuse holders | Fuse cap goes on to indicate that corresponding fuse has blown. |
| CABINET BLOWER 3.4 | F1006 to F1008 | Blown-fuse indicating fuse holders | Fuse cap goes on to indicate that corresponding fuse has blown. |
| HIGH VOLTAGE | S1006 | Toggle switch | Provides means of reducing plate power during performance of aging klystron. |

Step 3. Turn the EMERGENCY SWITCH S901 (fig 3-6) to ON (arrow pointing up or down). When EMERGENCY SWITCH is set to ON, both OVEN and NORMAL lamps on the front panel of the Frequency Multiplier Oscillator will light. After the oven has reached its operating temperature, the NORMAL 1 amp will go out. Thereafter, the NORMAL lamp will go on and off as the heating element in the crystal oven goes on and of $f$ to maintain the correct oven temperature. In those beacons where the Control Duplexer filter cavities are fitted with heating elements, the CAVITY HEATER ON 'lamp DSllos, on the Control Duplexer front panel, will go on and off as the heating element goes on and off.

Step 4. Turn MASTER SWITCH S1101 on panel of control-duplexer (figure 3-5) to STANDBY.

Step 5. Set ON-OFF switch S502 on radio receiver panel (figure 3-1) to ON, CODERINDICATOR switch S601 on coder-indicator panel to

ON, and ANTENNA CONTROL S1102 and FIL ON switch S1108 on control-duplexer panel to ON.

## Note

All on-off switches on test equipment should be left in off position, anless test equipment is to be used for checking operation of radio beacon.

Step 6. Turn MASTER SWITCH S1 101 to ON. One minute will elapse from the time that MASTER SWITCH is moved to STANDBY before voltage is available for blue LV-MV READY light DSI605 on low voltage power supply panel. This lamp will light after this delay only if MASTER SWITCH and FIL ON switch S1108 are at ON.

AP116C-0701-1A6A (2nd Edition)

Step 7. After LV-MV READY light DS 1605 comes on, set LV switch S1601 on low voltage power supply panel (figure 3-7) to ON.

Step 8. Set MV switch S1801 on medium voltage power supply panel (figure 3-9) to ON. Five minutes will elapse from time that MASTER SWITCH is turned to STANDBY position before voltage is available for blue HV READY light DS1902 on high-voltage power supply panel. This lamp will light after 5-minute delay only if MASTER SWITCH, LV, and FIL ON switches are ON.

## WARNING

Operation of this equipment involves use of high voltages which are dangerous to life. Operating personnel must at all times observe all safety regulations. Do not change tubes or make adjustments inside equipment with high-voltage supply on. Do not depend upon safety interlock switches for protection. Under certain conditions dangerous potentials may exist in the circuits, with power controls in the off position, due to charges retained by capacitors. To avoid shock and severe burns, always discharge and ground circuits prior to touching them. Never service or adjust equipment without the presence or assistance of another person capable of rendering aid.

## CAUTION

If the equipment has not been used for a period of three months, it will be necessary to age the klystron prior to application to it of full beam voltage. (Refer to paragraph $2-5$ of Section 2 if aging is necessary.)

Step 9. When HV READY DS 1902 is on, place HV switch S 1902 on high voltage power supply panel (figure 3-8) at ON. The equipment is now fully energized and operating. Make sure that red HV lamp DS1901 is on.
(b) NORMAL STARTING. - Ordinarily, when the radio beacon is functioning normally, EMERGENCY SWITCH S901 (figure 3-6) is left at ON; that is, with the arrow pointing either up or down. The power on-off switches on the various units are left on. Power to the entire radio beacon is then under the control of MASTER SWITCH S1101 on the controlduplexer panel (figure 3-5). The radio beacon may be turned on, off, or placed in standby condition by means of this switch. The power on-off switches for the test set components mounted in the power supply assembly are normally left off, and are set to on only when the test units are to be used.

## Note

When starting the radio set for the first time, or after a shutdown period, refer to paragraph 3-2c(1)(a) of this section for the initial starting procedure.

To turn the radio beacon on by means of the MASTER SWITCH after the equipment has been shut off,turn MASTER SWITCH S1101 on the panel of the control-duplexer first to STANDBY, and then immedaitely to ON.

When the MASTER SWITCH is at ON and the radio beacon is functioning normally. the following lamps will go on: MAIN POWER ON lamp DS1102, FIL ON lamp DS 1101 , and ANTENNA CONTROL ON lamp DS1 103 on the control-duplexer panel (figure 3-5), LV-MV READY lamp DS 1103 after a 1 -minute delay, on the low-voltage power supply (figure 3-7), and HV READY lamp DS 1902, after a 5 -minute delay, on the high voltage power supply (figure 3-8).

## Note

OVEN lamp DS 1105, on cóntrol-duplexer panel, will go on and off as the cavity heating element goes on and off. (ITT Models only)
The following lamps should not go on: MV OVERLOAD lamp DS 1803 on the medium voltage power supply panel (figure 3-9), HV OVERLOAD lamp DS 1903 on the high voltage power supply panel (figure 3-8), and BATTLE SHORT ON lamp DS1 104 on the control-duplexer panel (figure 3-5).

## CAUTION

BATTLE SHORT switch S1107 (figure 3-5) should be at NORMAL. This switch is set to INTLK SHORTED only when one or more of the interlocks fail during an extreme emergency, such as battle conditions. The operator should not turn the switch to INTLK SHORTED unless told to do so by an authorized person, because opening the amplifiermodulator or high voltage power supply drawer units with the BATTLE SHORT switch at INTLK SHORTED would cause serious damage to the equipment.

The following lamps should also go on: POWER ON lamp DS501 on the radio receiver panel (figure 3-1), POWER ON lamp DS601 and ANTENNA CONTROL lamp DS602 on the coder-indicator panel (if the ANTENNA CONTROL lamp flashes, trouble in the antenna system is indicated), FILAMENT lamp DS1401 and OVEN lamp DS1403 on the frequency multiplier-oscillator panel (figure 3-3), FIL lamp DS 1301 on the amplifier-modulator panel (figure 3-4), LV lamp DS 1603 and - 375 lamp DS 1601 on the low voltage power supply panel (figure 3-7), HV lamp DS 1901 on high voltage power supply panel (figure $3-8$ ), and +1000 V la mp DS 1801 on the medium voltage power supply panel (figure 3-9).

## Note

The NORMAL lamp on the front panel of the frequency multiplier-oscillator will turn on and off as the oven thermostat turns on and off to maintain the correct crystal oven temperature.


Figure 3-11. Coder-Indicator Tone Wheel Assembly

## Note

Check that the AIR SW OPEN lamp DS 1303 on the amplifier-modulator is not on.
(2) DLRING USE.'
(a) CHANGINÔ CRYSTALS. - It may be necessary to change the channel frequencies used by the radio beacon: 126 crystal frequencies are available for use. Refer to table 2-5 for a list of channel numbers and corresponding crystal frequencies.

To change crystals, open the front panel tuning access door on the frequency multiplier-oscillator and insert a crystal oven assembly containing the crystal of the desired frequency in the crystal oven socket. For channels 1 to 63 the low-band r-f chassis is used with the crystal oven assembly plugged into socket XY1501. For channels 64 to 126 the highband $R-F$ chassis is used with the crystal oven assembly plugged into socket XY1502. After changing crystals, retune the frequency multiplier-oscillator and output circuits.

## Note

Operators shall not perform any of the frequency multiplier-oscillator and output circuit adjustments without proper authorization. Detailed tuning and adjusting procedures are presented in Section 2, paragraph 2-5.

## (b) CHANGING IDENTIFICATION CALL

 CODE. $-\bar{I}$ it is necessary to change the identification code proceed as follows (figures $3-11$ and $3-12$ ):
## Note

If the radio beacon must provide bearing and distance information to aircraft during the time taken to set up the code, turn the BATTLE SHORT switch on the controlduplexer to INTLK SHORTED. The radio beacon will continue to transmit a signal normal in every way except for the absence of the identification call tone. After setting the code, turn the BATTLE SHORT switch to NOR (normal operating). Shut off the equipment if supplying bearing and distance information is not necessary.

Step 1. Loosen the four captive screws on coderindicator panel and pull out unit.

Step 2. Snap code switch S 605 to OFF.
Step 3. Remove the nut on the code wheel by rotating it counterclockwise.

Step 4. Remove the code wheel by pulling it forward with the handles provided.

## CAUTION

During removal or replacement of code wheel, use care when lifting coding switch cam to prevent damage to switch S 607 .

Step 5. Change code on cam wheel by loosening screws in segments, pulling out or pushing back necessary cam segments, and then tightening screws. Always set up code by starting with cam segment marked START CODE. It is desirable to let three segments. including segment marked START CODE, remain pushed back before code is actually started. Therefore, unless code used more than 50 segments, the first segments should not be used and code should be set up starting with fourth segment. A dot consists of a single pulled out segment. A dash consists of three pulled out segments. To separate dots and a dash, two dots, or two dashes, push back three segments between characters of the code.

The code for USA is inserted in the following manner (figure 3-12): Push back the segment marked

START CODE and the next two segments and pull out the fourth segment; this comprises the first dot of the character U. Push back the fifth segment, pull out the sixth (second dot of character U), push back the seventh, and pull out the next three; this completes the character $U$, "dot-dot-dash". Pull out three alternate segments, forming "dot-dot-dot", the character S; push these three segments back to separate the $S$ from the next character, A. To form the character $A$, pull out the next segment, push back the following one, and pull out the three following segments; this forms the "dot-dash" of the A. The complete code, USA, has now been installed. Push back all other segments.

Step 6. Replace the coding wheel by engaging the two locating pins on wheel hub. Use caution during this procedure to avoid damaging coding switch. Replace hub nut and tighten securely by turning it in the clockwise direction. Manually turn switch S605 to ON. While code changes are made, as outlined in previous paragraph, no identification is being transmitted from radio beacon. However, bearing and distance information may continue uninterrupted during this interval.
(c) REMOTE OPERATION. - By means of a remote control unit, it is possible to place the radio beacon in off, on, or standby operating condition from a remote point. To operate the radio from a remote position, follow the normal starting procedure described in paragraph 3-2c(1)(b) and then set the MASTER SWITCH S 110 on the control-duplexer panel (figure 3-5) at REMOTE. With switch S1 on


Figure 3-12. Seting the Code
the remote control unit set at OFF, the radio set will be off and all three pilot lights on the remote unit will be off. When switch S1 is set to STANDBY, filament voltages are switched on and white ON lamp DS1 on the remote control unit will go on. To turn the radio set on, turn switch S1 to ON. After a time delay of 1 minute, red READY lamp DS2 will go on, indicating that the low voltage and medium voltage power supples are ready for operation. Five minutes after the filaments are turned on the radio set will be completely energized, and red HV ON lamp DS3 on the remote control unit will go on.
(3) STANDBY OPERATION.-Standby operation provides a means of keeping the radio set ready for immediate operation when no r-f signal is being generated by the radio set. When the MASTER SWITCH is at STANDBY, all filament voltages are on and all d-c voltages are off. After the filament voltages have been on for 5 minutes, all time delays will have been completed, and the radio set can be fully energized immediately by switching the MASTER SWITCH from STANDBY to ON.

To operate the radio beacon in standby condition, follow the normal starting procedure described in paragraph 3-2c(1) (b) and then set the MASTER SWITCH to STANDBY.
(4) AFTER USE.-Turn MASTER SWITCH SI 101 on the panel of the control-duplexer (figure 3-5) to OFF.

## Note

Under ordinary conditions, the EMERGENCY SWITCH at the bottom of the receiver-transmitter cabinet (see figure 3-6) is left at ON, and all the on-off switches except those on the built-in test equipment are left on.
(5) STOPPING THE EQUIPMENT.--When the radio beacon is being completely shut down (that is, when all switches are being turned off) set MASTER SWITCH S1 101 to OFF, wait at least 1 minute, and then turn off EMERGENCY SWITCH S901. This delay is necessary because the cooling blowers will continue to run for 1 minute after the MASTER SWITCH has been turned off but will stop immediately when the EMERGENCY SWITCH is turned off. If the blowers are turned off too soon, excessive residual heat may seriously damage the equipment.

## d. INDICATOR PRESENTATIONS.-After the equipment

 has been started in accordance with the procedures outlined, the following observations should be made to determine whether the equipment is functioning properly. Compare the readings obtained in the following checks with those entered in the equipment $\log$ to make sure they are within 10 percent of logged readings.
## Note

These observations do not constitute a complete operationa check but are intended to give the operator reasonable
assurance that the equipment is functioning normally. Refer to paragraph 3-6a for complete operator's check procedures.
(1) TUNING meter M1401, located on the front panel of frequency multiplier-oscillator (figure 3-3).
(2) BEAM CURRENT meter M1301, located on the front panel of the amplifier-modulator (figure 3-4).
(3) HV SUPPLY meter M1302, located on the front panel of the amplifier-modulator (figure 3-4).
(4) TEST METER M501, located on the front panel of the receiver (figure 3-1).
(a) The squitter-control voltage should read within 5 percent of the initial entry.
(b) The crystal rectifier CR201 and CR202 currents should read within 10 percent of the initial entry.
(5) ANTENNA SPEED ERROR meter M601, located on the front panel of the coder-indicator (figure 3-2), reads in the green portion of its scale; a reading in the red portion indicates trouble in the antenna control circuits.

## 3-3. SUMMARY OF OPERATING PROCEDURES.

After the radio beacon equipment has been inspected and adjusted as specified in Section 2, paragraphs 2-5 a through 2-51, the radio beacon may be operated. The following subparagraphs present step-by-step procedures for operating the equipment.

## Note

The equipment is shipped with a crystal installed in the frequency multiplier-oscillator. The instructions outlined in Section 2, paragraph 2-5, pertain to all adjustments made prior to operating the equipment to ensure optimum performance.
a. STARTING PROCEDURE.--To energize the equipment for the first time, or after all power switches have been turned off, proceed as follows:

## Note

Under normal operating conditions, the radio set is turned off and on by means of the MASTER SWITCH on the control-duplexer, and the EMERGENCY SWITCH is left at ON. All other power switches except those on the built-in test equipment are left at ON . When the MASTER SWITCH is turned to ON, the radio set will be ener-
sized with the proper time delays applied to the various power supplies.

## WARNING

Operation of this equipment involves the use of high voltages which are dangerous to life. Operating personnel must at all times observe all safety regulations. Do not change tuhes or make adjustments inside the ampli-fier-modulator or the high voltage power supply chassis with the high voltage supply on. Do not depend upon safety interlock switches for protection. Under certain conditions, dangerous potentials may exist in the circuit with power controls off because of charges retained by capacitors. To avoid shock and severe burns, always discharge and ground circuits before touching them. Never service or adjust the equipment without the presence or the assistance of another person capable of rendering first aid immediately.

Step 1. Turn switches on antenna control unit to ON.

Step 2. Turn EMERGENCY SWITCH S901, on blower compartment panel of receiver-transmitter group cabinet, (figure 3-6), to right until it checks into ON ; that is, with arrow pointing up or down.

Step 3. Check that white crystal oven lamps OVEN lamp DS 1403 and NORMAL lamp DS1402, on frequency multipher-oscillator panel (figure 3-3), are on. Check that OVEN lamp DS1105, on control-duplexer panel goes on.


#### Abstract

Note After the crystal oven and the cavity compartment have reached proper operating temperatures. NORMAL lanp and OVEN lamp will go out. Thereafter, NORMAL lamps will turn on and off as their respective thermostats turn the respective heaters on and off to maintain the proper operating temperatures.


Step 4. Turn MASTER SWITCH S1101, on controlduplexer panel (figure 3-5) to STANDBY.

Step 5. Check that blue MAIN POWER lamu DS 1102 , on the control-duplexer, goes on.

Step 6. Check that amber AIR SWITCH OPEN lanps DS 1303 (on anıplifier-modulator panel), DS902 (on blower compartment panel of receiver-transmitter cabınet), and DS 1001 (on bottom panel of power supply-test set group) are not on. When on, these lamps mdicate that blowers which operate air switches are not working properly.

## CAUTION

If amber lamps are on, blowers may be rotating in wrong direction. Shut off equipment immediately and check wiring for possible phase reversal by comparing equipment wiring and interconnection with schematic and wiring diagrams in Section 6. Operating equipment with blowers rotating in wrong direction may cause serious damage because of overheating.

Step 7. Set switch S 502 on radio receiver panel (figure 3-1) to ON. Check that POWER ON white lamp DS501 on radio receiver is on.

Step 8. Set CODER-INDICATOR switch S601 on coder-indicator panel (figure 3-2) to ON. Check that white POWER ON lamp DS601 on coder-indicator panel is on.

## Note

Check that all switches on antenna control unit are at ON. These switches are intended for use during servicing, and are normally left at $O N$.

Step 9. Set ANTENNA CONTROL switch S1102 on control-duplexer panel (figure 3-5) to ON. Check that white ANTENNA CONTROL lamp DS1103, on control-duplexer panel is on.

Step 10. Check that ANTENNA CONTROL lamp DS602 on coder-indicator panel (figure 3-2) is constantly on. If this lamp flashes, there is trouble in antenna or in antenna control circuits.

Step 11. Turn MASTER SWITCH S1101 to ON.
Step 12. Snap FIL ON switch S 1108 on the controlduplexer panel to ON. Check that following white la mps go on:

> FIL ON lamp DS1101 on control-duplexer. FIL lamp DS 1301 on anplifier-modulator.
> FILAMENT lamp DS 1401 on frequency multiplieroscillator.
> LV-MV READY lamp DS 1605 on the low-voltage power supply (after 1 -minute time delay).

Step 13. When blue LV-MV READY lamp goes on, set LV switch S 1601 on panel of the low voltage power supply to ON. Check that red LV lamp DS 1602 and green -375 V lamp DS 1601 , both on panel of low voltage power supply, are on. Green lamp indicates that low voltage power supply is delivering $d-c$ power to the other transmitter units of radio beacon.

Step 14. Set MV switch S 1801 on the medium voltage power supply panel to ON. Check that red +1000 V lamp DS 1801 on medium voltage power sipu!s panel is on. Check that amber MV OVERLOAD iamp DS 1803 on the medium voltage power supply pane! does not go on.

## CAUTION

When starting radio set for first time, or when starting radio set containing klystron not in use for a period of 3 months or more, the klystron must be aged before applying full power to it. Refer to Section 2 for instructions on aging klystron.

Step 15. When the HV READY lamp DS 1902 goes on, set HV switch S 1902 to ON. Check that read HV lamp DS 1901 on high voltage power supply panel is on. Check that amber HV OVERLOAD lamp DS 1903 on high voltage power supply panel is not on.
b. TUNING AND ADJUSTING PROCEDURE. - For proper operation of the radio beacon equipment, perform the following adjustments:

## Note

It is the duty of technical personnel to perform these adjustments; operators should not perform any of the adjustments without proper authorization. Detailed tuning and adjusting procedures are presented in Section 2, paragraph 2-5.
(1) Adjust regulated filament voltage.
(2) Adjust squitter control voltage.
(3) Adjust pre-selector cavities in controlduplexer.
(4) Tune crystal oscillator.
(5) Tune carrier frequency generating chain.
(6) Tune klystron and r-f output circuits.
c. CHANGING FREQUENCIES. - If it is necessary to change the channel frequency used by the radio beacon, proceed as follows:

## Note

There are 126 crystal frequencies available for use. Refer to table 2-5 for a list of channel numbers and corresponding crystal frequencies. If the desired frequency falls within the range of 962 mc to 1024 mc , use the low-band r -f chassis. If the frequency falls within the 1151- to $1213-\mathrm{mc}$ range, use the high-band r-f chassis.

Step 1. Select crystal oven assembly containing crystal of desired frequency.

## Note

If desired frequency falls within frequency range associated with $r-f$ chassis installed in frequency multiplier-oscillator, perform steps 2 through 4. If desired frequency falls
outside frequency range associated with installed r -f chassis, perform steps 5 through 12.

Step 2. Open front panel tuning access door on frequency multiplier-oscillator panel (figure 3-3).

Step 3. Remove crystal oven asse mbly inserted in crystal oven socket and insert selected crystal oven assembly.

Step 4. Retune frequency multiplier-oscillator and trans mitter output circuits.

Step 5. Open frequency multiplier-oscillator drawer to gain access to r-f chassis mounted on top of unit (figure 2-17).

Step 6. Loosen 11 captive screws securing cover to r-f chassis. Separate cover from chassis.

## Note

Operators shall not perform adjustments specified in steps 7 and 10 without proper authorization. Detailed tuning and adjusting procedures are presented in Section 2, paragraph 2-5.

Step 7. Make following disconnections within r-f chassis:
a. Disconnect power plug P1514 from jack J 1509 (high band) or jack J 1510 (low band).
b. Disconnect plug P1514 from jack J 1502 (high band) or jack J 1505 (low band).
c. Disconnect plug P1513 from jack J 1503 (high band) or jack J 1506 (low band).

Step 8. Remove four screws (two screws per side) securing r-f chassis to frame assembly. Separate $\mathrm{r}-\mathrm{f}$ chassis from frame assembly.

Step 9. Install r-f chassis associated with frequency range that covers desired frequency into frame assembly. Insert the four screws and tighten in order to secure r-f chassis to assembly.

Step 10. Make following connections within r-f chassis.
a. Connect plug P1514 to jack J1509 or jack J 1510.
b. Connect plug P1514 to jack J1502 or jack J 1505.
c. Connect plug P1513 to jack J1503 or jack J1506.

Step 11. Install cover on frame assembly by reversing procedure specified in step 6. Close frequency multiplier-oscillator drawer.

Step 12. Open front panel tuning access door on frequency multiplier-oscillator panel and insert selected crystal oven assembly into crystal oven socket.

## Step 13. Perform step 4.

## d. CIIANGING IDENTIFICATiON CALL CODE.- When-

ever a new code is to be assigned to the radio beacon, reset the code wheel as follows:

## Note

If the radio beacon must provide bearing and distance information to aircraft during the time taken to set up the code, turn BATTLE SHORT switch on controlduplexer to INTLK SHORTED. The radio beacon will continue to transmit a signal normal in every way except for the absence of the identification call tone. After setting the code, turn BATTLE SHORT switch to NOR (normal operating). Shut off the equipment if supplying bearing and distance information is not necessary.

Step 1. Loosen the four captive screws holding coder-indicator in place and slide drawer forward. Code wheel and coder switch will be exposed on right side of drawer.

Step 2. Turn off code switch S605 located below and to right of center of keying wheel.

Step 3. Remove hub nut from keying wheel shaft by rotating hub nut counterclockwisc.

## CAUTION

During removal of keying wheel, care should be taken to lift keying switch S 607 cam to prevent danraging cam.

Step 4. Remove the keying wheel by pulling it forward with the handles provided.

Step 5. Starting with segment indicated by START CODI arrow and going in clock wise direction, set back first three segments before starting first code character.

Step 6. Set up first character of code, using one segment pulled out for each dot, three segments pulled out for each dash, and one segment set in for space between dots and dashes (figure 3-12).

Step 7. Continuing in clockwise direction, set three seg. ments in to provide one full space between characters.

Step 8. Set up remaining characters of code, following procedure outlined in steps 6 and 7.

Step 9. Replace keying wheel and restore coder-indicator

## c. SECURING TIIE EQUIPMINT

(1) TURNING OFF RADIO BEACON. I/nder mormal operating conditions, all on-off switches except those located on the built-in test equipment are left on. To turn of the radio beacon, turn MASTER SWITCII SIIO1, located on the control duplexer panel to OFF.

## Note

EMERCENCY SWITCII, located on the blower compartment panel of receiver-transmitter cabinet, is left at ON.
(2) SIIUTTING DOWN RADIO BEACON. To completely shut down (de-energize) radio beacon, proceed as follows:

Step 1. Set IIV switch S1902 on high voltage power supply panel to OFF.

Step 2. Set MV switch S1801 on medium voltage power supply panel to OFF.

Step 3. Set LV switch S1601 on low voltage power supply panel to OFF.

Step 4. Set FIL ON switch S 1108 and ANTENNA CONTROLSWITCII S1102, both on control-duplexer pancl, to OFF.

Step 5. Set CODER-INDICATOR switch S601 on coderindicator panel to OFF.

Step 6. Set switch S502 on receiver panel to OFF.
Step 7. Set all switches on antenna control unit to OFF.
Step 8. Set MASTER SWITCH S1101 on control duplexer panel to OFF.

Step 9. At least 1 minute after setting MASTER SWITCH to OFF, set EMERGENCY SWITCH S901 to OFF.

## CAUTION

The delay specified in step 9 is necessary in order to dissipate the residual heat remaining in the cabinets. The blowers will continue to run for 1 minute after MASTER SWITCH has been set to OFF, but they will stop immediately when EMERGENCY SWITCH is set to OFF. If blowers are turned off too soon, equipment may be seriously damaged.

## 3-4. EMERGENCY OPERATION

If the radio beacon must provide bearing and distance information to aircraft during the time taken to make certain operational changes (when changing crystal frequency or identification call code, for ex-
ample) set BATTLE SHORT switch on controlduplexer panel to INTLK SHORTED.

## Note

Operators should not set BATTLE SHORT switch to INTLK SHORTED without proper authorization.

3-5. TEST PROCEDURES (FOR TEST EQUIPMENT ONLY).
Test Equipment is provided to permit a rapid check of operating characteristics of the Radio Beacon.
a. ORIGINAL TEST EQUIPMENT (TABLE 1-2). - This test equipment includes the following five units:
(1) Pulse Sweep Generator SG-212A/URN-3.
(2) Pulse Analyzer/Signal Generator TS-890A/ URV-3.
(3) Power Meter/Pulse Counter TS-891/URN-3.
(4) Oscilloscope OS-54/URN-3.
(5) Switch-Test Adapter SA-420/URN-3.

The first four units are mounted in the upper part of the Power Supply Cabinet. The location of the Switch-Test Adapter is optional. The functions of the test equipment and the principles upon which the various tests are made are included in Section 4.

Refer to Para 4-3a(7) for the functional description of the test equipment and to Para 43c for a description of the test principles.

Although the Control Monitor Group AN/GRA-34 and its associated Remote Switching Unit C-2234/ GRA-34, are not regarded as part of the built-in test equipment they are used to provide monitoring facilities and unattended, and automatic, operation of one or two radio beacons.
b. REPLACEMENT TEST EQUIPMENT (TABLE l-2b). This equipment includes the following three units:
(1) Spectrum Analyzer/Test Generator MM-705.
(2) Oscilloscope MM-504.
(3) Power Metér - Pulse Counter - Marker Gemerator MM-109.

These units are mounted with a Transfer and Switching Unit, a Transfer and State Transmission lnit (TELOTEL), and its associated interface unit, and two Transponder Monitors in the Electrical Equipment Cabinet 212A and are interconnected through a cable harness and (for certain tests) two function switches, all of which permit rapid cunnection for standard test procedures. Refer to Para 4-3a(7)(f) for a functional description of the test equipnent and to Para 3-6a(12) for a description of the test procedures.

## 3-6. OPERATOR'S MAINTENANCE.

Original Test r quiment (TABLE 1-2) Only.
a. OPERATING (HLenS AND ADJUSTMENTS.

It is desirable to make sure that the radio beacon
meets certain minimum pertormance requirements. The series of tests described in the followiny paragraphs serve to determine whether or not the radio beacon is operating properly, and whether or not optimum performance adjustments are required. The test procedures are based on using the built-in test equipments. The checks should be performed dalv. It is not necessary to turn off the radio beacon to perform the checks.

The built-in test equipment must be interconnected as shown in figure $3-13$ so that the special test described in this section may be performed.

## Note

All references to the pulse analyzer-signal generator throughout this manual are for Pulse Analyzer-Signal Generator TS-890A/ URN-3 or TS-890B URN-3 unless otherwise noted.
(1) PRELIMINARY SETTINGS OF FRONT PANEL CONTROLS ON PULSE ANALYZER-SIGNAL GENERATOR TS-890A/URN-3. - Before making any
tests with TS-890A/URN-3, set up the front panel controls as follows (figure 3-14):

Step 1. Set OUTPUT ATTENUATOR to 0 DBM.
Step 2. Set INPUT ATTENUATOR SELECTOR control to maximum attenuation.

Step 3. Set BAND SHIFT switch on 0.
Step 4. Set MODULATION SELECTOR to C.W.
Step 5. Set CHANNEL SELECTOR control to applicable channel.

## Note

If built-in crystal oscillator is to be used as frequency generating source. omit steps 6 .
7. and 8.

Step 6. Set MAIN TUNING control to applicable channel.

Step 7. Set OSCILlator SELECTOR to V. F. O. CALIBRATE.

Step 8. Adjust V., F. O. CALIBRATE control until zero beat is heard in headphone plugged into V. F. O. CALIBRATE JACK.

Step 9. Set OSCILLATOR SELECTOR switch to either REF. OSC. (for crystal control) or to V. F. O.. depending on which oscillator is to be used as generating source.

Step 10. Adjust for a zero reading on OUTPUT LEVEL indicator, using its ZERO SET control.

Step 11. Set INTERROGATE switch to ON.

## Note

Before performing step 12, energize the Pulse-
Sweep Generator SG-121A/URN-3 (figure 3-15) and allow it to warm up for at least 2 minutes.

Step 12. Set POWER SET control to midscale.
Step 13. Adjust PULSE AMPLITUDE control, located on the SG-121A/URN-3 to obtain a midscale reading (100) on OUTPUT LEVEL INDICATOR (figure 3-15).

Step 14. Adjust CHANNEL SELECTOR slightly for a maximum reading on OUTPUT LEVEL INDICATOR.

## Note

There is a time lag between the application of signal to OUTPUT LEVEL INDICATOR and indication of power level. When taking readings on this meter, allow time for stabilization of needle.

note I When checking zero distance or, ay 'ris veag must be wonnected to the antenna incident jack in plame of the lead shown
NOTE 2 WHEN CHECKING RECEIVER SENS:TIVIT YHIS LEAD MUST BE GNNECTED TO ine antenna incident jack in place of the lead shown

| TRANSFER AND SWITCHING UNIT MM-1602 |  | RADIO RECEIVER |
| :---: | :---: | :---: |
| SPECTRUM ANALYZER/TEST GENERATOR MM-705 <br> ATTEN <br> 0 |  |  |
|  |  |  |
| OSCILLOSCOPE MM-504 |  |  |
| POWER METER-PULSE COUNTERMARKER GENERATOR MM-IO9 |  | ATOR |
| TRANSFER AND STATE TRANSMISSION UNIT (TELOTEL) |  |  |
| TACAN TRANSPONDER MONITOR MM-209 | TACAN TRANSPON DER MONITOR MM-209 | FREQUENCY MULTIPLIER OSCILLATOR |
|  |  | MENT |



Figure 3-14. Pulse Analyzer-Signal Generator TS-890A/URN-3, Front Panel View

Step 15. Readjust PULSE AMPLITUDE control on SG-121A/URN-3 to obtain midscale reading (100) on OUTPUT LEVEL INDICATOR.

Step 16. Adjust ZERO SET control of POWER COMPARISON INDICATOR to obtain zero on POWER COMPARISON INDICATOR.

Step 17. Set MODULATION SELECTOR to PULSE.

## Note

The TS-890A/URN-3 is now ready for use in making tests. Upon completion of tests, shut down equipment by turning INTERROGATE and POWER switches to OFF.
(2) PEAK POWER MEASUREMENTS.- Peak power delivered to the antenna must be 7.5 kw , or greater; to obtain this measurement, proceed as follows:

Step 1. Turn FUNCTION switches on Oscilloscope OS-54/ URN-3 (figure 3-16) and power meter-pulse counter (figure 3-17) to OPERATING TEST.

Step 2. With radio set fully operative, observe transmitter r-f envelope on oscilloscope. It should appear as shown in figure 3-18. Note that gain, sweep speed, and trigger selection controls on oscilloscope are automatically set as required for this test by internal controls associated with position 1 , OPERATING TEST, of FUNCTION switch. Adjust-


Figure 3-15. Pulse Sweep Generator SG-121A/URN-3, Front Panel View


Figure 3-16. Oscilloscope. Front Panel View
ment procedures for these controls are described in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope. The SCALE ILLUMINATION, TRIG AMP. and SWEEP STABILITY controls, and the SIGNAL DELAY SELECTOR and MARKER SEL switches are the only other controls which remain effective. These should be set, respectively, to counterclockwise. 5. 5. OUT, and OFF. If a stable sweep is not achieved with the se settings, adjust TRIG AMP and SWEEP STABILITY controls as required.

Step 3. Turn PEAK PWR VOLTAGE control on power meter-pulse counter completely counterclockwise to its minimum setting.

Step 4. Depress RF POWER switch on power meter-pulse counter and maintain it in that position while making measurement.

Step 5. While observing pulse envelope on oscilloscope (figure 3-18), turn PEAK PWR VOLTAGE control clockwise until negative pulses just touch baseline. At this point, stop advancing control and read $r-f$ power directly in kilowatts on PEAK RF POWER meter. Release RF POWER switch. A reading of 7.0 kw or more is considered normal. If this requirement is not met, report trouble to technical persomel.


Figure 3-17. Power Meter-Pulse Counter TS-891/URN-3, Front Panel View


Figure 3-18. Transmitter Output R-F Envelope
(3) VISUAL PULSE SHAPE.

Step 1. Turn the FUNCTION SWITCH on the oscilloscope to position 1, OPERATING TEST.

Step 2. With the radio set fully operative, observe r-f envelope on oscilloscope; it should appear as shown in figure 3-18.

Step 3. Utilizing 1-microsecond MARKER SEL switch on oscilloscope, measure spacing between pulses; spacing should be $12 \pm 0.5$ microseconds.

Step 4. Measure pulse width at half-amplitude points. The correct pulse width is $3.5 \pm 0.5$ microseconds. If this requirement is not met, report trouble to technical personnel.

## (4) OUTPUT PULSE COUNT.

Step 1. Turn FUNCTION SWITCH on power meter pulse counter to position 1, OPERATING TEST.

Step 2. Set COUNTER SELECTOR switch to ${ }^{+}$.

Step 3. Set RANGE SWITCH to X10. Output pulse count with radio set operating properly, should be $7200 \pm 180$ pulses per second ( 3600 pulse pairs). If rerequirement is not met, report trouble to technical personnel.
(5) OUTPUT PULSE SPECTRUM TEST.-The built-in test equipment includes a sharply tuned relative power meter (analyzer portion of TS-890A/URN-3) which is used to compare sideband energy with center frequency energy for an accurate check of pulse shape. The test equipment is highly specialized for this purpose. The test is made with the beacon operating under normal traffic conditions. Proceed as follows:

Step 1. Make preliminary setup of TS-890A/URN-3 as directed in paragraph 3-6a(1).

Step 2. Remove connection at RECEIVER INPUT jack of TS-890A/URN-3.

Step 3. Perform output pulse spectrum test in accordance with detailed procedure covered in Technical Manual for the TS-890A/URN-3 and TS-890B/URN-3 (NAVSHIPS 93231). The test procedure is in Section 3, paragraph 3-4a of the issue of this manual incorporating change number 2 .
(6) SQUITTER COUNT.

Step 1. Turn FUNCTION SWITCH on TS-891/URN-3 to
position 2, RECEIVER SENSITIVITY.

Step 2. Set COUNTER SELECTOR switch on TS-891/URN3 to SQUITTER.

Step 3. Set RANGE SWITCH on TS-891/URN-3 to X10. The squitter rate, as read on PULSE COUNT METER, should be $2700 \pm 90$ pulses per second. If this requirement is not met, report trouble to technical personnel.

## (7) REPLY COUNT (RECEIVER SENSITIVITY).

Step 1. Make preliminary setup of front panel controls of pulse analyzer-signal generator as directed in paragraph 3-6a(1).

## Note

Before proceeding, check that setting of OUTPUT ATTENUATION SELECTOR on TS-890A/URN-3 is at maximum attenuation so as not to load the beacon and cause the squitter voltage to become positive.

Step 2. Set MODULATION SELECTOR switch on TS-890A/ URN-3 to PULSE.

Step 3. Connect coaxial test lead from RF OUTPUT jack on TS-890A/URN-3 to ANTENNA INCIDENT jack on controlduplexer.

Step 4. Set FUNCTION SWITCH ON TS-890A/URN-3 to position 2 , RECEIVER SENSITIVITY.

Step 5. Set COUNTER SELECTOR SWITCH on TS-891/ URN-3 to REPLY RATE.

Step 6. Set RANGE SWITCH on TS-891/URN-3 to X10.
Step 7. Set PRF RANGE on SG-121 A/URN-3 to 1000 and PRF MULTIPLIER to X1.

Step 8. Set PULSE CODING $\mu$ SEC switch on SG-121A/URN3 to 12.

Step 9. Advance OUTPUT ATTENUATOR on TS-890A/ URN-3 until reply count is reduced to 600 .

Step 10. Read RF OUTPUT DBM scale on OUTPUT ATTENUATOR. The RF OUTPUT DBM should be -53 dbm or more. If this requirement is not met, report trouble to technical personnel.

## Note

Receiver sensitivity is defined as the signal level required to obtain 60 percent reply to an interrogating signal. With pulse-pair repetition rate set at 1000 pulse pairs per second, a reply rate of 600 will indicate 60 percent response. A properly coded signal having a level of -93 dbm will cause receiver
to reply to at least 60 percent of interrogating pulses. Since directional coupler DC1156 through which test signal is fed has a coupling loss of 40 db , a test signal at a level of -53 dbm will cause receiver to respond to at least 60 percent of interrogating pulses. If the antenna were disconnected from RF OUTPUT jack on control-duplexer and the test signal fed into RF OUTPUT jack, receiver would then respond to 60 percent of interrogating pulses of test signal having level of -93 dbm or less.

Step 11. Test the 12-microsecond acceptance decoder of radio receiver to determine whether it is working properly; this is done by observing whether reply rate remains the same for the $11.5 \mu \mathrm{SEC}$ and $12.5 \mu \mathrm{SEC}$ positions of PULSE CODING switch. The number of replies should be reduced considerably for the 11 and 13 :SEC positions of switch. The radio recenver decoder is designed to pass all pulse pairs with a spacing of from 11.5 to 12.5 microseconds between pulses of a pair. Pulse pairs with spacings of 11 micruseconds or less. and those of 13 mic roseconds urgreater, will be either attenuated or decoupled.

Step 12. Repeat steps 7 through 9. changing PRF RANGE setting to 200 and PRF MULTIPLIER to X1. A minimum reply count of 120 at -53 dbm should be olitaned.

Step 13. Repeat steps 7 through 9. changing PRF RANGE setting to 250 and PRF MULTIPLIER to X10. A manmum reply count of 1500 repilies at -53 dbm chuala be obtained. If this requirement is not met, sewor trouble to technical personnel.
(8) CHECKING RECEIVER BLANKING TIME.

Step 1. Allow at least 10 minutes for receiver warmap time.

Step 2. Connect TEST OUTPUT jack on front panel of recelver to oscilloscope EXT TRIG INPUT (figure 3-16). Use positive sync on oscilloscope.

Step 3. Connect blanking pulse test point TP9 to vertical input of oscilloscope. Test point TP9 is located on radio receiver video chassis (figure 6-5). Make necessary adjustments on oscilloscope to synchronize blanking pulses. Total horizontal sweep should be between 50 and 100 microseconds.

Step 4. The blanking pulse should be $40+2$-microseconds wide. If necessary, adjust potentiometer R443 to set pulse duration at $40 \pm 2$ mic roseconds. BLANKING TIME ADJUST control R443 is located on the radio receiver video chassis (figure 6-3).
(9) CHECKING RECEIVER LOCAL OSCILLATOR SIGNAL. -Set METER SELECTOR SWITCH S501 on receiver front panel to CR201 and CR202. The METER should read halfscale deflection at each position. If necessary. local signal strenirth may be adjusted by moving pickup prube on electron tube V1504 tripler cavity in or out to obtain the optinum meter reading.
(10) REFERENCE BURST PULSE COUNT.

Step 1. Turn FUNCTION SWITCH on oscilloscope to position 2, RECEIVER SENSITIVITY.

## Note

TRIGGER AMP and SWEEP STAB. controls of oscilloscope may have to be adjusted carefully to obtain waveform showin in figure 3-19.

Step 2. Check oscilloscope: the presentation shown in figure 3-19 should appear. Normal indication, as shown in figure 3-19, is six auxiliary reference burst pulse pairs (heavy pulses) and 12 north reference burst pulse pairs (light pulses). Five of the north reference pulse pairs will be superimposed on the auxiliary pulse pairs. A north pulse pair should be visible; one pulse of the pair to the left. and one pulse of the pair to the right of the fourth and ninth auxiliary pulses. Seven more north burst pulse pairs should be counted at the end of the auxiliary burst. If the requirement is not met. report the trouble to technical personnel.

Figure 3-19. Composite Waveform, North and Auxiliary Reference Burst


Figure 3-20. Zero Distance Delay Measurement Waveforms
(11) ZERO DISTANCE CHECK.

Step 1. Set FUNCTION switches on oscilloscope and TS-891/URN-3 to position 3. SYSTEM DELAY.

Step 2. Set SG-121A/URN-3 INT-SWEEP-EXT switch to SWEEP and PULSE CODING $\mu$ SEC switch to 12. Set OVERALL DELAY-VIDEO DELAY switch to 1 .

Step 3. Adjust TS-890A/URN-3 to provide a modulated sisnal by following the preliminary setup procedure in paracrraph 3. At completion of those steps. set MODULATION SELECTOR to PULSE and set RF OUTPUT attenuator to - 35 DBM.

Step 4. Observe display on oscilloscope and, if necessary, adjust controls in top row for clear presentation. Note that there are two sets of pulses displayed; the radio beacon output pulse and a pair of reference pulses. Adjust SG-121A.URN-3 BALANCE control so that pulses from TS-890A, URN-3 are shghtly larieer in amplitude than pulses from ANTENNA INCIDENT jack.

Step 5. If pattern such as waveform in figure 3-20 is obtained ( $u$ ith radio beacon output pulse pair to left of reference pulse parr), overall delay is less than $50.2^{\circ}$ microseconds and next step may be performed.

If it is to right, zero delay is too great and must be adjusted. If requirement is not met, report trouble to technical personnel.

Step 6. Change switch setting on SG-121A/URN-3 to OVERALL DELAY 2. Observe that pattern is like waveform b of figure 3-20. If not (that is, if radio beacon output is to left of reference pulse pair), zero distance relay is less than 49.8 microseconds and must be adjusted. Ideally, output pulses should be as much to right of reference pulse (switch position 1) as they are to left (switch pesition 2).

## Note

Delay error indicated by above check is marnified by type of presentation used. The check is intended as an accurate. readable go-no go gauge and should be so used.

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| DAILY'CHECKS |  |  |
| POWER DISTRIBUTION AND CONTROL |  |  |
| Panet fuses (table 3-4) | Inspect all indicating fuseholders on receiver-transmitter group cabinct and power supply cabinet. | A glowing fuseholder indicates a blown fuse. Replace iuse. |
| Cabinet blowers (fagures 3-6 and 3-10) | Inspect amber AIR SW OPEN lamps on amplifier-modulator DS1303. blower compartment panel of the receiver-transmitter cabinet (DS901). and blower and transformer compartment of power supply cabinet (DS1001). | If one of the lights is on. a blower is not working properly. De-enercrize equipment and repair or replace blower. Blower filters should be cleaned in accordance with procedure in pararraph 3-6t, (1)(b). |

12. TEST PROCEDURES USING REPLACEMENT TEST EQUIPMENT (TABLE 1-2b) ONLY. - For easy reference the following abbreviations are used to denote specific pieces of test equipment:

XFER UNIT for Transfer and Switch Unit MM-1602
CTR Unit for Power Meter - Pulse Counter Marker Generator MM-109

SA/TG for Spectrum Analyzèr/Test Generator MM-705

CABLE for Calibrated Cable BOO2314 (a) SQUITTER RATE MEASUREMENT AND TOTAL PULSE COUNT. - If the operational beacon is to be tested, it must be removed from service before proceeding. To do this, inhibit both Transponder Monitors, turn the standby beacon MASTER SWITCH to $O N$ and set the ANTENNA XFER SEL switch on the XFER 时T to the standby position.

1 On ther XFER UNIT and CTR unit, set the PRIMARY POWER switches to ON. Allow the test equipment five minutes to stabilize.
2. On the CTR Unit, confirm that the coaxial link is connected between the NON-CAL COUPLER and LIN DET INPUT jacks
3. a. Sel the BATTLE SHORT switch to INTLK SHORTED.
b Release the bolts securing the Coder Indicator and draw the unit fully forward.

4 a. Set the Coder switch 5605 to OFF
b. At the rear of the beacon, remove the cables.from the NORTH INPUT and AUXILIARY INPLT sockets. Mark/identify the cables to ensure correct reconnection.

5 On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
6. On the CTR unit, set the controls as follows:
a. FUNCTION switch to TRANSPONDER TEST
b. MODE switch to FUNCTION TEST
c. Momentarily depress the COUNTER

INPUT READ switch and adjust the COUNTER INPUT COARSE and FINE controls for a reading within the green zone of the PEAK RF POWER meter.

## Note

Use the lowest setting of the COUNTER INPUT COARSE control that allows adjustment of the FINE control to give the green zone reading.
d. COUNTER/MARKER SELECT switch to any COUNT position.
e. TIME INTERVAL selector to $1 \cdot 0$ SECS. Set the DISPLAY TIME control as desired.
f. MARKERS switch to GATED

Squitter Rate
7. On the CTR unit, observe the Nixie readout. The count should be between 5220 and 5580 pulses per second (nominally 5400 pulses per
second). If necessary, adjust the squitter rate as detailed in Paragraph 6-2h (1)
8. a Replace the NORTH and AUXILIARY cables at the rear of the beacon.
b. Set the Coder switch S605 to ON and return the Coder Indicator to the rack. Tighten and secure the bolts.
c. Set the BATTLE SHORT switch to NOR.

## Total Pulse Count

9. On the CTR unit, observe the Nixie readout. The count should be between 7020 and 7380 pulses per second, (nominally 7200 pulses per second).

Note
During identity transmission, the total pulse count is reduced to approximately 6660 pulses per second for the duration of a tone transmission.
10. If the beacon was removed from service, return beacon and Monitors to normal operation.
(b) PULSE PaIR analysis. -

1. On the XFER UNIT, Oscilloscope and CTR unit, set the PRIMARY POWER switches to ON. Allow the test equipment approximately five minutes to stabilize.
2. On the CTR unit, confirm that the coaxial link is connected between the NON-CAL COUPLER and LIN DET INPUT jacks.
3. On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
4. On the CTR unit, set the FUNCTION switch to TRANSPONDER TEST.
5. Set the Oscilloscope controls as follows:
a. MAG switch to OFF.
b. Vertical MODE switch to CH2.
c. Vertical TRIGGER switch to NORM
d. CH2 input selector to SYSTEM TEST AC.
e. A TRIG SOURCE selector to SYSTEM P.
f. A TRIGGER MODE selector to AUTO.
g. Depress the TRACE FINDER button and use the INTENSITY and POSITION controls to centralize the trace
6. Set the Oscilloscope timebase controls:
a. HORIZ DISPLAY switch to A.
b. A TIME/CM (outer control) to $5 \mu$ sec.
c. B TIME/CM (pull to unlock) to
$1 \cdot{ }^{\circ} \mathrm{H} \sec$.
d. VARIABLE TIME/CM A and B fully
clockwise.
7. Set the Oscilloscope CH 2 VOLTS $/ \mathrm{CM}_{1}$ and VARIABLE VOLTS/CM controls for a 6 cm vertical deflection and inspect the displayed pulse
pairs for normal gaussian configuration. If a positive-going waveform is desired, pull the CH2 PULL TO INVERT knob and re-adjust the CH 2 vertical POSITION control.
8. On the CTR unit, calibrate the markers as follows:
a. Turn the COUNTER/MARKER SELECT switch to the $0.5 \mu$ SEC position.
-b. Set the MARKERS switch to FREE RUN and the MODE switch to FUNCTION TEST.
c. Set the TIME INTERVAL selector to 0.01 SECS, momentarily lift the CTR RESET switch and adjust the 2 MC SET control for a Nixie readout of 20000 (disregard the decimal).
d. Set the MARKERS switch to GATED.
9. Use the MARKERS INTENSITY and POSITION controls on the CTR unit, also the oscilloscope INTENSITY control, to position one $0.5 \mu \mathrm{sec}$ marker (intensified) on the leading or trailing edge of the first pulse, at the half-amplitude point.
10. Set the Oscillos cope HORIZ DISPLAY switch to the left-hand B DLY'D BY A position. Pulse Spacing
11. Using the DELAY TIME MULT control, count markers to measure the time interval to the same point on the second pulse. The pulse spacing should be between 11.75 and $12.25 \mu \mathrm{sec}$. (nominally $12 \mu \mathrm{sec}$ ).

## Pulse Width

12. Carefully measure the pulse width at the half-amplitude point; the pulse width should be between 3.0 and $4.0 \mu \mathrm{sec}$, (nominally) $3 \cdot 5 \mu \mathrm{sec}$ ).

Rise- and Fall-time
13. Use the $0 \cdot 5 \mu$ sec markers to measure the pulse rise and fall-time. These should be between 2.0 and $3 \cdot 0 \mu$ sec between the $10 \%$ and $90 \%$ amplitude points. Three minor graticule divisions represents $10 \%$ of 6 cm .
14. Repeat sub-clause (8) to determine marker accuracy; if the 2 MC SET control requires adjustment, sub-clauses 9 to 13 must be repeated.
(C) REFERENCE BURST ANALYSIS.-

1. On the XFER UNIT, Oscilloscope and CTR unit, set the PRIMARY POWER switches to ON. Allow the test equipment five minutes to stabilize.
2. On the CTR unit, confirm that the coaxial link is connected between the NONCAL COUPLER and LIN DET INPUT jacks.
3. On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
4. On the CTR unit, set the REF MKR switch to NORTH and the FUNCTION switch to REF BURSTS/ANTENNA SPEED. Calibrate the markers as follows:
a. Turn the COUNTER/MARKER SELECT switch to $0.5 \mu \mathrm{sec}$
b. Set the MARKERS switch to FREE RUN and the MODE switch to FUNCTION TEST.
c. Set the TIME INTERVAL selector to 0.01 SECS, momentarily lift the CTR RESET switch and adjust the 2MC SET control for a readout of 20000 on the Nixie display (disregard the decimal).
d. Set the MARKERS switch to GATED.
5. On the CTR umit, set the COUNTER/ MARKER SELECT switch to the $1 \cdot 0 \mu$ SEC position.
6. Set the Oscilloscope controls as follows:
a. MAG switch to OFF.
b. Turn the VARIABLE TIME/CM A and B controls fully clockwise.
c. Vertical MODE switch to CH1.
d. Vertical TRIGGER switch to NORM.
e. CHI input selector to SYSTEM TEST AC.
f CHI VOLTS/CM selector to 0.5
$g$ DELAY TIME MULT control fully counterclockwise
h. A TRIG SOURCE selector to SYSTEM TEST $P$ and the TRIGGER MODE switch to AUTO.
j. HORIZ DISPLAY switch to the leit-hand side A INTEN BY B position:
$k$. Set the A TIME/CM and DELAY TIME combined or integral control (outer control) to the $50 \mu$ SEC position and the B TIME/CM AND DELAY TIME control (pull to unlock) to the $2 \mu \mathrm{SEC}$ position.
7. Depress the TRACE FINDER biatton and use the DELAY TIME MULT control to place the intensified $B$ timebase onto the first pulsepair of the North burst. (See Figure 3-22).
8. On the oscilloscope, set the HORIZ DISPLAY switch to the left-hand side B DLY'D BY A position. Measure the average North Brust jitter in microseconds and record the jitter obtained. The average jitter should not exceed $6 \mu \mathrm{sec}$.
9. On the CTR unit, set the REF MKR switch to AUX.

9 Measure the average Auxiliary Burst jitter in microseconds and record the jitter obtained. The average jitter should not exceed $6 \mu \mathrm{sec}$.
10. On the CTR unit, set the REF MKR switch to NORTH and turn the INTENSITY control fully counter-clockwise.
11. Set the oscilloscope controls as follows:
a. HORIZ DISPLAY switch to the righthand side A INTEN BY B position.
b. B TIME/CM to the $5 \mu \mathrm{sec}$ position.
c. B TRIG SOURCE selector to -AC INT.

d. Adjust the DELAY TIME MULT and INTENSITY controls to centre the intensified $B$ timebase about the first pulses of the North Burst. If the B timebase is not visible, adjust the B TRIGGER LEVEL control.
12. Set the oscilloscope HORIZ DISPLAY switch to the right-hand side B DLY'D BY A position and adjust the B TRIGGER LEVEL and INTENSITY controls to obtain a stable display.
13. Use the oscilloscope HORIZ POSITION control, $10 \mu \mathrm{sec}$ and $1 \mu \mathrm{sec}$ markers and (on the CTR unit) the marker INTENSITY and POSITION controls to measure the pulsepair spacing. The spacing should be between 29.7 and $30.3 \mu$ sec. Record the spacing obtained.
14. Set the REF MKR switch to AUX, and in a similar manner, measure the pulse-pair spacing of an Auxiliary Burst. The spacing should be between 23.75 and $24.25 \mu \mathrm{sec}$. Record the spacing obtained. Recalibrate the markers as described in sub-clause 4.
15. Reset the oscilloscope controls to observe a complete Auxiliary Burst. Observe that there are six pulse-pairs and that there is no pulse mis-firing (intermittent base-line under pulse).
16. Set the CHl VARIABLE VOLTS/CM control for an average vertical deflection of 6 cm on the graticule and measure the droop or boost of the Auxiliary burst. Droop of boost should not exceed one minor graticule division (3.2\% of the average burst amplitude).
17. Set the REF MKR switch to NORTH Repeat the procedure described in sub-clauses 15 and 16; observe that the Notth Burst consists of twelve pulse-pairs.
18. If the above specifications are not met, set up as described in Paragraph 6-2h 5 and 6.
d. MEASUREMENT AND ADJUSTMENT OF IDENTITY AND EQUALIZING PULSE SPACING.-- The beacon should operate into the dummy load in order to prevent transmission of continuous identity tone.

1. On the XFER UNIT, Oscilloscope and CTR unit, set the PRIMARY POWER switches to ON. Allow the test equipment five minutes to stabilize.
2. On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
3. On the CTR unit, confirm that the coaxial link is connected between the NON-CAL COUPLER and LIN DET INPUT jacks.
4. On the Beacon:--
a. Set the BATTLE SHORT switch to INTLK SHORTED.
b. Withdraw the Coder Indicator to the fullest extent of its slides and set switch S603 to CONTINUOUS TONE.
5. On the CTR unit, calibrate the markers as follows:-
a. Turn the COUNTER/MARKER SELECT switch to $0.5 \mu \mathrm{sec}$.
b. Set the MARKERS switch to FREE RUN and the MODE switch to FUNCTION TEST.
c. Set the TIME INTERVAL selector to 0.01 SECS; momentarily lift the CTR RESET switch and adjust the 2MC SET control for a Nixie readout of 20000 (disregard the decimal).
d. Set the MARKERS switch to OFF.
6. Turn the FUNCTION switch to REF BURSTS/ANTENNA SPEED and set the REF MKR switch to AUX.

Identity Pulse Spacing
7. Set the oscilloscope controls as follows:-
a. Vertical MODE switch to CH 2 .
b. Vertical TRIGGER switch to NORM.
c. CH2 INPUT selector to SYSTEM TEST DC.
d. CH 2 VOLTS/CM selector to 0.5 and the VARIABLE VOLTS/CM control fully clockwise.
e. HORIZ DISPLAY switch to the right-hand side A INTEN BY B position.
f. A TRIG SOURCE selector to SYSTEM TEST P and the B TRIG SOURCE selector to - DC INT.


Figure 3-23
g. A TIME/CM control to 0.5 mSEC and the B TIME/CM control (pull to unlock) to 0.1 mSEC .
h. DELAY TIME MULT control to $3 \cdot 00$.
j. Adjust the TRIG LEVEL, INTENSITY and HORIZ POSITION controls to obtain a brightened section of the trace and set the DELAY TIME MULT control to observe two brightened pulse-pairs in the centre of the trace.
8. Set the HORIZ DISPLAY switch to B DLY'D BY A (right-hand side) and use the HORIZ POSITION control to place the second pulse-pair of the first group on the centreline. Set the MAG switch to the X10 position.
9. On the CTR unit, set the COUNTER/ MARKER SELECT switch to the $10 \mu$ SEC position and the MARKERS switch to GATED.
10. Adjust the MARKERS POSITION control on the CTR unit and the INTENSITY control on the oscilloscope to place a 100 , sec marker (intensified) on the halfamplitude point of the leading edge of the third pulse of the first pulse group. (See figure 3-23).

11 Using the Oscilloscope HORIZ POSITION and INTENSITY controls, measure the time interval from this point to the identical place in the second pulse group as shown in figure 3-23. The pulse spacing should be between 690 and $790 \mu \mathrm{sec}$ (nominally 740 usec ). Record the spacing obtained. If the spacing is not between 690 and $790 \mu \mathrm{sec}$, set up as described in Paragraph 6-2h 4.

Equalizing Pulse Spacing
12. On the Oscilloscope, set the $B$ TIME/CM control to the $0 \cdot 2 \mu$ SEC position.
13. On the CTR unit, adjust the MARKERS POSITJON control to place a marker on the half-amplitude point of the leading edge of the second pulse of the first pulse group (see figure 3-24).
14. Measure the time interval from this point to the identical place on the fourth pulse of the same group, as shown in figure $3-24$. The pulse spacing should be between 95 and $105 \mu \mathrm{sec}$, nominally $100 \mu \mathrm{sec}$. Record the spacing obtained.
15. If necessary, set the spacing as described in Paragraph 6-2h 4
16. On the beacon:-
a. Set switch S603 to NORMAL KEYING
b. Return the Coder Indicator to the rack and tighten the securing bolts.
c. Set the BATTLE SHORT switch to NOR.
(e) reply delay measurement. -

1. On the XFER UNIT, SA/TG, Oscilloscope and CTR units, set the PRIMARY POWER switches to $0 N$. Allow five minutes for the test equipment to stabilize.
2. On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.


Figure 3-24
3. Confirm that the coaxial links are connected as follows:-
a On the XFER UNIT, between the SA/TG and SEL SW'S jacks.
$b$ On the SA/TG unit, between the ATTEN and XFER UNIT jacks and between the PWR BRIDGE and FUNCTION SW jacks.
c On the CTR unit, between the NON-CAL COUPLER and LIN DET INPUT jacks.
4. On the CTR unit, set the FUNCTION switch to the DELAY/RCVR SENS position and the COUNTER/MARKER SELECI switch to any COUNT position.
5. Set the SA/TG unit controls as foilews:-
a. ATTENUATOR to 100 dB , or higher.
b. PULSE SPACING switch to NON.
c. PRR selector to 1 KC .
d. RF SIG GEN MODE switch to OFF.
e. FREQ SEL selector to ON CHAN.
f. FUNCTION switch to RF SIG GEN.
g. Adjust the ZERO SET control for a

ZFRO SL. 1 reading on the AVERAGE POWER meter.
6. Set the oscilloscope controls as follows:-
a. Vertical MODE switch to CH 2
b. Vertical TRIGGER switch to NORM
c. CH2 INPUT selector to SYSTEM TEST DC.
d CH2 VOLTS/CM selector to $0 \cdot 2$.
e HORIZ DISPLAY switch to the A
position.
f. A TRIG SOURCE selector to SYSTEM TEST P.
g A TRIG MODE selector to AUTO.
h. MAG switch to OFF.
7. Set the oscilloscope TIME/CM AND DELAY TIME controls as follows:-
a. Time base A (outer control) to $10 \mu$

SEC.
b. Time base B (pull to unlock) to $1 \cdot 0 \mu$

SEC.
c. Turn the VARIABLE A and $B$ controls fully cıockwise.
8. Depress the TRACE FINDER button and use the INTENSITY and POSITION controls to centralize the trace.
9. On the SA/TG unit, set the RF SIG GEN MODE selector to CW and adjust the PWR SET control for a red line reading on the AVERAGE POWER meter.

## Note

The SA/TG signal generator is now adjusted to give an output power of $1 \cdot 0 \mathrm{~mW} \mathrm{CW}$.
Issued June 73
10. Set the oscillos cope CH2 vertical POSITION and VARIABLE VOLTS/CM control to establish a $D C$ reference for 1.0 mW CW .
11. On the SA/TG unit, set the RF SIG GEN MODE selector to PULSE and set the AMPL ADJ control to position the peaks of the pulse-pair on the $D C$ reference level established in subcląuse 10.

Note
The SA/TG signal generator is now adjusted to give an output of 1.0 mW pulse power.
12. Adjust the oscilloscope ASTIG and FOCUS controls to obtain the best presentation of the displayed pulses. If necessary repeat sub-clause 11.
13. Set the oscilloscope MODE selector to $A D D E D$ and the CH1 and CH2 INPUT selectors to SYSTEM TEST DC.
14. On the SA/TG unit, set the ATTENUATOR to 30 dB .
15. Observe the displayed waveform and confirm that both the interrogation and reply pulses appear on the same sweep. Adjust the CH2 VOLTS/CM and/or VARIABLE controls to obtain a 6 cm display of interrogation pulse-pairs and adjust the CH1 VOLTS/CM and/or VARIABLE controls for a 6 cm display of reply pulsepairs.
16. On the CTR unit, calibrate the markers as follows:-
a. Set the COUNTER/MARKER SELECT switch to $0.5 \mu \mathrm{SEC}$.
b. Set the MARKERS switch to FREE RUN and the MODE switch to FUNCTION TEST.
c. Set the TIME INTERVAL switch to 0.01 SECS: momentarily lift the CTR RESET switch and adjust the 2 MC SET control for a counter reading of 20000 (disregard the decimal).
d. Set the MARKERS switch to GATED.
17. Adjust the INTENSITY control on the oscillos cope and the MARKERS INTENSITY control on the CTR unit until the markers are clearly observed.

Note
The markers are spaced $0 \cdot 5 \mu$ sec apart, every tenth one being intensified; although the first brightened marker appears after the ninth interval.
18. Set the HORIZ DISPLAY switch to the left-hand B DLY'D BY A position.
19. Adjust the oscillos cope DELAY TIME MULT control to position the second pulse of the interrogation pulse-pair near the centre of the trace.
20. On the CTR unit, set the COUNTER/ MARKER SELECT switch to $1 \cdot 0$ SEC and adjust the MARKERS POSITION control to superimpose a marker on the half-amplitude point of the leading (or trailing) edge of the second interrogation pulse.

3-6a(12) (e)
21. Using the oscillos cope DELAY TIME MULT control, count the markers in the interval to the same point on the reply pulse pair. The time interval should be between 49.8 and 50.2 u sec. Record the reading obtained.
(f) RECEIVER SENSITIVITY MEASUREMENT AND PULSE PAIR DECODER EFFICIENCY.

## Note

On the Amplifier Modulator, ensure that the HV SUPPLY and BEAM CURRENT meters indicate their normal readings.

1. On the XFER UNIT, SA/TG, Oscillos cope and CTR unit, set the PRIMARY POWER switches to ON. Allow five minutes for the test equipment to stabilize.
2. On the XFER UNIT set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
3. Confirm that the coaxial links are connected as follows:-
a. On the XFER UNIT, between the SA/TG and SEL SW'S jacks
b. On the SA/TG unit, between the ATTEN and XFER UNLT jacks and between the PWR BRIDGE and FUNCTION SW jacks.
c. On the CTR unit, between the NONCAL COUPLER and LINE DET INPUT jacks.
Receiver Sensitivity

> 4. On the CTR unit, set the controls as follows:-
a. The FUNCTION switch to DELAY/RECVR SENS .
b. The COUNTER/MARKER SELECT swi.tch to any counts position.
c The TIME INTERVAL selector to 1.0 SEC.
d. The MODE switch to REPLY RATE
5. Set the SA/TG unit controls as follows:-
a. The PRR selector to 1 KC .
b. The PULSE SPACING selectar to NOM $(12 \mu \mathrm{sec}$.
c. The RF SIG GEN MODE switch to OFF.
d. The FREQ SEL selector to ON CHAN.
e. The ATTENUATOR to 100 dB , or higher.
f. The FUNCTION switch to RF SIG GEN.
g. Adjust the ZERO SET control for ZERO SET reading on the AVERAGE POWER meter.
6. Set the oscilloscope controls as follows:-
a. The vertical MODE switch to CH2.
b. The vertical TRIGGER switch to
c. The CH2 INPUT selector to SYSTEM TEST DC.
d. The CH2 VOLIS/CM selector to 0.2 .
e. The HORIZ DISPLAY switch to the A position.
f. The A TRIG SOURCE selector to SYSTEM TEST P.
g. The A TRIG MODE selector to AUTO.
h. The MAG switch to OFF.
j. The A time base TIME/CM AND DELAY TIME control (outer knob) to the 21 SEC positiqn
k. Turn the VARIABLE VOLTS/CM $A$ and $B$ controls fully clockwise.

1. Depress the TRACE FINDER button and use the POSITION and INTENSITY controls to centre the trace.
2. On the SA/TG unit, set the RF SIf GEN MODE switch to CW and adjust the PWR SET rontrol for a POWER SET (red line) reading on the AVERAGE POWER meter.

## Note

The SA/TG unit signal generator is now adjusted to give an output power of 1.0 mW CW .
8. Adjust the oscillos cope CH2 vertical POSITION and VARIABLE VOLTS/CM controls ro obtain a 5 cm deflection when switching the CH2 INPi'T selector from GND to SYSTEM TEST DC. This establishes a $D C$ reference level for 1.0 mW .
9. On the SA/TG mit:
a. Set the RF SIG GEN MODE switch to PULSE and set the AMPL ADJ control to position the peaks of the pulse-pair on the DC reference level established in sub-clause 8 .

## Note

The SA/TG signal generator is now adjusted to give an output of 1.0 mW pulse power.
b. Set the ATTENUATOR to 30 dB .
10. On the oscilloscope, set the CH2 INPIJT selector to SYSTEM TEST AC. Adjust the ASTIG and FOCUS controls to obtain the best present ${ }^{-}$ tion of the displayed pulses. If necessary repeat sub-clause 9 .
11. On the CTR unit, depress the COUNTER INPUT READ switch and adiust the COARSE and FINE controls for a reading within the green zone of the PEAK RF POWER meter.

## Note

The CTR unit is counting the synchronous replies to the SA/TG signal generator, which is set to 1000 interrogations per second. Due to normal beacon action, it is not possible to obtain 1000 replies per second.
12. Set the DISPLAY TIME control for a minimum time of display and observe that the counter readout is approximately 700 to 800 synchronous replies per second.
13. Increase the SA/TG ATTENUATOR reading until the average counter readout is 600 . Note the ATTENUATOR reading and add this to the system losses, to obtain the beacon receiver sensitivity, which should be between -91 and -97 dBm . Record the reading obtained.

Notes

1. A typical set of system losses is shown below, together with the resultant receiver sensitivity:
a. SA/TG ATTENUATOR reading
( 61.8 to 67.8 dB )
$64 \cdot 8 \mathrm{~dB}$ Typical
b. TMC RACK - Switch, cable and connector losses. ( $2 \cdot 3$ to 3.7 dB ) 3.0 dB Typical
c. XFER UNIT - Precision directional coupler. ( 22.5 to 23.5 dB )
23.0 dB Typical
d. BEACON

Preselector Loss. ( 1.0 to 3.0 dB )

$$
1.5 \mathrm{~dB} \text { Typical }
$$

e. Receiver, Duplexer transmission line, cable and connector losses. ( $1 \cdot 0$ to 2.0 dB ) 1.7 dB Typical
f. Total dB below 1 mW at Receiver input
g. Receiver sensitivity
$94 \cdot 0 \mathrm{~dB}$
$-94 \cdot 0 \mathrm{dBm}$
2. The beacon RF losses may be found by comparing the ATTENUATOR reading obtained in subclause 13 with that obtained in Paragraph 3-6a (i2) (g) (14) a; subtract the CALIBRATED CABLE loss from the reading obtained in this paragraph and the difference between the two readings is now equal to the beacon $R F$ loss, including the 10 dB coupler at the receiver input.
Receiver Decoder Test

## Note

The receiver sensitivity for a pulse spacing of $12 \mu \mathrm{sec}$ must be obtained before performing this test.
14. On the CTR unit, calibrate the markers as follows:
a. Turn the COUNTER/MARKER SELECT switch to $0 \cdot 5 \cdot \mathrm{sec}$.
b. Set the MARKERS switch to FREE RUN and the MODE switch to FUNCTION TEST.
c. Set the TIME INTERVAL switch to $0.01 \mu$ SEC. Momentarily lift the CTR RESET button and adjust the 2 MC SET control for a readout of $20000 \pm 1$ on the Nixie display (dis regard the decimal).
d. Set the MARKERS switch to GATED, taking care not to disturb the 2MC SET control.
15. On the CTR unit, use the markers POSITION and INTENSITY controls to observe the $0.5 \mu \mathrm{sec}$ markers on the oscilloscope. Note that every tenth marker is intensified.
16. Measure the spacing between the half-amplitude points of the leading edges of the pulses. The pulse spacing should be 11.75 to 12.25 sec . Record the spacing obtained.
17. On theSA/TG unit, set the PULSE SPACING switch to VAR and use the variable PULSE SPACING control to adjust the pulse spacing at the half-amplitude points to $12 \cdot 5 \mu \mathrm{sec}$.
18. Measure the receiver sensitivity as detailed in sub-clauses 1 to 13 inclusive. The receiver sensitivity should not decrease by more than 3 dB from the value obtained in 13. Record the receiver sensitivity in - dBm .
19. Using the variable PULSE SPACING control, set the pulse spacing to $11 \cdot 5 \mu \mathrm{sec}$ at the half-amplitude points and repeat sub-clause 18.
20. Using the variable PULSE SPACING control, set the pulse spacing to $1500 \mu \mathrm{sec}$ at the half-amplitude points. Measure the receiver sensitivity as described in sub-clauses 1 to 13 inclusive and record the reading obtanned, in -dBm . The receiver sensitivity should be reduced by at least 50 dB from the value obtained in sub-clause 13.
21. Using the variable PULSE SPACING control, set the pulse spacing to $9 \sim \mathrm{sec}$ and repeat sub-clause 20 .
(g) RECEIVER SELECTIVITY MEASUREMENT. -

1. On the SA/TG, Xfer Unit, Oscilloscope and CTR unit, set the PRIMARY POWER switches to ON .
2. On the XFER UNIT set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
3. Confirm that the coaxial links are connected as follows:-
a. On the SA/TG unit, between the PWR BRIDGE and FLNCTION SW jacks.
b. On the CTR unit, between the NONCAL COUPLER and LIN DET INPUT jacks.
4. On the SA/TG unit:
a. Remove the link from between the ATTEN and XFER UNIT jacks
b. Connect the CALIbrated TEST CABLE between the ATTEN jack and the 10 dB COUPLER jack on the beacon receiver front panel.
5. Set the controls on the CTR as follows:-
a. FUNCTION switch to DELAY/RCVR SENS.
b. COUNTER/MARKER SELECT switch to any COUNT position.
c. TIME INTERVAL selector to $1 \cdot 0$ SECS.
d. MODE switch to REPLY RATE.
6. On the SA/TG unit set the controls as follows:-
a. PRR selector to 1 KC .
b. PULSE SPACING selector to NOM (12, sec).
c. RF SIG GEN MODE switch to OFF.
d. FREQ SEL selector to ON CHAN.
e. ATTENUATOR to 100 dB , or higher.'
f. FUNCTION switch to RF SIG GEN.
g. Adjust the ZERO SET control for a

ZERO SEI reading on the AVERAGE POWER meter.
7. Set the Oscillos cope controls as follows:-
a. Vertical MODE switch to CH2.
b. Vertical TRIGGER switch to NORM.
c. CH2 INPUT selector to SYSTEM TEST DC.
d. CH 2 VOLTS/CM selector to $0 \cdot 2$.
e. HORIZ DISPLAY switch to the A position.
f. A TRIG SOURCE selector to SYSTEM

TEST P.
g. A TRIG MODE selector to AUTO.
h. A time base TIME/CM AND DELAY TIME control (outer knob) to the $\mathrm{S}_{\mu} \mathrm{sec}$ position.
j. Depress the TRACE FINDER button and adjust the INTENSITY and POSITION controls to centre the trace.
8. On the SA/TG unit, set the RF SIG GEN MODE switch to CW and adjust the PWR SET control for a POWER SET (red line) reading on the AVERAGE POWER meter.

## Note

The SA/TG signal generator is now adjusted to give an output power of 1.0 mW CW .
9. Adjust the oscilloscope CH2 vertical POSITION and VARIABLE VOLTS/CM controls to obtain a 5 cm deflection when switching the CH2 INPUT selector from GND to SYSTEM TEST DC. This establishes $\dot{a}$ DC reference level for $1^{\circ} \mathrm{O} \mathrm{mW} \mathrm{CW}$.
10. On the \&A/TG unit, set the RF SIG GEN MODE switch to PULSE and set the AMPL ADJ control to position the peaks of the pulsepair on the DC reference level established in sub-clause 9 .

## Note

The SA/TG signal generator is now adjusted to give an output of 1.0 mW pulse power.
11. Adjust the oscilloscope ASTIG and FOCUS controls to obtain the best presentation of the displayed pulses. If necessary repeat sub-clause 10 .
12. Set the SA/TG ATTENUATOR to approximately 30 dB . On the CTR unit, depress the

COUNTER INPUT READ switch and adjust the COARSE and FINE controls for a reading within the green zone of the PEAK RF POWER meter.

Note
The CTR unit is counting the synchronous replies to the SA/TG signal generator, which is set to 1000 interrogations per second, Due to normal beacon action, it is not possibie to obtain 1000 replies per second.
13. Set the DISPLAY TIME control for a minimum time of display and observe that the counter readout is approximately 700 to 800 synchronous replies per second.
14. Increase the SA/TG ATTENUATOR reading until the average counter readout is 600 . Note the ATTENUATOR reading and add this to the system losses to obtain the beacon receiver sensitivity as measured at the 10 dB COUPLER jack. Calculate the receiver sensitivity in - dBm as follows:-
a. SA/TG ATTENUATOR READING ( 80 to

b. CALIBRATED CABLE LOSS ( 0.5 to 1.5 dB ) 1.0 dB Typica?
c. PRECISION DIRECTIONAL COUPLER

$$
(9.5 \text { to } 10.5 \mathrm{~dB}) \quad 10.0 \mathrm{~dB} \text { Typical }
$$

d. TOTAL dB BELOW

1 mW at receiver input
$94 \cdot 0 \mathrm{~dB}$
e. Receiver sensitivity $-94 \cdot 0 \mathrm{dBm}$

Note the receiver sensitivity, which should be between -91 and -97 dBm .
15. On the SA/TG unit, set the FREQ SEL switch to +200 KC .
16. Adjust the ATTENUATOR to obtain an average counter readout equal to that obtained in sub-clause (14); the ATTENUATOR reading should not deviate by more than 3 dB from the reading obtained in that sub-clause. Record the deviation.
17. Set the FREQ SEL switch to -200 KC and repeat sub-clause (16).
18. Set the FREQ SEL switch to -900 KC .
19. Decrease the ATTENUATOR until the counter readout is equal to that obtained in sub-clause (14); the ATTENUATOR reading should decrease by at least 80 dB from the reading obtained in that sub-clause.
20. Return the ATTENUATOR to the reading obtained in 14 set the FREQ SEL switch to ON CHAN and confirm the counter readout obtained in 14.
21. Set the FREQ SEL switch to +900 and repeat 19 and 20.
22. Disconnect the CALIBRATED CABLE: reconnect the co-axial link between the ATTEN and XFER UNIT jacks.

## (h) ANTENNA SPEED MEASUREMENT

1. On the CTR unit, set the controls as follows:-
a. PRIMARY POWER switch to ON.
b. FUNCTION switch to REF BURSTS/ANTENNA SPEED.
c. MODE switch to GEN TEST +
d. COUNTER/MARKER SELECT switch to INTV.
e. MARKERS switch to GATED.
f. REF MKR switch to NORTH.

Allow five minutes for the test equipment to stabilize.
2. Depress the COUNTER INPUT READ switch and adjust the COARSE and FINE controls for a reading within the green zone of the PEAK RF POWER meter. Use the lowest setting of the COARSE control that allows adjustment of the FINE control for a green zone reading.
3. Momentarily lift the CTR RESET switch. Observe the counter readout, which should be $6660 \pm 134$. This indicates an antenna speed of between 882 and 918 rpm .
4. Set the REF MKR switch to AUX and repeat 2 Momentarily lift the CTR RESET switch. The counter readout should be $7407 \pm 15$. Occasionally the readout will be 14815 $\pm 30$.

## (j) RADIATED ANTENNA PATTERN ACCURACY.

1. Confirm that:
a. A TACAN beacon is on and operating into the antenna.
b. Monitors A6 and A7 are both on and serviceable.
2. On the Oscilloscope and the CTR unit, set the PRIMARY POWER switches to ON. Allow five minutes for the test equipment to stabilize.
3. On the CTR unit, set the FUNCTION switch to ANT PATTERN MON AG RCVR.
4. On the Oscilloscope set the controls as follows:-
a. Vertical MODE switch to CH .
b. Vertical TRIGGER switch to NORM.
c. CHI VOLTS/CM selector to 0.5 .
d. CHI INPUT selector to SYSTEM TEST AC.
e. HORIZ DISPLAY switch to the A position.
f. A TIME/CM AND DELAY TIME selector to 10 m SECS.
g. A TRIG SOURCE selector to SYSTEM TEST $P$ and the TRIGGER MODE switch to AUTO.
h. Adjust the remaining controls for the best antenna pattern presentation.
5. Use the Oscilloscope time base controls and the REF MKR switch on the CTR unit to analyze the antenna pattern. Pay particular attention to the following points:-
a. 15 Hz and 135 Hz modulation.
b. Phase relationships of the North and Auxiliary Bursts, relative to the 15 and 135 Hz amplitude modulation.
c. Examine the squitter texture and ensure that there is no abnormal pulse bunching.
d. Carefully compare the antenna pattern with the pattern obtained on initial installation, or with the pattern obtained on replacement of the TACAN antenna.
6. On the CTR unit, set the FUNCTION switch to the ANT PATTERN MON A7 RCVR position and repeat 5 .

Note
The following illustrations show some of the correct and incorrect patterns which may be obtained.

WAVEFORMS CORRECT IN PHASE

Figure 3-25


$$
\begin{aligned}
& \mathrm{A}=\mathrm{E} \quad: \quad \mathrm{B}=\mathrm{D} \\
& \text { CORRECT PATTERN } \\
& \text { WAVEFORMS IN PHASE }
\end{aligned}
$$

Figure 3-26


$$
\mathrm{A}=\mathrm{E} \quad: \quad \mathrm{B}=\mathrm{D}
$$

incorrect pattern $20^{\circ}$ PHASE SHIFT
$\mathrm{A}=\mathrm{E}$
$B=D$

WAVEFORMS INCORRECT
$20^{\circ}$ PHASE SHIFT

Figure 3-28
(k) BLANKING TIME ADJUSTMENT.-Allow at least 10 minutes for the beacon receiver to warm up.

1. Connect the TEST OUTPUT jack on the front pancl of the receiver to the Oscilloscope A time base TRIG IN jack.
2. Locate TP9 on the right-hand side of the receiver video chassis and connect a lead from TP9 to the Oscilloscope CHI INPUT jack. Set up the oscilloscope to observe the blanking pulse as shown in figure 6-9a of Section 6.
3. Calibrate the markers and use them to measure the pulse width at the ha!f-amplitude point.
4. Adjust R443, BLANKING TIME ADJUST, on the video chassis to obtain a pulse width of exactly $40 \mu \mathrm{sec}$.
(1) OUTPUT FREQUENCY SPECTRUM.--Ensure that the meter readings of the Amplifier Modulator HV SUPPLY and BEAM CURRENT meters are normal.
5. On the XFER UNIT and SA/TG unit, set the PRIMARY POWER switches to ON. Allow five minutes for the test equipment to stabilize.
6. Ensure that the coaxial links are connected as follows:-
a. On the XFER UNIT, between the SA/TG and SEL SW'S jacks.
b. On the SA/TG unit, between the ATTEN and XFER UNIT jacks and between the PWR BRIDGE and FUNC. TION SW jacks.
7. On the XFER UNIT, set the XPONDER SEL switch to PRIM or STBY. This selects the beacon to be tested.
8. On the $\mathrm{SA} / \mathrm{TG}$, set the controls as follows:-
a. ATTENUATOR to 100 dB .
b. BAND SHIFT selector to 0 .
c. FREQ SEL switch to SA.
d. FUNCTION switch to PWR MTR ZERO SET.
e. Adjust the ZERO SET control for a

ZERO SET reading on the AVERAGE. POWER meter.
f. FUNCTION switch to SA.
g. Adjust the NOISE SET control for a NOISE SET reading on the AVERAGE POWER meter.
5. Set the ATTENUATOR to obtain a red line reading on the meter. Record the ATTENUATOR setting.
6. Set the BAND SHIFT selector to +0.8 MC.
7. Reduce the ATTENUATOR setting to obtain a red line reading on the meter. Record the ATTENUATOR setting; this should be at least 50 $d B$ less than the setting obtained in (5).

## CAUTION

The ATTENUATOR must be set to 100 dB , or higher, before turning the BAND SHIFT selector switch through the 0 position or meter may be damaged.

8, Set the ATTENUATOR to 1.00 dB , or higher, and turn the BAND SHIFT selector to -0.8 MC . Repeat the procedure outlined in (7).
9. Repeat the procedures outlined in (7) and 8, for BAND SHIFT selector settings of $-2 \cdot 0 \mathrm{MC}$ and $+2 \cdot 0 \mathrm{MC}$. The ATTENUATOR settings obtained should be reduced by at least 60 dB from those obtained in (5).

## Note

If the ATTENUATOR settings do not fall within the required specifications, tune the Amplifier Modulator and Control Duplexer as detailed in Paragraph 6-2h.
(m) BEaCON PEAK POWER MEASUREMENT. -

1. Ensure that the coaxial links are connected as follows:-
a. On the XFER UNIT, between the SA/TG and SEL SW'S jacks.
b. On the SA/TG unit, between the ATTEN and XFER UNIT jacks and between the PWR BRIDGE and FUNCTION SW jacks.
2. On the XFER UNIT, CTR and SA/TG units, set the PRIMARY POWER switches to ON.

## Note

Allow thirty minutes for the peak power diode oven in the CIR unit to stabilize.
3. On the XFER UNIT, set the XPONDER SEL switch to the beacon under test.
4. On the SA/TG unit, turn the FUNCTION switch to the PWR MTR ZERO SET position. Depress the ZERO SET switch on the CTR and adjust the SET ZERO control for zero reading on the PEAK RF POWER meter
5. On the SA/TG, set the FUNCTION switch to the RF PEAK POWER position.
6. On the SA/TG, set the ATTENUATOR to the reading established for the desired range of power. Approximate settings are:-
a, 13 dB for the 200 W to 2 kW range
b. 23 dB for the 2 kW to 20 kW range.
7. On the CTR, read the peak power on the PEAK RF POWER meter. Multiply this reading by 10,000 if in the 2 kW to 20 kW range, or by 1000 if in the 200 W to 2 kW range. Record the reading obtained.
(n) BEACON RF AVERAGE POWER OETPUT.-

1. On the XFER UNIT, SA/TG and CTR units set the PRIMARY POWER switches, to ON. Allow half an hour for the test equipment to stabilize.
2. On the Amplifier Modulator, ensure that the HV SUPPLY and BEAM CURRENT meters indicate their normal readings.
3. Confirm that the coaxial links are connected as follows:-
a. On the XFER UNIT, between the SA/TG and SEL SW'S jacks.
b. On the SA/TG unit, between the ATTEN and XFER UNIT jacks and between the PWR BRIDGE and FUNCTION SW jacks.
4. On the XFER UNIT, set the XPONDER SEL switch to PPIM or STBY. This selects the beacon to be tested.
5. On the SA/TG:-
a. Set the FUNCTION switch to the PWR

METER ZERO SET position and adjust the ZERO SET control for a zero reading on the AVERAGE POWER meter.
b. Set the FUNCTION switch to the RF AVERAGE PWR position and adjust the attenuator for a red line reading on the meter. Note the ATTENUATOR reading.
6. Add the ATTENUATOR reading to the system losses to obtain the beacon average power in dB . A typical set of readings is given below:-
a. Attenuator Reading: 19 dB
b. Attenuation inser- 5 dB (not greater tion loss: than 6 dB )
c. TMC switch, cable and connector loss: 3 dB
d. XFER UNIT, direc-
tional coupler loss: 23 dB
e. Total average beacon power: $\quad+50 \mathrm{dBm}$
f. Total average power in watts: 100 Watts.
(o) FREQUENCY MULTIPLIER OSCILLATOR - RF aVERaGE POWER OUTPUT.

## Note <br> a. It is assumed that the transmitter circuits are correctly aligned.

b. Verify that the beacon total pulse count is within the specification in Paragraph 3-6a (12) (a)

1. On the SA/TG unit:-
a. Set the PRIMARY POWER switch to ON.
b. Remove the coaxial link from between the ATTEN and XFER UNIT jacks.
c. Confirm that the coaxial link is connected between the PWR BRIDGE and FUNCTION SW jacks.
2. Turn the FUNCTION switch to the PWR MTR ZERO SET position and adjust the ZERO SET control for zero reading on the AVERAGE POWER meter.
3. Set the ATTENUATOR to 100 dB , or higher.
4. On the beacon to be tested:
a. Set the BATTLE SHORT switch to INTLK SHORTED.
b. Release the bolts securing the Frequency Multiplier Oscillator (FMO) and draw the unit fully forward.

## WARN ING

The FMO employs high voltages. Exercise caution when proceeding with 5 .
5. Remove the lead, complete with crystal detector, from the $B$ socket of the directional coupler DC 1401 on the left-hand side of the FMO chassis. Connect the CALIBRATED TEST CABLE between the B socket of DC 1401 and the ATTEN socket on the SA/TG.
6. On the High Voltage Power Supply, set the HV ON/OFF switch to OFF.
'7. Observing the AVERAGE POWER meter, reduce the ATTENUATOR setting to obtain a red line reading on the meter. Note the ATTENUATOR reading.
8. Set the HV ON/OFF switch to ON.
9. Determine the FMO average power output as follows:-
a. ATTENUATOR reading: 8 dB Typical
b. CALIBRATED CABLE loss: 1.2 dB Typical
c. DC 1401 loss: 25 dB
d. Total loss: $34 \cdot 2 \mathrm{~dB}$ Typical
e. RF average power: 2.6 watts Typical
10. a. Disconnect the CALIBRATED CABLE and reconnect the crystal detector to the $B$ socket of directional coupler DC 1401.
b. Return the FMO to the rack and tighten the securing bolts: Set the BATTLE SHORT switch to NOR.
c. On the SA/TG unit, reconnect the coaxial link between the ATTEN and XFER UNIT jacks. Set the PRIMARY POWER switch to OFF.
b. ROUTINE CHECKS. - A general routine pre-ventive-maintenance chart is shown in table 3-3. This table lists mantenance within scope of operatur. Reference should be made to the Maintenance Standards Book. NAVSHIPS 93881.42. for a detailed list of routine checks within scope of operator.

For installations where the Test Monitor Control Rack 212A is incorporated, Paragraph 3-6a (12) should be consulted where specific tests are called for in TABLE 3-3.

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART (cont)

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| DAILY CHECKS (cont) |  |  |
| POWER DISTRIBUTION AND CONTROL (cont) |  |  |
| Control-duplexer front panel | Inspect blue MAIN POWER ON lamp DS1 102. | If lamp is not on, check for blown fuse. If blown fuse is not found, refer to trouble-shooting procedure in Section 5. |
|  | Inspect white FIL ON and ANTENNA CONTROL ON lamps DS1101 and DS1103, respectively. | Both lamps should be on. If not, check to see that switches are on; if they are, de-energize equipment and refer to troubleshooting procedue in Section 5. |
| Regulated filament transformer voltage | Read SUPPLY VOLTS meter M1 101 on front panel of controlduplexer. | Meter should read exactly 120 volts. If not, open control-duplexer unit, manually close interlock, loosen lock on the ADJUST FOR 120 V knob, and adjust knob until voltage is correct; then tighten lock. |
|  | Set LINE-REG FIL BUS switch to LINE | If line voltage is not $120 \mathrm{~V} \pm 10$ percent, check external power source. |
| RADIO RECEIVER R-824/URN |  |  |
| Panel lamps | Check white POWER ON lamp DS501 | If light is not on, check receiver, switch on radio receiver panel; if switch is set to ON, refer to troubleshooting procedure in Section 5. |
| Voltages | Set METER SELECTOR switch to $\mathrm{B}+, 200 \mathrm{VFS}$. | Correct voltage is $+150 \pm 5$ volts. Full-scale deflection is equivalent to $\pm 200$ volts; therefore, TEST METER should read $75 \pm 2.5$ divisions on calibrated scale. If reading is incorrect, refer to troubleshooting procedure Section 5. |
|  | Set METER SELECTOR switch to C-200 VFS | Correct voltage is $-105 \pm 2.5$. The TEST METER should read 52.5 $\pm 2.5$. If the reading is incorrect, refer to troubleshooting procedures in Section 5. |
|  | After ten minutes warmup, set METER SELECTOR switch to SQUITTER CONTROL -10VFS. | Correct voltage is $-5 \pm 1.0$ volts (rapid 0.1 -volt fluctuation is normal). Fullscale deflection is equivalent to -10 volts; therefore, TEST METER should read $50 \pm 10$ divisions on calibrated scale; if not, refer to troubleshooting procedures in Section 5. |

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART (cont)

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| DAILY CHECKS (cont) |  |  |
| CODER-INDICATOR KY-382/GRN-9D |  |  |
| Power | Inspect white POWER ON Jamp DS601. <br> Check amber ANTENNA CONTROL lamp DS602; it should burn steadily. | If lamp is not on, check CODERINDICATOR switch on coderindicator panel; if switch is ON , refer to troubleshooting procedure in Section 5. <br> Blinking of lamp indicates trouble in antenna control unit or antenna. Refer to troubleshooting procedure in Section 5. |
| Speed, indicator reading | Check to see that speed error reading is not in red portion of ANTENNA SPEED ERROR meter scale. | Trouble is indicated by steady reading in red portion of meter scale. Refer to troubleshooting procedures in Section 5 for corrective measures. <br> Note <br> A temporary reading in red portion of scale while servo system is correcting is normal. |
| Identification keyer | Check to see that keyer motor and code wheel are rotating and that keyer switch is operating smoothly. | If operation is faulty, refer to Section 5 for troubleshooting and replacement procedures. |
| POWER SUPPLIES |  |  |
| Panel lamps | Inspect LV-MV READY and HV READY lamps on low and high voltage power supplies, respectively. | LV-MV READY lamp DS1601 should go on after 1 minute of operation. HV READY lamp DS1902 should go on after 5 minutes of operation. If lamps are not on after proper time interval, refer to troubleshooting procedure in Section 5. |
|  | Inspect LV lamp DS1 603 and -375V lamp DS1 601 on low voltage power supply panel, +700 V +1000 V lamp DS 1801 on medium voltage power supply panel, and HV lamp DS1901 on high voltage supply panel. | The LV, -375 V , and +700 V +1000 V lamps should go on after 1 minute of operation, and the HV lamp should go on after 5 minutes of operation. If the lamps are not on after proper time interval, refer to troubleshooting procedures in Section 5. |
|  | Inspect amber MV OVERLOAD lamp DSI 803 on low voltage power supply panel, and HV OVERLOAD lamp DS 1903 on high voltage power supply panel. | If one or both of these lamps are on, refer to troubleshooting procedures in Section 5. |

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART (cont)

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| DAILY CHECKS (cont) |  |  |
| CODER-INDICATOR KY-382/GRN-9D (cont) |  |  |
| Output voltages | Set meter selector switch under DC SUPPLY VOLTAGE meter on frequency multiplieroscillator to each indicated voltage. | If meter does not read within 2 percent of what meter selector switch indicates it should read, refer to troubleshooting procedures in Section 5. |
| TRANSMITTER |  |  |
| Frequency muitiplieroscillator lamps | Check white CRYSTAL OVEN HEATERS lamps. | Whenever EMERGENCY SWITCH S901 is at ON, OVEN lamp DS1403 should be on. <br> NORMAL lamp DS1402 will go on when EMERGENCY SWITCH S901 is first turned to ON. After crystal oven reaches operating temperature. NORMAL lamp will switch off and on as oven heater goes off and on to maintain proper oven te mperature. |
| Frequency multiplieroscillator tuning meter | Read TUNING METER M1401 on frequency multiplieroscillator front panel in each position of switch S1401. | Note any variation from values given in $\log$ showing daily readings of all switch positions on this meter. If any readings indicate variation irom readings of more than 5 percent. refer to troubleshooting procedures in Section 5. |
| Amplifier-modulator lamps | Check that white FIL lamp DS1301 is on. | FIL lamp should come on as soon as amber aurflow switch lamp goes out. |
| Klystron beam current | Read BEAM CURRENT meter M1301 on amplifier-modulator front panel. | Bearn current should be be tween 80 and 100 ma . |
| High-voltage power supply | Read HV SUPPLY meter on amplifier-modulator front panel. | High voltage should be approximately 12.000 volts $\pm 1000$ volts. If reading is incorrect. refer to troubleshooting procedures in Section 5. |
| WEEKLY CHECKS |  |  |
| RADIO RECEIVER R-824/URN |  |  |
| Squitter count | Check squitter rate once a week or after replacing any tube or repairing receiver. Refer to paragraph 3-6a(6). | $2700 \pm 90$ pulses per second. |

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART (cont)

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| WEEKLY CHECKS (cont) |  |  |
| RADIO RECEIVER R-824/URN (cont) |  |  |
| Receiver sensitivity | Check the receiver sensitivity once a week or after replacing any tube or repairing receiver. Refer to paragraph 3-6a(7). | -53 dbm signal level for $60-$ percent reply to a properly coded interrogation signal. |
| CODER-INDICATOR KY-382/GRN-9D |  |  |
| Output pulse count | Refer to paragraph 3-6a(4) for method of checking output pulse count. | Output pulse count should be $7200 \pm 180$ pulses per second. If pulse count is incorrect, refer to troubleshooting procedures in Section 5. |
| North reference burst pulse count and auxiliary reference burst pulse count | Refer to paragraph 3-6a(10) for method of checking reference bursts. | North reference burst should consist of $12 \pm 1$ pulse pairs. Auxiliary reference burst should consist of $6 \pm 1$ pulse pairs. |
| Identification code keyer | Connect a set of headphones to TEST OUTPUT jack on coderindicator front panel and listen to identification code. | Identification code should be transmitted every 37-1/2 seconds. |
| FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D |  |  |
| Zero distance time | Refer to paragraph 3-6a(11). | Refer to paragraph 3-6a(11). |
| AMPLIFIER-MODULATOR AM-1701/URN |  |  |
| Output pulse shape | Refer to paragraph 3-6a(3). | See figure 3-18. |
| Peak power output | Refer to paragraph 3-6(ㅢ) 2 . | Peak power output should be at least 7.5 kw . |
| MONTHLY CHECKS |  |  |
| Klystron output incident signal | Using Oscilloscope OS-54/URN3, observe signal at KLYSTRON OUTPUT INCIDENT jack on control-duplexer front panel. | Compare amplitude of signal with previously logged readings (figure 3-18). |
| Klystron output reflected signal | Using oscilloscope, observe signal present at KLYSTRON OUTPUT REFLECTED jack. | Compare amplitude of signal with previously logged readings. |
| Antenna incident signal | Using oscilloscope, observe signal at ANTENNA INCIDENT jack on control-duplexer front panel. | Compare amplitude of signal with previously logged readings (figure 3-18). |

TABLE 3-3. ROUTINE MAINTENANCE CHECK CHART (cont)

| WHAT TO CHECK | HOW TO CHECK | INDICATIONS AND CORRECTIVE ACTION |
| :---: | :---: | :---: |
| MONTHLY CHECKS (cont) |  |  |
| ELECTRICAL EQUIPMENT CABINETS |  |  |
| Cabinet blower air filters 0901, 0902 , and 01001 | Open blower compartments at bottom of receiver transmitter cabinet and power supply cabinet and check blower filter (figures 3-6 and 3-10). | Clean filter if dirty in accordance with paragraph $3-6 \mathbf{b}(1)(b)$ |
| SEMIANNUAL CHECKS |  |  |
| CODER-INDICATOR KY-382/GRN-9D |  |  |
| Identification keyer | Check that keyer motor and code wheel are rotating and that keyer switches are operating smoothly. Lubricate according to paragraph 3-6b(3). | If contacts are worn, replace switches S604 and S607. |

(1) CLEANING.

## WARNING

Be sure to de-encrgize the equipment before proceeding with the steps outlined in the following paragraphs. Set the master power switch and the auxiliary power switch to OFF, and tag these switches to warn other personnel against turning them on while work is being performed on the equipment.
(a) GENERAL.--In addition to specific cleaning and inspection procedures outlined in foregoing paragraphs, service personnel are directed to inspect and clean all units listed in tables $1-1$ and 1-2 at least twice yearly. General cleaning instructions are as follows:

Step 1. Using a vacuuin cleaner or air hose (compressed air), remove all dirt and dust from the interior of each of the compartments. Excess dirt may be removed with a clean, dry cloth.

Step 2. Using drycleaning solvent 140-F (SNSN 51-S-471810 for 5 -gallon drum) clean ceramic or glass surfaces, and highvoltage insulators. This solvent may also be used to clean or wash grease or oil from the transmitter-receiver and antenna components.

Step 3. With a clean, lint-free rag, remove all dust and dirt from the ventilating louvers of the cabinet enclosure.

## WARNING

Dry-cleaning solvent is flammable and should not be used near an open flame. A fire extinguisher should
be provided when cleaning solvents are used. Solvents evaporate rapidly and have a drying and cracking effect on the skin; occasionally they cause a nilk irritation or inflammation. Use solvents only in well-ventilated places. The use of gasoline or benzene for cleaning is prohibited.

## (b) CLEANING BLOWER FILTERS IN ELECTRICALEQUIPMENT CABINETS.

Step 1. Shut off equipment and remove front panel blower compartment.

Step 2. Remove blower filter retaining screw (long threaded rod with wing head) holding filter in place (figures 3-6 and 3-10).

Step 3. Remove cylindrical filter. Clean filter with vacuum cleaner and wash with dishwashing compound SNSN-G-51-C-1576-100 in solution of water.

Step 4. Shake out excess water and let filter dry.

## CAUTION

Do not oil filters
Step 5. Replace filter in cabinet.
(2) INSPECTION.-Each item must be externally inspected to see whether it is in good condition or
damaged beyond safe or serviceable limits. Inspect as follows:
Step 1. Inspect all lug and screw connections for tightness. Check that cables and leads are properly dressed to prevent short circuits or strains on wires and lugs.

Step 2. Inspect resistors, capacitors, coils and transformers for evidence of overheating. Carbonized or discolored surfaces as well as loss of potting compound are indications of overheating.

Step 3. Inspect front panel knobs and switches for looseness.

Step 4. Inspect vacuum tubes, making certain that all tubes are properly seated in their sockets.

Step 5. Inspect for rust and corrosion on metal surfaces. If rust or corrosion is detected, sand the area with emery cloth and touch up with varnish or paint. Do not use paint or varnish on or near switches or tube socket connections.
(3) LUBRICATION.-Lubrication of the identificationkeyer assembly installed in the coder-indicator is required every 6 months. To lubricate the identification-keyer assembly, proceed as follows:

## Note

Shut off the equipment if it is not needed to provide bearing and distance information.
Step 1. Loosen the four captive screws on panel of coderindicator unit and pull out unit. The identification-keyer assembly is mounted on right side of unit.

Step 2. Fill gear box with grease, Military Specification MIL-G-3278. Using a grease gun, feed grease through grease fittings shown in figure 3-21. Fill oil cup with oil, Military Specification MIL-L-6085.

Step 3. Slide coder-indicator unit back into recessed position and tighten the four captive screws.

## c. EMERGENCY MAINTENANCE.

## Note

Operators shall not perform any of the following emergency maintenance procedures without proper authorization.
(1) FUSE FAILURE.-All fuses used in the radio beacon are held in fuseholders that have neon lamps in their caps that go on when the fuse is blown. When any apparent improper functioning of the radio beacon occurs, the indicating fuses should be checked before proceeding with other tests. For fuse locations, refer to table 3-4.


Figure 3-21. Coder-Indicator Identification Keyer, Lubrication Points

## CAUTION

Never replace a fuse with one of higher rating unless continued operation of the equipment is more important than probable damage. Use spare fuses located adjacent to the faulty fuse. If a fuse burns out immediately after replacement, do not replace it a second time until the cause of burnout has been corrected.
(2) TUBE FAILURE.- To replace defective electron tubes, loosen the captive screws holding the particular units in the cabinet and slide the units to its fully extended position. For tube locations, refer to table 3-5.

## (a) REPLACING TRIPLER TUBE V1504 AND

 FINAL R-F AMPLIFIERS VI 503 AND V1506 IN FRE. QUENCY MULTIPLIER-OSCILLATOR.--Whenever a tube is replaced in one of the r-f cavities, $\mathrm{Z} 1501, \mathrm{Z} 1502$ or Z 1503 , the cavities should be inspected and cleaned. Examine the cavity contacts to make sure that they have not been bent as a result of an improperly seated tube. It is possible that metal filings from the threads on the tube holder and anode clip have entered the cavity as a result of extensive tube replacement. The cavity should be cleaned with compressed air of moderate pressure to blow out any filings or dirt.
## WARNING

Operation of this equipment involves the use of HIGH VOLTAGES which are dangerous to life. Operating personnel must at all times observe all safety regulations. Do not change tubes inside the frequency multiplieroscillator with the MEDIUM VOLTAGE supply ON. Do not depend upon safety interlock switches for protection. Under certain conditions, dangerous potentials may exist in the circuit with power controls at OFF because of charges retained by capacitors. To avoid shock and severe burns, always discharge and ground circuits before touching them. Never service the equipment without the presence or the assistance of another person capable of rendering first aid immediately.

To remove a type 2C39A tube from cavity Z1501, Z.1502, or Z1503, proceed as follows:

Step 1. Disengage the spring clip on the cavity cover.

Step 2. Lift off the cavity cover.
Step 3. Remove the 2C39A by pulling straight out with a tube puller. If a tube puller is not available the tube may be removed by gently prying on opposite sides of the anode with two screw drivers.

Step 4. Replace the 2C39A by holding it in the center of the cavity and pressing straight in on the anode to seat the tube in the tube socket.

Step 5. Press the cavity cover in place making certain that the contact fingers around the edge of the cover are on the outside of the cavity.

Step 6. Engage the cavity cover spring clip on the lugs on either side of the cavity.

Step 7. After replacement of this tube, return the cavity and check overall tuning of the radio set.
(b) REPLACING KLYSTRON. -The procedure for installing a new klystron is described in Section 2, paragraph 2-4c. After the klystron is installed it should be aged according to the procedure described in Section 2, paragraph 2-5k.

TABLE 3-4. FUSE LOCATIONS


TABLE 3-4. FUSE LOCATIONS (cont)

| SYMBOL | LOCATION | PROTECTS | AMPS |
| :---: | :---: | :---: | :---: |
| F1402 | Frequency multiplier-oscillator ${ }^{1}$ | Crystal oven | 2 |
| F1403 | Frequency multiplier-oscillator ${ }^{1}$ | Crystal oven | 2 |
| F1601 | Low voltage power supply ${ }^{2}$ | Filaments | 0.75 |
| F1602 | Low voltage power supply ${ }^{2}$ | Filaments | 1 |
| F1603 | Low voltage power supply ${ }^{2}$ | Rectifier plates ( +250 V ) | 2 |
| F1604 | Low voltage power supply ${ }^{2}$ | Rectifier plates (-375V) | 1 |
| F1801 | Medium voltage power supply ${ }^{2}$ | Rectifier plates | 5 |
| F1901 | High voltage power supply ${ }^{2}$ | Rectifier plates | 3 |

${ }^{1}$ Receiver Transmitter OA-3352/GRN-9D
${ }^{2}$ Power Supply Assembly OA-1537A/GRN-9A

TABLE 3-5. TUBE LOCATION

| LOCATION | SYMBOL | FUNCTION | TYPE |
| :---: | :---: | :---: | :---: |
| RADIO RECEIVER |  |  |  |
| Preamplifier subassembly | $\begin{aligned} & \text { V201 } \\ & \text { V202 } \\ & \text { V203 } \end{aligned}$ | I-f amplifier <br> I-f amplifier <br> I-f amplifier | 5654/6AK5W 6J4WA 5654/6AK5W |
| I-f amplifier subassembly | V301 <br> V302 <br> V303 <br> V304 <br> V305 <br> V306 <br> V307 <br> V308 | I-f amplifier <br> I-f amplifier <br> I-f amplifier <br> I-f amplifier <br> I-f amplifier <br> Discriminator <br> Video amplifier <br> Clamper | 5654/6AK5W <br> 5654/6AK5W <br> 5654/6AK5W <br> 5654/6AK5W <br> 5654/6AK5W <br> 5654/6AK5W <br> 12AT7WA <br> 5726/6AL5W |
| Video amplifier subassembly | V401 <br> V402 <br> V403 <br> V404 <br> V405 <br> V406 <br> V407 <br> V408 | Blanking gate <br> Video amplifier <br> Decoder <br> Multivibrator <br> Cathode follower <br> Blanking multivibrator <br> Phase inverter <br> Pulse amplifier | $\begin{aligned} & \text { 5725/6AS6W } \\ & \text { 12AT7WA } \\ & 5725 / 6 \mathrm{AS} 6 \mathrm{~W} \\ & 5670 \\ & \text { 12AT7WA } \\ & 5670 \\ & 5670 \\ & 6005 / 6 \mathrm{AQ} 5 \mathrm{~W} \end{aligned}$ |
| Power supply subassembly | $\begin{aligned} & \text { V501 } \\ & \text { V502 } \\ & \text { V503 } \\ & \text { V504 } \\ & \text { V505 } \\ & \text { V506 } \end{aligned}$ | Full-wave rectifier <br> Full-wave rectifier <br> Voltage regulator <br> Amplifier <br> Voltage reference <br> Voltage reference | 5R4WGB 6X4W 6080WA 5654/6AK5W 5627/OB2WA 6627/OB2WA |

TABLE 3-5. TUBE LOCATION (cont)

| LOCATION | SYMBOL | FUNCTION | TYPE |
| :---: | :---: | :---: | :---: |
| CODER-INDICATOR |  |  |  |
| Video amplifier subassembly | V601 V602 V603 V604 V605 V606 V607 V608 V609 V610 V611 V612 V613 V614 V615 | 15-cps amplifier <br> $15-\mathrm{cps}$ gate generator <br> Oscillator <br> Amplifier <br> Multivibrator <br> Blocking oscillator <br> Amplifier <br> Tuning fork oscillator <br> 135 -cps gate generator <br> Oscillator <br> Priority gate <br> 1350-cps tone oscillator <br> Amplifier <br> Multivibrator <br> Multivibrator | 12AT7WA <br> 12AT7WA 5670 <br> 12AT7WA <br> 12AT7WA <br> 5687WA <br> 5687WA <br> 12AT7WA <br> 12AT7WA <br> 5670 <br> 12AT7WA <br> 5670 <br> 5670 <br> 5670 <br> 5687WA |
| Power supply subassembly | V701 <br> V702 <br> V703 <br> V704 <br> V705 | Plate supply rectifier <br> Bias supply rectifier <br> Series regulator <br> Control tube <br> Bias voltage regulator | $\begin{aligned} & \text { 5R4WGR } \\ & \text { 6X4W } \\ & \text { 6080 } \\ & \text { 6AH6 } \\ & \text { 6627/OB2WA } \end{aligned}$ |
| AMPLIFIER-MODULATOR |  |  |  |
| Power amplifier | V1304 | Power amplifier | SAL-89 |
| Bias supply | $\begin{aligned} & \text { V1370 } \\ & \text { V1371 } \\ & \text { V1372 } \end{aligned}$ | Regulator amplifier <br> Voltage reference <br> Series regulator | $\begin{aligned} & \text { 5654/6AK5WA } \\ & \text { 5651WA } \\ & \text { 5687WA } \end{aligned}$ |
| FREQUENCY MULTIPLIER-OSCILLATOR |  |  |  |
| Video subassembly | $\begin{aligned} & \text { V1401 } \\ & \text { V1402 } \\ & \text { V1403 } \\ & \text { V1404 } \\ & \text { V1405 } \\ & \text { V1406 } \\ & \text { V1407 } \\ & \text { V1408 } \\ & \text { V1409 } \\ & \text { V1410 } \\ & \text { V1411 } \end{aligned}$ | Multivibrator <br> Multivibrator <br> Amplifier <br> Amplifier <br> Amplifier <br> Series diode <br> Cathode follower <br> Multivibrator <br> Cathode follower <br> Voltage regulator <br> Cathode follower | 5814A <br> 5687WA <br> 6293 <br> 6293 <br> 6293 <br> 6V3A <br> 6293 <br> 5687WA <br> 5687WA <br> 5687WA <br> 6293 |
| R-f subassembly | V1501 <br> V1502 <br> V1503 <br> V1504 <br> V1505 <br> V1506 <br> V1507 <br> V1508 <br> V1509 | Oscillator-first doubler <br> Second doubler <br> Third doubler <br> Tripler <br> First amplifier <br> Second amplifier <br> Oscillator-first doubler <br> Second doubler <br> Third doubler | 5670 <br> 5654/6AK5W <br> 6 J 4 WA <br> 2C39A <br> 2C39A <br> 2C39A <br> 5670 <br> 5654/6AK5W <br> 6J5WA |

# SECTION 4 PRINCIPLES OF OPERATION 

## 4-1. INTRODUCTION.

Radio Set AN/GRN-9D is a shore-based radio set intended for use with Antenna Group AN/GRA-60 or AN/GRA-61. The radio set and the antenna group together function as a radio beacon that provides navigational information for aircraft within a $200-$ mile radius of the radio beacon. The radio beacon is part of the tactical air navigation system known as TACAN. An overall functional description of this system is presented in paragraph 4-2.

The radio beacon is divided into six major circuits: antenna circuits, control-duplexer circuits, receiving circuits, transmitting circuits, coderindicator circuits, and power supply circuits. A detailed description of these circuits, with the exception of the antenna circuits, is presented in paragraph 4-3. Refer to Technical Manual for Shore Antenna Group (NAVSHIPS 94118) for a functional and detailed description of the antenna circuits.

## 4-2. OVERALL FUNCTIONAL DESCRIPTION.

a. GENERAL. - The TACAN System is designed
 tion to aircraft equipped with the proper equipment. The airborne equipment consists of a receivertransmitter unit (referred to as an interrogator) and visual bearing and distance indicators. The ground equipment (reterred to as the radio beacon) consists of a radio set and associated antenna group and accessories. Because the system operates at high frequency, line-of-sight transmission is required between the aircraft and the radio beacon. Therefore, a number of radio beacons are necessary over large geographic areas. Each radio beacon is capable of receiving air-to-ground transmissions on one of the 126 assigned frequencies in the 1025-through 1150mc band. The radio beacon can transmit on any one of 63 frequencies from 962 through 1024 mc (low band operation), or on any one of 63 frequencies from 1151 through 1213 mc (high band operation). Thus, the pilot selects a specific radio beacon in his area for navigation information. Signals from the radio beacon provide the pilot with meter indications, in nautical miles, of the aircraft distance and the bearing, in degrees, from the radio beacon. With the distance and bearing established from a specific location, the pilot can fix his position on a chart.

The basic elements of the radio beacon are shown in figure 4-1. The radio beacon consists of a radio set containing a receiver-transmitter group and a power supply group, and an antenna group. Essentially, the radio beacon is a transmitter-receiver combination (transponder) for the reception and transmission of information used in determining aircraft distance from the radio beacon. The addi-
tion of a rotating directional antenna permits the transmission of bearing information to the aircraft.

The radio beacon output consists of replies to distance interrogations from the aircraft interrogator, bearing information signals, radio beacon identification signals, and random pulses. Signals from both the ground station and the aircraft are transmitted in the form of coded pairs of $3.5-$ microsecond wide pulses having a 12 -microsecond spacing between pulses of a pair. Each of the information elements supplied (in the order of the priority established for each within the radio beacon) is analyzed briefly in the following paragraphs.

## b. BEARING INFORMATION.

(1) BEARING INFORMATION COMPONENTS. The bearing information presented to the pilot is the direction of the beacon with respect to the aircraft, measured in degrees clockwise from magnetic north. This is the reciprocal ( 180 degrees removed) of the information obtained from the modulated antenna pattern, which actually shows the direction of the aircraft from the beacon. The bearing information supplied by the beacon is originated by the beacon, and consists of four components, discussed in the paragraphs (a) to (d) that follow.
(a) 15-CPS AMPLITUDE MODULATION. A $15-\mathrm{cps}$ àmplitude-modulation component is imposed on the $r$-f energy radiated by the beacon antenna. Figure 4-2 shows how modulation is imposed on the field of $r-f$ energy radiated by the antenna.

Waveshape A in figure 4-2 shows a conventional circular antenna pattern. Waveshape $B$ in figure 4-2 shows the same antenna pattern as it is affected when ${ }^{a}$ fixed reflector is placed in the field of energy radiated by the antenna. The pattern becomes a cardioid. The field of $r$ - $f$ energy is at its maximum in the direction ( E ) opposite to the reflector.

When the reflector is rotated about the radiating element of the antenna the effect is a cardioid pattern, similar to waveshape $B$, shown in figure $4-2$, which rotates about the axis of the antenna at the same rate as the reflector. Waveshape C, shown in figure 4-2, shows five of the positions taken by the antenna pattern during the 360 -degree rotation of the reflector. In the case of pattern No. 1, an aircraft located at a position due south of the beacon antenna would receive a half-amplitude signal. If the antenna were rotated through 90 degrees (pattern No. 2), the same aircraft would receive a signal at maximum amplitude. Rotating the antenna another 90 degrees (pattern No. 3) would cause the aircraft to receive a half-amplitude signal of diminishing strength. Still another 90 -degree rotation of the antenna (pattern


Figure 4-1. Radio Beacon Overall Functional Block Diagram


Figure 4-2. Development of Radio Beacon Radiation Pattern

No. 4) would cause the aircraft to receive a minimum-amplitude signal. Finally, completion of the 360 -degree rotation of the antenna reflector (pattern No. 5) would return the signal received by the aircraft to half amplitude (increasing in strength).

The relative amplitudes of the signals received by the aircraft for one complete revolution of the antenna reflector are shown for comparison purposes in waveshape $D$ of figure 4-2. Although the total beacon output is of constant amplitude through the full 360 -degree rotation of the reflector, the signal received by an aircraft at any given point around the beacon will vary in amplitude, as explained above.

The amplitude variation of the envelope of the pulses received by the aircraft follows a sine-wave (approximate) pattern (waveshape $E$ of figure 4-2), the frequency of which corresponds to the rate of rotation of the reflector around the antenna. Since the reflector rotates about the beacon antenna at a 15 -cps rate, an aircraft at any given point in space within range of the beacon will detect the complete sine wave 15 times per second. Note that a $15-\mathrm{cps}$ rate of rotation corresponds to 900 revolutions per minute ( rpm ).
(b) NORTH REFERENCE (15-CPS) BURST.-To orient the bearing information of the beacon with respect to magnetic north (figure 4-3), a group of coded pulses is introduced into the $15-\mathrm{cps}$ amplitude-modulated field of energy radiated by the radio beacon antenna. This group of pulses (or coded burst) is generated once during each revolution of the reflector, and occurs every time the peak of the radiation lobe points due east (with respect to magnetic north). At that moment, a trigger pulse, generated by the antenna, is used by the radio beacon to initiate the formation of the burst.

Figure 4-3 shows the positions of the north reference burst on the $15-\mathrm{cps}$ amplitude-modulated sine wave, as seen by four aircraft at four different points around the beacon. Waveshape A of figure $4-3$ shows the position of the north reference burst on the $15-\mathrm{cps}$ modulation as observed by an aircraft due south of the beacon, flying on bearing 000 . As seen by the aircraft, this burst occurs at the positive going half-amplitude point, or 0 -degree point, of the sine-wave modulation. Waveshape B of figure $4-3$ shows the north reference burst as observed by an aircraft due west of the beacon, flying on bearing 90 degrees. This burst occurs at the minimum-amplitude, 270degree point of the sine wave. Waveshape $C$ of figure 4-3 shows the position of the burst for an aircraft due


Figure 4-3. Employment of North Reference Burst to Mark Bearing of Aircraft Relative to Radio Beacon
north of the beacon, flying on bearing 180 degrees. Here, the burst occurs at the half-amplitude (going negative), or 180 -degree point of the sine wave. Waveshape C of figure 4-3 shows the burst at the maximum-amplitude, 90 -degree point of the $15-\mathrm{cps}$ modulation (sine wave), as it would be observed by an aircraft to the east of the beacon, flying on bearing 270 degrees. This illustrates how the phase of the 15 -cps modulation shifts with respect to the $15-$ cps north reference burst, as the aircraft moves on a 360 -degree circle around the radio beacon.

This phase difference is detected by the aircraft receiver of Radio Set AN/ARN-21 and converted to a meter reading in degrees showing the bearing from the aircraft to the beacon with respect to magnetic north.

Figure 4-4 illustrates the signals received by four aircraft located at four different points around the radio beacon, as well as the corresponding meter readings (indicating their bearings) relative to the beacon. Note that all aircraft receive the north reference burst at the same instant of time, but at different phases of the 15 -cps amplitude modulation.
(c) 135-CPS AMPLITUDE MODULATION. A $135-\mathrm{cps}$ amplitude-modulation component (figure $4-5$ ) is also imposed on the $r-f$ energy radiated by the radio beacon antenna. The $135-\mathrm{cps}$ modulation is produced, in a manner similar to that described above, by directors spaced 40 degrees apart around
the radiating element, and which rotate about it at a 15-cps rate.

This $135-\mathrm{cps}$ component, acting alone, would shape the antenna pattern as shown in pattern No. 2 of figure 4-5. The resultant antenna pattern, caused by the combined effect of the $15-\mathrm{cps}$ reflector and the $135-\mathrm{cps}$ directors, is also shown in patterns No. 3 and No. 4 of figure $4-5$. Note that $135-\mathrm{cps}$ is the ninth harmonic of 15 cps .
(d) AUXILIARY REFERENCE (135-CPS)

BURST. - Ir $r$ n slugs passing through the field of a magnetic pickup coil initiate the formation of the $135-\mathrm{cps}$ reference bursts, as in the case of the $15-$ cps reference bursts, but at 40 -instead of 360 -degree intervals. The $135-\mathrm{cps}$ amplitude-modulated component and the 135 -cps reference burst are used in a manner similar to that described in paragraph 4-2 b (1) (a) for the 15 -cps signals.
(2) COMBINING BE ARING INFORMATION COMPONENTS. - Figure 4-6 summarizes the steps involved in the development of the composite $15-\mathrm{cps}$ and $135-\mathrm{cps}$ signal elements into the total bearing information supplied by the radio beacon to the aircraft. The signals (including the $15-\mathrm{cps}$ and $135-\mathrm{cps}$ amplitude modulation and the $15-\mathrm{cps}$ and $135-\mathrm{cps}$ reference bursts) received by the aircraft in positions due east, south, west, and north, relative to the beacon, appear as shown. Again, the phase of the modulation relative to the bursts depends on the


2. HORIZONTAL PATTERN OF 135 CYCLE, (NINTH HARMONIC) MODULATION

3. HORIZONTAL PATTERN COMBINATION OF FUNDAMENTAL a NINTH HARMONIC MODULATION

4. THREE-DIMENSIONAL ANTENNA RADIATION PATTERN

Figure 4-5. Development of Composite Radiation Pattern
position of the aircraft relative to the beacon. The 135 -cps bursts have simply refined the measurement of angle relative to magnetic north.
c. DISTANCE INFORMATION. -Of all the signals trañsmitted by the radio beacon, distance measuring information alone is not originated within the beacon. Distance reply signals are supplied by the radio beacon only in response to interrogations from an airborne AN/ARN-21. Thus, such information is actually originated by the airborne portion of the TACAN system. Each AN/ARN-21 transmits, at the frequency of the radio beacon, a sequence of paired pulses with a random pulse-pair spacing peculiar to itself. This signal is received by the radio beacon receiver. The beacon adds a 50 -microsecond delay to the received distance measuring interrogations, and retransmits them to the aircraft as replies at the transmitting frequency of the radio beacon and the coded puise-pair spacing of the interrogating aircraft. The aircraft radio receiver selects the particular distance measuring reply from all other signals by comparing the repetition rate of the relay pulse pairs with the repetition rate of the originally transmitted interrogation pulse pairs. Then it subtracts the 50 -microsecond zero distance delay time from the total time between transmission and recep-
tion of interrogation pulse pairs and converts the remaining round trip travel time of the signal into distance between the aircraft and the beacon. A continuous display indicator on the AN/ARN-21 displays this distance in nautical miles.
d. RADIO BEACON IDENTIFICATIONS. -The radio beacon periodically transmits its identifying call in International Morse Code, thus enabling the aircraft to determine which radio beacon it is in contact with. The characters of the code consist of a train of 1350 double pulses per second, keyed by a coding wheel built into the radio beacon. The aircraft receiver of the AN/ARN-21 decodes the pulses representing the identification call, and reproduces them as 1350 -cps identification call signals.

## e. INFORMATION ELEMENT PRIORITY IN

 RADIO BEACON. -The three elements of information (bearing, identification code, and distance measuring information) discussed in the preceding subparagraphs are transmitted by the radio beacon as a train of pulse pairs. To prevent interference between the three signal elements, the radio beacon is arranged to assign a sequence or priority in which each enters into the overall pulse train.(1) The bearing reference bursts are first in the order of priority because they occur at a fixed rate and are of relatively short duration. Accordingly, reference bursts can break in on any other information element being transmitted by the radio beacon.
(2) Second in the order of priority are the identifica-tion-code signals, which also occur at a fixed rate. However, the duration of the identification-code signal is such that the utilization of the portion required for the insertion of bearing reference bursts does not materially affect the reception of intelligible identification code by the aircraft.
(3) Third in the order of priority are the distance interrogation signals. The interrogation pulses are not initiated within the beacon, and their arrival within the pulse train must therefore be controlled if their interfering with the other signal elements of the radio beacon is to be prevented. This is done by allowing the interrogation pulses to enter the pulse train only during a time interval not occupied by the reference bursts or identification-code signals. This is possible because the time occupied by the reference bursts is small in comparison with the time allowed for the total radio beacon signal cycle. In addition, a memory circuit built into the aircraft receiver of the AN/ARN-21 makes it possible to compensate for the time interval during which identity tone is transmitted, and no reply pulses are received because of the priority system within the beacon.
(4) Last in the order of priority are squitter pulses, which are used as fill-in signals when the maximum number of aircraft are not interrogating the beacon; this maintains the modulation pattern and permits constant duty-cycle operation of the radio beacon.

## Note

The relative duration of the signal elements is such that effectively there is no interruption of bearing, identification call, or distance information received by the aircraft.

## 4-3. FUNCTIONAL DESCRIPTION

Radio Set AN/GRN-9D contains seven functional sections; a receiver, coder-indicator, transmitter, control-duplexer, power supplies, power distribution and control circuits, and built-in test equipment. Figure $4-7$ shows in block diagram form the receiver-transmitter group circuits discussed by functional sections with associated power supplies, and government-furnished test equipment described in detail and illustrated separately.

## a. BLOCK DIAGRAM ANALYSIS.

(1) RECEIVER. - Distance interrogation pulse pairs are received by the antenna and passed through the duplexer, and then pass through a low-pass filter to the mixer stage of the receiver. The low-pass filter rejects frequencies between

1650 and $10,000 \mathrm{mc}$ to prevent interference from other pulse producing equipment operating in the band. To prevent interference from the transmitter portion of the radio set, a blanking pulse blanks out the receiver whenever the transmitter klystron is operating.

The receiver uses the output from the frequency multiplieroscillator section of the transmitter as its local oscillator signal. The mixer and preamplifier consists of a balanced hybrid T-type mixer and a three-stage preamplifier. The local oscillator signal is fed into one arm of the mixer and the interrogation r-f pulses are fed into the other arm; the resultant intermediate frequency of 63 mc is amplified in the three-stage preamplifier.

The i-f amplifier receives the interrogation pulses and random noise pulses from the preamplifier at the intermediate frequency. These voltages are amplified to a level sufficient to operate the Ferris discriminator, which detects the interrogation and random noise pulses at 63 mc and effects adjacent and near-adjacent channel rejection. The video signal output of the Ferris discriminator is fed to the receiver video amplifiers. Echo-suppression circuits employed in the i-f amplifier permit operation in areas where large reflecting objects are present. Squitter-control voltage, fed into the i-f amplifier from the squitter-voltage generator, maintains the receiver output at $2700 \pm 90$ pulses per second.

The video amplifiers receive the i-f amplifier output (noise and interrogation pulses) and further amplify these video signals to a level that can operate the coincidence-type decoder. The decoder produces a single pulse for each input pulse pair having pulses separated by 12 microseconds. The decoding of each pulse pair is followed by a 40 -microsecond blanking of the receiver to ensure that the 2700 pulses at the receiver output will be distributed over a period of 1 second. Although the squitter-control circuits set the pulse output of the receiver at $2700 \pm 90$ pulses per second, the entire pulse output for 1 second could occur during the first quarter-second; likewise, the entire pulse output for the following second could occur during the second quarter-second and a period of $1-1 / 2$ seconds would be left during which there would be no output from the receiver. By introducing a blanking period of 40 microseconds after the decoding of each pulse pair, the minimum spacing between receiver output pulses is set at 65 microseconds, owing to the total effect of the 40 -microsecond blanking period plus the coding time of 12 microseconds, and the 10 -microsecond blanking of the receiver by the transmitter.

While the transmitter is transmitting output pulses, a sample of the 10 -microsecond pulse generated in the frequency multi-plier-oscillator video chassis is fed to the receiver blanking gate to disable the receiver. Disabling the receiver during the transmission of output pulses prevents the radio set from respnnding to its own transmitted signal. In addition, a pulse-counter circuit produces a squitter-control voltage which is fed back to the i-f amplifier and controls the gain of the i-f amplifier circuit. The


result is that decoding of 12 -microsecond-interval pulse pairs (interrogations) and of random noise groups causes the desired output of 2700 pulses per second. When the rate of interrogation pulse pairs falls below 2700 pulse pairs per second, i-f amplification is increased until the number of random noise pulse pairs decoded is sufficient to maintain receiver output at the required rate. Under normal conditions, the maximum interrogation rate should not be above 2500 pulse pairs per second.

The pulse output of the decoder triggers a one-shot multivibrator having three outputs: one output initiates a blanking gate to the video amplifiers; the second output initiates the squitter-control voltage to the i-f amplifiers; and the third output drives the receiver output cathode-followers. The output of the cathode-followers is fed to the coder-indicator.
(2) CODER-INDICATOR. - The coder-indicator produces a multiplexed output signal consisting of three components: reference burst, distance reply pulses. Generation of the reference bursts component has priority over generation of all other output components.

For each revolution of the antenna, the $135-\mathrm{cps}$ reference burst generator receives eight trigger pulses from the antenna and the $15-\mathrm{cps}$ reference burst generator receives one $15-\mathrm{cps}$ trigger pulse. The $135-\mathrm{cps}$ trigger pulse applied to the $135-\mathrm{cps}$ reference burst generator is approximately 12 volts peak-topeak and 150 microseconds wide. Upon reception of the 135 cps trigger pulse, a reference burst generator produces six pulses spaced 24 microseconds apart.

The 15 -cps reference pulses are generated in a similar manner in the $15-\mathrm{cps}$ reference burst generator. The output of the 15 -cps reference burst consists of 12 pulses, 30 microseconds apart. At the input to the shaping amplifier stage, the $15-\mathrm{cps}$ and 135 -cps reference pulse groups are mixed; from this point on, both pulse groups pass through the same stages. This action is possible because two reference pulse groups never occur simultaneously.

For each reference burst sent to the shaping amplifiers, a blocking gate is sent to the priority gate which blocks out the identification call and distance reply signals during transmission of reference bursts. This establishes the priority of reference burst over all other signals.

The output of the shaping amplifiers drives encoding delay line DL601, which is inductively tapped at 32 -microsecond delay and at 44-microsecond delay. The encoding delay line introduces the major portion of the standard zero distance delay for distance reply pulses and provides a pulse pair having a 12 -microsecond spacing for each pulse fed into the delay line.

The double-pulsed output of DL601 is coupled to the out put amplifier stages. These stages provide gain in signal ampli-
tude, improvement in waveshape and uniformity, of output, and impedance matching to the transmitter input.

The other coder-indicator output components are distance reply pulses and beacon identification code tone pulses. Selection of one or the other of these components is controlled by the mechanical switching action of the identification call mechanical keyer. The voltage on pin 10 of testboard TB604 is 0 volt with a -50 -volt gate appearing whenever the code keying wheel indicates that a $1350-\mathrm{cps}$-tone dot or dash is to be sent.

During transmission of identification code characters, the -50-volt gate cuts off the gate-blocked distance-reply amplifier that normally passes distance reply pulses from the receiver to the priority gate. Simultaneously, the -50 -volt gate keys on the normally cut off 1350 -cps-tone signal and permits the 1350 -cps-tone output to be sent to the priority gate. In this manner, the code keying wheel controls the selection of the code and establishes the priority of the 1350 -cps-tone oscillator signal over the distance reply signals.

The priority gate passes identification code and distance reply signals to the shaping amplifiers. Whenever a reference burst is generated, a blocking gate is applied to the priority gate, cutting it off and establishing priority of the reference burst over the identification code and distance reply signals.

All signals from the priority gate to the shaping amplifiers are shaped, double-encoded, amplified, and sent to the transmitter as components of a multiplexed signal in the same manner as previously described for the reference bursts signals.

The antenna-synchronization, 1350 -cps-oscillator is not dependent on the signal output of any other coder-indicator circuit. The frequency output of this oscillator is controlled by a $1350-\mathrm{cps}$ tuning fork. The oscillator output is used in conjunction with the antenna tachometer output to obtain a Lissajous pattern for speed comparison.
(3) TRANSMITTER. - Each pulse from the coderindicator initiates the formation of a 3.5 -microsecond shaped pulse and a 10 -microsecond keying pulse. The 3.5 -microsecond shaped pulse is amplified in the video portion of the frequency multiplier-oscillator to a power level sufficient to key-on and grid-modulate the klystron beam current. Square pulses of 10 -microsecond duration are applied to the cathodes of the keyed r-f amplifiers to key-on these stages that are normally cut off by a positive voltage applied to the cathodes. A sample of the 10 -microsecond pulse is fed from the frequency multi-plier-oscillator to the receiver to be used as a blanking pulse as previously described.

The output of the keyed r-f amplifiers consists of a $10-$ microsecond pulse of r-f energy which drives the klystron. While 10 -microsecond pulses are being applied to the klystron r-f input jack, the 3.5 -microsecond shaped pulse is applied to the klystron control grid. Klystron beam current, normally cut
off by negative bias from the regulated bias supply in the amplifier modulator, is keyed on and grid modulated by the 3.5 -microsecond shaped pulse. As the beani current passes through the first resonant cavity of the klystron, it is velocity modulated by the application of the 10 -microsecond $r$-f pulse to the first cavity of the klystron. The combined effect of the above-mentioned grid modulation and velocity modulation of the klystron beam current results in a high-powered r-f pulse having an envelope which is controlled in shape to ensure that the radiated $\mathbf{r}-\mathrm{f}$ power will occupy a minimum of frequency spectrum about the assigned carrier frequency.
(4) CONTROL-DUPLEXER. -The controlduplexer consists of a duplexer circuit and control circuits. The duplexer circuit permits feeding both the transmitter output signal and the receiver input signal through the same transmission line and antemna; the control circuits permit operating the radio set by means of switches on the front panel of the control-duplexer drawer. Also included in the control-duplexer drawer are two resonant cavity filters inserted in series with the transmission line to limit the overall spectrum of the transmitter output.
(5) POWER SUPPLIES. -The power supplies provide regulated voltages at the various output levels required tor radio set operation. These power supplies include low, medium, and high voltage supplies for the transmitter, a coder-indicator power supply and a receiver power supply.
(6) POWER DISTRIBUTION AND CONTROL CIRCUITS. - The functioning of power distribution and control circuits is such that the various components of the equipment are energized in their proper sequence: the failure of one component will sesult in the de-energizing of other components that micht be damared by its failure. Safety interlocks, on component drawers and compartments in which high voltages are present, disconnect parts of the system when the drawers are pulled out or the compartments opened. The radio set receives 208 -volt a-c, 60-cycle, three-phase, four-wire primary power. Rectithers in the various d-c power supplies throughout the radio set convert a-c power to d-c power of the required voltage. Additional a-c power is supplied from the 117 -volt, single-phase, $60-$ cycle lighting carcuit to the convenience outlets on the radio set antenna control units and antenna base.
(7) BUILT-IN TEST EQUIPMENT. - Test equipment is provided to permit rapid check of the important operating characteristics of the Radio Beacon. In this paragraph the first five Sections (a) to (e) concern the original test equipment (TABLE 1-2) whilst Section (f) describes the facilities provided by the replacement test equipment (TABLE 1-2b).

Pulse-Sweep Generator SG-121A, URN-3 (Technical Manual NAVSHIPS 92745).

Pulse Analyzer-Signal Generator TS-890A/URN-3 (Technical Manual NAVSHIPS 93231).

Power Meter-Pulse Counter TS-891/URN-3 (Technical Manual NAVSHIPS 92809).

Oscilloscope OS-54/URN-3 (Technical Manual NAVSHIPS 92778).

Switch-Test Adapter SA-420/URN-3 (Technical Manual NAVSHIPS 92809).

The first four units are mounted in the upper half of the power supply assembly directly above the low and medium voltage power supplies. The location of the SA-420, URN-3 is optional. However, it should be located in such a way that the lengths of cable connecting it to the rest of the equipment are kept to a minimum.

The units are interconnected through a cable harness to permit rapid connection for standard test procedures, as selected by means of an integral switching system. The switching system includes two four-position function switches located on the front panels of the oscilloscope and the power nieterpulse counter and a two-position coaxial $r$ - $f$ switch on the switch-test adapter. Also, it is necessary to interconnect front panel jacks of the units by means of coaxial patch cords. The interconnection harness is shown in figure 2-11 and front panel comections are shown inf igure 3-13.

The tests which may be made in each of the four positions of both function switches are listed in table 4-1.

## Note

Both function switches should be in the same position during a specific test.

The following paragraphs include the theoretical principles upon which the tests listed in table 4-1 are based, a functional description of each of the units involved in these tests, and a brief circuit description of each of the equipments. These discussions are based on the block diagrams, figures 4-8 through -4-12. For more detailed information, reference should be made to the technical manuals for these equipments. Overall schematic diagrams of the test equipments are given in Section 6 of this handbook.
(a) PULSE-SWEEP GENERATOR SG-121A/

URN-3. - The pulse-sweep generator (figure 4-8) provides pulsed pairs at a controlled variable rate to simulate the pulse output of one or more airborne $\mathrm{AN}^{\prime} \mathrm{ARN}$-21. The pulse-sweep generator output is a video signal applied as modulation to Pulse Analyzer Signal Generator TS-890A/URN-3 to provide the required pulsed r-f signal, which simulates the normal input to the radio beacon receiver.

The paired-pulse output of the pulse-sweep generator is carefully timed to facilitate measurement of the characteristics of the radio beacon. The spacing between pulses in the pair may be varied from 11 to 13 microseconds, in $0.5-$ mic rosecond steps, to permit checking that radio beacon output pulse-pair spacing is within the specified limit of 11.5 to $12.5 \pm 0.2$ microseconds and that the beacon will decode for retransmission only those pulse pairs

TABLE 4-1. FUNCTION SWITCH POSITIONS FOR TESTING

| SWITCH POSITION | PANEL NAME | TEST |
| :---: | :---: | :---: |
| 1 | OPERATING TEST | R-f peak power <br> Visual pulse shape <br> Output pulse count <br> AN/URN-3 transmitter spectrum |
| 2 | RECEIVER SENSITIVITY | Reference burst pulse count Squitter count |
| 3 | DELAY SYSTEM | Overall zero-distance time delay Video zero-distance time delay |
| 4 | GENERAL TEST | Maintenance testing |

within the same limits. The pulse repetition rate is variable. Continuous variation over the range of 40 to 4000 pulse pairs per second permits interrogating the radio beacon at rates which simulate different numbers of AN/ARN-21 within the operating range. Fixed, crystal-controlled rates are also provided. Separate crystal timing frequencies produce sweep rates for checking the upper and lower tolerance limits of the overall zero distance delay, 50.2 and 49.8 microseconds, respectively.

Sweep voltage in the form of a sawtooth is provided at exactly one half of specified rates. A modulation trigger is also provided which is an exact multiple, at an interval of approximately 1000 microseconds, of the sweep rate, i.e., the modulation trigger times the output pulse pair; the reason for this arrangement is given in the discussion of test principles. A sync trigger is also provided; this trigger is developed from the modulation trigger, which times the pulse pair at the continuously variable or crystal-controlled rates.

## (b) PULSE ANALYZER-SIGNAL GENERATOR TS-890A/URN-3 or TS-890B/URN-3

## Note

The TS-890A/URN-3 and the TS-890B/URN-3 are similar except for $r$-f spectrum measuring capabilities. Either unit may be used for all tests requiring a pulse analyzer-signal generator except for the spectrum test. When checking r-f output spectrum, the TS-890A/URN-3 model must be used.

The TS-890A/URN-3 (figure 4-9) provides an r-f carrier for testing the beacon and a calibrated receiver for spectrum analysis of the beacon output signal. The pulse analyzer-signal generator is capable of supplying an r-f signal over the complete range of the beacon receiver and analyzing radio beacon output signals over the complete range of output frequencies.

The r-f signal provided by the signal generator portion of this unit is continuously variable over the range of 1023 to 1152 mc . Means are also provided for plugging in crystals corresponding to the frequency of any channel within this range, as a fixed frequency source. The amplitude of this signal may be varied over an accurately calibrated range of 0.1 microvolt to 0.5 volt. The specified voltages are for a 50 -ohm output. This r-f signal may be either continuous wave or pulsed.

The receiver (analyzer) portion of this unit may be tuned to any frequency in the two bands of 962 to 1024 and 1151 to 1213 mc . Once tuned to a channel, the receiver may be detuned to a narrow band of frequencies 0.8 mc or 1 mc above or below the channel. An attenuator associated with this feature provides a particular discrete loss when tuned $0.8-\mathrm{mc}$ off channel, and when tuned on channel. This arrangement varies receiver sensitivity in such a way that, if the radio beacon output signal has the correct spectral distribution, a meter in the receiver output circuit will read midscale for all five on-channel and off-channel conditions. A separate attenuator having a range of 30 db permits varying receiver output so that the meter may be set to mid-scale for the on-channel condition. Thus, any deviations from the specified spectral characteristics of the radio beacon output will be indicated by corresponding deviations of the meter reading.
(c) POWER METER-PULSE COUNTER TS-891/

URN-3. - The power meter-pulse counter (figure 4-10) includes two functionally separate circuits in the one unit.

1. POWER METER CIRCUIT. - The power meter circuit is a metered variable d-c source used to bias the diode in Switch-Test Adapter SA-420/URN-3 for power measurement. Varying the bias changes the diode clipping level and causes less detected positive pulse to be passed on for display on the oscilloscope. By adjusting the bias to the point at which the detected pulse is just eliminated from the scope presentation, the d-c voltage is made equal to the peak amplitude of the pulse. Since the d-c voltage is a measured quantity, a direct indication of


Figure 4-8. Pulse-Sweep Generator SG-121A/URN-3, Simplified Functional Block Diagram


Figure 4-9. Pulse Analyzer-Signal Generator TS-890A/URN-3, Simplified Functional Block Diagram


Figure 4-10. Power Meter-Pulse Counter TS-891/URN-3, Simplified Functional Block Diagram
peak-pulse amplitude, and hence peak power, is obtained. The meter that indicates the magnitude of the d-c voltage is calibrated in kilowatts.

## 2. PULSE COUNTER CIRCUIT. -The

 pulse counter circuit is arranged to perform several functions.When counting the beacon squitter output pulses, the pulse counter accepts these pulses, shapes them for uniformity, and applies them to a vacuum tube measuring circuit which varies the meter current in direct proportion to pulse rate. The associated meter is calibrated directly in pulses per second, and has two ranges of 80 to 800 to 8000 pulses per second. Thus, the circuit measures the squitter output directly. Squitter count is defined as the random output of the beacon not due to interrogation.

When counting the reply rate (pulses that pass through the beacon receiver as a direct result of interrogations), the pulses are applied to the pulse counter exactly as for squitter count. In addition, interrogation pulses from the pulse-sweep generator are applied to the counter circuit and a gate circuit. The gate circuit prevents the passage of pulses through the counter, except for a 14-microsecond period following delivery of an interrogation signal. The start of the 14 -microsecond gate is delayed 12 microseconds to compensate for a corresponding delay through the receiver. Thus the counter is gated off for all pulses except direct replies.

In addition to squitter count and reply count, a four-position FUNCTION switch also permits the
counter to accept either negative or positive pulses from any external source.
(d) OSCILLOSCOPE OS-54/URN-3. -The oscilloscope (figure 4-11) is a versatile, wide-band oscilloscope with a triggered sweep. Sweep trigger may be from a recurrent source within the oscilloscope or from an external source. Sweep speed may be varied over the range of 0.4 to 40,000 microseconds per inch. Sweep blanking is provided, the sweep is inactive and blanked out in the absence of a trigger. The vertical amplifier bandwidth, between those frequencies which are 3 db down, is 5 cycles to 3 mc .

The oscilloscope provides timing markers and calibrating voltage to permit accurate measurement of signal waveform amplitude and pulse width.
Markers are at intervals of 1 and 10 microseconds, and may be superimposed on the signal at will. The calibrating voltage permits peak-to-peak amplitude measurement over a range of 0.1 volt to 100 volts. An additional feature, which permits observation of the leading edge of sharply rising wavefronts, is an optional signal delay of 0.3 microsecond.

## (e) SWITCH-TEST ADAPTER SA-420/

URN-3. -The switch-test adapter (figure 4-12) consists of a heavy duty coaxial switch and a pick-off diode. The switch transfers the radio beacon transmitter output power from the antenna to a dummy load and the pick-off diode supplies a detected signal to the test equipment. A biasing voltage developed


Fisure 4-11. Oscilloscope OS-54 URN-3, Simplified Functonal Block Diagram

Figure 4-12a. REPLACEMENT TEST EQUIPMENT MM-TMC-212a.


Figure 4-12. Switch-Test Adapter SA-420 LiRN-3. Simplified Block Diagram
in the power meter-pulse counter is applied to the diode to permit power measurement by the slide-back method.
(f) REPLACEMENT TEST EQUIPMENT (TABLE 1-

2b). - This test equipment comprises the following pieces of test equipment, a functional description of which is given in this section.

Spectrum Analyzer/Test Generator MM-705
Technical Manual: AP 116C-0702-1H6H
Oscilloscope MM-504
Technical Manuals: AP 116C-0702-1J6J
AP $116 \mathrm{C}-0702-1 \mathrm{~K} 6 \mathrm{~K}$
Power Meter - Pulse Counter - Marker Generator MM-109
Technical Manual: AP 116C-0702-1G6G
These units are mounted with a Transfer and Switching Unit, a Transfer and State Transmission Unit (TELOTEL), and its assocated interface unit, and two Transponder Monitors in the Electrical Equipment Cabinet 212A and are interconnected through a cable harness and (for certain tests) two function switches, all of which permit rapid connection for standard test procedures. A block diagram of the equipment is shown in Fig 2-11a whilst Fig 3-13a shows the front panel connections required to perform certain standard tests described in Para 3-6a(12).

1. SPECTRUM ANALYZER/TEST GENERATOR MM-705 ( $\bar{F}$ ig.4-12a). - This unit is designed to function separately or as an integrated unit with other special test components of the MM-TMC-212A Group.
a. The spectrum analyzer section consists of a double superheterodyne receiver, with 2 crystalcontrolled local oscillators, and is capable of measuring an r.f. spectrum over a power range of 70 dB at a maximum signal of +14 dBw and a minimum signal of +5 dBw peak at the standard TACAN transponder duty cyle (specified in MIL-STD-291A), with a measurement accuracy of 3 dB . A crystal filter (at the input of the second IF amplifier) provides a well-defined bandpass response with high selectivity. A thermistor bridge at the output of the second IF amplifier is used to measure the transmitted energy in each of the six bands adjacent to the transponder transmitting frequency as well as the on-channel energy. A first local oscillator provides crystal-controlled operation at any single frequency in the range 960 to 1215 MHz to within $+0.002 \%$ of the assigned frequency.

The second local oscillator is tunable to any one of seven crystal-controlled frequencies by means of a front panel BAND SHIFT switch. The operation of this switch enables measurement of relative transmitted energy in seven bands 500 kHz wide, each with an accuracy of $+0.002 \%$ centred as follows:

## 1. On-channel frequency

2. $\pm 0 \cdot 8 \mathrm{MHz}$ away from the on-channel
frequency.

## frequency.

3. $\pm 1.0 \mathrm{MHz}$ away from the on-channel
4. $\pm 2 \cdot 0 \mathrm{MHz}$ away from the on-channel
frequency.

When the BAND SHIFT switch is in the EXT OSC position an external oscillator input can be used to shift the second IF bandpass and this enables the measurement of energy levels at frequencies other than those provided for by the specified crystals. The external oscillator must provide an input whose signal level is 1 mW into 50 ohms. A precision direct-réading input attenuator, with 3 to 5 dB insertion loss, is provided at the front panel for control of the input signal. The attenuator is calibrated over the range 0 to 120 dB in increments of 1 dB with the following accuracies:

| Frequency | Range | Accuracy |  |
| :---: | :---: | :---: | :---: |
| $60-66 \mathrm{MHz}$ | $0-110 \mathrm{~dB}$ | $\pm 1 \cdot 5 \mathrm{~dB}$ in the range $0-100 \mathrm{~dB}$ |  |
| $958-1217 \mathrm{MHz}$ | $0-120 \mathrm{~dB}$ | $+0 \cdot 7 \mathrm{~dB}$ in the range $0-100 \mathrm{~dB}$ |  |
| $958-1217 \mathrm{MHz}$ | $0-120 \mathrm{~dB}$ | $\pm 1 \cdot 0 \mathrm{~dB}$ in the range $100-115 \mathrm{~dB}$ |  |

The nominal frequency bandpass of the second IF amplifier, determined primarily by the crystal filter, is 500 kHz . Ripple in the bandpass is within $+1 \frac{1}{2} \mathrm{~dB}$.of a selected reference level. The bandwidth at 3 dB below this reference level is greater than 500 kHz whilst the bandwidths at 50 and 70 dB below this reference are less than 825 and 1020 kHz respeetively.
b. The test generator section consists of a 63 MHz CW IF signal generator and an RF signal generator providing CW or pulsed operation over the frequency range 1024 to 1151 MHz . The purpose of the 63 MHz IF signal generator is to provide' a signal for aligning the IF stages of the beacon receiver. The purpose of the RF signal generator is to provide RF energy (at the beacon receiver frequency) for testing and maintenance.

1. IF Signal Generator .- The output frequency of the IF signal generator is variable from 60.5 to 65.5 MHz with a capability of being set to $63.000 \mathrm{MHz}+0.005 \%$ and the output power is variable from $0^{-}$to -110 dBm , calibrated to an accuracy of $\pm 2 \mathrm{~dB}$ over the range 0 to -100 dBm . The modulation of the amplitude is less than $2 \%$ whilst that of the frequency is less than 1 kHz . Spurious output is at least 40 dB down from signal output.
2. Microwave Signal Generator.- The

RF Signal generator has a crystal-controlled master oscillator which establishes the operating frequency to an accuracy and stability within $0 \cdot 002 \%$. The generator provides RF output signals for interrogation at any single channel frequency from $1024 \cdot 0$ to $1151 \cdot 0 \mathrm{MHz}$. A FREQ SEL switch is provided for the selection of onchannel frequency. The only other adjustment required when selecting any of the five opera-
ting frequencies is the output power level which can be adjusted to a reference level by means of the front panel PWR SET control and the AVERAGE POWER meter. A portion of the signal generator output is detected by a linear detector whose 'detected envelope' output can be displayed on the MM-504 Oscilloscope for examination of the pulse characteristics. The front panel PRR coarse and vernier controls enable the repetition rate of the generator output pulse pairs to be varied from 4 to 4000 pulse pairs per second, whilst the VAR and NOM controls provide a fixed 12 or $36 \mu \mathrm{sec}$ pulse spacing or a variable pulse spacing $\pm 3 \mu \mathrm{sec}$ with a mean of 12 or $36 \mu \mathrm{sec}$. A synchronization pulse triggers the oscilloscope $3 \mu \mathrm{sec}$ before the generation of the interrogation pulse pair. When an external pulse generator is used to control the pulse repetition rate, the PRR coarse control is set to its EXT TRIG position.

## 2. OSCILLOSCOPE MM-504 (Fig 4-12a).--

This unit is a general purpose, high performance oscilloscope designed to operate in a wide range of environmental conditions. Sweep trigger may be from a recurrent source within the unit or from an external source. The sweep speed may be varied over the range 5 seconds to 0.1 microseconds $/ \mathrm{cm}$ in calibrated steps although a variable facility enables an uncalibrated sweep rate at least 2.5 times the TIME/CM switch settings. The vertical amplifier bandwidth (at the -3 db point) is DC to 30 MHz , or greater when cascaded with Channel 1 . Timing markers are provided by the Marker Generator (part of the Power Meter Pulse Counter Marker Generator MM-109) and are synchronized with the associated oscilloscope sweep and may be positioned upon the waveshape being viewed. Each tenth marker is automatically brightened. A COUNTER/MARKER SELECT switch is located on the front panel of the MM109 and enables selection of marker pulses at intervals of 0.5 , $1 \cdot 0,10,100,1000$ and $10.000 \mu \mathrm{sec}$. The calibration voltage enables peak-to-peak amplitude measurement over the range of 0.2 mV to 100 V (square waves) in 18 steps, and 100 V DC.

## 3. POWER METER - PULSE COUNTER -

MARKER GENERATOR MM-109, (Fig 4-1 2a). -- Whilst constituting one chassis within the MM-TMC-212A Group, the MM-109 comprises three separate functions as follows:-
a. POWER METER. This measures the peak r.f. power output of the beacon and associated test equipment, in the frequency range 960 to 1215 MHz . The meter is used in conjunction with the Transfer and Switching Unit MM-1602 which. in this instance of its use, provides the necessary facilities for sampling the transmitter output-signal and interrogation pulses. Sample pulses are routed via the Spectrum Analyzer/Test Generator, MM-705, reference attenuator and fed into diode detector network CR1 of the Peak Power Dectector. The resultant video output, which is from $-0 \cdot 3$ to $-1 \cdot 1 \mathrm{~V}$ peak, is fed to the various stages of the Peak Power Detector where it is amplified, sampled at the pulse peak and fed to a peak power/input level amplifier as a d.c. voltage whose amplitude is proportional to the peak amplitude of the input pulse. The output of the peak power/input level amplifier is applied across the PEAK RF POWER meter, which is calibrated in watts.
b. PULSE COUNTER. Whilst it can be used as an individual unit, the pulse counter/timer is incorporated within the TMC 212A to measure the average repetition rates of all the pulse sources of the beacon. The unit provides a direct readout of the number of pulses counted up to a total of 99 . 999 at a pulse spacing of $0.5 \mu \mathrm{sec}$, or more, as required for the following:-

1. North Burst interval; hence, indirectly, antenna speed.
2. Auxiliary Burst interval.
3. Reference Burst Count.
4. Squitter Count.
5. Total Pulse Count.
6. Receiver Reply Count.
7. Identity tone and burst pulse count.

After initial amplification the pulses to be counted are applied, via various switching routes, to the Counter Control circuit which is the heart of the system and creates all commands. After further processing the puises are fed to the counter MAIN gate and then to the Decade Counting Unit where they are usec to trigger a series of flip-flops which, in turn, change the conditions of a set of AND gates associated with the Nixie indicator tubes.

The display time is variable from 0.5 to 30 seconds and means are provided to 'hold' the display indefinitely.
c. MARKER GENERATOR. The unit provides marker pulses at six intervals of $0.5,1 \cdot 0,10,100$, and 10,000 $\mu \mathrm{sec}$. Each tenth marker is automatically brightened for easier measurement of pulse intervals although the first brightened marker appears after the ninth interval.

The marker generator operation is controlled by two external inputs. Input 1 requires a positive-going pulse to start the generator whilst input 2 requires a negative-going pulse to stop it. For simplification both inputs are connected to the positivegoing intensity gate of the oscilloscope; the leading edge is usec to start the generator and the trailing edge to stop it.

When operated into the oscilloscope Z-axis, through the inter-unit cable harness, the marker rise- and fall-times and pulse widths vary according to the markers selected, but in general provide a mark-space ratio of $30: 1$. The nominal pulse widt is stable to $\pm 20 \%$. Accuracy of the marker intervals is dependent upon the stability of the Marker Generator 2 MHz oscillator and means are provided internally to check its
accuracy against the Pulse Counter frequency standard. A front panel control is used to adjust the Marker Generator oscillator to precisely 2.0000 MHz provided a 5 -minute warmup is allowed prior to adjustment.
d. TRANSFER AND SWITCHING UNIT MM-1602 (Fig 4-12a).- Although not actually part of the test equipment this unit, in response to a command from the TELOTEL, provides automatic transfer of TACAN beacons between antenna and dummy load and between beacons and test equipment. The transfer circuitry has an adjustable delay of approximately 1 second, initiated by a transfer command from the transfer control unit which, at the same time, opens the high voltage control line by actuating a relay. When the delay time expires, beacon transfer occurs and once completed, the high voltage control line is restored to that beacon which is connected to the antenna. The transfer and switching function also selects the identity keyer signal of the beacon connected to the antenna and routes it to the monitors, provides primary and standby pre-trigger logic switching and XPONDER ON ANT indication operation. The transfer time delay is incorporated to allow the main line RF to completely decay prior to transfer.

The unit also includes the following facilities:

1. An adjustable coupler, MM-801, which provides coupling to the main RF line for the purpose of injecting monitor interrogations.
2. A critical-switches-mis-set function whereby, providing certain critical switches in the Spectrum Analyzer/Test Generator and Transponder Monitors are correctly set, a NORMAL indication is shown on the front panel. If any critical switch is mis-set, continuity is lost, a relay is de-energized and a MIS-SET indication is shown on the front panel.
3. A manual switching facility is also incorporated in the event of automatic transfer failure.
e. TRANSFER AND STATE TRANSMISSION

UNIT (TELOTEL) and INTERFACE. (Fig 4-12a).- These units provide the facility whereby, on receiving an alarm signal (confirmed by both of the Transponder Monitors) of any beacon parameter failure, the unit sends a command signal to the Transfer and Switching Unit thereby initiating a transfer of beacons between antenna and dumny load. The unit is also capable of accepting specific failure data from the Monitors and other nonelectronic parts of the system (eg frequency converter) and transmitting indication of such a failure to a remote indicator.

Facilities are also provided whereby the unit can automatically call a central station, remote from the installation, and pass such failure data as it has received.

## f. TACAN TRANSPONDER MONITOR MM-209

 (Fig 4-12a).- There are two of these units within the MM-TMC-212A MONITOR CONTROL RACK and they are interconnected such that a failure must beregistered by both units before an alarm condition is signalled.

The units automatically provide, every 4 seconds, a detailed analysis of 13 TACAN transponder parameters and upon detecting a fault in any parameter, the monitor will automatically 'lock on' to that parameter and sample it continuously until either the fault clears or, after a short delay period, an alarm condition is registered and a transfer or shut-down, as the case may be, is initiated. If the failure is intermittent or temporary and the beacon returns to proper operation prior to the end of the alarm delay time, the monitor will accept the parameter and advance to the next parameter and at the same time reset the alarm delay circuitry.

In addition, the monitor provides quick, easy readout of important counts or measurements, which results in a considerable decrease in routine maintenance time.

The following operational characteristics are evaluated by the monitor.

1. General Transponder operation.
(a) Pulse pair spacing
(b) Receiver sensitivity
(c) System replay delay
(d) Average peak radiated power
(e) Average pulse rate.
2. Azimuth information.
(f) North reference.burst count
(g) Auxiliary reference burst count
(h) North reference burst spacing
(i) Auxiliary reference burst spacing
(j) 15 Hz azimuth deviation
(k) 135 Hz azimuth deviation
3. Identity functions
(1) Identity pulse spacing
(m) Equalising pulse spacing
(n) Keyer operation
(o) Failure of identity tone
(p) Continuous identity tone
4. Antenna function
(q) Antenna rotation rate

All of the monitoring functions are indicated at the front panel except those of $2(\mathrm{~g})$ and ( h ) and $3(n)$. The continuous identity tone and identity tone failure functions have been combined in one indicator.

All beacon parameters are monitored digitally with the exception of average radiated peak power, continuous identity signal and failure of identity signal. When a beacon parameter has failed and the monitor units have initiated an alarm, and transfer, the fault is held in memory.
b. CIRCUIT ANALYSIS.

## (1) RADIO RECEIVER R-824/URN.

(a) MIXER AND PREAMPLIFIERS. (See
crystal circuit. The low-pass filters in series with the meters prevents extraneous signals in the i-f pass band from entering the i-f amplifiers.

The output of the mixer is applied to the control grid (1) figures 4-13 and 4-14.)-The distance interrogation pulse pairs pass of first preamplifier stage V201 (figure 4-14). Slug-tuned coil through low-pass filter $\mathbf{Z 5 0 1}$, which rejects frequencies between 1650 and $10,000 \mathrm{mc}$ and passes interrogations to the mixer stage of the receiver (figure 4-13). A local oscillator signal from the frequency multiplier-oscillator in the transmitter is also applied to the mixer stage. At the mixer stage, the local oscillator signal, distance interrogations, and random noise pulses generated in the mixer itself are combined to produce an i-f signal of 63 mc . output of the mixer stage, consisting of distance interrogation pulse pairs have pulses spaced 12 microseconds apart and random noise pulses at a random spacing, is fed to the preamplifiers (figure 4-14).

The output of $\mathbf{Z} 501$ is fed into one arm of the coaxial hybrid balanced T-type mixer; local oscillator power from the frequency multiplier-oscillator stage is fed into the other mixer arm. Essentially, all power put into the mixer and local oscillator arms is delivered to two crystal mixers CR201 and CR202. The balanced signal output of the mixer plus random noise is fed through impedance-matching transformer T201 to the grid of tube V201.

To facilitate metering the current in the crystal mixers, position CR201 or CR202 of METER SELECTOR switch S501 connects the receiver panel meter to the appropriate

L206 in the plate circuit of tube V201 is tuned to 63 mc . The combination of coils L206, L209, L210, and L211 produces a relatively flat i-f response centered at 63 mc . The signal is amplified in stage V201 and applied to the cathode of grounded grid amplifier V202.

The signal is further amplified in stage V202. Bias voltage for stage V202 is developed by the flow of cathode current through registor R205 which is bypassed by capacitor C210; the combination of resistor R205 with coil L205 and transformer T201 forms the d-c grid return path for tube V202. Coupling between tubes V202 and V203 is provided by a Tequivalent of a para-llel-tuned transitionally coupled transformer. Slug-tuned coils L209 and L210 are tuned to 63 mc . The signal is applied to the control grid of final preamplifier V203.

Stage V203 further amplifies the signal. The plate load for stage V203 is a parallel resonant circuit consisting of the tube's output capacitance, coils L211 and L213, and capacitors C221 and C220. The output voltage is obtained across coil L213 and capacitors C220 and C221 at a low impedance level


Figure 4-I3. Radio Receiver R-824/URN, Hybrid Balanced Mixer, Simplified Schematic Diagram


Figure 4-14. Radio Receiver R-824/URN, Preamplifier, Simplified Schematic Diagram
that matches the 50 -ohm coaxial line feeding the signal to the following stage, first $i-f$ amplifier V301.
(b) I-F AMPLIFIERS. - The receiver i-f amplifiers (figure 4-15) increase the amplitude of the signal and noise received from the preamplifiers to a level sufficient to operate the Ferris discriminator. A variable negative bias (squitter-control voltage), dependent on the number of interrogation and noise pulses out of the receiver, is applied to first and second i-f amplifiers V301 and V302. This negative voltage controls the gain of these stages and thereby controls the number of pulses out of the receiver. Also, echo-suppression circuits that allow operation of the equipment in the vicinity of large reflecting objects are employed in the i-f amplifiers.

The signal output of the preamplifier stages is applied to the control grid of i-f amplifier V301. The input circuit to the control grid of tube V301 consists of capacitor C304, coil L301, capacitor C302, coil L302, and the input capacitance of tube V301. Inductance coil L302 and the tube capacitance form a series resonant circuit which provides a stepup in voltage and impedance from the 50 -ohm coaxial line. Because of the impedance matching afforded by the circuits at the input and output of the coaxial line, the i-f response is substantially independent of the cable length between the preamplifier and the i-f amplifier.

The i-f voltage is amplified in tubes V301 through V303. Inductance coils L303 through L306 are stagger tuned to center the i-f response around 63 mc and to provide an i-f bandwidth of 2 mc .

A negative bias (squitter-control voltage equal to approximately -5 volts under normal operating conditions) is applied to the control grids of tubes V301 and V302. The squitter-control voltage is derived in circuits of the video amplifier chassis of the receiver and is dependent on the number of interrogation and noise pulses received. The total number of pulses out of the receiver must be 2700 per second to sustain the sine-wave modulation envelope of the transmitted $r$-f carrier. When the total number distance interrogation pulses and noise pulses passing through the decoder falls below 2700 pulses per second, the squitter-control voltage is made less negative and greater i-f amplification results. Therefore, the number of pulses sufficiently amplified to pass through the coincidence decoder is increased to the point where the receiver output is 2700 pulses per second. If the number of distance interrogations received is more than 2700 pulses per second, the squitter-control voltage is made more negative and the i-f gain is reduced to the point where the excess interrogations are not amplified sufficiently to pass through the coincidence decoder.

Echo suppression is obtained by means of RC discharge networks in the grid circuits of V302, V304, and V305. Thus, in the presence of large signals, networks C308 and R304, C320 and R315, C328 and R319 each develop sufficient bias voltage to reduce the i-f gain for a period proportional to the signal level input.
(c) FERRIS DISCRIMINATOR. -The Ferris discriminātor circuit (figure 4-16) consists of highand low-Q $63-\mathrm{mc}$ tuned input tank circuits, two detecting diodes, and the r-f bypass and voltage divider loading network. The two clamping diodes and two video amplifiers associated with the Ferris discriminator are included in figure 4-16 and explained in conjunction with the Ferris discriminator.

The Ferris discriminator circuit receives its input signal from the final i-f amplifier, V305. Its function is to detect the i-f signal and provide adjacent and near-adjacent channel rejection. The tank circuits are tapped at low impedance points; therefore, the tank circuits are relatively unaffected by differences in diode tube capacitance. In addition, the circuits are temperature compensated to maintain frequency stability over the temperature range of from $-54^{\circ} \mathrm{C}\left(-65.2^{\circ} \mathrm{F}\right)$ to $+85^{\circ} \mathrm{C}\left(+185^{\circ} \mathrm{F}\right)$. The circuit functions as follows: Both tank circuits feeding tube V306 are tuned to 63 mc . Because of loading differences, the $\mathbf{Q}$ of the tank circuit feeding tube V306B is reduced to approximately one-third the $Q$ of the tank circuit feeding tube V306A. Each half of tube V306 has a different frequency characteristic because of the differences in the signal developed by each tank circuit and the voltage-dividing connection to tube V306. Tube V306A and its associated tank will pass only a negative-going narrow band of frequencies centered at 63 mc . The characteristics of the tube V306A tank circuit are shown in waveshape A of figure 4-17. Tube V306B and its associated tank will pass a positive-going wider band of frequencies also centered at 63 mc . The characteristics of tube V306B are shown in waveshape $B$ of figure 4-17. The algebraic sum of the voltages at the input to the first triode amplifier is shown in figure 4-17. With the sum bandwidth and negative signal passing characteristics of the Ferris discriminator, as shown in waveshape $C$ of figure 4-17, it can be seen that this circuit will only pass negative-going pulses in a narrow band of frequencies centered at 63 mc .

The output of the detecting diodes is coupled through capacitor C362 to the control grid of tube V307A and plate of tube V308A. If the incoming pulses are negative-going, tube V308A will remain inoperative and the signal will be amplified by tube V307A and passed on to tube V307B. If the incoming pulses are positive-going, tube V308A will go into conduction, shorting grid control resistor R329 and passing the positive pulses to ground. The positive portion of the signal is further rejected in stages V307B and V308B, which act in a manner similar to tubes V307A and V308A, taking into account the $180-$ degree phase inversion that took place in tube V307A.

The signal is then applied through plug P302 and jack J402 to the first video amplifier V402A in the video amplifier chassis.
(d) VIDEO AMPLIFIERS. - The video signal and noise pulses from the i-f amplifier chassis are routed through jack J402 to the control grid (2) of the first video amplifier V402A (figure 4-18). The video



Figure 4－16．Radio Receiver R－824／URN，Ferris Discriminator，Simplified Schematic Diagram


Figure 4-17. Radio Receiver R-824/URN, Ferris Discriminator, Continuous-Wave Response Curve
signal is amplified and passed through coupling capacitor C401 to the control grid (1) of the blanking gate tube V401.

The output of the i-f amplifier chassis, which is the input of the first video amplifier, can be checked at test point TP5 (Jack J409).

The blanking gate, which functions as a gate-blanked video amplifier, amplifies the signal and feeds it through coupling capacitor C402 to the control grid (7) of final video amplifier V402B.

After every pulse pair is decoded however, a negative 40 microsecond blanking pulse from the blanking-gate amplifier is applied to the suppressor grid of tube V401, blanking out tube V401 and preventing pulses from passing through it. Tube V401 is also blanked out by a positive blanking pulse to its catloode circuit from the transmitter whenever the klystron is keyed on.

The second video amplifier V402B further amplifies the signal, which is then fed to a coincidence-type decoder tube V403 through coupling capacitor C403 directly to the suppressor grid (7) and through 12-microsecond delay line DL401 to the control grid (1).
(e) COINCIDENCE DECODER. -- Coincidence decoder V403 (figure 4-19) is a semi-remote cutoff pentode biased to cutoff by a positive voltage applied to its cathode.

As used in this circuit, conduction of tube V403 requires a simultaneous positive voltage on both the control grid (1) and suppressor grid (7). The circuit functions in the following manner: each pulse from tube V402B is applied first to the suppressor grid of tube V403 and then through a 12-microsecond delay line to the control grid of tube V403.

When a pair of interrogation pulses or random noise pulses separated by 12 -microseconds arrives at the decoder, the arrival of the first pulse, delayed by 12 -microseconds, at the control grid is coincidental with the arrival of the second pulse at the suppressor grid. The decoder conducts when the second pulse of a pulse pair is on the suppressor grid and the first pulse is on the control grid. This characteristic ensures the decoding of pulses (noise or interrogations) separated by 12 -microseconds. However, it should be noted that since the decoder is biased to cutoff, the strength of the pulse input must be sufficient to cause conduction. This means that only those 12 -microsecond spaced noise or interrogation pulse pairs above a minimum value will be decoded. The number of pulses above this value is controlled by varying the i-f gain with the squitter-control voltage. The receiver is designed to maintain this number rate at $2700 \pm 90$ pulses per second. The decoder out put consists of a single pulse for each decoded pulse pair. These pulse trigger one-shot multivibrator V404.
(f) ONE-SHOT MULTIVIBRATOR. - One-shot multivibrator V404 (figure 4-20) is triggered once for each pulse received from the decoder tube. The pulses out of the one-shot multivibrator are all of equal amplitude and width. Stage V404 output is routed to three different stages. The plate (4) output of tube V404 is fed to blanking one-shot multivibrator V406. The cathode (2) output is routed to two different stages: one to pulse amplifier V408 (squitter-voltage generator stage) and the other to cathode follower V405 (receiver output to the coder-indicator).
(g) BLANKING GATE GENERATOR. - Blanking gate one-shot multivibrator V406 (figure 4-21) is triggered by one output of multivibrator V404. Tube V406 supplies a 40 microsecond blanking pulse for each pulse received from multivibrator V404. Blanking time adjustment potentiometer R443 controls the blanking time from 20 to 65 microseconds by changing the time constant of the multivibrator R-C network. Equipments as delivered have the blanking time preadjusted at 40 microseconds. The 40 -microsecond pulse output is fed to blanking gate amplifier V407B.

Blanking gate amplifier V407B is heavily biased by the application of a fixed negative bias on its grid; conduction takes place only on strong positive pulse signals. Because of the 180-degree phase inversion in the tube, a negative output pulse of 40 -microsecond duration is produced. This pulse is applied to the suppressor grid of gating tube V401, causing tube V401 to cut off for 40 -microseconds. Therefore, a receiver output with a minimum of 65 -microsecond spacing between pulses is accomplished due to the sum of the 40 - and 10 -microsecond blanking from the frequency multiplier oscillator.


Figure 4-18. Radio Receiver R-824/URN, Video Amplifier, Simplified Schematic Diagram


Figure 4-19. Radio Receiver R-824/URN, Coincidence Decoder, Simplified Schematic Diagram
(h) SQUITTER VOLTAGE GENERATOR. The second output of tube V404 feeds pulse amplifier V408 (figure 4-22). Grid limiting is used in this stage to keep its output substantially independent of the amplitude of the input pulses. The output of amplifier V408 is fed by transformer T401 to the pulse stretcher and counter diode V409B.

The long time constants of the R-C networks in the plate circuit of pulse stretcher diode V409B make the voltage on the grid of tube V407A essentially dc. The cathode of tube V407A is connected through potentiometer R426 to the -105 -volt source. When the bias voltage on the grid of tube V407A is the value required to effect a squitter rate of $2700 \pm 90$ pulse pairs per second, the voltage on the cathode, because of the drop across R426, is approximately -5 volts with respect to ground. This voltage, which is the squitter-control voltage, is applied to the grids of i-f amplifiers V301 and V302 and controls the i-f amplifier gain. If the receiver pulse output tends to fall below $2700 \pm 90$ pulses per second, the number of pulses fed to pulse amplifier V408 also decreases. This condition results in a lower d-c output from pulse stretcher diode V409B and a less negative bias on the grid of tube V407A. Increased current flow in this stage results in a greater voltage drop across potentiometer R426 and consequently a less negative voltage at the cathode of tube V407A with respect to
ground. This reduced squitter-control voltage to the i-f amplifiers results in an increase in the level of the signal reaching the decoder. Therefore, a greater number of decodable pulses attain enough amplitude to operate the decoder and bring the receiver output back up to $2700 \pm 90$ pulses per second. If the pulse output tends to rise above $2700 \pm 90$ pulses per second, the circuit operates in the opposite manner, increasing the negative squittercontrol voltage to the i-f amplifiers. Potentiometer R427 is used for squitter-voltage adjustment.

Without the application of a negative bias to the grid of tube V407A, the voltage drop across potentiometer R426 may result in application of a high positive voltage (in excess of +20 volts) to the i-f amplifiers. This would result in a complete blocking of the receiver. Therefore, tube V409A is used as a d-c clamp and prevents the voltage from rising above +5 volts while the receiver is warming up. As soon as pulses are decoded, the applied bias to tube V407A reduces the voltage drop across potentiometer R426 and the squitter-control voltage becomes negative; tube V409A then has no effect.
(i) RECEIVER OUTPUT CATHODE FOLLOWERS. - The third output of V404 is to cathode follower stage V405 (figure 4-20). V405 is a twin triode; one triode output is not used at this time. The


Figure 4-21. Radio Receiver R-824/URN, Blanking Gate Generator, Simplified Schematic Diagram


Figure 4-22. Radio Receiver R-824/URN, Squitter Control Voltage Regulator, Simplified Schematic Diagram
output of stage V405, consisting of decoded distance interrogations and random noise pulses at a $2700 \pm 90$ pulse per second rate with a minimum of $65-$ microsecond spacing between pulses, is the receiver output. It is fed through jack J404 to the input of the coder-indicator. This output can be checked at jack J411. A sample of the output is also brought out to the front panel of the receiver through TEST OUTPUT jack J507.

## (2) CODER-INDICATOR KY-382/GRN-9D.

## (a) 135-CPS REFERENCE BURST

GENERATOR. - This stage consists of tubes V601A, V609, and V610. Figure 4-23 illustrates the 135-cps reference generator. Pulse amplifier V601A receives the trigger pulse from the $135-\mathrm{cps}$ pulsing coil of the antenna system. Since its cathode is grounded, bias to pulse amplifier V601A is zero. The trigger pulses from the antenna contain both positive and negative excursions; the polarity is chosen so that the positive occurs first. When fed into tube V601A, the positive excursion is clipped; grid current produces a voltage drop across potentiometer R658, reducing the net signal at the grid to almost zero. When the trigger pulse from the antenna is negative, a sharp change in plate current occurs. This sharp change triggers multivibrator V609, which functions as a $135-\mathrm{cps}$ gate. Stage V609 is a one-shot keying multivibrator which, because of the circuit constants used, has a natural period longer than the time required for the generation of six pulses by the 41. 7-kc pulsed oscillator. When tube V609 is in a stable condition, tube V609B is conducting owing to $\mathrm{B}+$ applied to the grid through potentiometer R663. Because of the cathode bias developed across resistor R665, tube V601A is cut off. When a positive pulse is applied to the grid of triode V609A, plate current flows, producing a negative pulse which is coupled to grid pin 2, cutting off the plate current in tube V609B. This action causes development of a positive pulse on the plate of tube V609B and a negative pulse on the cathode. The positive pulse is fed to priority gate V611 as a blocking gate, and the negative pulse keys 41.7-kc oscillator V610. Pulses originating in keyed oscillator V610 are fed back from the output of tube V606 after passing through shaping and amplitude setting circuits to the grid of tube V609A, where they appear as small negative spikes. The natural period of multivibrator V609 is determined by the time constant of the R-C circuit, capacitor C625. Section V609B remains cut off until capacitor C625 charges from the $\mathrm{B}+$ supply through potentiometer R663. The feedback pulses originating in the pulsed oscillator ride on the charging curve of capacitor C625 (figure 4-24). Potentiometer R672 (figure 4-24), provides a means of adjusting the amplitude of the feedback pulses so that the sixth pulse will start tube V609B conducting and cut off the $135-\mathrm{cps}$ keying gate pulse. The spacing between the 135 -cps reference burst pulses is 24 microseconds at this point.

The negative keying gate from the cathode of tube V609B is applied to the grid of pulsed oscillator tube V610A, cutting off this section of the oscillator tube. When tube V610A is cut off, the ringing circuit com-
posed of capacitors C626 and C650, and coil L602 is shock excited to produce a sine wave at a frequency of 41.7 kc to which the ringing circuit is tuned. The signal from the ringing circuit is passed through tube V610B where power amplification takes place. Capacitors C626 and C650 function as a capacitive voltage divider which feeds a portion of the signal voltage developed across Although the voltage gain through a cathode follower is always less than one and signal voltage is reduced because of tapped capacitor division, sufficent feedback voltage from the cathode of tube V610B is provided to the grid circuit of tube V610B to replace tank circuit losses and sustain oscillation. Any greater feedback would drive the tube to cut off and yield a clipped output. When the negative gate on the grid of tube V610A ends, tube V610A conducts and acts as a low resistance circuit which heavily damps the ringing circuit, thus terminating oscillation. The pulsed oscillator remains in a nonoscillating condition until the next negative keying gate is impressed on the grid of tube V 610 A , cutting off plate current, and repeating the cycle as previously described. For each gate pulse applied to the grid of tube V410, 6 cycles of a 41.7 -kc sine wave are produced. This signal is coupled through capacitor C627 and diode CR604 to the grid of tube V604A. Since only the negative portion of each cycle of the sine wave is required, diode CR604 is inserted in series with the signal path and limits the sine wave to a series of negative pulses, and, in conjunction with diode CR605, isolates the $15-\mathrm{cps}$ and 135 -cps pulsed oscillators.

The 135 -cps reference burst pulses from the 41. 7 -kc keyed oscillator are amplified in reference burst amplifier V604A, the output of which is coupled to one-shot multivibrator V605.

## (b) 15-CPS REFERENCE BURST

 GENERATOR. - The operation of this circuit consisting of tubes V601B, V602, and V603 is similar to that of the 135 -cps reference burst generator. However, a $33.3-\mathrm{kc}$ keyed oscillator is employed and the output consists of 12 pulses spaced 30 microseconds apart. Like the 135 -cps reference burst generator, the $15-\mathrm{cps}$ reference burst generator sends blocking pulses to the priority gate and passes its output through reference burst amplifier V604A to one-shot multivibrator V605.(c) SHAPING AMPLIFIERS. - This stage consists of one-shot multivibrator V605 and triggered blocking oscillator V606 (figure 4-25). Dual triode V605 is a one-shot multivibrator which receives interrogation signal pulses from priority gate V611 and reference bursts from amplifier V604A. Triggering signal pulses to the multivibrator vary in amplitude and waveshape, while output pulses are of uniform amplitude and waveshape. The time spacing of multivibrator output pulses are an exact duplicate of the trigger pulses. In the stable condition, multivibrator V605B conducts because of a positive bias applied to grid pin 7 through potentiometer R623. Plate current through potentiometer R625 produces a positive voltage on the cathode of triode V605A, which biases this half of tube V605 to cutoff. When a



Figure 4-24. Coder-Indicator KY-382/GRN-9D, V609B Grid Voltage Curve During Charge Time of C625
positive trigger is applied to grid pin 2, triode V605A conducts and passes a negative pulse to grid pin 7 which cuts off triode V605B. Multivibrator V605 is then in the unstable condition until capacitor C611 discharges through potentiometer R623, causing grid pin 7 to go positive. Multivibrator V605 then returns to the stable condition, with triode V605B conducting and triode V605A cut off. The time required for the multivibrator to go through one complete cycle is determined by the time constant of R-C circuit, consisting of potentiometer R623 and capacitor C611. Multivibrator V605 is triggered by positive pulses from reference burst amplifier V604A applied to grid pin 2, and by negative pulses from priority gate V611 applied to grid pin 7. Negative pulses are taken from plate pin 1 of tube V605A and shaped by the network of capacitor C630 and resistors R674, R675, and R676 to provide sharp negative spikes for timing the 15 -cps reference burst generator V602 as explained previously. (Negative pulses from priority tube V611 may pass through the same network to the input of tube V602 but have no effect on the multivibrator because triode V602A is already biased to cutoff during the time priority tube V611 is passing pulses.)

Sharp positive pulses from multivibrator V605 excite triggered blocking oscillator V606. In its quiescent stage, both sides of tube V606 are cut off by negative bias applied to both grids through voltage divider resistors R632, R633, and R634. A sharp positive pulse on the grid of triode V606A causes a pulse of plate current to flow through the primary of transformer T602. While the plate current is increasing from zero in the primary of transformer T602, the secondary of transformer T602 develops a positive voltage on the grid of triode V606B; this causes plate current to flow through triode V606B
and the primary of transformer T602. This additional increase in current in the primary of transformer T602 causes a further increase in the positive voltage induced in the secondary of transformer T602 and applied to the grid of tube V606B. This action continues until the plate current of triode V606B has reached saturation and no further increase in plate current is possible. Since a positive feedback voltage is induced on the grid only while current through the primary of transformer T602 is increasing, the grid swings back in the negative direction toward its original voltage, thereby reducing plate current through triode V606B. Current through transformer T602 is now changing in a direction which induces a negative voltage on the grid of tube V606B.

This action continues until triode V606B is biased to cutoff. Potentiometers R627 and R629 across transformer T602 produce a damping effect, allowing the oscillator to operate effectively for only 1 cycle on application of each trigger pulse. Triode V606A is not actually a part of the oscillator, but primarily acts as a trigger amplifier converting sharp pulses of voltage from tube V605 into sharp pulses of current in transformer T602. The output signal of the blocking oscillator is developed across resistor R625 and is fed to the primary of transformer T603.
(d) ENCODING DELAY LINE. - The output pulses of tube V606 are coupled to delay line DL601 (figure 4-26) through transformer T603. Choke coil L604 and capacitor C614 filter out reflections from the input circuit delay line DL601. Transformer T603, an auto-transformer, matches the input impedance of encoding delay line DL601 and delivers a signal of approximately 500 volts peak-to-peak to the input of the encoding delay line.



Figure 4-26. Coder-Indicator KY-382/GRN-9D, Double Encoding Circuit, Simplified Schematic Diagram

Pulses having an amplitude of approximately 15 volts peak-to-peak are tapped from encoding delay line DL601 after 32-microsecond delay and after a $44-$ microsecond delay. For each pulse input to encoding delay line DL601, two positive pulses spaced 12 microseconds apart are delivered to the grid of pulse amplifier V607A. Pulse amplifier V607A inverts and amplifies the doubled pulses from encoding delay line DL601.
(e) OUTPUT AMPLIFIERS. -These circuits include tubes V615 and V607B (figure 4-27).

The negative pulse output of pulse amplifier V607A is applied to one-shot multivibrator stage V615. The output of V615 consists of 1.5 -microsecond pulses. Multivibrator V615 delivers one pulse to tube V607B for each pulse it receives. In the quiescent stage, because of negative bias applied to the grid of the V615B half of the multivibrator, tube V615B is cut off and tube V615A is conducting.

The application of negative pulses from tube V607A to the control grid (2) of tube V615A drives tube V615A into cutoff. Its rise in plate voltage is coupled to the grid (7) of tube V615B and drives that half of the multivibrator into conduction. The period of conduction of tube V615B is 1.5 microseconds as determined by the RC time constant of capacitor C621 and potentiometer R639. At the end of the $1.5-$ microsecond period, tube V615A goes into conduction, cutting off tube V615B. The multivibrator remains in this condition until the application of the next negative input pulse.

Cathode-follower stage V607B receives the uniform positive output pulse of tube V615. The positive input pulse to stage V607B causes the state to conduct. The output of stage V607B is taken off cathode resistors R649 and R650. The output of tube V607B, consisting of the north reference burst, auxiliary reference burst, identification time, distance interrogations and random noise pulses, is fed through jack J602 and plug P407 to the transmitter. The output pulses of tube $V 607 \mathrm{~B}$, which are the output of the coder-indicator, are pulse pairs having pulses 12 microseconds apart and 1.5 microseconds wide. Cathode follower V607B isolates multivibrator V615 and matches the output to the 50 -ohm load which feeds the signal to the transmitter.

A portion of the output of tube V607B, taken off resistor R650, is delivered to TEST OUTPUT jack $J 607$ on the front panel of the coder-indicator and enables the operator to examine the output of the unit.

## (f) IDENTIFICATION CALL MECHANICAL

KEYER. - The motor-driven code keying wheel controls the selection of either distance reply or identification tone pulses as input signals to priority gate V611 (figure 4-28).

The keying wheel, in coniunction with the code start timing cam, initiates a beacon identification coded call every 37.5 seconds. The keying wheel revolves at a speed of 8 rpm . Sections of the wheel are set farther from its center to indicate selection of a dot or dash. Each set section causes the keying


Figure 4-27. Coder-Indicator KY-382/GRN-9D, Output Amplifier, Simplified Schematic Diagram
switch S 607 connection to the B - voltage divider to open.

The B- voltage divider produces, by the action of potentiometers R788 and R686, a gate potential of -50 volts whenever it is not grounded through the identification call mechanical keyer. The keying switch removes the ground connection from the $B$ voltage divider to initiate a dot or dash tone pulse. When the B- voltage divider is grounded, distance reply pulses are selected as the input to the priority gate.

Code start timing switch 5604 is controlled by a cam revolving at 1.6 rpm . This spdt timing switch grounds either the B- voltage divider or one side of the keying switch. The timing switch control cam is designed so that the timing switch will ground one side of the keying switch for one of every five revolutions of the code keying wheel.

With one side of the keying switch connected to ground through the timing switch, the mechanical action of the keying switch will control the application of ground potential ( 0 volt) to the B - voltage divider.

Both the keying switch and the timing switch connections from the $B$ - voltage divider to ground must be open simultaneously to produce a code tone pulse. Therefore, no code tone pulses are possible during the time the timing switch applies ground potential to the B- voltage divider. This condition exists for
the four revolutions of the keying wheel directly following each cycle initiating a beacon identification call.

Potentiometer R687 and capacitor C637 form a filter circuit that suppresses extraneous pulses generated by the make and break of keying contacts in the mechanical keyer.

From the preceding explanation, it is evident that the identification call keying wheel alternately keys the distance reply pulses and identification call tone, permitting only one of these two signals to reach the grid of priority gate V611 at any one time.
(g) GATE BLOCKED DISTANCE REPLY AMPLIFIER. - The application of either ground potential or -50 volts from the B - voltage divider controls the operation of tube V604B, the gateblocked distance reply amplifier (figure 4-28). When the grid resistor for tube $V 604 \mathrm{~B}$ is returned to -50 volts, the tube is biased beyond cutoff and therefore blocks passage of the distance reply pulses. When the action of switch S 607 or switch S 604 returns the grid resistor to ground, tube V604B functions as a cathode follower and passes distance reply output pulses to priority gate V611.
(h) KEYED 1350-CPS TONE GENERATOR. The circuit consists of tubes V612, V613A, V614, and V613B and capaeitor CR603 (figure 4-29).


Figure 4-28. Coder-Indicator KY-382/GRN-9D, Control Function of Identity Call Mechanical Keyer, Simplified Schematic Diagram

The identification call tone of 1350 cps is generated by oscillator V612. Coil L603 is adjusted to provide the proper inductance for oscillation at 1350 cps . A positive-synchronizing $135-\mathrm{cps}$ pulse from the 135 -cps reference burst generator is applied to triode V612A. The plate load circuit for this tube consists of capacitors C652 and C653, and coil L603, which form a parallel resonant circuit tuned to 1350 cps , i.e., the tenth harmonic of the $135-\mathrm{cps}$ pulse. The same LC combination also serves as the tank circuit for Hartley oscillator stage V612B. The output of the oscillator appears across potentiometers R692 and R693, and is coupled to tube V613A through capacitor C641.

Stage V613A amplifies and shapes the tone signal so that it can be used as a trigger for multivibrator V614. Potentiometer R798, which in conjunction with potentiometer R797 and capacitor C643 determines the period of one-shot multivibrator V614, is adjusted to provide a period of 100 microseconds. An output pulse is taken off each plate of the multivibrator and is differentiated and combined to produce sharp negative pulse pairs on the grid of identification call keyer tube V613B.

The manner in which two sharp negative pulses are obtained from each cycle of multivibrator V614 is shown in figure 4-30. Waveshape No. 1 shows the voltage changes on plate pin 6 of triode V614A as the multivibrator goes through two complete cycles, due to the application of two trigger pulses. In the quiescent state of the multivibrator, triode V614A is cut off and plate voltage is at +250 volts, the full $B+$ supply voltage. At the instant a trigger pulse is applied, plate voltage at pin 6 takes a sharp negative swing. This sharp negative change is passed through capacitor C645 as a negative spike as shown in waveshape No. 2 of figure 4-30. At the end of the period of multivibrator V614, the plate voltage on pin 6 changes in a positive direction until it is back to +250 volts. Since the change in the positive direction is relatively slow, a small positive pulse is passed through capacitor C645 to the grid of triode V613B as shown by waveshape No. 2 . Waveshape No. 3 shows the change in plate voltage of triode V 614 B , which is pulsed in the positive direction during the period of multivibrator V614. A positive pulse is derived through capacitor C644 during the rise in plate voltage, and a negative pulse is derived through capacitor C644 during the fall in plate voltage. Since the change in the negative direction is very sharp as compared with



Figure 4-30. Coder-Indicator KY-382/GRN-9D, Development of Pulse Pairs on Grid of V613B
the change in the positive direction, the negative pulse passed through capacitor C644 is much larger than the positive pulse, as shown by waveshape No. 4. Waveshape No. 5 shows the signal present on grid pin 7 of triode V613B because of the addition of waveshapes No. 2 and No. 4. Each pair of pulses is separated by 740 microseconds, with the pulses in each pair separated by 100 mic oseconds. In this manner, a constant duty cycle of 2700 pulses per second is maintained while the tone frequency of 1350 cps is preserved in the form of pulse pairs. Clamping diode CR603 presents a low or high impedance path to ground for the identification call tone signals, depending on the position of the identification call mechanical keyer. When the microswitches in the mechanical keyer assembly are closed, ground is applied to the plate of diode CR603 through potentiometer R687. With the plate grounded, diode CR603 becomes a low impedance path to ground for negative pulses fed to the grid of tube V613B. Therefore, the tone signal is grounded out through the diode and no tone signal pulses will appear at the grid of tube V613B. When the keying wheel assembly removes ground from potentiometer R687, a negative bias of approximately -50 volts from the voltage divider, potentiometers R788 and R686, is applied to the plate of diode CR603. With -50 volts on the plate, diode CR603 will not bypass the negative signal pulses. Under these conditions, keyer tube V613B will receive and pass the 1350 -cps pulse pairs to priority gate V611.
(i) PRIORITY GATE. (See figure 4-31.)When neither reference burst gates, identification call pulses, nor distance reply pulses are present at tube V611, tube V611A has approximately zero bias and tube V611B will be at cutoff with - 10 volts applied to its grid from the voltage divider, resistors R682 and R651 (figure 4-31). If only distance reply or identification call pulses appear at tube V611B, the positive input signals override grid bias, are amplified, and passed on to the shaping amplifiers. However, whenever reference burst pulses are being generated, a positive gate from the reference burst generator causes tube V611A to conduct heavily. This action causes a large voltage drop across potentiometer R 681 which is the cathode bias resistor for tube v611.

This cathode bias, in combination with its fixed -10 -volt grid bias, drives tube V611B so far into cutoff that the positive identification call or distance reply pulses on its grid can no longer override the cutoff bias; these signals are now blocked. Therefore, the priority of the reference burst pulses over the identification call and distance reply pulses is established.

The signals permitted to pass through the priority gate are coupled to the output a mplifier circuits at tube V605. These signals are then shaped, double


Figure 4-31. Coder-Indicator KY-382/GRN-9D, Priority Gate, Simplified Schematic Diagram


Figure 4-32. Coder-Indicator KY-382/GRN-9D, Antenna Synchronization 1350-CPS Oscillator, Simplified Schematic Diagram
encoded, amplified, and sent to the transmitter as components of a multiplexed signal as previously described for the reference burst signals.
(j) ANTENNA SYNCHRONIZATION 1350CPS OSCILLATOR. - The frequency of this oscillator circuit is controlled by tuning fork Y601 (figure 4-32). The 1350 -cps output of the tuning fork output coil is applied to the grid of tube V608A. Part of the tube V608A output is used as a 1350 -cps reference frequency in checking the speed of rotation of the antenna. This voltage is coupled to tube V608B, which acts as a cathode follower with the input coil of the tuning fork as its cathode load. In this manner, the voltage generated within the oscillator circuit and fed back to the tuning fork is sufficient to sustain oscillation.
(3) TRANSMITTER.

## (a) FREQUENCY MULTIPLIER-

OSCILLATOR CV-1171/GRN-9D. -Refer to Section 6 of this manual for complete schematic diagrams of the frequency multiplier-oscillator video chassis and r-f chassis. Figure 4-33 shows a simplified functional schematic of the transmitter output circuits described in the following paragraphs. Figure 4-34 shows the sequence of pulse formation for the radio set.

## 1. CARRIER GENERATING CHAIN. -

 The carrier generating chain, located on the $r-f$chassis, contains a crystal oscillator circuit which originates the radio frequency from which the transmitter carrier frequency and receiver local oscillator frequencies are derived. The oscillator circuit is a Butler or Navy-Type crystal oscillator and frequency doubler stage having an oscillator frequency output of between 40.083333 and 42.6666667 mc for the low-, or between 47.958333 and 50.541667 mc for the highband frequencies. The low- and high-band circuits are similar except for several tuning components which have slightly different values to compensate for the difference in the frequency range to which they must tune. The following discussion refers only to the high-band circuit components. The frequency output of the following circuits is for channel 113, a typical high-band channcl. The frenuency output from the oscillator portion of tube V1501 is 50.000000 mc and the output from the doubler portion of tube V1501 is 100 mc .

An oscillator is basically an amplifier with a positive feedback path. Tube V1501 is a double triode connected as two separate amplifiers. Tube V1501A is a grounded grid amplifier; its input is the crystal frequency developed across potentiometer R1502. The plate circuit of tube V1501A is tuned to the oscillator frequency ( 50 mc ); tuning is accomplished by adjustment of coil L1502. The oscillator frequency is coupled through capacitor C 1504 to control grid pin 3 of tube V1501B. Triode V1501B is an harmonic generator paraphase amplifier. The cathode-follower

# AN/GRN-9D PRINCIPLES OF OPERATION 

output of triode V1501B developed across potentiometer R1503 provides regenerative feedback to the grounded grid amplifier V1501A as necessary to sustain oscillations. The frequency at which feedback takes place is established by crystai v 1501 . The feedback path through the crystal is a low impedance path only at oscillator frequency.

The plate of tube V1501B is tuned to the second harmonic of the oscillator frequency ( 100 mc ). Tuning is accomplished by adjustment of coil L1503. The output is coupled through capacitor C1505 to the second doubler stage V1502.

Coil L1501 is an r-f choke, and capacitors C1501, C1502, and C1503 are r-f bypass capacitors. Potentiometer R1501 is a decoupling resistor for tube V1501A. The combination of capacitor C1506 and coil L1504 ensures that oscillator frequency stability is maintained by cancelling the capacitive component of the crystal circuit impedance. Potentiometers R1504 and R1505 are grid leak resistors. When the TUNING meter selector is set to OSC, the oscillator V1501A grid current is fed through choke coil L1528 to the TUNING meter for checking oscillator grid current.

A frequency of 100 mc , the output of oscillator first doubler stage V1501, is fed to the control grid pin 1 of the second doubler stage V1502. Triode V1502 is tuned to the second harmonic of the input frequency. Tuning is accomplished by adjustment of coil L1509. The output frequency of second doubler stage V1502 is 200 mc and is fed to third doubler stage V1503.

Potentiometers R1507 and R1508 are grid leak resistors. The grid current is fed through choke coil L1530 to the TUNING meter for checking the first doubler output when tuning. Capacitors C1512 and C 1513 are cathode bypass capacitors. Potentiometer R1510 is the cathode resistor. C1514 is a coupling capacitor. and C1515 is a screen grid bypass capacitor. Coil L1508 effectively isolates the plate from the screen while providing a d-c $\mathrm{B}+$ path for the plate. Coil L1509 and capacitor C 1516 form a series resonant circuit which is tuned to the second harmonic of the input frequency of second doubler stage V1502.

A frequency of 200 mc , the output of the second doubler stage V1502, is applied to the cathode of grounded grid amplifier V1503. The output of tube V1503 is coupled through tuned cavity Z1507 to the cathode of the tripler stage V1504. This circuit is tuned to the second harmonic of its input frequency by capacitors C1519 and C1522. The output frequency of this stage, the third doubler stage, is 400 mc . Coils L1510 and L1511 are r-f chokes, capacitors C 1520 and C 1521 are r-f bypass capacitors, and potentiometers R1511 and R1513 are cathode resistors. Cathode current is taken off potentiometer R1513, passes through choke coil L1529, and is fed to terminal 13 of jack J 1509 for checking the second doubler tuning when the TUNING meter selector switch is at 2ND DOUBLER. Capacitors C 1518 and C 1558 are coupling capacitors. The series resonant
tuned output circuit is composed of capacitor C1519, stub Z1507, and capacitor C 1522.

A frequency of 400 mc , the output of third doubler V1503, is fed to tripler stage V1504, which produces an output of 1200 mc . Tripler stage V1504 employs a 2C39A lighthouse tube in conjunction with a broad band coaxial type of resonant circuit.

The third doubler output is fed to the cathode circuit of tube V1504, amplified, and appears with a large third harmonic content in the plate circuit. A coaxial line cavity is connected between the plate and grid of this circuit. The cavity is tuned by means of tuning screws. As the screws are tuned, the capacity applied across the cavity is varied, changing the resonant frequency of the grid plate circuit.

The tripler signal is picked up by loops connected to the grid line. Tripler stage V1504 has two outputs; one is fed to the mixer stage of the receiver to be used as the receiver local oscillator signal and the other is fed to the cathode of first r-f amplifier V1505.

Physically, the grid plate cavity of tripler stage V1504 consists of a concentric line. The shell and the anode cap capacity coupled to it form the outer conductor. The grid line forms the inner conductor. A screw-mounted tuning ring fits into the cavity shell. As the screw is turned, the capacity applied across the cavity is varied, changing the resonant frequency of the grid plate circuit.

Filament voltage is applied to tube V1504 through r-f chokes Z1511 and Z1512. Capacitors C1546 and C1547 are r-f bypass capacitors which effectively place the heater at zero r-f potential.

The output of this final multiplier stage is coupled to first r-f amplifier stage V1505. Circuit analysis of the r-f a mplifier stage V1505 is presented in paragraph 4-3b(3)(a)3.
2. SHAPED PULSE GENERATOR. - Positive pulses from the coder-indicator video chassis are applied to jack J1401 on the frequency multiplieroscillator chassis (figure 4-35). The pulses are 1.5 microseconds wide. This is a considerable portion of the period of multivibrator V1402. To prevent the negative-going trailing edge of the trigger pulse from affecting the operation of multivibrator V1402. crystal diode CR1402 is inserted inseries with the signal path of the trigger pulse. The positive-going leading edge of the trigger pulse is passed through crystal diode CR1402 and triggers multivibrator V1402. Multivibrator V1402 is a monostable multivibrator with triode V1402B conducting during the quiescent state. The grid of tube V1402B is returned to the 250 -volt B+ supply through potentiometers R1403 and R1466. The grid of tube V1402A is connected to a voltage divider consisting of potentiometers R1468. R1446, R1469. and R1407 connected between the +250 - and -375 -volt power supplies. With tube V1402B conducting, plate current flowing through potentiometers R1468 and R1446 causes a drop in voltage at the plate of tube V 1402 B and changes the voltage distribution in the voltage divider so that approximately -30 volts is


Figure 4-33. Radio Set AN/GRN-9D, Transmitter
Output Circuit, Simplified Schematic Circuit


Figure 4-34. Radio Set AN/GRN-9D, Transmitter Pulse Sequence

applied to the grid of tube V1402A. Triode V1402A is held at cutoff until positive trigger pulse is applied to its grid. A positive pulse on the grid of tube V1402A causes a negative pulse to be developed at the plate which is coupled through capacitor C1423 to the grid of tube V1402B. As the grid of tube V1402B swings negative, the plate voltage rises and a positive signal is coupled through capacitor C1421 back to the grid of tube V1402A. The positive signal fed back to the grid of tube V1402A continues the action started by the trigger pulse until tube V1402B is cut off. Triode V1402B remains cut off until capacitor C1423 discharges through potentiometers R1466 and R1403. When plate current starts to flow in tube V1402B, the multivibrator returns to its stable condition with tube V1402A cut off and tube V1402B conducting heavily. The time constant of the R-C circuit consisting of capacitor C1423 and potentiometers R1403 and R1466 determines the width of the pulse generated in multivibrator V1402 Potentiometer R1466 is adjusted to provide a square pulse approximately 2.5 microseconds wide at the output of tube V1402B.

Power amplifier pentodes V1403, V1404 and, V1405 are operated in parallel in order to obtain the high-powered pulse required to drive subsequent shaping circuits. Grid resistors R1410, R1413, and R1414, and plate networks Z1401, Z1402 and Z1403 are parasitic suppressors. Grid resistor R1408 is common to all three tubes, and is returned to the -375 -volt supply to obtain enough grid bias to cut off the power amplifiers in the absence of a signal on the grid. Pulse transformer T1402 is the common plate load for the power amplifiers and provides impedance matching and phase inversion between the output of the power amplifiers and the input of the shaping network. When a positive pulse from tube V1402 is applied to the grids of power amplifiers V1403, V1404, and V1405, plate current flows through the power amplifiers and pulse transformer T1402, causing a negative rectangular pulse approximately 800 volts in amplitude to be impressed across the primary of transformer T1402. A positive pulse approximately 2300 volts in amplitude is induced in the secondary of transformer T1402 and is applied to the shaping network through series diode V1406. Potentiometer R1416 loads the secondary of transformer T1402, damping out ringing caused by the sudden collapse of the inductive field in transformer T 1402 when plate current in the power amplifiers is cut off. Series diode V1406 passes the positive pulse to the shaping network while preventing negative transients in the secondary of T1402 from being passed to the shaping network. Capacitors C1406, C1407, C1408, and C1417, and coils L1401, L1402, and L1403 form a low-pass filter, which is used as the 3.5 -microsecond pulseshaping network. Triangular pulses 3.5 microseconds wide at the input of the shaping network are reduced in amplitude and shaped into pulses 3.5 microseconds wide having a gradual rise and decay time. Control of the pulse shape at this point ensures that a minimum of r-f spectrum will be occupied by the final transmitted r-f output pulse. Potentiometers R1417 and R1418 provide the proper termination for the shaping network. Potentiometer R1417 provides a means of adjusting the terminating impedance to match the characteristic impedance of the
shaping network,thereby preventing reflection in the shaping network and distortion of the pulse.

The delay time through the shaper network is approximately 2.8 microseconds. Although coils L1401, L1402, and L1403 have adjustable cores, they are set to the inductance values shown on the schematic and are not to be adjusted in the field.

Positive pulses from the shaping network are coupled through capacitor C1410 and parasitic resistor R1422 to the grid of cathode followers V1407 and V1411.

The cathode-follower output stage consists of two pentodes V1407 and V1411 connected in parallel. Operation of the two tubes in parallel causes the output impedance of the 3.5 -microsecond shaped pulse generator to lower. It is essential that the shaped pulses applied to the grid of the klystron in the amplifier modulator be derived from a low impedance source. Potentiometer R1471 and capacitor C1424 form a compensating network in the grid circuit of the cathode-follower output stage. Potentiometer R1471 is adjusted to eliminate droop in the north and auxiliary reference bursts. It is required that the amplitude of any pulse in the north reference burst of 24 pulses shall not deviate from the average amplitude by more than $\pm 2.0$ percent. Any tendency toward pulse droop in the output of the radio set may be compensated for by adjustment of potentiometer R1471 to introduce enough pulse boost to equalize pulse droop.

The output output of the cathode followers, which is a specially shaped video pulse approximately 800 volts in amplitude and 3.5 microseconds wide, is fed through tube V1402 to the plates of the r-f amplifiers.

A sample of the 3.5 -microsecond shaped pulse is tapped off the cathode resistance of tube V1407 and fed to SHAPED PULSE jack J1405 on the front panel of the frequency multiplieroscillator.

## 3. KEYED R-F AMPLIFIERS. - Stages V1505 and

 V1506 are r-f amplifiers operated in cascade employing 2C39A lighthouse tubes in conjunction with a broad-band coaxial type resonant circuit. The operation of stages V1505 and V1506 is similar to that of tripler stage V1504, the only difference being that stages V1505 and V1506 are keyed. The lighthouse tube cavities are tuned by means of tuning screws (maximum output at resonance). Capacitors C1548, C1549, C1550, and C1551 are r-f bypass capacitors which effectively place the heater at zero r-f potential.Plate current in both r-f amplifiers is cut off by a positive cathode bias of approximately 25 volts obtained from the voltage divider consisting of potentiometers R1460 and R1457 located on the video chassis of the frequency multiplier-oscillator. Negative 10-microsecond pulses from transformer T1404 are fed through jack J 1509 to the cathodes of r-f amplifiers V1505 and V1 506 to override the positive cathode bias and key on plate current. A constant $r$-f carrier signal is applied to the grid line of r-f amplifier V1 505 from tripler stage V1504. The r-f carrier signal is passed through the r-f amplifiers only during the
time that a negative keying pulse is present on the cathodes of the r-f amplifiers.

The r-f output signal of the frequency multiplieroscillator, which consists of 10 -microsecond pulses of r-f energy at the carrier frequency, is fed to the klystron in the amplifier-modulator drawer.

## 4. VOLTAGE REGULATOR STAGE

V1410. -Twin triode V1410 is used as a voltage regulator to provide 150 volts $B+$ for the oscillator and doubler stages in the frequency multiplier-oscillator r-f chassis.
5. GATE PULSE GENERATOR. - Pulses from the coder-indicator are fed through delay lines DL1401 and DL1402 in series to the one-shot multivibrator stage consisting of tubes V1401 and V1408 (figure 4-36). The one-shot multivibrator generates one pulse 10 microseconds wide for each trigger pulse applied to the grid of tube V1408.

Vacuum tubes V1401 and V1408 form a one-shot multivibrator stage which is similar in operation to one-shot multivibrator V1402 described in paragraph 4-3b(3)(a)2. The principal difference is that the gate pulse generating multivibrator has a longer period in order to produce a 10 -microsecond output pulse. The R-C circuit, consisting of capacitor C1416 and resistors R1402 and R1465, determines the period of the one-shot multivibrator. Resistor R1465 is adjusted to set the output pulse width at 10 microseconds. Both sections of the one-shot multivibrator consist of twin triodes connected in parallel to ensure conservative operation of tubes V1401 and V1408.

Cathode-follower stage V1409 consists of a twin triode with both triodes operating in parallel. Pulses from the plate of tube V1401 are coupled to the grids of tube V1409 through capacitor C1414 and parasitic suppressors R1435 and R1440. Approximately 25 volts of negative bias is applied to the grids of tube V1409 from a voltage divider consisting of potentiometers R1433 and R1436. Pulse transfor mer T1404 is the plate load of tube V1409, coupling the 10 -microsecond output pulse from the plate of tube V1409 to the cathodes of r-f amplifiers V1505 and V1506. Potentiometers R1460 and R1457 serve as a voltage divider on the 250 -volt d-c bus, and provide a source of positive bias voltage which is fed through the secondary of transformer T1404 to the cathodes of r-f amplifiers V1505 and V1506. Capacitor C1418 provides a low impedance path to ground from terminal 3 of T 1404 for 10 -microsecond pulses induced in the secondary of transformer T1404. A second output from tube V1409 is taken off the unbypassed cathode resistor R1458 and fed to the receiver video amplifier to provide a 10 -microsecond blanking pulse. This blanking pulse will cause the receiver to be disabled during trans mission of r-f output pulses to ensure that transmitted energy will not be routed back into the radio beacon.
(b) AMPLIFIER-MODULATOR AM-1701/

URN. -The a mplifier-modulator (figure 4-37) consists of r-f power amplifier V1304, a regulated bias supply, and associated control circuits. R-f power amplifier

V1304 employs a klystron (SAL-89), which is a threecavity amplifier having a control grid used to intensitymodulate the klystron beam current, and an r-f input jack in the first cavity used to velocity-modulate the klystron beam current. A constant negative potential of 12 kv is applied to the klystron cathode. Klystron beam current is cut off by approximately 120 volts of negative bias developed in the regulated bias supply and fed to the klystron control grid through the secondary of pulse transformer T1372. Shaped 3.5microsecond pulses from cathode-follower stage V1407 and tube V1411 in the frequency multiplieroscillator are fed to the primary of pulse transformer T1372. Positive pulses from the secondary of pulse transformer T1372 are applied between the control grid and cathode of klystron V1304, causing the klystron to conduct beam current. The instantaneous value of beam current is directly proportional to the instantaneous voltage of the 3.5 -microsecond shaped pulse. In this manner, the flow of beam current is intensity-modulated by the 3 . 5 -microsecond shaped pulse on the klystron grid. As the klystron beam current passes through the first resonant cavity of the klystron, it is velocity-modulated by the 10 -microsecond r-f pulse fed into the r-f input jack on the klystron input cavity.

The output of the klystron, consisting of specially shaped r-f pulses having a minimum peak power of 11 kw and a repetition rate identical to the repetition rate of the pulse train at the output of the coderindicator, is fed to cavity Z1303. Double-slug tuner Z1303 provides a means of matching the output impedance of the klystron with the impedance of the transmission line filters $\mathbf{Z 1 1 5 6}$ or Z1157 in the con-trol-duplexer. The r-f output signal is fed, via coaxial line, from the amplifier-modulator to the control duplexer. The regulated power supply, included in the amplifier-modulator to provide negative bias between klystron cathode and grid, is a conventional series-regulated supply similar in operation to series-regulated supplies used in this equipment. In place of rectifier tubes employed in other series-regulated supplies in the radio set, crystal rectifiers CR1370 and CR1371 are used as power supply rectifiers. In addition to saving space and reducing heat dissipation, crystal rectifiers eliminate the need for filament transformers. The output of the bias supply is applied between the cathode and control grid of klystron SAL-89, with the positive terminal connected to the cathode and the negative terminal connected to the grid through the secondary of transformer T1372. As the cathode of the klystron is operated at -12 kv below ground, all components in the bias supply are insulated from ground to withstand potential differences in excess of 12 kv between components of the bias supply and ground. Power for the primary of bias supply transformer T1371 is obtained from a 120 -volt secondary winding on transformer T1370, which provides filament power to the klystron. Insulation between the primary and secondary of transformer T1370 is capable of withstanding voltages in excess of 20 kv rms ; therefore, bias supply transformer T1371 can be a conventional low-voltage power supply transformer having low-voltage insulation ( 1800 -volt rms) between windings.


(4) CONTROL-DUPLEXER C-2226A/GRN-9. The duplexer (figure 4-38) is a passive network which permits both the transmitter and receiver to be connected simultaneously to one antenna. Pulsed r-f transmitter output from the klystron r-f amplifier is fed to a transmission filter consisting of a pair of tunable resonant cavities critically coupled. The transmission filter is located in the line between the transmitter and the antenna, with the receiver line branching off on the antenna side of the transmission filter. The performance standards for the filter system are as follows:
(a) Signal loss at transmitter frequency, 1.4 db maximum.
(b) Response at transmitter frequency of $\pm 0.2 \mathrm{mc}$ is within $\overline{3} \mathrm{db}$ of response at transmitter frequency.
(c) Response at transmitter frequency of $\pm 0.75 \mathrm{mc}$ is a minimum of 20 db down from response at transmitter frequency.
(d) Response signals are essentially completely rejected at receiver frequencies (transmitter frequency of $\pm 63 \mathrm{mc}$ ).
(e) Temperature operating range from $-54^{\circ} \mathrm{C}$ $\left(-65.2^{\circ} \mathrm{F}\right)$ to $+65^{\circ} \mathrm{C}\left(+149^{\circ} \mathrm{F}\right)$ (ambient).

Filter cavity operating temperature is maintained by a thermostatically controlled electrical heater system consisting of an auxiliary thermostat, a main thermostat, a blanket heater surrounding each cavity and an anticipator heater placed over the main thermostat. The system óperates as follows: When first energized, power is applied to the blanket heaters but not to the anticipator heater. This minimizes warm-up time by preventing main thermostat operation under influence of heat from the anticipator heater while the cavity temperature is still below that required for normal operation. As the cavities approach operating temperature, the auxiliary thermostat applies power to the anticipator heater.

After operating temperature has been reached, the main thermostat shuts down blanket heater power. The main thermostat applies power again only after a drop in temperature but shuts down quickly due to heat from the anticipator heater (approximately 8 to 10 seconds at normal ambient temperatures).

Spaced half a wave length from the output terminal of the filter is a T-connection to which are connected the receiver preselector cavity Z1153. As the transmission filter is tuned 63 mc above or below the receiver frequency, it appears as an open circuit at the receiver frequency. From the T-junction at the transmitter, output is fed to the antenna and transmitted The preselector cavities are tuned to the receiver frequency. Therefore, signals at the receiver frequency are routed to the radio receiver while signals at the transmitter frequency are rejected. In effect, transmitter frequency signals travel from the transmitter down the line to the antenna; the receiver preselector cavities, as far as transmitter frequency is concerned, do not exist. Receiver frequency is picked up by the antenna
and is routed directly to the receiver preselector cavities; the transmission filter does not exist electrically at this frequency.

Samples of the klystron incident and klystron reflected voltage are fed via directional coupler DC1 151 to test jacks J1152 and J1157, respectively. In the same manner, samples of the antenna incident and antenna reflected voltages are fed via directional coupler DC1156 to test jacks J1154 and J1153. These test jacks are used during klystron and duplexer tuning as described in Section 6.

Control circuits contained in the control-duplexer are described in paragraph 4-3b(6).

## (5) POWER SUPPLIES.

(a) RECEIVER POWER SUPPLY. - The receiver power supply (figure 4-39) provides regulated - 105 -volt dc for the video amplifier stages and regulated $B+, 150$-volt dc for the complete receiver. The B+ supply is regulated by tubes V503, V504, and V505. The - 105 -volt supply is regulated by V506.

Gas diode V505 provides a fixed negative bias for control tube V504. The voltage on the grid of tube V505 is set by the voltage divider consisting of potentiometers R506, R507 and R508 at a fixed fraction of the voltages between B+ and -105 volts. The voltage drop across the plate resistor R505 is the bias voltage for the regulator tube V503. If the $\mathrm{B}+$ voltage remains constant, the voltage on the grid of tube V504 does not change, therefore the bias voltage for tube V503 remains constant. The voltage at the cathode of tube V503, because of the voltage drop across the tube, is 150 volts. If the output drops, the bias on the grid of tube V504 becomes more negative; the drop in plate current causes the voltage at the plate of tube V504 to become more positive. The bias on the grid of tube V503 becomes more positive, causing a drop in the resistance of this tube. The B+ voltage at the cathode of V503 increases, counteracting the original drop in voltage. Increases in the $B+$ voltage are corrected by the same principle of the variable resistance of V503.
(b) CODER-INDICATOR POWER SUPPLY.-

The power supply for the coder-indicator (figure 6-22) employs a single power transformer with two separate windings for the plate and bias voltages. Stage V701 constitutes a full-wave rectifier for the plate supply voltages, and stage V702 rectifies the bias voltage.

The filter circuit of the plate supply is of the choke input type consisting of choke L701 and shunting filter capacitor C701. This type of filter network has been selected because it subjects the rectifier to less peak inverse voltage and provides better regulation.

Voltage regulation is accomplished by series regulator tube V703, amplifier V704, and regulator V705. This regulator circuit produces an output voltage which is independent of fluctuations in the a-c supply and changes in load over a wide range. The output voltage is developed across potentiometers R708,


Figure 4-38. Control-Duplexer C-2226A/GRN-9, Functional Schematic Diagram


R710, and R711 in parallel with the effective load resistance. The other resistance, through which all the load current must flow, is the plate-to-cathode resistance of vacuum tube V703. The other elements in the circuit control the resistance of tube V703 and thereby maintain a constant voltage across the load.

The cathode voltage of tube V703 is the regulated output voltage. The cathode potential of tube V703 is held at a constant positive value by grid biasing through potentiometer R710 and tube V705, and glow tube OB2. Grid potential of tube V704 is set through potentiometer R710, which is set so that the grid voltage is slightly negative by an amount (the bias) which causes tube V704 to pass a certain plate current. The magnitude of the voltage across potentiometer R705 is the bias on tube V703. Therefore, the adjustment of potentiometer R710 establishes the normal resistance of tube V703. This adjustment is used to set the value of load voltage which the regulator is to maintain.

If the load voltage tends to rise, whe ther from a decrease in the load current or from an increase in the input voltage, the voltage on the grid of tube V704 also tends to rise (become less negative). Tube V704 then conducts more current because the bias is smaller. A greater current flows through potentiometer R705 and causes a greater voltage drop across it; this voltage, the bias voltage for tube V703, causes the plate resistance of tube V703 to increase. $\bar{A}$ larger potion of the available voltage appears across the high resistance of tube V703, and the load voltage remains practically constant. If the load voltage tends to fall, the voltage on the grid of tube V704 atso tends to fall (become more negative). Tube V704 then conducts less and a smaller current flows through potentiometer R705 and causes a smaller voltage drop across it. This bias voltage for tube V703 causes the plate resistance of tube V703 to decrease. A smaller portion of the available voltage appears acioss tube V703, and the load voltage remains constant.

Bias voltage is obtained from an independent secondary winding on transformer T702. Stage V702 is used as a fullwave rectifier. A T-connected R-C network is used for both filtering and for current limiting the gas regulator tube V705; a bias voltage of -105 volts results. Capacitor C703 is made large enough to have low impedance to the ripple frequency.

Warning light DS701 is prominently displayed on the chassis and warns the technician when the interlock is shorted and voltage is still applied to the power supply.

## (c) LOW VOLTAGE POWER SUPPLY

PP-I766/UR $\bar{N}$. The low voltage power supply unit (figure 6-24) contains two full-wave rectifiers employing tubes 5R4WGB. The rectifier plate transformers are connected to the 120 -volt single-phase power by contactor K 1603 , operated by the control circuit. The red indicator lamp DS1603 goes on when the rectifier plate transformers are energized. Simple capacitor input filters are connected in the two unregulated d-c output circuits of the rectifiers. Two series-type voltage
regulators are used. Capacitor filters are connected in the output circuits of the regulators.

Magnetic relay K1601 is connected across the -375 -volt output. One set of contacts on the relay is connected in series with the control circuit to prevent the medium voltage power supply from functioning unless the -375 -volt output is available. Another set of contacts on the relay closes the circuit of the green indicating lamp DS 1601 when the -375 -volt output is present.

The low voltage power supply contains two series voltage regulator circuits. One series regulator provides regulated +250 volt de to the low voltage circuits in the frequency multiplieroscillator and amplifier-modulator. This is a conventional voltage regulating circuit, employing a gas diode reference tube, two triode voltage amplifiers, and a parallel pair of twin pentodes as series regulators. As this is a common circuit, similar to other power supplies employed in this radio set, a detailed description will not be given here.

The second series regulator provides -375 volts to circuits in the frequency multiplier-oscillator and amplifier-modulator . Although this circuit has many features in common with conventional series regulators that provide a positive output voltage, there are basic differences in the first voltage amplifier stage that warrant a detailed explanation. Gas regulator tube V1613 maintains the grid of the first voltage amplifier stage at a negative potential that is a fixed voltage more positive than the output voltage. If the output voltage should go more positive or more negative, the voltage on grid (7) of tube V1612 will also go more positive or more negative by exactly the same amount. Assuming that the output voltage of -375 -volt de should go more positive due to an increase in load or decrease in line voltage, the regulator would function as follows: The voltage on grid (7) of tube V1612 will go more positive by the same amount as the output voltage. The voltage on the cathode will also go more positive but, due to the voltage divider action of resistors R1663, R1664, R1665, R1669, and R1666, the positive change in voltage on the cathode will be less than the positive change on the grid. This action will cause the bias on the grid to become more positive with respect to the cathode. As the grid bias becomes more positive, plate current will increase and cause the voltage on plate (6) and grid (2) to go more negative. As the bias on grid (2) goes more negative, plate current through that half of tube V1612 will decrease and cause the plate voltage on pin 1 to increase. Since the contrel grids of series regulator V1611 are connected to plate (1) through parasitic suppressors R1654 and R1655, the bias on these control grids will also go more positive. This feature will result in a reduction in the voltage drop from plate to cathode of the series regulator V1611. The output voltage of the power supply is equal to the output of rectifier V1610 minus the voltage drop across tube V1611. Therefore, as the voltage drop across tube V1611 is reduced, the output will be increased to correct for low output voltage.

If the output voltage should increase above -375volt dc, the voltage regulator will function as explained for conditions of low output voltage except that the polarity of voltage changes will be reversed.
(d) MEDIUM VOLTAGE POWER SUPPLY

PP-1765/URN. - The medium voltage power supply unit (figure 6-25) contains one full-wave rectifier employing two tubes 836. The rectifier plate transformer T1801 primary is connected to the incoming 120 -volt, single-phase power by the contactor K1804, operated by the control circuit. A capacitor input filter is connected in the unregulated rectifier output circuit. A series-type regulator (figure 4-40), is connected in the filter output circuit to provide the 1000 -volt output. The 1000 -volt series-type regulator uses five pentodes 829B in parallel. Capacitor filter C 1802 is connected in the 1000 -volt output circuit of the voltage regulator. A positive 700 volts'is obtained by voltage dropping across series resistors

R1875 and R1876 connected to the 1000 -volt regulated output bus.

The medium voltage power supply contains overload relay K1805; when an excessive current is sustained, this relay disconnects the plate voltage. Very brief transients do not trip the overload relay. This time delay feature is necessary so that large charging currents that occur when the equipment is started do not trip the overload relay.

Relay K1801 is connected across the 1000 -volt regulated output. When the coil is energized, the contacts of the relay make, activating red indicating lamp DS 1801 on the front panel of the medium voltage power supply unit.

The 1000 -volt output is applied across potentiometer R1874 and tubes V1810 through V1814 in series. The grid bias for the series regulators is obtained in the following manner (figure 4-40): The cathode (3)


Figure 4-40. Medium Voltage Power Supply PP-1765/URN, Voltage Regulator, Simplified Schematic Diagram

# PRINCIPLES OF OPERATION 

of tube V1808 is kept at a constant potential by regulator tubes V1810 through V1814. The grid (2) bias is obtained from the divider network consisting of resistors R1846, R1842, and R1850. Potentiometer R1842 makes it possible to set the initial bias at the proper bias for the desired output voltage. If the load increases, the regulator input voltage decreases because of the voltage drop in the rectifier. As the voltage drop in the divider network decreases, the bias on grid (2) of tube V1808 becomes more negative, resulting in a reduction in the plate current of this tube. The reduced plate current decreases the voltage drop in potentiometer R1845 and consequently reduces the bias on series tubes V1803 through V1807, thereby lowering impedance. The reduced drop in tubes V1803 through V1807 compensates for the increased load voltage drop, and the output voltage is restored to normal. An increase in input voltage to the regulator would act in an opposite manner to increase the impedance of tubes V1803 through V1807.

The resistors in the plate, screen grid, and control grid circuits of the series tubes are parasitic suppressors.

The output of the medium voltage power supply is indicated on a voltmeter on the front panel of the frequency multiplier-oscillator chassis.

The transmitter medium voltage power supply contains overload relays so that in the case of an overload the incoming power to the medium voltage power supply plate transformer primary is disconnected. The operating point of the time delay relay K1803 circuit is set by variable resistor R1872. When an overload is sustained long enough to actuate relay K1803, contacts 3 and 4 make, energizing the coil of magnetic relay K1802. Contacts 3 and 4 of relay K1802 make, as do contacts 5 and 6; contacts 7 and 8 break. Contacts 3 and 4 of relay K1802 keep relay K1802 energized after contacts 3 and 4 of relay K1803 reopen. When contacts 7 and 8 of relay K1802 open, the holding coil of K1804 (the medium voltage power supply plate contactor) is de-energized and the medium voltage power supply is disconnected. When contacts 5 and 6 of relay K 1802 make, the motor of motor-driven reclosing relay K1305 is energized. Three seconds later contact B of relay K1805 swings momentarily to the number 6 position ( 120 -volt ac), energizing resetting relay K1806. All the contacts of relay K1806 break. When contacts T3 and L3 of relay K1806 break, the path holding relay K 1802 energized is broken, and relay K1802 is de-energized. Contacts 7 and 8 of relay K 1802 close, energizing relay K1804, thus restoring the equipment to normal operation. Overload reclose relay K 1805 will swing contact $A$ to the No. 5 position ( 120 -volt ac) three times in case of a continuous overload or successive trips occurring less than 1.2 seconds after the preceding reclosure; then, contact $C$ will open and contact A will close (No. 4 position), breaking the overload reset relay K 1806 circuit and shutting down the equipment. The equipment will remain shut down until switch S1802 is manually closed. (Switch S 1802 must be held closed or it returns to the open position.) The closing of switch S 1802 closes contacts A
(No. 5 position) and C of relay K1805. If the overload trips occur 1.2 seconds or later after each previous reclosing, K1805 will continue to reclose automatically.

## (e) HIGH VOLTAGE POWER SUPPLY

PP-1763/URN. -The high voltage power supply (figure 4-41) contains a three-phase, full-wave rectifier employing tubes 8020. The plate power is supplied by transformer T1001, which is mounted separately in the blower compartment of the power supply assembly cabinet. A means for reducing this plate power during the performance of the klystron-aging procedure is provided by HIGH VOLTAGE switch S1006. Connection of transformer T1001 in a delta-wye-wye arrangement depends upon the setting of this switch. If switch S1006 is set to OPERATE, transformer T001 is connected in a delta-wye arrangement; hence the secondary voltage (plate power) is equal to the product of the primary voltage and the turns ratio, multiplied by a factor of 1.73 . If switch S 1006 is set to BREAK IN, the transformer is connected in a wyewye arrangement; hence the secondary voltage is equal to just the product of the primary voltage and the turns ratio.

A simple capacitor filter is connected in the 12,000volt rectifier output circuit; the high voltage power supply does not use a voltage regulator.

The negative side of the power supply is $\mathbf{- 1 2} \mathbf{k v}$ with respect to ground. The positive side of the power supply output is grounded through the BEAM CURRENT meter on the front panel of the amplifiermodulator chassis. Output voltage from the highvoltage power supply is fed through intercabinet cabling and applied directly to the klystron cathode as a negative potential of 12 kv which establishes the required accelerating potential between the klystron cathode and plate. Resistor R1918, which is connected between the positive side of the high voltage power supply and chassis ground, is a voltagesensitive resistor. This resistor provides a path to ground for the positive side of the high-voltage power supply in case an open occurs in the circuit from the positive side of the power supply through the BEAM CURRENT meter to ground.

Power supply filter capacitors C 1901 and C 1902 are insulated from ground and connected directly across output of the high voltage rectifiers. Therefore, when the high voltage power supply is first energized, the initial surge of charging current to the power supply filter capacitors does not pass through overload relay K1904 and shunting resistor R1906.

Relay K1904, in series with potentiometers R1918 and R1912, is connected in parallel with potentiometer R1906, which is in the return path for the total output current of the high voltage power supply. A portion of the output current will be shunted through the coil of relay K1904, depending on the setting of variable resistor R1912. With resistor R1912 properly adjusted, relay K 1904 will close when the current drain on the high voltage power supply exceeds approximately 125 ma . When relay K1904 closes, power is applied to the coil of overload auxiliary

relay K1902, and the high-voltage plate supply is switched off, subject to automatic resetting (paragraph $4-3 \mathrm{~b}(5)(\mathrm{d})$ ).

Elapsed time indicator M1901 on the front of the high voltage power supply unit operates when the plate contactor is closed and power is supplied to the unit. Thus, it records the total time that the $-12,000$-volt de has been supplied to the klystron. Red indicating light DS1901, in parallel with elapsed time indicator M1901, warns the operator that the 12,000 -volt output is present. Elapsed time indicator M1902 records the total time that the high voltage power supply filament transformer is energized and the time that power is supplied to other filaments of the transmitter. Protective switch S1901 is provided on the high voltage power supply drawer that discharges the filter capacitors through a resistor, whenever the unit is pulled out.

A voltmeter on the front panel of the amplifier-modulator chassis indicates the output of the high voltage supply.

## (6) POWER DISTRIBUTION AND CONTROL CIRCUITS.

The functioning of the power distribution and control circuits is described in the following paragraphs, with reference to the power distribution diagrams included in Section 6 (figure 6-15). All controls are in the off position.
(a) When EMERGENCY SWITCH S901, mounted on the receiver-transmitter cabinet, is closed, the following take place: The line power is connected to the antenna motor contactor. Power is connected to the terminals of main contactor K1101 and blower contactor K1103. Power (120-volt, singlephase, 60 -cycle) is connected to the crystal oven transformer in the frequency multiplier-oscillator drawer. This power may be obtained from the convenience outlet circuit. Phase failure relays K901 and K902 are energized.
(b) When MASTER SWITCH S1101 on the control panel is set to STANDBY, the following occurs: Primary contactor K1 101 closes, connecting 208-volt, three-phase, 60cycle power to the terminals of high-voltage plate contactor K1001, and connecting 120 -volt, single-phase, 60 -cycle power to FIL ON switch S1108, the low and medium-voltage plate contactors, K1603, K1604, and K1804, the control circuit bus, the ANTENNA CONTROL switch, the test set switch, CODER-INDICATOR switch S601, receiver switch S502, MAIN POWER indicating lamp DS1102, and the coil of blower contactor K1 103. Blower contactor K1 103 closes, connecting cabinet blowers B901, B902, and B1001 to the three-phase, 60 -cycle power line. When the power is shut off by the MASTER SWITCH, the blower contactor is kept closed by time delay relay K1102 for 1 minute after primary contactor K1 101 has opened so that the residual heat will be dissipated rapidly.

## CAUTION

Except in an emergency, the equipment must not be shut down by EMERGENCY SWITCH S 901 until 1 minute has elapsed after returning the MASTER SWITCH to OFF.

ANTENNA CONTROL switch S1102, CODER-INDICATOR switch S601, RECEIVER switch S501, and FIL ON switch Sl 108 may now be set to the on position. ANTENNA CONTROL switch S1102 energizes the antenna control circuit. If the spin motor switch on the antenna control is closed, the antenna spin motor will rotate. CODER-INDICATOR switch S601 energizes the coder-indicator circuit and RECEIVER switch S501 energizes the receiver circuit. FIL ON switch S1108 energizes the filament transformer circuits and FIL ON white indicating lamp DS1101. The ADJUST FOR 120 V knob on the control panel operates filament voltage adjusting variac T1101. Ordinarily, SUPPLY VOLTS voltmeter M1 101 is connected to the regulated filament bus by LINE-REG FIL BUS switch S1106. This meter may also be used to check the unregulated voltage when switch S1106 is held at LINE. When the FIL ON switch is closed, the filament transformers of the low, medium and high voltage power supplies, filament transformers T1501 and T1403 in the frequency multiplier-oscillator, and filament transformer T1350 in the amplifier-modulator are immediately energized. Relay K1401 energizes time delay relay K1605, which prevents the low and medium voltage power supply plate voltages from being applied until the filaments have been connected for 1 minute. Filament transformers T1301 and T1303 and white indicating lamp DS1301 in the amplifier-modulator are energized through relay K1301. Simultaneously, time-delay relay K1106 is energized, providing a 5 minute delay before the high voltage power supply plates (and, indirectly, the klystron) can be energized.
(c) With the MASTER SWITCH at STANDBY, the equipment will remain in the condition just described. With the MASTER SWITCH set to ON, the drawer interlocks are connected to the 120 -volt a-c control power. The low-voltage power supply is ready to be activated if the following conditions are met: the drawer and compartment covers are in place, or the INTERLOCKS SHORTED switch is closed, or the individual interlocks have been manually closed, as may be the case during tuning procedures, the 1 -minute time delay relay K1605 is closed, and the blue LV-MV READY lamp is on.

If the MASTER SWITCH is set to ON without stopping at STANDBY, the equipment will arrive at operating condition after the various time delays have been completed. LV switch S1 601 may now be closed; this action energizes low-voltage plate contactor K1603, causing the low voltage power supply to function. Medium voltage power supply plate contactor

K1804 will close, energizing that unit if the following conditions exist:

1. Relay K1601 is energized by the -375 -volt d-c output of the low-voltage power supply.
2. Medium-voltage overload relay K1802 is deenergized.
3. Overload reset relay KI 806 is de-energized.
4. MV switch S1801 has been turned on by the operator.
(d) The d-c output of the medium-voltage power supply closes screen supervisory relay K1801, which connects 120 -volt ac to I000-volt lamp DS1801. High voltage power supply plate contactor K1001 will close, connecting 208-volt three-phase, 60 -cycle power to the primary of plate transformer T1001 if the following conditions exist:
5. Relay K1804, the plate contactor of the medium voltage power supply, is energized.
6. The contacts of 5 -minute time-delay relay KI 606 are closed. This relay is energized at the same time as filament transformer T1 370 which heats the filaments of the klystron.
7. Blue indicating lamp DS1902 shows HV READY, signifying that conditions $a$ and $b$ have been met.
8. Overload relay K1902 in the high voltage power supply drawer is de-energized.
9. HV switch S1902 is set to ON.
(e) Additional information on the normal functioning of the control and power distribution circuits is as follows:
10. All the ON switches on the control panels may be closed before the master switch is advanced to STANDBY or ON .
11. If the master switch is moved to ON while all ON switches are closed, the equipment will be automatically energized in its proper sequence, a period of 5 minutes being required before it is fully energized.
12. Once the equipment has been fully energized, with all ON switches remaining closed, the master switch may be moved back to STANDBY, then returned to ON, and the equipment will then be fully energized immediately. Therefore the equipment may be left in the STANDBY position when not required to send or receive information.
13. If the high voltage power supply unit or the amplifier-modulator unit is pulled out or the transformer and blower compartment panel is removed, the high voltage power supply will be disconnected, but the low and medium voltage power supplies will remain functioning. If the low and medium voltage power supply units, the receiver unit, and the frequency multiplier-oscillator unit are pulled out the low medium and high voltage power supplies will be disconnected.
14. Overload protection is provided for the medium and high voltage power supplies. An overload in the medium voltage power supply disconnects that unit and also the high voltage power supply. An overload in the high voltage power supply disconnects only the high voltage power supply. Automatic reclosing relay K 1805 restores the power through resetting relay K 1806 after 3 seconds. The automatic relay will reset three times and then shut down until reset manually by reset switch SI 802. In either case, if the cause of the overload has not been removed, the overload relay will trip again.
15. BATTLE SHORT switch S1107, used only in emergencies, in addition to shorting the drawer interlocks of the control circuit, shorts the unit interlocks on the receiver and on the coder-indicator, thereby connecting the 120 -volt a-c input to the individual power supplies. The individual unit interlocks may be closed manually with the unit pulled out when necessary for tuning. Units in which high voltage is exposed have additional contacts in the interlocks which connect the red warning lamp. Interlocks closed in this manner are restored to normal functioning when the unit is closed.
16. The equipment may be energized by a remote control switch if all the ON switches on the control panel are closed and the MASTER SWITCH has been turned to REMOTE CONTROL. A white indicating lamp on the remote control switch shows that it is ready for use. The remote control switch has OFF, STANDBY and ON positions that perform the same functions as those positions on the MASTER SWITCH with identical designations. There are two red indicating lamps on the remote control unit; one tells when the low voltage power supply and the medium voltage power supply are ready for energizing, and the other shows that the high voltage power supply is ON .
c. TEST PRINCIPLES. - This paragraph shows how the test units previously described are connected together for the various positions of the test function switches. explaining the theory behind each test thus made possible.
(1) Original Test Equipment (TABLE 1-2), FUNCTION SWITCH IN POSITION 1. - Front panel connections shown in Fig 3-13 with the test function switches in position 1 enable the operating tests to be made by the adjustment of just a few of the unit controls. The oscilloscope is reset for the correct sensitivity and the required $25 \mu \mathrm{sec}$ sweep.

## PRINCIPLES OF OPERATION

The signal at the video input of the beacon is fed through switch contacts of the Power Meter - Pulse Counter to the trigger input of the oscilloscope. This action synchronizes the oscilloscope so that the video pulse pair triggers a sweep trace. The r.f. output of the beacon is fed to the antenna through the switch-test adapter. This r.f. signal is detected by the diode in the switch-test adapter, fed through switch contacts in the Power Meter - Pulse Counter and applied to the oscilloscope signal input terminals. Thus the detected r.f. signal will be displayed on the oscilloscope for all position 1 tests.

The paired pulses generated by the pulse-sweep generator are fed directly to the modulator input of the TS-890A/URN-3. The resulting pulsed r.f. signal is used to interrogate the radio beacon. The radio beacon r.f. output signal is fed back to the Pulse Analyzer section, from the ANTENNA INCIDENT jack to the RECEIVER INPUT connector.
(2) Replacement Test Equipment (TABLE 1-2b).For the following operating tests no external connections are required between the beacon and the test equipment; all connections are automatically made as the switch positions and coaxial links are selected in accordance with the specified setting up instructions.

RF peak power and beacon spectrum tests are achieved by applying the r.f. output of the beacon, via the Transfer and Switching Unit, to the Spectrum Analyzer/Test Generator and Power Meter. A total pulse count is provided when the beacon output is fed via the Transfer and Switching Unit to the Pulse Counter.

The following sub-paragraphs describe how the various signals of the Original and Replacement Test Equipment are used to provide the operating tests.

## (a) RF PEAK POWER TEST.

1. Original Test Equipment. - RF peak power output is determined by observation of the video waveform on the oscilloscope. By means of the variable d.c. voltage in the Power Meter - Pulse Counter, the bias on the cathode of the detector diode is varied to cut off the diode. When the diode is cut off to just the point where the video signal is no longer presented on the oscilloscope, the d.c. voltage is equal to the peak value of the r.f. signal. Because the deflection of the PEAK POWER METER corresponds to the d.c. voltage, peak power may be read directly from the meter in kilowatts.
2. Replacement Test Equipment. - Sample r.f. out put pulses are routed via the Spectrum Analyzer/Test Generator ATTENUATOR into diode detector network CR1 of the Peak Power Detector. The resultant video output is amplified by the peak power detector, sampled at the pulse peak and fed to a peak power/input level amplifier, as a d.c. voltage whose amplitude is proportional to the peak amplitude of the input pulse and attenuator setting. The output of the peak power/input level amplifier is applied across the PEAK RF POWER METER, which is calibrated in watts.
(b) VISUAL PULSE SHAPE. - The relative amplitude of any point on the video pulse may be readily determined by means of the graticule on the oscilloscope which also allows for measurement of pulse time relationships by means of accurately calibrated markers.

## (c) OUTPUT PULSE COUNT. -

1. Original Test Equipment. - The detected output of the radio beacon is fed directly to the counter circuit for the operating test. By proper setting of the Power Meter Pulse Counter controls, the PULSES PER SECOND meter will provide a continuous indication of the number of radio beacon output pulses per second.
2. Replacement Test Equipment. - After initial amplification the pulses to be counted are fed to the counter control circuit for further processing and then to the counter MAIN gate. The output of the MAIN gate is used to trigger a series of flip-flops in the Decade Counter Unit and these, in turn, change the conditions of a set of AND gates associated with the Nixie indicator tubes.
(d) BEACON SPECTRUM TEST. - The radio beacon spectrum test is made by applying beacon output r.f. pulses to the Pulse/Spectrum Analyzer. Basically the analyzer is a sharply tuned r.f. voltmeter which provides an indication of relative output power.
3. Original Test Equipment. - The analyzer is essentially a super-heterodyne receiver which uses a signal generator as its local oscillator.

The beacon transmitter output is fed through an attenuator and a filter-mixer circuit in the analyzer RF unit, before being applied to the receiver i.f. stage as a 63 MHz signal.

The filter-mixer circuit heterodynes the beacon transmitter output with that of the signal generator. The 8.5 MHz output of the 63 MHz i.f. amplifier is fed through a stepped attenuator to an 8.5 MHz i.f. unit which acts as a metering amplifier, operating an indicating meter whose readings are a function of the signal level at the output of the stepped attenuator.
2. Replacement Test Equipment.- The analyzer is a double-super-heterodyne receiver with crystal-controlled local oscillators. A crystal filter at the input of the 2 nd i.f. amplifier provides a well-defined bandpass response with high selectivity. A thermistor bridge assembly at the output of the 2nd i.f. amplifier operates an indicating meter the readings of which are a function of the average power output of the spectrum analyzer receiver.
3. In the case of both types of test equipment a reference indication is first made at the centre frequency of the channel by adjusting a variable attenuator for a mid-scale reading on a power comparison indicator/ average power meter. When the analyzer is set to this
frequency a fixed attenuator reduces the meter sensitivity. The analyzer is next tuned to any one of a number of spot frequencies (there are slight differences between the Original and Replacement test equipment) either side of the centre channel frequency. Simultaneously, the attenuation is reduced. The power comparison meter will remain at the reference point if the beacon pulse characteristics are correct; if they deviate from the specification, the meter deviates correspondingly. Similar measurements are made for the other spot frequencies.
(3) Original Test Equipment (TABLE 1-2). FUNCTION SWITCH IN POSITION 2.- The interconnections shown in Fig 3-13, as applicable to position 2 of the test function switches, permit the receiver sensitivity tests. The oscilloscope sensitivity is correctly preset and a $500 \mu \mathrm{sec}$ sweep is provided. North and Auxiliary bursts at the SYNC OUT jack of the beacon are fed to the TRIGGER IN jack of the oscilloscope through switch contacts in the Power Meter - Pulse Counter. This action synchronizes the sweep trace from the reference bursts so that the number of pulses in the bursts may be visually counted. The signal at the video input of the beacon is fed through switch contacts of the Power Meter - Pulse Counter to the SIGNAL IN jack of the oscilloscope. Thus, the video signal at the receiver output is displayed on the oscilloscope screen and the reference bursts may be observed for counting.

The TEST OUTPUT signal, at the radio beacon receiver output, is applied directly to the counter input. This condition enables a check to be made to ensure that the squitter count is correct and that the reply pulses are going through the receiver.

A paired-pulse output from the Pulse-sweep Generator is applied to the Pulse Analyzer/Signal Generator and used to interrogate the beacon at any desired rate.
(4) Replacement Test Equipment.- For the following operating tests no external connections are required between the beacon and test equipment. All connections are automatically made as the switch positions and coaxial links are sedected in accordance with the specific setting up instructions.

North and Auxiliary sync. pulses are fed into the Power Meter - Pulse Counter where they are routed via contacts of the REF MKR and FUNCTION switches (a) to provide system trigger for the oscilloscope and (b) for application to the Counter Control circuit whose output is coupled to a Decade Counting Unit associated with a set of Nixie tubes which register the burst interval.

Transmitted pulses from the Transfer and Switching Unit are also fed into the Power Meter Pulse Counter where they are detected before being fed to the oscilloscope for viewing.

The principle for squitter measurement is similar to that of the total output pulse count
except that during the operating test, the coder switch S605 in the beacon Coder Indicator Unit is set to OFF and the NORTH and AUX cables from the antenna base to beacon must be disconnected.

Pair'ed-pulse output from the r.f. signal generator of the Spectrum Analyzer is used to interrogate the beacon at any desired rate. The following sub-paragraphs describe how the various signals of the Original and Replacement Test Equipment are used to provide the operating tests.
(a) REFERENCE BURST PULSE COUNT.- The number of pulses in the reference burst, as well as the spaces between the pulses, may be readily checked by observation on the oscilloscope. By manipulation of the REF MKR switch it is possible to lock the trace to the NORTH or AUX bursts. The 1- and $10 \mu s e c$ markers in the oscilloscope enable accurate measurement of pulse spacing.
(b) SQUITTER COUNT.- The squitter is the output of the receiver not attributable to an actual interrogation. This signal is readily counted by stopping the interrogation signal from being generated and by adjusting the Power Meter - Pulse Counter controls for squitter count. In addition to supplying the squitter pulses when the interrogation rate is below 270 s pulse pairs per second, the squitter control circuits in the receiver limit the number of output pulses when the radio set is being interrogated by more than 2700 pulse pairs per second. Both of these squitter control circuit functions may be checked by varying the interrogation rate of the test signal from the generator.
(c) REPLY COUNT.- The reply count provides an indication of the number of interrogation pulses which pass through the receiver. The pulse counter circuit is made responsive only to reply signals from a specific gate circuit. The gate is activated by the interrogation signals and permits the counter to indicate those receiver output signals which are the result of an interrogation signal.
(d) RECEIVER SENSITIVITY.- An accurate indication of receiver sensitivity may be obtained by noting the amplitude of that output signal from the Pulse/Spectrum Analyzer required to obtain a replay count equal to 60 per cent of the interrogation rate.
(5) Original Test Equipment (TABLE 1-2). FUNCTION SWITCH IN POSITION 3.
(a) Overall Zero Distance Delay.- Front Panel connections shown in Fig 3-13 with the test function switches in position 3, enable a check to be made of the overall zero distance delay of the radio beacon.

The sawtooth sweep output of the Pulse-sweep Generator is fed to the oscilloscope as the sweep deflection voltage. Paired-pulse output of the pulse-sweep generator is fed through the TS-890A/URN-3 to interrogate the beacon. For the overall zero distance delay measurement, detected r.f. output of the TS-890A/URN-3 is fed to one
input of a two-channel mixer in the pulse-sweep generator. The r.f. output of the radio beacon is detected by the diode in the Switch Test Adapter and fed to the remaining input of the two-channel mixer. The input signals to the mixer are selected by switch contacts ganged to a crystal selector switch.

The mixer presents the interrogation signal, at both the input and output of the beacon, to the oscilloscope for display.

Assuming proper delay, the input and output signals will be almost superimposed. By means of crystal timing circuits in the pulse-sweep generator, the interrogation signals are spaced at precise intervals to provide a time reference used for measurement of the overall delay of the radio beacon. This reference delay will be either 49.8 or $50.2 \mu \mathrm{sec}$, depending on the setting of the crystal selector switch. The sweep period will be exactly half this figure so the two sweeps correspond to one reference delay interval. The output pulse will be displayed approximately $1000 \mu \mathrm{sec}$ after the input pulse at a precise multiple of the reference delay. Because of the sweep multiplication provided by using two sweeps per delay interval, any small error in the timing of the overall zero distance radio beacon delay will cause a noticeable shift in the superimposition of the input and output pulse pairs displayed on the oscilloscope screen. By checking the superimposition at the 49.8 and $50.2 \mu$ sec reference delays, it may readily be determined that the beacon delay is between these two figures and is, therefore, within tolerance.
(6) Replacement Test Equipment (TABLE 1-2b).
(a) Overall Zero Distance Delay. -For the following operating test no external connections are required between the radio beacon and the test equipment; all connections are automatically made as the switch positions and coaxial links are selected in accordance with the specific setting up instructions. A 1 kHz signal, from the Power Meter - Pulse Counter MM-109, is fed to the Spectrum Analyzer modulator circuit whose $3 \mu \mathrm{sec}$ output pulse provides (i) MOD SYNC pre-trigger (via MM-109) for the oscilloscope, (ii) initiation of gate triggering in the pulse counter circuitry and (iii) an output to the modulator final driver assembly, hence the RF modulator. The output of the modulator is fed (a) via the Transfer and Switching Unit for use as interrogation pulses and (b) via the function switch of the MM-109 to the oscilloscope, where it is displayed as the interrogation pulse.

The beacon reply pulses are fed from the Transfer and Switching Unit to the Power Meter - Pulse Counter and simultaneously to the oscilloscope for display.

For this operating test, by displaying both the interrogation pulse and the reply pulse on the same sweep, and using the 10 and $1 \mu \mathrm{sec}$ markers it is possible to determine the overall delay time between interrogation of the radio beacon and the transmission of the reply pulses.

## (7) GENERAL TEST PURPOSES.

(a) Original Test Equipment (TABLE 1-2). FUNCTION SWÏTCH IN POSITION 4. - When the TEST FUNCTION switches are placed in position 4 , the input connections of the oscilloscope are removed. Each one of the test units may then be used as an independent piece of test equipment. The oscilloscope sweep and signal circuits may then be adjusted by means of front panel controls for observation of any desired waveform in the equipment. Signal and sync. voltages may be fed to the oscilloscope by means of flexible test leads. With this arrangement, the number of operating tests is extended to include any which may be later conceived and the test equipment may be used as an aid in troubleshooting the radio beacon.
(b) Replacement Test Equipment (TABLE 1-2b).When the FUNCTION switches of the Power Meter - Pulse Counter - Marker Generator MM-109 and spectrum Analyzer/ Test Generator MM-705 are set to the positions listed below each one of the test units may be used as an independent piece of test equipment. This facility extends the number of operating tests to include those which may be used as an aid in troubleshooting the radio beacon.

1. Power Meter - Pulse Counter - Marker Generator MM-109. Function Switch Position: GEN TEST.-In this position any suitable input at the front panel COUNTER INJPUT socket is routed via the Input Amplifier, Counter Control circuit etc., to the Decade Counting Unit. With the MODE switch also set to the GEN TEST position both positive and negative pulses may be counted. The counter will operate properly only when the output of the Input Section has a positive output of the proper amplitude. Thus, when the MODE switch is in the minus position, an inverter with a gain of 1 is switched into the circuit to invert the signal from negative to positive; when the MODE switch is set for a 'plus' input, the connection is straight through and the inverter is by-passed.

The Oscilloscope MM-504 has no built-in marker generator facility, therefore when these are required it is necessary to have the MM-109 switched on in order to provide them. On the MM-109, a facility is provided whereby the marker generator output is available at the front panel MARKER OUTPUT socket and may be used for more accurate measurement of pulse intervals.
2. Spectrum Analyzer/Test Generator MM-705. Function Switch position: IF SIG GEN. - In this position the 63 MHz signal generator provides a CW sinusoidal signal, via the front panel ATTEN socket, whose frequency is variable from 60.5 to 65.5 MHz with a capability of being set to $63.0000 \mathrm{MHz} \pm 0.005 \%$. The power output is variable (via the attenuator) from 0 to -110 dBm ; calibrated to an accuracy of $\pm 2 \mathrm{~dB}$ over the range from 0 to -100 dBm . The signal at the FUNCTION SW socket has the same frequency characteristics as described above except that the power output is fixed at 0 dBm . When the connection link is placed between PWR BRIDGE and FUNCTION SW the

AVERAGE POWER meter is used to monitor the output signal power level of the IF Signal Generator.

POWER METER ZERO SET.- When the FUNCTION switch is in this position the input to the AVERAGE POWER meter circuitry is disconnected enabling the meter to be 'zero set' by means of that control adjacent to the meter.

SA.- This the spectrum analyzer position of the FUNCTION switch whereby the variable attenuator output is connected to the input of the double super-heterodyne receiver. The output of the receiver, at the 2 nd IF amplifier, is connected to the AVERAGE POWER meter.

The BAND SHIFT selector switch on the front panel selects the second local oscillator frequency, which positions the centre frequency of the 500 kHz bandpass filter in the spectrum being measured. The attenuator adjusts the input signal amplitude until the AVERAGE POWER meter indicates POWER SET.

By repeating the foregoing at the various frequencies of the BAND SHIFT selector switch, and comparing the ATTENUATOR readings, the frequency spectrum can be measured. The spectrum analyzer gain is adjusted by the NOISE SET control on the front panel, for a NOISE SET indication on the AVERAGE POWER meter.

RF AVG PWR, - When in this position the FUNCTION switch provides the facility whereby the beacon average power may be measured on the AVERAGE POWER meter.

RF SIG GEN.- In this position the FUNCTION switch energizes the RF Signal Generator multiplier chain, which multiplies the master oscillator frequency to the RF output frequency before it is fed into the RF modulator. The output of the modulator is fed into a final RF cavity which has three outputs: (i) to the AVERAGE POWER meter for output level calibration (ii) via a linear detector in the MM-109, to the Oscillos cope MM-504 (if required) for viewing the RF envelope shape and calibration of the output when in the PULSE mode and (iii) via the attenuator as the RF Signal Generator output. Output (iii) can be taken from the ATTEN socket on the front panel.

RF PEAK PWR.- In this position the FUNCTION switch is responsible for routing the beacon primary or standby REF/INC power from the Transfer and Switching Unit to the peak power circuitry in the MY-109 where it is measured on the PEAK RF POWER meter of that unit. The signals are routed via the attenuator in the Spectrum Analyzer/Test Generator.

## SECTION 5

## TROUBLESHOOTING

## 5-1. GENERAL.

a. To localize troubles quickly and efficiently, the technician should become thoroughly familiar with the radio beacon, giving special attention to the following:
(1) The relationship between the radio beacon and Radio Set AN/ARN-21 in the aircraft, and how the radio beacon produces bearing and distance information and its identification call.
(2) The functions of the receiver-transmitter group, the power supply assembly, and the antenna group which comprise the radio beacon, and the relationship between these groups.
(3) The functions of each of the units that make up the groups.
(4) The symptoms of malfunctioning of the radio beacon, of any of the groups, and of any component unit of a group.
(5) The most probable unit or circuits in which the observed trouble may be localized.
b. When a symptom, such as failure of the transmitter output from the radio beacon, is encountered, the cause of the trouble may be localized to the exact assembly or component item by a systematic procedure. Initially, the defective group must be determined and then the defective unit within the group. Next the defective circuit must be found. Finally the trouble must be isolated to the defective assembly or part.
c. To save time and minimize disturbance of the equipment, the following troubleshooting sequence should be used as much as possible:
(1) Check for external indications of trouble.
(2) Check electronic assemblies, making a complete waveshape and voltage check.
(3) Check mechanical assemblies, making a complete visual inspection: if necessary, disassemble and examine component items.
(4) If an electrical trouble has not been isolated following completion of waveshape and voltage checks, use an ohmmeter to check resistances throughout the suspected circuit. Plugs should be disconnected and the circuit isolated from other circuits, as far as possible, to remove all resistance-shunting paths.
d. The troubleshooting information provided in this section is arranged in a manner designed to facilitate performance of the foregoing procedures. A system troubleshooting chart is included as an aid in determining the equipment group and the major components within the group which contains the trouble. The system troubleshooting chart is supplemented by
individual component unit troubleshooting charts. Each such chart includes a systematic guide to trouble localization, a servicing block diagram, a comprehensive set of signal-tracing waveshapes, and a tube socket voltage and resistance diagram. Schematic and wiring diagrams for each component unit are supplied in Section 6.
e. The troubleshooting charts contain test points which are indicated by stars 1 and circles A These test points are similarly marked by stars and circles on schematic diagrams, servicing block diagrams, and photographs to facilitate their location. The test points designated by a star (major test points) are for checking the overall functions and for localizing trouble to a functional section. The circled test points (secondary and minor test points) are for isolating causes of abnormal performance both within a specific functional section and within a specific circuit.

## 5-2. TEST EQUIPMENT AND SPECIAL TOOLS.

a. TEST EQUIPMENT.-The test equipment required to check the operational characteristics and troubleshoot the radio set are listed in tables 5-1 and 5-1a. The test equipment includes two main groups,(1) built-in test equipment and (2) standard test equipment. The test equipment of the earlier models is installed within the beacon power supply cabinet whilst that of the MM-TMC-212A is housed, with two Transponder Monitors MM-209, a Transfer and Switching unit MM-1 602 and a Transfer and State Switching Unit (TELOTEL) in the Electrical Equipment Cabinet 212A. The information contained in Section 5 applies equally to the Original and the Replacement Test Equipment, but where differences occur, these are explained in the text and appropriate drawings.

## b. SPECIAL TOOLS.-No special tools are required.

## 5-3. OVERALL TROUBLESHOOTING

Some of the troubles encountered with the radio beacon will first be detected by the aircraft and reported to the radio beacon location. The radio beacon troubleshooting chart indicates the probable cause of the trouble and refers to the appropriate unit troubleshooting chart or test procedure.
a. PRELIMINARY CHECK. - When the trouble encountered with the radio is localized.

TABLE 5-1. ORIGINAL TEST EQUIPMENT

| FIGURE <br> NO. | NAME | AN TYPE <br> DESIGNATION | ALTERNATE | USE |
| :---: | :--- | :--- | :--- | :--- |
| $3-17$ | Power Meter- <br> Pulse Counter | TS-891/URN-3 |  | Provides metered variable d-c source <br> used to bias diode of Switch-Test adapter <br> SA-420 URN-3 in power measurement. |
| $5-1$ | Switch-Test <br> Adapter | SA-420/URN-3 |  | Transfers radio beacon transmitter output <br> power from antenna to dummy load and <br> supplies detected signal to equipment. |
| $3-16$ | Oscilloscope | OS-54/URN-3 |  | Provides timing markers and calibrating <br> voltage to permit accurate measurement <br> of signal waveshape amplitude and pulse <br> width. |
| $3-14$ | Pulse Analyzer- <br> Signal Generator | TS-890A/URN-3 <br> or <br> TS-890B/URN-3 |  | Provides r-f carrier for testing beacon <br> and calibrator receiver for spectrum <br> analysis of beacon output signal. |
| $3-15$ | Pusle Sweep <br> Generator | SG-121A/URN-3 |  | Provides pulsed pairs at controlled rate <br> to simulate pulse output of one or more <br> airborne Radio Sets AN ARN-21. |
| - | Multimeter | AN/PSM-4 | TS-352/U | Checks various voltages and resistances <br> throughout Radio Set AN GRN-9D. |



Figure 5-1. Switch-Test Adapter SA-420 URN-3
table 5-1a. REPLACEMENT TEST EQUIPMENT

to Radio Set AN/GRN-9D, the initial check should be for an a-c power input.

## Note

Under normal operating conditions, EMERGENCY SWITCH S901, located on blower compartment panel of receiver-transmitter group cabinet, and MASTER switch S1101, located on control-duplexer panel, are in their ON position.

When the radio beacon is functioning normally, the following lamps are on:
(1) MAIN POWER ON lamp DS1 102, FIL ON lamp DS1101, and ANTENNA CONTROL ON lamp DS1 103 on control-duplexer panel.
(2) POWER ON lamp DS501 on receiver panel.
(3) ANTENNA CONTROL lamp DS602 on coderindicator panel.
(4) FILAMENT lamp DS1401 and OVEN lamp DS1403 on frequency multiplier-oscillator panel.
(5) FIL lamp DS1301 on amplifier-modulator panels.
(6) LV lamp DS1603, LV-MV READY lamp DS1605, and - 375 lamp DS1 601 on low-voltage power supply panel.
(7) HV lamp DS1901 and HV READY lamp DS1902 on high-voltage power supply panel.
(8) +1000 V lamp DS 1801 on medium-voltage power supply panel.
b. TEST EQUIPMENT AND SPECIAL TOOLS.-The test equipment required to perform the Radio Set troubleshooting procedure is based on using the test equipment described in tables 5-1 and 5-1a.
c. CONTROL SETTINGS.-Table 5-2 lists all preliminary control settings required when troubleshooting.

## d. SYSTEM TROUBLESHOOTING CHART.-When

 trouble develops in the radio beacon, the trouble may be localized to a particular functional section by following the instructions given in table 5-3. Technical personnel who are thoroughly familiar with the radio beacon may be able to determine which unit is not functioning properly from the trouble symptom without reference to table 5-3. In this case, the technician may refer directly to the troubleshooting chart pertaining to the unit suspected of malfunctioning.Servicing block diagrams and waveshape charts, with the waveshapes arranged in signal-tracing sequence, accompany the troubleshooting charts. It is necessary to use the servicing block diagrams together with the troubleshooting charts to isolate defective units or components. The servicing block diagrams indicate the flow of signal or power. It should be
noted that in figure 5-2 (the radio beacon servicing block diagram) the flow of the signal is from the antenna, through the radio set and back to the antenna. Where provided, monitoring jacks should be used as an aid in isolating the trouble to an individual unit or group.

Where trouble has been traced to power failure, reference should be made to the power distribution and control circuit troubleshooting chart in table 5-10. The primary power distribution schematic diagram (figure 6-15) will assist in tracing troubles in these circuits. Further assistance in trouble localization in the power distribution and control circuits is provided by the servicing block diagram presented in figure 5-25.

## 5-4. FUNCTIONAL SECTION TROUBLESHOOTING.

Tables 5-3 and 5-3a contain the necessary information to isolate a trouble existing in the radio set to a specific functional section.
a. PRELIMINARY CHECK.-Refer to paragraph 5-3a for preliminary check information.
b. TEST EQUIPMENT AND SPECIAL TOOLS.-Troubleshooting procedures included in this section require the use of built-in test equipment. Unless otherwise stated, the information contained in the following text and tables of Section 5, is equally applicable to both the Original and Replacement Test Equipment. In order to avoid confusion, information in the tables specifically referring to the Replacement Test Equipment, is printed in italics.
(1) Original Test Equipment (TABLE 5-1).-Pulse Analyzer-Signal Generator TS-890A/URN-3 operates in conjunction with Pulse-Sweep Generator SG-121A/URN-3 to provide a simulated interrogation signal that is identical to the signal received from interrogating aircraft, with the exception of the pulse pair repetition rate. Pulse pairs occur at a random frequency in aircraft interrogation signals, while the simulated signals from the pulse analyzer-signal generator contain pulse pairs which occur at a fixed frequency, dependent upon the setting of the PRF RANGE and PRF MULTIPLIER controls on the front panel of the pulse-sweep generator. By using the simulated interrogation signal provided by this test equipment, the signal can be traced from the radio receiver input, through the radio set, to the transmitter output. Before making any tests with the pulse analyzer-signal generator, the front panel controls should be set up as follows:

## Step 1. Set OUTPUT ATTENUATOR to 0 DBM.

Step 2. Set INPUT ATTEN SELECTOR control to maximum attenuation.

Step 3. Set BAND SHIFT switch to 0 .
Step 4. Set MODULATION SELECTOR to C.W.
Step 5. Set CHANNEL SELECTOR control to applicable channel.

TABLE 5-2. INITIAL CONTROL SETTINGS PRIOR TO TROUBLESHOOTING

| CONTROL | LOCATION | SETTING |
| :---: | :---: | :---: |
| EMERGENCY switch S901 | Front panel of receiver-transmitter group blower compartment | ON |
| MASTER switch S1101 | Panel of control-duplexer | ON |
| ANTENNA CONTROL switch S1102 | Panel of control-duplexer | ANTENNA CONTROL |
| FIL ON switch S1108 | Panel of control-duplexer | FIL ON |
| BATTLE SHORT switch S1107 | Panel of control-duplexer | NOR |
| Receiver ON ${ }^{\prime}$ OFF switch S502 | Panel of radio receiver | ON |
| CODER INDICATOR switch S601 | Panel of coder-indicator | ON |
| LV switch S1601 | Panel of low-voltage power supply | ON |
| MV switch S1801 | Panel of medium-voltage power supply | ON |
| HV switch S 1902 | Panel of high-voltage power supply | ON |
| HIGH VOLTAGE BREAK <br> IN OPERATE switch S1106 | Panel of power supply assembly blower compartment | OPERATE |

## Nofe

If built-in crystal oscillator is to be used as a frequency-generating source, omit steps
6. 7. and 8 .

Step 6. Set MAIN TUNING control to applicable channel.

Step 7. Set OSCILLATOR SELECTOR to V. F: O. CALIBRATE.

Step 8. Adjust V.F. O. CALIBRATE control until zero beat is heard in headphone plugged into V.F.O. CALIBRATE jack.

Step 9. Set OSCILLATOR SELECTOR switch to either REF. OSC. (for crystal control) or to V.F.O. . depending upon oscillator used as generating source.

Step 10. Adjust for zero reading on OUTPUT LEVEL indicator, using its ZERO SET control.

Step 11. Set INTERROGATE switch to ON.

## Note

Before proceeding with step 12. energize and warm up Pulse-Sweep Generator SG-121A URN-3 (figure 3-15) for at least 2 minutes.

Step 12. Set POWER SET cuntrol to midscale.
Step 13. Adjust PULSE AMPLITUDE controi on pulse-sweep generator to obtain midscale reading (100) on OUTPUT LEVEL INDICATOR.

Step 14. Adjust CHANNEL SELECTOR slightly for maximum reading on OUTPUT LEVEL INDICATOR.

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There is a time lag between application of signal to OUTPUT LEVEL INDICATOR and indication of power level. When taking readings on this meter. allow time for needle to stabilize.

Step 15. Readjust PULSE AMPLITUDE control on pulse-sweep generator to obtain midscale reading (100) on OUTPUT LEVEL INDICATOR.

Step 16. Adjust ZERO SET control of POWER COMPARISON INDICATOR to obtain zero reading on this indicator.

Step 17. Set MODULATION SELECTOR to PULSE.

TABLE 5-3. RADIO SET AN/GRN-9D. SYSTEM TROUBLESHOOTING CHART (Original Test Equipment, Table 5-1)

| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: |
| SYMPTOM: Aircraft reports that it receives no bearing, distance, and identification call information. |  |  |  |
| 1 | Check reports from other aircraft in area. | Aircraft in area report that bearing, distance, and identification information is correct. | If all aircraft in area report loss of three signal elements, beacon is at fault. Refer to step 2 and to radio beacon servicing block diagram (figure 5-2). If fault is not found, trouble is in aircraft equipment. |
| 2 | Check transmitter output bỳ connecting Oscilloscope OS-54/URN-3 through probe E1152 to each of two test points on control-duplexer panel: ANTENNA INCIDENT jack J1154 and ANTENNA REFLECTED jack J1153. Observe waveshape and measure and record peak-to-peak voltage obtained for each. | Compare with previously logged readings. A minimum of 2 to 1 incident to reflected voltage ratio should be obtained. | If there is a considerable decrease in both INCIDENT and REFLECTED readings, check transmitter. Refer to transmitter troubleshooting chart (table 5-6). If ratio of incident to reflected meter readings is low (high reflected low incident), check out $r$ - $f$ cables and connectors from directional coupler up to and including antenna central array. |
| 3 | Check waveshape at TEST OUTPUT jack J607 (panel of coder-indicator) with Oscilloscope OS-54/URN-3 and Power Meter-Pulse Counter TS-891/URN-3 test switches in position 2. | Waveshape No. 24B shown in figure 5-11 should be obtained. | If normal indication is not obtained, trouble is probably in coder-indicator. Refer to coder-indicator troubleshooting chart (table 5-5). If normal indication is obtained, proceed to step 4. |
| 4 | Check readings of D. C. SUPPLY VOLTAGE meterM1402 on front panel of frequency-multiplier oscillator with METER SELECTOR switch in positions 1 through 5. | Meter should read: | Refer to low-voltage power supply troubleshooting chart (table 5-7) if voltages read in positions 1, 2, or 3 are incorrect. Refer to mediumvoltage power supply troubleshooting chart (table 5-8) if voltages read in position 4 or 5 are incorrect. |
| 5 | Check reading of H. V. SUPPLY meter M1302 on front panel of amplifiermodulator. | Meter should read between 10,800 and 13,200 volts. | Refer to high-voltage troubleshooting chart (table 5-9) if $12,000 \pm 10 \%$-volt reading is not obtained. |
| SYMPTOM: Aircraft reports that it receives distance and identification call, but does not receive bearing information. |  |  |  |
| 1 | Check waveshape at TEST OUTPUT jack on panel of coder-indicator, with Oscilloscope OS-54/URN-3 and Power Meter-Pulse Counter TS-891/URN-3 test switches in position 2. | Waveshape No. 24B shown in figure 5-11 should be obtained. | If required waveshape is not obtained, trouble is in coderindicator. Refer to coderindicator troubleshooting chart (table 5-5). |

TABLE 5-3. RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART (cont)

| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :--- | :--- | :--- |
| 2 | Check for presence of north <br> and auxiliary trigger pulses, <br> using oscilloscope at test <br> points TP1 and TP2 in <br> coder-indicator. | North trigger pulse obtained <br> at test point TP1 should <br> appear as shown in wave- <br> shape No. 1 of figure 5-11. <br> Auxiliary trigger pulse <br> obtained at test point TP2 <br> should appear as shown in <br> waveshape No. 25 of figure <br> $5-11$. | If either one or both triggers <br> are not obtained, trouble is in <br> portion of antenna concerned <br> with trigger generation. Refer <br> to technical manual for appro- <br> priate antenna. |

SYMPTOM: Aircraft reports that it receives bearing and identification call information, but does not receive distance information.
$\left.\begin{array}{|c|l|l|l|}\hline 1 & \begin{array}{l}\text { Check readings on TEST } \\ \text { METER M501 on front panel } \\ \text { of radio receiver in all } \\ \text { positions of METER SE- } \\ \text { LECTOR Switch S501. } \\ \text { Use Power Meter-Pulse } \\ \text { Counter TS-891/URN-3 to } \\ \text { count receiver output pulses } \\ \text { at receiver TEST OUTPUT } \\ \text { jack J507. }\end{array} & \begin{array}{l}\text { Compare with logged } \\ \text { readings. }\end{array} & \begin{array}{l}\text { Reading of } 2700 \pm 90 \text { pulses } \\ \text { per second. }\end{array}\end{array} \begin{array}{l}\text { If meter readings obtained } \\ \text { differ considerably from } \\ \text { logged readings or pulse } \\ \text { count is incorrect, refer to } \\ \text { radio receiver troubleshooting } \\ \text { chart (table 5-4). }\end{array}\right\}$

SYMPTOM: Aircraft reports that it receives bearing and distance information, but does not receive identification call.

| 1 | Check waveshape at test <br> point TP8 in coder- <br> indicator. | $1,350-$ cps identification <br> tone pulses should be <br> obtained as shown in <br> waveshape No. 48 in fig- <br> ure 5-11. | If nor mal indication is present <br> at test point TP8, perform <br> step 2. If normal indication <br> is not present at test point <br> TP8, trouble is probably in <br> stages V612 through v614. <br> Signal trace through these <br> stages; refer to coder- <br> indicator troubleshooting <br> chart (table 5-5). |
| :---: | :--- | :--- | :--- |
| 2 | Check that keyer motor B602 <br> is rotating and that switch <br> S605 is closed. | Motor is rotating. | If motor is not rotating, check <br> voltages at terminals 2 and 3 <br> of terminal board TB601; <br> voltage should read 120 volts <br> ac. If voltage at terminals 2 <br> and 3 is correct, motor B602 <br> is at fault and should be <br> replaced. |

TABLE 5-3. RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART (cont)

| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: |
| 3 | Refer to identification keyer test in paragraph 6-2e(3) of Section 6. | Keyer switches operate correctly. | Reset or replace switches, if necessary. |
| SYMPTOM: Aircraft reports that it receives all message elements, but bearing information is in error. |  |  |  |
| 1 | Check antenna rotation speed and tachometer. | Required antenna rotation speed of 15 cps , or 900 rpm , will be indicated if tachometer reads 675 cps and/or 120 pps is counted at test point TP2. | If normal indications are not obtained, cause of trouble is in antenna. Refer to technical manual for appropriate antenna group. |
| 2 | Check direction of rotation of antenna spin motor. | Check that antenna is rotating in a clockwise direction, as viewed from above. | Check wiring of three-phase power to antenna from receiver-transmitter cabinet to spin motor. |
| 3 | Check reading of ANTENNA ERROR meter on panel of coder-indicator. | Meter should read in green area of scale. | If meter reads in red area, cause of trouble is in antenna. Refer to technical manual for appropriate antenna group. |
| 4 | Check 40-microsecond blanking gate at test point TP9 in radio receiver as described in paragraph 3-6a(8) of Section 3. | Blanking gate should be 40 microseconds wide and appear as shown in waveshape No. 17 of figure 5-4. | If blanking pulse is not present or is of insufficient amplitude, check stages V406 and V407B in radio receiver. Refer to radio receiver troubleshooting chart (table 5-4). If pulse is present but is of incorrect duration, adjust potentiometer R443 to obtain 40-microsecond duration. |
| SYMPTOM: Aircraft reports that it receives all message elements, but that distance information is in error. |  |  |  |
| 1 | Check overall delay as described in paragraph 3-6a(11) of Section 3. | Waveshape indicating proper delay should appear as shown in figure 3-20. | If normal indication is not obtained, check as follows: If 50 -microsecond delay is not correct, adjust delay line DL601 as described in paragraph 6-2e(5) of Section 6. If delay line does not respond to adjustment, check electrical characteristic of delay line. Replace delay line, if necessary. |

TABLE 5-3. RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART (cont)

| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :--- | :--- | :--- | :--- |
| SYMPTOM:Aircraft reports that it does not receive bearing and distance information over entire 200- <br> mile range. | Using built-in test equip- <br> ment, make peak r-f power <br> output measurement ac- <br> cording to instructions <br> given in paragraph 3-6a(2) <br> of Section 3. | Radio beacon power output <br> should be at least.7. 5 <br> kilowatts. | If normal indication is ob- <br> tained, proceed to step 2. If <br> power output is low, refer to <br> power supply troubleshooting <br> charts (tables 5-7 through 5-9) <br> and transmitter troubleshooting <br> chart (table 5-6). |
| 1 | Check transmitter output <br> by connecting Oscilloscope <br> OS-54/URN-3 through probe <br> E1152 to each of two test <br> points on control-duplexer <br> panel: ANTENNA INCI- <br> DENT jack J1154 and AN- <br> TENNA REFLECTED jack <br> J1153. Observe waveshape <br> and measure and record <br> peak-to-peak voltage ob- <br> tained for each. | Compare with previously <br> logged reading. A min- <br> imum of 2 to 1 incident to <br> reflected voltage ratio <br> should be obtained. | If normal indication is ob- <br> tained, check that siting re- <br> quirements are fulfilled. If <br> normal indication is not <br> obtained, refer to technical <br> manual for appropriate <br> antenna. |
| 2 |  |  |  |

## Note

Pulse Analyzer-Signal Generator TS-890A URN-3 is now ready for use in making tests. Upon completion of tests, shut down equipment by turning INTERROGATE and power switches to OFF position.

Step 18. Set PRF RANGE switch on pulse-sweep generator panel to 500 position.

Step 19. Set PRF MULT switch on pulse-sweep generator panel to X 1.0 position.

Step 20. Set PULSE CODING $\mu$ SEC switch on pulse-sweep generator panel to 12 position.

Step 21. Connect coaxial test lead from RF OUTPUT jack on pulse analyzer-signal generator panel to ANTENNA REFLECTED jack on control-duplexer panel.
(2) Replacement Test Equipment (TABLE 5-1a) The setting up procedure described in Para 3-6a (12), of Section 3, enables the test equipment to be used for troubleshooting the radio set. In the event of unserviceability, checks of the radiated antenna pattern accuracy, as described in Para 3-6a(12)(j), and the presence of the correct beacon parameters, according to the Monitor, will be sufficient to localize any fault to a particular area. The procedures outlined in TABLE 5-3a should serve as a broad guide in the event of system troubleshooting.
c. .CONTROL SETTINGS. - Under normal operating conditions. all power switches are left in ON position. Refer to table 5-2 for a list of control settings required prior to troubleshooting.
d. FUNCTIONAL SECTION TROUBLESHOOTING CHĀRTS. - Radio Set AN/GRN-9D includes the following five functional sections: radio receiver, coderindicator, transmitter, power supplies, and power distribution and control circuits. When used in conjunction with the voltage and resistance measurement charts, the functional section troubleshooting charts serve to isolate the defective component in any one of the five functional sections.

## Note

Safety interlocks on drawer units in which high voltages are present disconnect parts of the circuits when the drawers are pulled out. Therefore, when signal tracing or making voltage checks, the safety interlocks must be closed manually.

## WARNING

Operation of this equipment involves high voltages which are dangerous to life. Maintenance personnel must observe all safety regulations at all times when servicing the equipment. Never service equipment without the presence or assistance of another person capable of rendering first aid immediately.

## (1) TROUBLESHOOTING RADIO RECEIVER.

 (See figure 5-3). -When trouble has been localized to the radio receiver, follow the troubleshooting procedure presented in the following paragraphs to further localize the trouble to a specific component part of the receiver. After the defective part has been replaced, refer to the adjustment and alignment procedures given in paragraphs $6-2 \mathrm{~d}$ and $6-3 \mathrm{~b}(3)$ of Section 6 to restore the receiver to proper operatingTABLE 5-3a, RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART Replacement Test Equipment (TABLE 5-1a)

| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: |
| SYMPTOM: Aircraft reports that it receives no bearing, distance, and identification call information. |  |  |  |
| 1 | Check reports from other aircraft in the area and check for serviceability of beacon parameters according to the Transponder Monitor MM-209. | Aircraft in area report that bearing, distance and identification information is correct. Monitor shows beacon parameters to be present and correct. | If all the aircraft in the area report loss of three signal elements and/or if the Monitor indicates parameter failure, beacon is at fault. Refer to Step 2 and to the radio beacon servicing block diagram (Figure 5-2a). If fault is not indicated on the Monitor or found in the beacon, the trouble is in the aircraft equipment. |
| 2 | Connect the Oscilloscope MM-504, in turn, to the ANTENNA INCIDENT (J1154), jack and the ANTENNA REFLECTED (J1 153) jack on the front panel of the Control Duplexer. Observe the wave shape and measure, and re record, the peak-to-peak voltage obtained for each. | Compare with previously logged readings. A minimum of 2 to 1 incident to reflected voltage ratio should be obtained. | If there is a considerable decrease in both INCIDENT and REFLECTED readings, check the transmitter. Refer to transmitter troubleshooting chart (Table 5-6). If ratio of incident to reflected meter readings is low (high reflected low incident), check out r.f. cables and connectors from directional coupler up to and including antenna central array. |
| 3 | Connect the Oscilloscope MM-504 to the TEST OUTPUT (J607) jack on the front panel of the Coder Indicator. Adjust the Oscilloscope for a 'normal indication'. | Waveshape No 24B shown in figure 5-11 should be obtained. | If normal indication is not obtained, trouble is probably in Coder Indicator. Refer to Coder Indicator troubleshooting chart (Table 5-5). If normal indication is obtained proceed to Step 4. |
| 4 | Check readings of DC SUPPLY VOLTAGE meter M1402 on the front panel of the Frequency Multiplier Oscillator with METER SELECTOR switch in positions 1 through 5. | Meter should read: | Refer to low-voltage power supply troubleshooting chart (Table 5-7) if voltages read in positions 1,2 or 3 are incorrect. Refer to medium-voltage power supply troubleshooting chart (Table $5-8$ ) if the voltage read in position 5 is incorrect. |
| 5 | Check reading of HV SUPPLY meter M1302 on the front panel of the Amplifier Modulator. | Meter should read between 10,800 and 13,200 volts . | Refer to high-voltage troubleshooting chart (Table 5-9) if $12,000 \pm 10 \%$ volts reading is not obtained. |

SYMPTOM: Aircraft reports that it receives bearing and distance information but does not receive identification call.

| 1 | Check waveshape at Test <br> Point TP8 in Coder Indi- <br> cator. | $1,350 \mathrm{~Hz}$ identification <br> tone pulses should be <br> obtained as shown in wave- <br> shape No 48 in figure 5-11. | If normal indication is present at Test <br> Point TP8, perform Step 2. If normal <br> indication is not present at Test Point <br> TP8, the trouble is probably in stages |
| :---: | :--- | :--- | :--- |
| V612 through V614. Signal trace |  |  |  |
| through these stages; refer to Coder |  |  |  |
| Indicator troubleshooting chart (Table 5-5). |  |  |  |


| TABLE 5-3a. RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART, (cont) Replacement Test Equipment (TABLE 5-1a) |  |  |  |
| :---: | :---: | :---: | :---: |
| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| 2 | Check that keyer motor B602 is rotating and that switch S605 is closed. | Motor is rotating | If motor is not rotating, check voltages at terminals 2 and 3 of terminal board TB601; voltage should read 120 volts ac. If voltage at terminals 2 and 3 is correct, motor B 602 is at fault and should be replaced. |
| 3 | Refer to identification keyer test in paragraph 6-2e(3) of Section 6. | Keyer switches operate correctly. | Reset or feplace switches if necessary. |
| SIMPTOM: Aircraft reports that it receives all message elements, but bearing information is in error. |  |  |  |
| 1 | Check antenna rotation speed and tachometer. | Required antenna rotation speed of 15 Hz , or 900 rpm, will be indicated if tachometer reads 675 Hz and/or 120 pps is counted at TP2. | If normal indications are not obtained, cause of trouble is in antenna. Refer to technical manual for appropriate antenna group. |
| 2 | Check direction of rotation of antenna spin motor | Check that antenna is rotating in a clockwise direction, as viewed from above. | Check wiring of three-phase power supply to antenna from receiver-transmitter cabinet to spin motor. |
| 3 | Check reading of ANTENNA ERROR meter on the front panel of the Coder Indicator. | Meter should read in green area of scale. | If meter reads in red area, cause of trouble is in antenna Refer to technical manual for appropriate antenna group. |
|  | Check $40 \mu \mathrm{sec}$ blanking gate at Test Point TP9 in radio receiver as described in paragraph 3-6a(12) of Section 3. | Blanking gate should be $40 \mu \mathrm{sec}$ wide and appear as shown in waveshape No 17 of fig 5-4. | If blanking pulse is not present or is of insufficient amplitude, check stages $V 406$ and $V 407 \mathrm{~B}$ in radio receiver. Refer to radio receiver troubleshooting chart (Table 5-4). If pulse is present but is of incorrect duration, adjust potentiometer R4; 3 to obtain $40 \mu s e c$ duration. |
| SYMPTOM: Aircraft reports that it receives distance and identification call but does not receive bearing information. |  |  |  |
|  | Connect the oscilloscope MM-504 to the TEST OUTPUT (J607) jack on the front panel of the Coder Indicator. Adjust the oscilloscope for a 'normal indication' | Waveshape No 24 B shown in figure 5-11 should be obtained. | If normal indication is not obtained, the trouble is probably in the Coder Indicator. Refer to the Coder Indicator troubleshooting chart (Table 5-5). |
| 2 | Check for the presence of North and Auxiliary trigger pulses, using the Oscilloscope at the Test Points TP1 and TP2 in the Coder Indicator. | North trigger'pulse obtained at Test Point TPI should appear as shown in waveshape No lof figure 5-11. Auxiliary trigger pulse obtained at Test Point TP2 should appear as shown in waveshape No 25 of figure 5-11. | If either one or both triggers are not obtained, trouble is in portion of antenna concerned with trigger generation. Refer to technical manual for appropriate antenna. |


| TABLE 5-3a. RADIO SET AN/GRN-9D, SYSTEM TROUBLESHOOTING CHART (cont)Replacement Test Equipment (TABLE 5-la) |  |  |  |
| :---: | :---: | :---: | :---: |
| STEP | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| SYMPTOM: Aircraft reports that it receives bearing and identification call information, but does not receive distance information. |  |  |  |
|  | Check readings on TEST METER M501 on the front panel of radio receiver, in all positions of METER SELECTOR switch S501. <br> Set the FUNCTION switch of the Power Meter - Pulse Counter - Marker Generator MM-109 to GEN TEST and connect the COUNTER INPUT socket to the TEST OUTPUT (J507) jack on the receiver front panel. | Compare with logged readings. <br> Reading of $2700 \pm 90$ pulses per second. | If meter readings obtained differ considerably from logged readings, or pulse count is incorrect, refer to radio receiver troubleshooting chart (Table 5-4). |
|  | Check tuning of preselector 21153. |  | If preselector is improperly tuned, retune according to the instructions given in paragraph 2-5f(2) of Section 2. Check cabling and connection between preselector and mixer stage of radio receiver. |
| Sympun: Aircraft reports that it receives all message elements, but that distance information is in error. |  |  |  |
|  | Check overall delay as described in paragraph 3-6a(12) of Section 3. | Waveshape indicating proper delay should appear as shown in figure 3-20 | If normal indication is not obtained, check as follows: If 50usec delay is not correct, adjust delay line DL601 as described in paragraph 6-2e (5) of Section 6. If delay $\overline{1} i n e$ does not respond to adjustment, check electrical characteristic of delay line. Replace delay line, if necessary. |
| Trn $\quad \ddot{u}_{\cdots}$ Aircraft reports that it does not receive bearing and distance information over entire 200 -mile range. |  |  |  |
|  | Using the built-in test equipment, make peak r.f. power output measurement according to instructions given in paragraph 3-6a(12) of Section 3. | Radio beacon power output should be at least 7.5 kilowatts. | If normal indication is obtained, proceed to Step 2. If power output is low, refer to power supply troubleshooting chart (Table 5-6). |
| 2 | Check transmitter output by connecting the Oscilloscope in turn to the ANTENNA INCIDENT (J1154) jack and the ANTENNA REFLECTED (J1153) jack on the front panel of the Control Duplexer. Observe the waveshape and measure, and record, the peak-to-peak voltage obtained for each. | Compare with previously logged readings. A minimum of 2 to 1 incident to reflected voltage ratio should be obtained. | If normal indication is obtained, check that siting requirements are fulfilled. If normal indication is not obtained, refer to technical manual for appropriate antenna. |
|  | If normal indication is. obtained, proceed to Step 2, If power output is low; refer to power supply troubleshooting charts (Tables 5-7 through 5-9) and transmitter troubleshooting chart (Table 5-6). |  |  |



condition. Illustrations containing information which will aid the technician in troubleshooting the radio receiver are included in both this section and in Section 6.
(a) PRELIMINARY CHECK, - When trouble has been Iocalized to the radio receiver, the initial check is for an a-c power input to the radio receiver. If POWER ON lamp DS501 is off when receiver ON/ OFF switch S502 is in the ON position, check the radio receiver interlock for damage and the condition of line fuses F501 and F502. Fuse failure is indicated by a glowing lamp in the fuseholder. Also check that all tube filaments are on.

## (b) TEST EQUIPMENT AND SPECLAL

TOOLS. - The test equipment required to perform the radio receiver troubleshooting procedure is based on using the built-in test equipment. This equipment is housed in the power supply assembly cabinet and consists of a power meter-pulse counter, an oscilloscope, a pulse analyzer-signal generator, and a pulse-sweep generator. No special tools are required to perform this procedure.
(c) CONTROL SETTINGS. -Table 5-2 lists the preliminary settings of all controls required when troubleshooting.
(d) RADIO RECEIVER TROUBLESHOOTENG

CHART. - When trouble has been localized to the radio receiver, follow the troubleshooting procedure given in table 5-4 to further localize the trouble to a specific component part of the radio receiver.
(e) ILLUSTRATIONS. - Illustrations containing information which will aid the technician in troubleshooting the radio receiver are as follows:

1. Figure 5-3. Radio Receiver R-824/ URN, Servicing Block Diagram
2. Figure 5-4. Radio Receiver R-824/ URN, Signal-Tracing Waveshapes
3. Figures 5-5 through 5-8. Radio Receiver R-824/URN, Tube Socket Voltage and Resist. ance Diagrams
4. Figures 5-9 and 6-5. Radio Receiver R-82\&/URN, Test Point Location Illustrations
5. Figure 6-17. Radio Receiver R-824/

URN, Schemätic Diagram

TABLE 5-4. RADIO SET AN/GRN-9D, RADIO RECEIVER, FUNCTIONAL SECTION
TROUBLESHOOTING CHART
(Information in italics refers to the Replacement Test Equipment of Table 5-1a).

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 1 | See figures 5-3 and 6-17 | Check readings of TEST METER M501 on radio receiver panel with METER SELECTOR switch S501 in the following positions: $\text { B }+200 \mathrm{VFS}$ <br> C-200VFS | Reading of $150 \pm 5$ volts is normal. (Meter reading of 75 indicates 150 volts.) <br> Reading of $-105 \pm 5$ volts is normal. (Meter reading of 52.5 indicates -105 volts.) | If readings show power supply to be operating normally, proceed to step 2. <br> If reading is incorrect, check that potentiometer R507 is set correctly and readjust if necessary. Replace tubes V501, V503, V504, and V505. If trouble persists, take voltage and resistance measurements from tube sockets and compare with values given in figure 5-5. <br> If reading is incorrect, replace tubes V502 and V506. If trouble persists, take voltage and resistance measurements from tube sockets and compare with values given in figure 5-5. |
| 2 | $\begin{aligned} & \text { See figures } \\ & 5-3 \text { and } 6-17 \end{aligned}$ | Set METER SELECTOR switch S501 to CR201 and then to CR202, noting reading on TEST METER M501 for each position. | Half-scale deflection at each position is normal | If normal indication is obtain ed, proceed to step 3. If reading is incorrect, replace diode CR201 and CR202. If trouble persists, check continuity of cable between jack J502 on preamplifier mixer chassis and jack J1502 on frequency multiplier-oscillator r-f chassis and refer to transmitter troubleshooting chart (table 5-6). |
| 3 |  | Check receiver sensitivity as described in paragraph 3-6a(7) and $3-6 \underline{a}(12)(f)$. <br> Check squitter count as described in paragraph 306a(6) and 3-6a(12)(a). | Minimum requirement is 93 db at 60 -percent replies. <br> Squitter circuit requirement is $2,700 \pm 90$ pps. | If requirement is not met, perform steps 4 through 16 , in the order given, until cause of trouble is located. <br> If squitter rate is low (less than 500 pps ), check for: Open circuit between plug P302 on i-f amplifier and jack J402 on receiver video chassis; replace cables, if necessary. Open circuit |

TABLE 5-4. RADIO SET AN/GRN-9D, RADIO RECEIVER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 3 \\ \text { (cont) } \end{gathered}$ |  |  |  | between plug P303 and jack J203 on i-f amplifier; replace cable, if necessary. Tube V405A weak or inoperative; replace tube, if necessary. If squitter rate is excessively high (above 15, 000 pps), check for: Open circuit between plug P401 on video chassis and jack J301 on i-f amplifier. (This condition is accompanied by squitter voltage above - 10 volts.) Replace cable if necessary. Defective stages V407, V408, V409A, and V409B; replace tubes, if necessary. If squitter rate is high or low. but holding constant, check that potentiometer R427 is set correctly; readjust if necessary. Perform steps 4 through 16 , in the order given, until cause of trouble is found. |
| 4 | See figures 5-3, 6-5, and 6-17 | Set oscilloscope sweep rate at 16 microseconds per inch and connect vertical input jack on oscilloscope to test prod. <br> Connect test prod to pin 2 at tube V401 ( 12 volts peak-to-peak). | Waveshape No. 19 shown in figure 5-4, (blanking pulse). | If blanking pulse is not present at pin 2 of tube V401, check for pulse at jack J506. If pulse is present, then diode CR402 is defective; replace diode. If pulse is not present at jack J506, check for open cable between video chassis of frequency multiplieroscillator and radio receiver; replace cable, if necessary. Check preselector tuning. Refer to paragraph 2-5f(2) of Section 2. Retēr to transmitter troubleshooting chart (table 5-6). |

TABLE 5-4. RADIO SET AN/GRN-9D, RADIO RECEIVER, FUNCTIONAL SECTION
TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 5 |  | Check tube voltage and resistance measurements of stages V201, V202 and V203 (figure 5-7). | Refer to tube voltage and resistance diagram (figure 5-7). | Check for faulty tubes, then check for faulty component. Replace defective tubes and components. Realignment of preamplifier stages should not be attempted unless test equipment required in preamplifier alignment procedure is available. |
| 6 | See figures 5-3, 5-9, and 6-17 | Set oscilloscope sweep rate to 36 microseconds per inch and connect vertical input jack of oscilloscope to test prod. <br> Connect test prod to test point TP2 and then TP3. | Ferris discriminator output pulses should appear as shown in waveshapes No. 1 and 2 of figure 5-4. | If normal indication is obtained. proceed to step 9. If normal indication is not obtained, proceed to step 7. |
| 7 | See figures 5-3, 5-9, and 6-17 | Set oscilloscope sweep rate to 10 microseconds per inch and connect test prod to test point TP1. | Pulse-pair waveshape with accompanying grass. | If normal indication is oltained, replace tubes V305 and V306. If substitution of these tubes does not clear receiver fault, take voltage and resistance measurements from tube sockets XV305 and XV306, comparing them with values given in figure 5-6. Replace defective components. If normal indication is not obtained, replace tubes V301 through V304. If trouble persists, proceed to step 8. |
| 8 |  | Check tube voltage and resistance measurements of stages V301 through V304. | Refer to i-f amplifier tube socket voltage and resistance diagram (figure 5-6). | Replace defective components. |
| 9 | See figures 5-3. 5-9, and 6-17 | Set oscilloscope sweep rate at 40 microseconds per inch and connect test prod to test point TP5 (7. 5 volts peak-to-peak). | Waveshape No. 5 shown in figure 5-4. | If normal indication is obtained, proceed to step 10. If normal indication is not obtained, replace tubes V307 and V308. If trouble persists, take voltage and resistance measurements from tube sockets XV307 and XV308, comparing them with values |

TABLE 5-4. RADIO SET AN/GRN-9D, RADIO RECEIVER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 9 \\ \text { (cont) } \end{gathered}$ |  |  |  | given in figure 5-6. Replace defective components. |
| 10 | See figures 5-3. 6-5. and 6-17 | Connect test prod to pin 1 at tube V402 ( 30 volts peak-to-peak). | Waveshape No. 6 shown in figure 5-4. | If normal indication is obtained, proceed to step 11. If normal indication is not obtained, tube V402 is defective. Replace tube V402. If trouble persists, take voltage and resistance measurements from tube socket, comparing them with values given in figure 5-8. |
| 11 | See figures 5-3. 6-5. and 6-17 | Connect test prod to pin 7 of tube V402 ( 20 volts peak-to-peak). | Waveshape No. 7 shown in figure 5-4. | If normal indication is obtained, proceed to step 13. If normal indication is not obtained, proceed to step 12. |
| 12 | See figures 5-3. 5-9. and 6-17 | Connect test prod to test point TP9 (18 volts peak-to-peak). | Waveshape No. 17 shown in figure 5-4. | If normal indication is obtained, replace tube V401. If pulse width is incorrect, readjust potentiometer R443. If pulse is not observed, replace tubes V406 and V407. If trouble persists, proceed to step 13. |
| 13 | (F1) <br> See figures 5-3. 6-5, and 6-17 <br> See figures 5-3, 6-5, and 6-17 | In sequential order, connect test prod to: Pin 7 at tube V403 (10 volts peak-to-peak). <br> Note <br> Adjust potentiometer R456 to eliminate negative overshoot. <br> Pin 1 at tube V403 (8 volts peak-to-peak). | Waveshape No. 8 shown in figure 5-4. <br> Waveshape No. 9 shown in figure 5-4. | If normal indication is observed at both pins, proceed to step 14. If normal indication is observed at pin 7 but not at pin 1, delay line DL401 or potentiometer R410 is defective. If normal indication is not obtained at both pins, tube V402B is defective. Replace tube V402. If trouble persists, take voltage and resistance measurements, comparing them with values given in figure 5-8. |
| 14 | See figures 5-3, 6-5, and 6-17 | Set oscilloscope sweep rate at 3 microseconds per inch and connect test prod to pin 5 at tube V403 (30 volts peak-topeak). | Waveshape No. 11 shown in figure 5-4 obtained only when 12 microsecond pulse pairs appear at output of tube V204B. | If normal indication is obtained, proceed to step 15. If normal indication is not obtained, replace tube V403. |

TABLE 5-4. RADIO SET AN/GRN-9D, RADIO RECE_VER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 15 | See figures 5-3, 5-9, and 6-17 | Connect test prod to test point TP8 (25 volts peak-to-peak). | Waveshape No. 15 shown in figure 5-4. | If normal indication is observed. proceed to step 16. If normal indication is not obtained, replace tube V404. |
| 16 | See figures 5-3 and 6-17 | Connect test prod to test point TP7 (25 volts peak-to-peak). | Waveshape No. 14 shown in figure 5-4. | Replace tube V405. If trouble persists, take voltage and resistance measurements from tube sockets XV404 and XV405, comparing them with values given in figure 5-8. |



## LOCATION: TP2

Sweep Rate: $36 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: $5 \mathbf{~ V} \mathbf{~ p p}$
Remarks: Discriminator V306B output.


## LOCATION: TP3

Sweep Rate: $36 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 2 V pp
Remarks: Discriminator V306A output.

LOCATION: Grid (pin 2) V307A video amplifier
Sweep Rate: $36 \mu \mathrm{sec} / \mathrm{in}$.
Measurement:
Remarks: Clipper V308A defective if excessive positive overshoot appears.

```
LOCATION: Grid (pin 7) V307B video ampli-
    fier
    Sweep Rate: 36 \musec/in.
    Measurement:
    Remarks: Clipper V308B is defective if any
        negative overshoot appears.
```



Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 1 of 6 )

LOCATION: TP5 grid (pin 2 V402) 1st video amplifier
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 7.5 V pp
Remarks: Negative pulse pair; $12 \mu \mathrm{sec}$ between pulses; $3 \mu$ sec pulse width.

## LOCATION: Plate (pin 1) V402

Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 30 V pp
Remarks: Positive pulse pair; $12 \mu \mathrm{sec}$ between pulses; $3 \mu$ sec pulse width.


## LOCATION: Grid (pin 7) V402

Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 20 V pp
Remarks: Negative pulse pair; $12 \mu \mathrm{sec}$ between pulses; $1 \mu \mathrm{sec}$ pulse width.


LOCATION: Suppressor grid (pin 7) V403, Decoder
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 10 V pp
Remarks: Undelayed pulse pair, $12 \mu \mathrm{sec}$ between pulses; $1 \mu \mathrm{sec}$ pulse width. Adjust R456 to eliminate negative overshoot.


Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 2 of 6)

LOCATION: Grid (pin 1) V403, Decoder
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 8 V pp
Remarks: Pulse pair delayed by $12 \mu \mathrm{sec} .12 \mu \mathrm{sec}$ between pulses; $1 \mu \mathrm{sec}$ pulse width.

9

LOCATION: Composite of waveforms at pins 1 and 7 of V403
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: (a) pin 7, V403
(b) pin 1, V403
(c) pin 5, V403

Remarks: Shows operation of delay line (DL401) - decoder (V403).


LOCATION: Plate (pin 5) of V403, Decoder
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 30 V pp
Remarks: Decoded pulse. Obtained only when $12 \mu \mathrm{sec}$ spaced pulse pairs appear at output of V402B.

LOCATION: TP8 Cathode (pin 2), V404 or grid (pin 7) V405
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 25 V Pp
Remarks: $4 \mu \mathrm{sec}$ pulse width.


Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 3 of 6)

```
LOCATION: TP8 - Same as above
    Sweep Rate: }3\mu\textrm{sec}/\textrm{in}
    Measurement: 25 V pp
    Remarks: 1 \musec markers added to measure
        4 \musec pulse width.
```


LOCATION: TP7 VIDEO OUTPUT
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 25 V pp
Remarks: Single pulse 3-4 $\mu \mathrm{sec}$ wide. Input
pulse to coder-indicator.


LOCATION: Grid (pin 3) V406 Blanking multivibrator input
Sweep Rate: $16 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 22 V pp; $40 \mu \mathrm{sec}$ wide Remarks:


```
LOCATION: Cathode (pin 8) V406 Blanking
    multivibrator output
    Sweep Rate: }16\mu\textrm{sec}/\textrm{in
    Measurement: 23 V pp, 40 \musec wide
    Remarks:
```



Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 4 of 6)

LOCATION: TP9) or suppressor grid (pin 7) V401 Blanking gate
Sweep Rate: $16 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 18 V pp, $40 \mu \mathrm{sec}$ wide
Remarks: If pulse is not $40 \mu \mathrm{sec}$, adjust R443 BLANKING TIME ADJ pot. (See waveform below)


## LOCATION: TP9 or V401, pin 7

Sweep Rate: $16 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 18 V pp, $40 \mu \mathrm{sec}$ wide
Remarks: $10 \mu \mathrm{sec}$ markers added to check pulse width and permit adjustment of R443.

LOCATION: Cathode (pin 2) V401, Blanking gate
Sweep Rate: $16 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 12 V pp, $10 \mu \mathrm{sec}$ width Remarks:


## LOCATION: TP6 or J403

Sweep Rate: $4 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: $3 \mathrm{~V} \mathrm{pp}, 3 \mu \mathrm{sec}$ pulse width
Remarks: $12 \mu \mathrm{sec}$ between pulses of pair.


Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 5 of 6)

```
LOCATION: TP6 or J403
Sweep Rate: \(4 \mu \mathrm{sec} / \mathrm{in}\).
Measurement: 3 V pp, \(3 \mu \mathrm{sec}\) wide
Remarks: Same as above, \(1 \mu \mathrm{sec}\) marker added for measurement, of pulse duration and spacing.
```



## LOCATION: J407 TEST OUTPUT jack

Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 25 V pp, 3-4 $\mu \mathrm{sec}$ wide Remarks:


LOCATION: J407 TEST OUTPUT jack
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 25 V pp, 3-4 $\mu \mathrm{sec}$ wide
Remarks: $1 \mu \mathrm{sec}$ markers added to measure pulse width.


LOCATION: J407 TEST OUPUT jack
Sweep Rate: $1600 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 25 V pp
Remarks: Part of video output pulse train of radio receiver. Complete pulse train should be 2700 pulse/second.


Figure 5-4. Radio Receiver R-824/URN, Signal-Tracing Waveshapes (Sheet 6 of 6 )


| $V$ | 105 |
| :--- | :--- |
| $R$ | $I$ MEG |
| $V$ | $150 V$ |
| $R$ | $6 K$ |
| $V$ | 265 |
| $R$ | 150 |
| $V$ | 1 MEG |

NOTES:
I. READINGS TAKEN WITH A MULTIMETER HAVING A RESISTANCE OF 1,000 AND 20,000-OHMS-PER-VOLT FOR AC AND DC MEASUREMENTS, RESPECTIVELY

KEY TO SYMBOLS
v indicates dc Voltage to ground unless OTHERWISE SPECIFIED
R INDICATES DC RESISTANCE TO GROUND

* MEASURED beTWEEN PINS 2 OR 8 OF V5OI
* 6.3V AC BETWEEN PINS MARKED WITH 2 ASTERISKS
$\cdots * * 5.0 \mathrm{~V}$ AC BETWEEN PINS MARKED WITH 3 ASTERISKS

Figure 5-5. Radio Receiver R-824/URN, Power Supply, Tube Socket Voltage and Resistance Diagram


Figure 5-6. Radio Receiver R-824/URN, I-F Amplifier, Tube Socket Voltage and Resistance Diagram


Figure 5-7. Radio Receiver R-824/URN, Preamplifier and Mixer, Tube Socket Voltage and Resistance Diagram


Figure 5-8. Radio Receiver R-824/URN, Video Chassis, Tube Socket Voltage and Resistance Diagram


Figure 5-9. Radio Receiver R-824/URN, Right Side View, Test Point Location
(2) TROUBLESHOOTING CODER-INDICATOR. (See figure 5-10). - When trouble has been localized to the coder-indicator, follow the troubleshooting procedure presented in the following paragraphs to further localize the trouble to a specific component part of the coder-indicator. After the trouble has been corrected, refer to paragraph 6-2e of Section 6 for circuit adjustment procedures. Chēck that circuits associated with repaired or replaced components are properly adjusted. Illustrations containing information which will aid the technician in troubleshooting the coder-indicator are included in both this section and in Section 6.
(a) PRELIMINARY CHECK. - When trouble has been Tocalized to the coder-indicator the initial check is for an a-c power input to the coder-indicator. If POWER ON lamp DS601 is off when CODER INDICATOR switch 5601 is in the ON position, check the coder-indicator interlock for damage and the condition. of line fuses F601 and F602. Fuse failure is indicated by a glowing lamp in the fuseholder. Also check that all tube filaments are on.

## (b) TEST EQUIPMENT AND SPECIAL

TOOLS. - The test equipment required to perform the coder-indicator troubleshooting procedure is based on using the built-in test equipment. This equipment is housed in the power supply assembly cabinet. No special tools are required to perform this procedure.
(c) CONTROL SETTINGS. - Table 5-2 lists the preliminary settings of all controls required when troubleshooting.
(d) CODER-INDICATOR TROUBLESHOOTING CHA $\overline{R T}$. - When trouble has been localized to the coder-indicator, follow the troubleshooting procedure given in table 5-5.
(e) ILLUSTRATIONS. -Illustrations containing information which will aid the technician in troubleshooting the coder-indicator are as follows:

1. Figure 5-10. Coder-Indicator KY-382/GRN-9D, Servicing Block Diagram
2. Figure 5-11. Coder-Indicator KY$382 /$ URN-9D, Signal-Tracing Waveshapes
3. Figures 5-12 and 5-13. CoderIndicator K $\bar{Y}-382 / G R N-9 D$, Tube Socket Voltage and Resistance Diagrams
4. Figures 5-14, 6-52, and 6-53. CoderIndicator KY-382/GRN-9D, Test Point Location Illustrations
5. Figures 6-21 through 6-23. CoderIndicator KY-382/GRN-9D, Schematic Diagrams

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATI ON | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 1 | See figures 5-10 and 6-23 <br> See figures 5-10 and 6-23 | Set oscilloscope sweep rate to 120 microseconds per inch. Connect coaxial test lead from TEST OUTPUT jack J607 on coder-indicator panel to vertical input jack of oscilloscope. <br> Connect coaxial test lead from SYNC OUTPUT jack J606 on coderindicator panel to external trigger input jack on oscilloscope. |  |  |
| 2 |  | Lock in signal on oscilloscope. | Waveshape No. 24A shown in figure 5-11.. | If oscilloscope presentation agrees with normal indication, verify correct output pulse count by performing steps 3 and 4 . If oscilloscope presentation is incorrect (output waveshape missing), perform steps 7 through 16, in the order given, until cause of trouble is located. |
| 3 |  | Set COUNTER SELECTOR switch and FUNCTION SWITCH on power meter-pulse counter panel to + and GENERAL TESTING positions, respectively. |  |  |
| 4 |  | Connect coaxial test lead from TEST OUTPUT jack J607 to counter input jack on power meter-pulse counter panel. | Reading of 2, 700 pps should be indicated on pulse count meter of power meter-pulse counter panel. | If normal pulse count is not obtained, proceed to step 5. |
| 5 | See figures 5-10 and 6-23 <br> See figures 5-10 and 6-23 | Connect coaxial test lead from TEST OUTPUT jack J607 to vertical input jack on oscilloscope. <br> Connect coaxial test lead from SYNC OUTPUT jack J606 to external trigger input jack on oscilloscope. |  |  |

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 6 |  | Check each component of output pulse train by varying horizontal sweep speed to lock in on each component. (See waveshapes No. 24A through 24C in figure 5-11 for recommended sweep speed.) <br> Note <br> If normal indications required in steps 1 through 6 are obtained, it may be assumed that coderindicator is operating properly. | Reference bursts should appear as shown in waveshape No. 24B of figure 5-11. Interrogation pulse from receiver should appear as shown in waveshape No. 24 C of figure 5-11. The 12-microsecond coding of output pulses should appear as shown in waveshape No. 24D of figure 5-11. | If both $15-$ and $135-\mathrm{cps}$ reference pulse bursts are missing or incorrect, proceed to step 8. If only $15-\mathrm{cps}$ reference bursts is missing or incorrect, proceed to step 12. If only $135-\mathrm{cps}$ reference burst is missing or incorrect, proceed to step 13. If both identification code and output of radio receiver -are missing, proceed to step 14. If output of radio receiver is missing (distance interrogations and squitter pulses). proceed to step 14 . If identification call pulses are missing, perform steps 15 and 16 . If pulses are not double coded. proceed to step 10. |
| 7 |  | Connect Multimeter AN/PSM-4 to the following points and ground: <br> Terminal 1 of terminal board TB701 (B+) <br> Terminal 6 of terminal board TB701 (bias voltage) | B+ Should be +250 volts dc <br> Bias voltage should be -105 volts de | If both B + and bias voltages are missing. check fuses F601 and F602 and POWER ON lamp DS601 on front panel of coderindicator. If POWER ON lamp and FUSE BLOWN indicator lamps are out, check interlocks, OFF-ON switch, and power wiring to unit. If fuse is blown, replace fuse and turn on equipment. If fuse continues to blow, a short in coder-indicator is indicated. To localize short, make the following checks: Isolate load by lifting wires at terminals 1 and 6 of terminal board TB704. If fuse does not blow when power is reapplied, short is in load circuits. If fuse does blow, proceed as follows: |

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 7 \\ \text { (cont) } \end{gathered}$ |  |  |  | Lift leads from terminals 2 and 3 of terminal board TB601 to isolate keyer motor B602. If fuse does not blow, check keyer motor. Replace keyer motor if necessary. If - 105-volt portion of power supply fails, replace tubes V702 and V705. If -250 -volt portion of power supply fails, replace tubes V701, V702, V704, and V705. If trouble persists after tube replacement, take voltage and resistance measurements and compare them with values given in figure 5-12: |
| 8 |  | Set oscilloscope sweep rate to 120 microseconds per inch and connect test prod to vertical input jack of oscilloscope. |  |  |
| 9 | See figures 5-10, 6-21, and 5-14 <br> See figures 5-10, 6-21, and 5-14 | Connect test prod to the following points: <br> Pin 2 at tube V605 (75 volts peak-to-peak). <br> Pin 1 at tube V605 (117 volts peak-to-peak). | Wareshape No. 13 'shown in figure 5-11. <br> Waveshape No. 14A shown in figure 5-11. | If nọrmal indication is not obtained at pin 2 of tube V605, proceed to step 11. <br> If normal indication is not obtained at pin 1 of tube V605, proceed to step 14. |
| 10 | See figures 5-10, 5-14. and 6-21 | Set oscilloscope sweep rate to 40 microseconds per inch and in sequenthal order, connect test prod to the following points: <br> Test point TP4 (70 volts peak-to-peak). | Waveshape No. 16 shown in figure 5-11. | If normal indication is not obtained, replace tube V605. |

TABLE 5-5. RADIO SET AN,'GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\stackrel{10}{(\text { cont })}$ | L <br> See figures 5-10, 6-21, and 5-14 | Pin 6 at tube V606 (90 volts peak-to-peak). | Waveshape No. 18 shown in figure 5-11. | If normal indication is not obtained, replace tube V606. |
|  | See figures 5-10, 5-14, and 6-21 | Tap 1 at delay line DL601 (500 volts peak-to-peak). | Waveshape No. 19 shown in figure 5-11. | If normal indication is not obtained, test transformer T603, L604, and capacitor C614. |
|  | See figures 5-10, 5-14, $6-21$, and 6-52 | Pin 2 at tube V607 (14 volts peak-to-peak). | Waveshape No. 20 shown in figure 5-11. | If normal indication is not obtained, test delay line DL601, diodes CR601 and CR602, and associated components. |
|  | see figures 5-10, 5-14, 6-21, and 6-52 | Pin 2 at tube V615 (63 volts peak-to-peak). | Waveshape No. 21 shown in figure 5-11. | If normal indication is not obtained, tube V607A is defective. Replace tube V607. |
|  | See figures 5-10, 5-14, 6-21, and 6-52 | Pin 6 at tube V615 (75 volts peak-to-peak). | Waveshape No. 23 shown in figure 5-11. | If normal indication is not obtained, replace tube V615. If normal indication is obtained, tube V607B is defective. Replace tube V607. <br> If trouble persists after tube substitution, take voltage and resistance measurements from tube sockets and compare them with values given in figure 5-13. |
| 11 |  | Set oscilloscope sweep rate to 120 microseconds per inch and, in sequential order, connect test prod to the following points: |  |  |
|  | See figures 5-10, 5-14, 6-21, and 6-52 | Pin 2 at tube V604 ( 17 volts peak-to-peak). | Waveshape No. 11A or 11B shown in figure 5-11. | If normal indication is not observed at both pins, proceed to step 12. If normal indication is observed at pin 2 but not at pin 1, tute V604A is defective. Replace tube |

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 11 \\ (\text { cont }) \end{gathered}$ | See figures 5-10, 5-14, $6-21$, and 6-52 | Pin 1 at tube V604 (75 volts peak-to-peak). | Waveshape No. 12 shown in figure 5-11. | V604. If trouble persists, take voltage and resistance measurements and compare them with values given in figure 5-13: |
| 12 | See figures 5-10 and 6-21 <br> See figures 5-10, 5-14, 6-21, and 6-52 <br> See figures 5-10, 5-14, $6-21$, and 6-52 | In sequential order, connect test prod to the following points: <br> Test point TP1 (10 volts peak-to-peak). <br> Pin 7 at tube V602 (40 volts peak-to-peak). <br> Pin 3 at tube V602 (48 volts peak-to-peak). | Waveshape No. 1 shown in figure 5-11. <br> Waveshape No. 3 shown in figure 5-11. <br> Waveshape No. 7 shown in figure 5-11. | Depending upon indications obtained, check one of the following: If waveshape at test point TP1 is not obtained, check cable from pulser coli to input of coder-indicator, north reference burst pickup coll, and north reference burst slug in pulse plate. Replace all defective components. If waveshape No. 3 is incorreci. replace tube V601. If trouble persists, take voltage and resistance measurements and compare them with values given in fugure 5-14. <br> If waveshape No. 7 is incorrect, replace tube V602. If waveshape No. 7 is correct. replace tube V603. Check capacitor C609 and diode CR605. |
| 13 | See figures 5-10 and 6-21 <br> See figures 5-10, 6-21, and 5-14 | In sequential order, connect test prod to the following points: <br> Test point TP2 (10 volts peak-to-peak). <br> Pin 3 at tube V610 (50 volts peak-to-peak). | Waveshape No. 25 shown in figure 5-11. <br> Waveshape No. 31 shown in figure 5-11. | If correct waveshape is not obtained at test point TP2, check cable from pulser coll to input of coder-indicator and auxiliary reference burst pickup coil. Check signal through tubes V601A and V609, comparing oscillsocope presentation with waveshapes No. 26 through 30. Check tube voltages and resistances. If |

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\stackrel{13}{\text { (cont) }}$ |  |  |  | correct waveshape is not obtained at pin 3 of tube V610, replace tubes V601 and V609. If correct waveshapes are observed at test point TP2 and at pin 3 of tube V610, replace tube $\mathbf{Y} 610$. If trouble persists, take voltage and resistance measurements from tube sockets V601, V604, and V610 and compare them with values given in figure 5-13. |
| 14 | See figures 5-10, 5-14, and 6-21 | Set oscilloscope sweep speed to 4 microseconds per inch. <br> Connect test prod to pin 7 at tube V604 ( 15 volts peak-to-peak). | Waveshape No. 37 shown in figure 5-11. | If pulse is not present, check as called for in radio receiver troubleshooting chart (table 5-4) and check cabling from radio receiver to coderindicator. |
| 15 | See figures 5-10 and 6-21 | Open switch 5603 on video chassis of coderindicator and set oscilloscope sweep speed to 100 microseconds per inch. <br> Connect test prod to test point TP8. | Waveshape No. 48 shown in figure 5-11. | If correct presentation is observed, trouble is in keyer assembly. Replace keyer assembly. |
| 16 | See figures 5-10, 5-14, $6-21$, and 6-52 | Close switch S603 and check tubes V612 through V613B by connecting test prod to the following points (refer to waveshapes No. 38 through 47 shown in figure 5-11 for recommended sweep speed): <br> Pin 7 at tube V612 (75 volts peak-to-peak). | Waveshape No. 38 shown in figure 5 ¢ 11 . | If correct waveshape is not observed, test capacitor C640 and resistors R792, R688, R689, and R690. |

TABLE 5-5. RADIO SET AN/GRN-9D, CODER-INDICATOR, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 16 \\ & \text { (cont) } \end{aligned}$ | See figures 5-10, 5-14, and 6-21 | Test point TP9 ( 15 volts peak-to-peak). | Waveshape No. 41 shown in figure 5-11. | If correct waveshape is not observed, replace tube V612. |
|  | See figures 5-10, 5-14, $6-21$, and 6-52 | Pin 4 at tube V613 (150 volts peak-to-peak). | Waveshape No. 42 shown in figure 5-11. | If correct waveshape is not observed, tube V613A is defective. Replace tube V613. |
|  | See figures 5-10, 5-14, $6-21$, and 6-52 | Pin 7 at tube V614 (28 volts peak-to-peak). | Waveshape No. 43 shown in figure 5-11. | If correct waveshape is not observed, test capacitor C642 and potentiometers R696 and R698. |
|  | See figures 5-10, 5-14, $6-21$, and 6-52 | Pin 7 at tube V613 | Waveshape No. 47 shown in figure 5-11. | If correct waveshape is not observed, replace tube V614. |
|  | See figures 5-10 and 6-21 | Test point TP8 | Waveshape No. 48 shown in figure 5-11. | If correct waveshape is not observed, tube V613B is defective. Replace tube V613. |




## LOCATICN: Plate, pin 6, V601B

Sweep Rate: $320 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 100 V pp
Remarks: Output of 15 cps trigger pulse amplifier.


LOCATION: Grid, pin 7, of V602A
Sweep Rate: $200 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 40 V pp
Remarks: Loading of probe CG-1509/URN-3 increased the period of multivibrator V602, so that 14 timing pulses were required before the multivibrator returned to the stable condition. Under normal operation 12 timing pulses would be required.


LOCATTION: Grid, pin 7, of V602A
Sweep Rate: $200 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 40 V pp
Remarks: 15 cps trigger pulse on grid of multivibrator V602 with 12AT7WA removed from socket XV602.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 1 of 15)

LOCATION: Grid, pin 2, of multivibrator V602B
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 220 V pp
Remarks: Loading of probe CG-1509/URN-3 caused multivibrator to trip after 11 timing pulses.

LOCATION: Grid, pin 2, of multivibrator V602B
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 220 V pp
Remarks: R675 adjusted to show 15 cps gate multivibrator tripping after 12 timing pulses. Note that reducing amplitude of timing pulses has increased the number of pulses required before MV602 will return to the stable condition.


## LOCATION: Plate, pin 1 of V602B

Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 24 V pp
Remarks: Output pulse from 15 cps gate forming multivibrator.

6

LOCATION: Cathode, pin 3, of V602B
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: $\mathbf{4 8} \mathrm{V}$ pp
Remarks: Keying pulse to 33.3 kc pulsed oscillator.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 2 of 15)

## LOCATION: TP 3

Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 26 V pp
Remarks: Output of pulsed oscillator.


LOCATION: Grid, pin 7, of V603B
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 20 V pp
Remarks: Grid of second half of 33.3 kc pulsed oscillator.


LOCATION: Cathode, pin 8, of V603B
Sweep Rate: $\mathbf{8 0} \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 9.5 V pp
Remarks: Cathode of second half of 33.3 kc pulsed oscillator.


LOCATION: Grid, pin 2, of amplifier V604A
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 17 V pp
Remarks: North reference burst only with sweep adjusted to show base line. Positive portion of sinewave output from pulsed osc. has been clipped.

11 A


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 3 of 15)

LOCATION: Grid, pin 2, of amplifier V604A
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 20 V pp
Remarks: Same as 11A except that both north and auxiliary bursts are present.

11B


LOCATION: Plate, pin 1, of V604A
Sweep Rate: $160 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Plate of trigger amplifier V604A.


LOCATION: Grid, pin 2, of V605A
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Grid of one-shot multivibrator.


LOCATION: Plate, pin 1, of one-shot multivibrator V605
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 117 V pp
Remarks: North burst only at plate of oneshot multivibrator V605.

14A


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 4 of 15)

LOCATION: Plate, pin 1, of one-shot multivibrator V605
Sweep Rate: $1600 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 117 V pp
Remarks: Identification code pulse pairs with auxiliary reference burst. Note that auxiliary burst occurs once for every 10 identification code pulse pairs.

14B

LOCATION: Plate, pin 6, of one-shot multivibrator V605
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Auxiliary burst at output of oneshot multivibrator V605.


LOCATION: TP 4
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 70 V pp
Remarks: Auxiliary burst at input grid of blocking oscillator V606. (Pin 2 of V606A).


LOCATION: Plate, pin 9, of V606B
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Auxiliary burst at plate of blocking oscillator V606B.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 5 of 15)

LOCATION: Cathode, pin 6, of V606.
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 90 V pp
Remarks: Auxiliary burst of cathode of blocking oscillator V606.

LOCATION: TAP 1 of DL601
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 500 V pp
Remarks: Auxiliary reference burst at input to delay line DL601.

## LOCATION: Grid, pin 2 of V607A

Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 14 V pp
Remarks: Output of delay line DL601. Auxiliary reference burst consisting of 6 pairs of pulses as a result of $12 \mu \mathrm{sec}$ coding.

LOCATION: Grid, pin 2, of V615A
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 63 V Pp
Remarks: Trigger input grid of one-shot multivibrator V615 showing auxiliary reference burst under normal operation.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 6 of 15)

## LOCATION: Grid, pin 2, of V615A

Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Trigger input grid of one-shot multivibrator V615, with tube V615 removed from socket. Auxiliary reference burst shown as a series of twelve trigger pulses on grid.

LOCATION: Cathode, pin 6, of V615B
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$;
Measurement: 75 V pp
Remarks: Auxiliary reference burts at output of multivibrator V615.


LOCATION: Cathode, pin 6, of V615B
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Identification code signal at output of multivibrator V615. Waveform shows two pulse pairs having a spacing of $100 \mu \mathrm{sec}$ between pairs with $12 \mu \mathrm{sec}$ between pulses in each pair. This pulse group is transmitted 1350 times per second during tone transmission.

23B

LOCATION: Cathode, pin 6, of V607 (cathode follower output of coder-indicator)
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V Pp
Remarks: North reference burst only. Waveforms taken at this point may be used to check the pulse count of reference bursts.

24A


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 7 of 15)

LOCATION: Cathode, pin 6, of V607
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Auxiliary and north reference bursts present.

$$
24 B
$$



LOCATION: Cathode, pin 6, of V607
Sweep Rate: $2 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Single output pulse with 1 mc markers.

$$
24 \mathrm{C}
$$



LOCATION: Cathode, pin 6, of V607
Sweep Rate: $16 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Identification code pulse pair with 1 mc markers.


LOCATION: Cathode, pin 6, of V607
Sweep Rate: $4,000 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Auxiliary reference bursts with identification code pulse pairs occuring once for every $\mathbf{1 0}$ auxiliary reference bursts.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 8 of 15)

## LOCATION: TP 2

Sweep Rate: $2400 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 10 V pp
Remarks: Auxiliary ( 135 cps ) reference trigger pulse from antenna.


LOCATION: Plate, pin 1, V601A
Sweep Rate: $2300 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 56 V pp
Remarks: Output of auxiliary reference burst trigger amplifier.


LOCATION: Grid, pin 7, of V609A
Sweep Rate: $1200 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 20 V pp
Remarks: Trigger pulse on trigger input grid of one-shot multivibrator V609. Tube V609 removed.


LOCATION: Grid, pin 7, of V609A
Sweep Rate: $160 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 45 V pp
Remarks: Signal on trigger input grid of oneshot multivibrator V609 under normal operation.

28


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 9 of 15)
Issued June 73

LOCATION: Grid, pin 2, of V609
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 220 V pp
Remarks: Grid of 135 cps gate multivibrator. Note that duration of gate is determined by pulses fed back from V606.

LOCATION: Plate, pin 1, of V609
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 80 V pp
Remarks: 135 cps gate pulse from multivibrator V609.

LOCATION: Grid, pin 3, of V610
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 50 V pp
Remarks: Timing pulse from 135 cps gate multivibrator to $p$.ed oscillator V610. R672 set for low amplitude of feedback pulses, causing pulsed oscillator to oscillate for 7 cycles.

31A

LOCATION: Grid, pin 3, of V610
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 50 V pp
Remarks: R672 set for high amplitude of feedback pulses, causing pulsed oscillator to oscillate for 5 cycles.

31B


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 10 of 15)

LOCATION: Grid, pin 3, of V610
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 50 V pp
Remarks: R672 set for correct amplitude of feedback pulses causing pulsed oscillator, V610, to oscillate for 6 pulses.

31C


LOCATION: TP 6
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 30 V pp
Remarks: Output of pulsed oscillator V610.

LOCATION: Grid, pin 7, of V610
Sweep Rate: $80 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 14 V pp
Remarks: Grid of second half of 41.7 kc pulsed oscillator.

LOCATION: Grid, pin 7, of V611
Sweep Rate: $120 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 48 V pp
Remarks: Both 15 cps and 135 cps : gate pulses at grid of priority gate.

Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 11 of 15)

LOCATION: Cathode, pin 3, of V611
Sweep Rate: $200 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 48 V pp
Remarks: 135 cps gate pulse at cathode of priority gate.


LOCATION: Grid, pin 2, of V611
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 34 V pp
Remarks: One pulse of identification tone signal at grid of priority gate.


LOCATION: Grid, pin 7, of V604B
Sweep Rate: $4 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 15 V Pp
Remarks: One interrogation pulse from receiver at grid of interrogation signal keyer.


LOCATION: Grid, pin 7, of V612
Sweep Rate: $200 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 75 V pp
Remarks: Locking pulse from 135 cps gate multivibrator to 1350 cps oscillator.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 12 of 15)

## LOCATION: Grid, pin 3, of V612

Sweep Rate: $2000 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 35 V pp
Remarks: 1350 cps oscillator signal without phase locking pulse from 135 cps gate multivibrator.

## LOCATION: Grid, pin 3, of V612

Sweep Rate: $2000 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: $\mathbf{3 5} \mathbf{V}$ pp Min
55 V pp Max
Remarks: 1350 cps oscillator signal with phase locking pulse from 135 cps gate multivibrator.


## LOCATION: TP 9

Sweep Rate: $2000 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 15 V pp
Remarks: 1350 cps oscillator output to amplifier V613A.


LOCATION: Plate, pin 4, of V613A
Sweep Rate: $2000 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 150 V pp
Remarks: Plate of 1350 cps amplifier V613A.
IUCDDDDDDODS

Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 13 of 15)

| LOCATION: Grid, pin 7, of V614 |
| :--- |
| Sweep Rate: $400 \mu \mathrm{sec} / \mathrm{in}$. |
| Measurement: 28 V pp |
| Remarks: Grid of $100 \mu \mathrm{sec}$ multivibrator under |
| normal operation. |
|  |
|  |
|  |
|  |
|  |



LOCATION: Grid, pin 7, of V614
Sweep Rate: $400 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 14 V pp
Remarks: Grid of $100 \mu \mathrm{sec}$ multivibrator with tube V614 removed.


LOCATION: Plate, pin 6, of V614A
Sweep Rate: $400 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 210 V pp
Remarks: Plate of first half of $100 \mu \mathrm{sec}$ multivibrator.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal-Tracing Waveshapes (Sheet 14 of 15)

LOCATION: Plate, pin 4, of V614B
Sweep Rate: $400 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 200 V pp
Remarks: Plate of second half of $100 \mu \mathrm{sec}$ multivibrator.


LOCATION: Plate, pin 4, of V614B
Sweep Rate: $40 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 200 V pp
Remarks: Plate of second half of $100 \mu \mathrm{sec}$ multivibrator (expanded to show rate of change of plate voltage).


LOCATION: Grid, pin 7, of V613B
Sweep Rate: $100 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 9 V pp first pulse
13 V pp second pulse
Remarks: Identification code pulse pair on grid of keyer tube V613B during transmission of code.


## LOCATION: TP 8

Sweep Rate: $100 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 33 V pp first pulse 58 V pp second pulse
Remarks: Identification code pulse pair on plate of keyer tube V613B during transmission of code.


Figure 5-11. Coder-Indicator KY-382/GRN-9D, Signal Tracing Waveshapes (Sheet 15 of 15)


NOTES:
1 READINGS TAKEN WITH A MULTIMETER HAVING A RESISTANCE OF 1,000 AND 20,000-OHMS-PER -VOLT FOR AC AND DC MEASURE MENTS, RESPECTIVELY.

$$
\begin{aligned}
& \text { KEY TO SYMBOLS } \\
& \checkmark \text { INDICATES DC VOLTAGE TO GROUND } \\
& \text { UNLESS OTHERWISE SPECIFIED } \\
& \text { AC INDICATES AC VOLTAGE TO GROUND } \\
& \text { UNLESS OTHERWISE SPECIFIED. } \\
& \text { R INDICATES DC RESISTANCE TOGROUND. } \\
& \text { * 5.0 VAC BETWEEN PINS MARKED WITH } \\
& \text { ONE ASTERISK. }
\end{aligned}
$$

Figure 5-12. Coder-Indicator KY-382/GRN-9D, Power Supply Chassis, Tube Socket Voltage and Resistance Diagram


NOTES:
I. READINGS TAKEN With a multimeter having RESISTANCE OF 1,000 ANO 20,000-OHMS -PER VOLT FOR AC AND OC MEASUREMENTS, RESPECTIVELY.

KEY TO SYMBOLS
v inoicates oc voltage to grouno UNLESS OTHERWISE SPECIFIED.
ac indicates ac voltage to grouno UNLESS OTHERWISE SPECIFIEO.
R indicates oc resistance to grouno

- Vgo4 Pin 7. ouring IOENTIFICATION transmission this value becomes-50V

Figure 5-13. Coder-Indicator KY-382/GRN-9D, Video Chassis, Tube Socket Voltage and Resistance Diagram


Figure 5-14. Coder-Indicator KY-382/GRN-9D, Left Side View, Test Point Location
(3) TROUBLFSHOOTING TRANSMITTER. (See figure $5-15$ ). - The transmitter portion of the radio beacon consists of the frequency multiplieroscillator and the amplifier-modulator. These two units are treated as a single unit inscfar as troubleshooting is concerned. The carrier signal, the 3.5microsecond video pulse (called the shaped pulse), and the 10 -microsecond video pulse (called the keying pulse) are traced through the transmitter by following the procedure outlined in the following paragraphs.
(a) PRELIMINARY CHECK. - When trouble has been localized to the transmitter portion of the radio set, the initial check is for a-c and d-c power inputs to the transmitter. If FILAMENT lamp DS 1401 on the frequency multiplier-oscillator panel is off, check the interlock for damage and inspect fuses F1401, F1402, and F1403. If FIL lamp DS1301 on the amplifier-modulator panel is off, check the interlock for damage and inspect fuse F1302. If LV lamp DS1603 and -375V lamp DS 1601 on the lowvoltage power supply panel are off when LV switch S1601 is in the ON position, troubleshoot the lowvoltage power supply (refer to table 5-7). If +1000 V lamp DS 1801 on the medium-voltage power supply panel is off when MV switch S1801 is in the ON position, troubleshoot the medium-voltage power supply (refer to table 5-8). If HV lamp DS 1902 on the high-voltage power supply is off when HV switch S1902 is in the ON position, troubleshoot the highvoltage power supply (refer to table 5-9).

## (b) TEST EQUIPMENT AND SPECIAL

TOOLS. - The test equipment required to perform the transmitter troubleshooting procedure is based on
using the built-in test equipment. This equipment is housed in the power supply assembly cabinet. No special tools are required to perform this procedure.
(c) CONTROL SE'TTINGS. - Table 5-2 lists the preliminary control settings of all controls required when troubleshooting.

## (d) TRANSMITTER TROUBLESHOOTING

 CHART. - When trouble has been localized to the transmitter, follow the troubleshooting procedure given in table 5-6.(e) ILLUSTRATIONS. - Illustrations containing information which will aid the technician in troubleshooting the transmitter portion of the radio set are as follows:

1. Figure 5-15. Radio Set, Transmitter, Servicing Block Diagram
2. Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes
3. Figures 5-18 through 5-20. Trans-
mitter, Tube Socket Voltage and Resistance Diagrams
4. Figure 5-21. Transmitter, Test Point Location Illustration
5. Figures 6-18 and 6-19. Frequency Multiplier-Oscillator, Schematic Diagrams
6. Figure 6-20. Amplifier Modulator, Schematic Diagram

TABLE 5-6. RADIO SET AN/GRN-9D, TRANSMITTER, FUNCTIONAL SECTION TROUBLESHOOTING CHART

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 1 |  | Set oscilloscope sweep speed to 4 microseconds per inch. <br> Connect coaxial test lead from vertical input jack on oscilloscope to VIDEO IN jack J 1404 on frequency multiplieroscillator panel. | Pair of 1.5 -microsecond wide pulses, with 12 -microsecond spacing between pulses, should appear as shown in waveshape No. 1 of figure 5-16. | If normal indication is not obtained, refer to coder-indicator troubleshooting chart (table 5-5). If normal indication is obtained, proceed to step 2. |
| 2 |  | Check readings of D. C. SUPPLY VOLTAGE meter M1402 on frequency multiplieroscillator panel with METER SELECTOR switch S1402 in position indicated. | Meter M1402 should read: | If normal indication is obtained, proceed to step 3. If-either the $-375-$ or $+250-$ volt d-c voltage is incorrect, refer to low-voltagepower supply troubleshooting chart (table 5-7). If +1000 voltage is incorrect, proceed to medium-voltage power supply troubleshooting chart (table 5-8). |
| 3 |  | Check reading of BEAM CURRENT meter M1301 on front panel of ampli-fier-modulator. | Compare with logged reading. | Amount of beam current depends upon number of shaped pulses fed to high-level modulator of amplifier-modulator. Required total number of pulses fed to ampli-fier-modulator is 3,600 pulse-pairs per second. Any reduction from this number of pulse-pairs will cause a corresponding reduction in beam current. Also, improper setting of klystron bias will cause an improper beam current reading. Proceed to step 4 to determine cause of change in shape or reduction in number of shaped pulses per second. Zero beam current indicates loss of shaped pulses or failure of either klystron or high-voltage power |

TABLE 5-6. RADIO SET AN/GRN-9D, TRANSMITTER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 3 \\ \text { (cont) } \end{gathered}$ |  |  |  | supply. If beam current is zero, proceed to step 4 as a first step toward isolating trouble. |
| 4 | See figures 5-15 and 6-18 | Set oscilloscope sweep speed to 3 microseconds per inch. Connect coaxial test lead from vertical input jack of oscilloscope to SHAPED PULSE jack J1405 on frequency multiplieroscillator panel. | Waveshape No. 9 as shown in figure 5-16. | If shaped pulse is not present, proceed to step 5. If shaped pulse is present, but not of proper shape, refer to frequency multiplieroscillator video adjustment procedure in paragraph 6-2 $\underline{\text { of Section }}$ 6. |
| 5 | See figures 5-15. 5-21, and 6-18 | -Set oscilloscope sweep speed to 2 microseconds per inch. <br> Connect test prod to pin 5 at tube V1403 (80 volts peak-to-peak). | Waveshape No. 5 as shown in figure 5-16. | If pulse is not present, replace tube V1402. |
| 6 | See figures 5-15, 5-21; and 6-18 | Set oscilloscope sweep speed to 3 microseconds per inch. Connect test prod to pin 2 or 7 of V1406 (2200 volts peak-to-peak). | Waveshape No. 6 as shown in figure 5-16. | If pulse is not present, replace tubes V1403, V1404, and V1405. If trouble persists, test transformer T1402 and also take voltage and resistance measurements from tube sockets and compare them with values given in figure 5-18. |
| 7 | See figures 5-15, 5-21, and 6-18 | Connect test prod to vertical input jack on oscilloscope. Then. connect test prod to pin 5 at tube V1407. | Waveshape No. 8 as shown in figure 5-16. | If pulse is not present, replace tube V1406. If pulse is present, replace tube V1407. |
| 8 |  | Check readings of TUNING meter M1401 with METER SELECTOR switch S 1401 in the following positions: | Compare with previously logged readings. | At stage where reading becomes abnormal, replace associated tube. Check tuning of frequency multiplier stages. Check associated circuits, using tube voltage and resistance charts (figure 5-19). Replace all defective tubes and components. |

TABLE 5-6. RADIO SET AN/GRN-9D, TRANSMITTER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 8 \\ \text { (cont) } \end{gathered}$ |  | OSC <br> 1ST DOUBLER <br> 2ND DOUBLER <br> 3RD DOUBLER <br> TRIPLER <br> AMPL <br> KLYSTRON INPUT <br> REFL <br> KLYSTRON INPUT <br> INCID |  |  |
| 9 |  | Set oscilloscope sweep speed to 8 microseconds per inch and connect test prod to vertical input of oscilloscope. |  |  |
| 10 | See figures 5-15, 5-21, and 6-18 | Connect test prod to pin 1 of tube V1409. | 10 -microsecond wide keying pulse. | If pulse is present, proceed to step 11. If pulse is not present, replace tubes V1409, V1401, and V1408. |
| 11 |  | Set oscilloscope sweep speed to 4 microseconds per inch. Connect coaxial test lead from vertical input jack of oscilloscope to KLYSTRON INPUT INCIDENT jack J1409 on frequency multiplier-oscillator panel. | Klystron input incident signal should be observed as a detected r-f pulse 10 microseconds wide. (Waveshape No. 16 shown in figure 5-16). | If normal indication is not obtained, repláce tubes V1505 and V1506. If trouble persists, test transformer T1404 and potentiometers R1530 and R1532. Also take voltage and resistance measurements and compare them with values given in figure 5-19. |

NOTE
In order to preserve waveshape of detected r-f pulse, a 50 -ohm termination must be provided for coaxial test lead. Figure 5-17 illustrates connection that should be used.

| 12 | See figure <br> $6-18$ | Set METER SELECTOR <br> switch S1401 to KLYS- <br> TRON INPUT REFL <br> position and check <br> reading of TUNING <br> meter M1401. | Compare with logged <br> reading. | If there is a considerable <br> increase in reading ob- <br> tained at this point, a <br> defective or improperly <br> tuned klystron is indi- <br> cated. Retune klystron <br> and replace, if neces- <br> sary. |
| :--- | :--- | :--- | :--- | :--- |

TABLE 5-6. RADIO SET AN/GRN-9D, TRANSMITTER, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)

| STEP | TEST POINT | 'PRELIMINARY ACTION | NORMAL INDICATION | NEXT STEP |
| :---: | :---: | :---: | :---: | :---: |
| 13 |  | Check bias voltage on SAL-89 klystron as follows: <br> Remove protective cover from klystron filament connections. Before attempting to measure voltage, short klystron filament terminals to ground with a grounding pick. Connect voltmeter between either filament terminal and grid. | Bias voltage between grid and cathode of -120 volts dc. | If necessary, adjust potentiometer R1382 to obtain a reading of -120 volts dc. If this voltage cannot be obtained, replace tubes V1370, V1371, and V1372. If trouble persists, take voltage and resistance measurements from tube sockets and compare them with values given in figure 5-20. |



```
LOCATION: VIDEO IN jack J1404
    Sweep Rate: 4 \musec/in.
    Measurement: 45 V pp
    Pulse width 1.4 \musec
    Pulse pair spacing 12 土.25 \musec
    Remarks: One pair of video pulses at input to
        FMO video circuits.
```



## LOCATION: V1402, pin 7

Sweep Rate: $2 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 40 V pp
$2.9 \mu \mathrm{sec}$
Remarks: Grid of one-shot multivibrator V1402 (shaped pulse generator).


## LOCATION: V1402, pin 7 <br> Sweep Rate: $2 \mu \mathrm{sec} / \mathrm{in}$. <br> Measurement: 15 V pp <br> $1.6 \mu \mathrm{sec}$

Remarks: Trigger pulse on grid pin 7 with V1402 removed from socket.

3

LOCATION: V1402, pin 9
Sweep Rate: $2 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 160 V pp
$2.9 \mu \mathrm{sec}$
Remarks: Plate of first section of one-shot multivibrator V1402.


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 1 of 7)


LOCATION: V1406, pin 2 or 7
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 2200 V pp
$3.7 \mu \mathrm{sec}$
Remarks: Plate of series diode V1405.


## LOCATION: V1406 Cathode Cap

Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 1400 V pp
$3.7 \mu \mathrm{sec}$
Remarks: Video pulse at input to shaper network.


LOCATION: Center tap of R1470
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 720 V pp
$5.0 \mu \mathrm{sec}$
Remarks: Shaped pulse at output of shaper network.


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 2 of 7)

LOCATION: SHAPED PULSE jack J1405
Sweep Rate: $3 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 10 V pp
$4.3 \mu \mathrm{sec}$
Remarks: Shaped pulse at output of frequency multiplier-oscillator.


LOCATION: Junction of R1428 and C1428
Sweep Rate: $2 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 40 V pp
$1.4 \mu \mathrm{sec}$
Remarks: Video pulse at output of delay line DL1402.


LOCATION: V1408, pin 2
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 40 V pp
$10.5 \mu \mathrm{sec}$ (each pulse)
Remarks: One pair of pulses on grid (pins 2 and 7) of one-shot multivibrator V1408.


LOCATION: Junction of R1462 and R1461.
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 180 V pp $10.4 \mu \mathrm{sec}$
Remarks: One pair of pulses on plate (pins 1 and 9) of first half of multivibrator V1401 and V1408.


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 3 of 7)

LOCATION: V1401, pin 2
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 90 V pp $10.4 \mu \mathrm{sec}$ (at base)
Remarks: Grid of second half of one-shot multivibrator V1401 and V1408.


LOCATION: Junction of R1435 and R1440
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 120 V pp
$10.4 \mu \mathrm{sec}$
Remarks: Grids of cathode follower V1409.


LOCATION: V1409, pin 6
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 20 V pp
$10.4 \mu \mathrm{sec}$
Remarks: $10 \mu \mathrm{sec}$ keying pulses at output of cathode follower V1409.


LOCATION: KLYSTRON INPUT INCIDENT jack J1409
Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$.
Measurement: 1.8 V pp
$10.0 \mu \mathrm{sec}$
Remarks: Typical waveform.


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 4 of 7)

| LOCATION: KLYSTRON INPUT |  |
| :--- | :--- |
| REFLECTED jack J1408 |  |
| Sweep Rate: $8 \mu \mathrm{sec} / \mathrm{in}$. |  |
| Measurement: 9 V pp |  |
| $10 \mu \mathrm{sec}$ |  |
| Remarks: Typical waveform. |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |



| LOCATION: KLYSTRON OUTPUT |  |
| :--- | :--- |
| INCIDENT jack J1157 |  |
| Sweep Rate: $8 \quad \mu \mathrm{sec} / \mathrm{in}$. |  |
| Measurement: $2 \mathbf{~ V ~ p p}$ |  |
| Remarks: $\quad 6 \mu \mathrm{sec}$ |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |



```
LOCATION KLYSTRON OUTPUT
    REFLECTED J1152
    Sweep Rate: }8\mu\textrm{sec}/\textrm{in}
    Measurement: 1.3 V pp
    Remarks:
```

```
LOCATION: ANTENNA INCIDENT
    jack J1153
    Sweep Rate: }8\mu\textrm{sec}/\textrm{in}
    Measurement: 1.75 V pp
    Remarks:
```



Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 5 of 7)

```
LOCATION: ANTENNA REFLECTED jack J1153
Sweep Rate: \(8 \mu \mathrm{sec} / \mathrm{in}\).
Measurement: . 15 V pp
Remarks: Pulse width not measured. Amplitude of this pulse should be low compared to previous waveform.

\section*{LOCATION: ANTENNA INCIDENT} jack J1154
Sweep Rate: \(\mathbf{8 0} \mu \mathrm{sec} / \mathrm{in}\).
Measurement: 1.75 V pp
Remarks: Auxiliary reference burst with R1471 improperly adjusted to show pulse droop.


\section*{LOCATION: ANTENNA INCIDENT} jack J1154
Sweep Rate: \(\mathbf{8 0} \mu \mathrm{sec} / \mathrm{in}\).
Measurement: 1.75 V pp
Remarks: Auxiliary reference burst with R1471 properly adjusted. Note that pulse amplitude remains constant.


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 6 of 7)

LOCATION: SHAPED PULSE jack J1405
Sweep Rate: \(80 \mu \mathrm{sec} / \mathrm{in}\).
Measurement: 10 V pp
Remarks: Auxiliary reference burst at J1405. R1471 correctly adjusted to boost video pulse train and correct for droop in r-f output pulse train.


LOCATION: Center tap of R1470
Sweep Rate: \(16 \mu \mathrm{sec} / \mathrm{in}\).
Measurement: 720 V pp
Remarks: One pair of shaped pulses at output of shaper network. R1417 properly adjusted to minimize reflections.
```

LOCATION: Center tap of R1470
Sweep Rate: }16\mu\textrm{sec}/\textrm{in}
Measurement: 720 V pp (primary pulse)
60 V pp (reflected pulse)

```
    Remarks: R1417 misadjusted to show reflection
        caused by improper termination of shaper
        network.
            \(26 B\)


Figure 5-16. Radio Set, Transmitter, Signal-Tracing Waveshapes (Sheet 7 of 7)


Figure 5-17. Klystron Input Incident Test Setup


\section*{NOTES:}

Figure 5-18. Frequency Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, Tube Socket Voltage and Resistance Diagram


\section*{notes}

1 readings taken with a multimeter having a RESISTANCE OF 1.000 AND 20.0DO-OHMS - PER -VOLT FOR AC AND DC MEASUREMENTS, RESPECTIVELY

KEY TO SYMEOLS
\(v\) INDICATES DC VOLTAGE TO GROUND UNLESS OTHERWISE SPECIFIED

AC INOICATES AC VOLTAGE TO GROUND UNLESS OTHERWISE SPECIFIED

R INDICATES OC RESISTANCE TO GROUND
* 55V ac aetween pins marked with ONE ASTERISK
* use a vtvin toread voltage at this point
*RH ZAV AC ON PIN I WHEN CRYSTAL OVEN NORMAL
LAMP, DS 1402 IS MOT LIT.

Figure 5-19. Frequency Multiplier-Oscillator CV-1171/GRN-9D, High or Low Band R-F Chassis, Tube Socket Voltage and Resistance Diagram
 BEEN DISCHARGED.

\section*{NOTES:}
1. READINGS TAKEN WITH A MULTIMETER OF \(1,000 \Omega / V\) FOR AC AND \(20,000 \Omega / V\) FOR DC.
2. TO OBTAIN POWER ON THE BIAS SUPPLY CHASSIS WITH THE AMPLIFIER-MODULATOR DRAWER OPEN, SHORT AIR SWITCH SIJOI WITH A JUMPER.
bltag measured between GRID TERMINAL AND EITHER H OR HK TERMINAL.


Figure 5-21. Frequency-Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, Bottom View, Test Point Location
(4) TROUBLESHOOTING POWER SUPPLIES. When trouble has been localized to one of the power supplies in the radio set, refer to troubleshooting table which pertains to that particular power supply and follow the step-by-step procedure indicated. Various checks and adjustments which will aid in restoring the power supplies to proper operating condition are given in paragraph \(5-4 \mathrm{c}(5)\). The klystron bias supply is covered under the troubleshooting procedure for the transmitter portion of Radio Set AN/GRN-9D. Radio receiver and coder-indicator power supply troubleshooting information is included with the troubleshooting data on the radio receiver and coder-indicator.
(a) PRELIMINARY CHECK. -When trouble has been localized to one of the power supplies, the initial check is for an a-c power input. If LV lamp DS1603 and -375 lamp DS 1601 on the low-voltage power supply are off when LV switch S1601 is in the ON position, check the condition of filament fuses F1601 and F1602 and plate fuses F1603 and F1604. If +1000 V lamp DS 1801 on the medium-voltage power supply is off when MV switch S1801 is in the ON position, check the condition of plate fuse F1801 and filament fuses F1802 and F1803. If HV lamp DS1902 on the high-voltage power supply is off when HV switch S 1902 is in the ON position, check the condition of filament fuse F1901. Fuse failure is indicated by a glowing lamp in the fuseholder.
(b) TEST EQUIPMENT AND SPECIAL

TOOLS. - Multimeter AN/PSM-4 is required to troubleshoot the power supplies. No special tools are required to perform the troubleshooting procedure.
(c) CONTROL SETTINGS. -Table 5-2 lists the preliminary control settings of all controls required when troubleshooting.
(d) TROUBLESHOOTING CHARTS. - When trouble has been localized to one of the power supplies, refer to the applicable troubleshooting chart. Table \(5-7\) is concerned with troubleshooting the low-voltage power supply and tables 5-8 and 5-9 cover troubleshooting of the medium- and low-voltage power supplies, respectively.
(e) ILLUSTRATIONS. -Illustrations containing information which will aid the technician in troubleshooting the power supplies are as follows:
1. Figure 5-22. Low-Voltage Power Supply, Tube Socket Voltage and Resistance Diagram
2. Figure 6-24. Low-Voltage Power Supply, Schematic Diagram
3. Figure 6-63. Low-Voltage Power Supply, Test Point Location Illustration
4. Figure 5-23. Medium-Voltage Power Supply, Tube Socket Voltage and Resistance Diagram
5. Figure 6-25. Medium-Voltage Power Supply, Schematic Diagram
6. Figure 6-66. Medium-Voltage Power Supply, Test Point Location Illustration
7. Figure 5-24. High-Voltage Power

Supply, Tube Socket Voltage and Resistance Diagram
8. Figure 6-26. High-Voltage Power Supply, Schematic Diagram
9. Figure 6-68. High-Voltage Power Supply, Test Point Location Illustration

TABLE 5-7. RADIO SET AN/GRN-9D, LOW-VOLTAGE POWER SUPPLY, FUNCTIONAL SECTION TROUBLESHOOTING CHART
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline 1 & See figure
\[
6-18
\] & Check reading of D. C. SUPPLY VOLTAGE meter M1402 on frequency multiplieroscillator panel with METER SELECTOR switch S1402 in the following positions:
\[
\begin{aligned}
& -375 \mathrm{~V} \\
& +250 \mathrm{~V}
\end{aligned}
\] & \begin{tabular}{l}
The following readings should be obtained: \\
-375 volts dc \\
+250 volts dc
\end{tabular} & \begin{tabular}{l}
If both voltages measure zero, check that front panel lamps DS 1605 LVMV READY and DS1603 L. V. are on. If both lamps are on, proceed to steps 2 and 3. If one or both lamps are off, proceed as follows: If LV-MV READY lamp DS1605 is off, trouble in control circuits or 1minute time delay relay K1605 is indicated. Isolate by checking for 120 volts ac at terminal \\
1 of terminal board TB1602. If voltage is present, relay K1605 is at fault. If voltage is not present, refer to control circuits troubleshooting chart (table \(5-10\) ). If LV-MV READY lamp DS1605 is on and L. V. lamp DS1603 is off, trouble in control circuits or relay K 1603 is indicated. Isolate by checking for 120 volts ac at terminal 6 of ter minal board TB1601. If voltage is present, check relay K1603 circuit. If voltage is not present, refer to control circuits troubleshooting chart (table 5-10). \\
Note \\
Power to relay K1603 is applied through terminals 3 and 5 at relay K 1605 , air switch S1005, interlock S1002A (mediumvoltage power supply), interlock S1001A (lowvoltage power supply), interlock S903 (frequency multiplieroscillator), interlock S902A (amplifiermodulator), and terminals A1 and A2 at relay K1101.
\end{tabular} \\
\hline
\end{tabular}

TABLE 5-7. RADIO SET AN/GRN-9D, LOW-VOLTAGE POWER SUPPLY, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline \[
\begin{gathered}
1 \\
\text { (cont) }
\end{gathered}
\] & & & & Check for 120 -volt a-c regulated filament voltage at terminal board TB1601, terminals 4 and 5. If voltage is present, check fuses F1601 and F1602 and transformers T1603 and T1604. Replace if necessary. If voltage is not present, refer to control circuits troubleshooting chart (table 5-10) and check regulated filament supply circuit. \\
\hline & & \begin{tabular}{l}
Before troubleshooting p load to determine whethe trouble. To remove load connected to terminals 2 minal board TB1602. \\
WARN \\
Before removing bias vo all B+ voltages. In additi resistance measurement supply and discharge all
\end{tabular} & \begin{tabular}{l}
er supply, isolate load is causing disconnect cables 3,6 , and 8 of ter- \\
NG \\
age, always remove before making any turn off power apacitors.
\end{tabular} & \\
\hline 2 & See figure 6-18 & Set METER SELECTOR switch S1402 to -375 V position and check reading of D. C. SUPPLY VOLTAGE meter M1402. & Meter M1402 should indicate -375 volts dc & If -375 -volt output is 0 , proceed as follows: Check fuse F1603 by noting whether its associated blown fuse indicator lamp is on. If fuse is blown, replace it. If fuse blows again, check transformer T1602 and tube V1610 for short. Replace defective components. If fuse F1603 is not defective, trouble is in stages V1610, V1611, V1612, or V1613. To troubleshoot these stages, first replace tubes and then take tube voltage and resistance measurements. Compare these measurements with values given in figure \(5-22\). If -375-volt output is incorrect (other than 0 ), adjust potentiometer \\
\hline
\end{tabular}

TABLE 5-7. RADIO SET AN/GRN-9D, LOW-VOLTAGE POWER SUPPLY FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|l|l|l|l|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & \multicolumn{1}{c|}{\begin{tabular}{l} 
NEXT STEP
\end{tabular}} \\
\hline (cont) & & & & \begin{tabular}{l} 
R1663, while observing \\
meter M1402, to obtain
\end{tabular} \\
\hline
\end{tabular}

TABLE 5-8. RADIO SET AN/GRN-9D, MEDIUM-VOLTAGE POWER SUPPLY, FUNCTIONAL SECTION TROUBLESHOOTING CHART
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline 1 & See figure
\[
6-18
\] & Set METER SELECTOR switch S1402 on frequency multiplieroscillator panel to -1000 V position and check reading of D. C. SUPPLY VOLTAGE meter M1402. & Meter M1402 should indicate +1000 volts dc & If indication is 0 or incorrect, check fuse F1801. If fuse is not blown, perform steps 4 and 5. If fuse is blown, replace fuse. If fuse blows again, proceed to step 2. \\
\hline 2 & & Remove tubes V1801 and V1802 and replace fuse. & & If fuse blows again, transformer T1801 or T1802 is defective. If fuse does not blow, proceed to step 3. \\
\hline 3 & & Check tubes V1801 and V1802 for shorts. & Tubes check good & If tubes check good, replace tubes. If fuse continues to blow, check stages V1803 through V1807. First replace tubes and then take voltage and resistance measurements. Compare these measurements with values given in figure 5-23. \\
\hline 4 & & Check fuses F1802 and F1803. & & \begin{tabular}{l}
If fuses are blown, check transformers T1802 and T1803 and tube filament circuits. If fuses are not blown, check that relay K1804 is closed when MV switch S1801 is in ON position. \\
Nofe \\
Low-voltage power supply must be on before mediumvoltage power supply can be started.
\end{tabular} \\
\hline 5 & & Check whether OVERLOAD lamp DS1803 on medium voltage power supply panel is on. & & If OVERLOAD`lamp is off, refer to control circuits troubleshooting chart (table 5-10). If OVERLOAD lamp is off, manually depress reset overload relay button. If lamp goes on again, check relays K1802 and K1803. \\
\hline
\end{tabular}

TABLE 5-9. RADIO SET AN/GRN-9D, HIGH-VOLTAGE POWER SUPPLY, FUNCTIONAL SECTION TROUBLESHOOTING CHART
\begin{tabular}{|l|l|l|l|l|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline
\end{tabular}

\section*{WARNING}

Voltages dangerous to life are exposed in this unit. Set MASTER switch S1101 on controlduplexer panel to OFF position before pulling out high-voltage power supply and return unit to its place in cabinet before setting MASTER switch to ON position. Capacitors may retain dangerous charges; therefore, always ground components before touching them.
\begin{tabular}{|c|c|c|c|c|}
\hline 1 & \[
6-20
\] & Check reading of H.V. SUPPLY meter M1302 on amplifier-modulator panel. & Meter M1302 should indicate 12,000 volts dc & If correct reading is not obtained, check fuses F1001, F1002, and F1003. If fuses are good, perform steps 3 and 4. If one fuse is blown, disconnect load and proceed to step 2. \\
\hline & \multicolumn{4}{|l|}{To disconnect load (observing WARNING), disconnect output cable from E1001 on power supply assembly. Secure cable with tape or string in position where it will be at least 3 inches from any high-voltage point in unit.} \\
\hline 2 & & Replace blown fuse and check fuses. & & If new fuses do not blow with load disconnected and blown fuses replaced, refer to transmitter troubleshooting chart (table 5-6). If fuses blow again with load removed, reconnect load and check to determine whether relays K1902 and K1904 are energized. If relays are deenergized, replace relays. If relays K1902 and K1904 check out satisfactorily, check tubes and components in high-voltage power supply. Take resistance measurements and compare them with values given in figure 5-24. Replace defective tubes and components. \\
\hline 3 & & Check fuse F 1901. & & If fuse is blown, check tube filament circuits. Replace fuse. \\
\hline
\end{tabular}

TABLE 5-9. RADIO SET AN/GRN-9D, HIGH-VOLTAGE POWER SUPPLY, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|l|l|l|l|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & \multicolumn{1}{c|}{ NEXT STEP } \\
\hline 4 & & \begin{tabular}{l} 
Check whether H.V. \\
OVERLOAD lamp \\
DS1903 on high-voltage \\
power supply panel is \\
on.
\end{tabular} & \begin{tabular}{l} 
H.V. OVERLOAD lamp \\
should not be on
\end{tabular} & \begin{tabular}{l} 
If H. V. OVERLOAD lamp \\
is on, manually depress \\
reset overload relay \\
button. If lamp goes on \\
again, check relay K1904 \\
and potentiometers R1906 \\
and R1912. Replace \\
defective components. \\
Overload relay may trip \\
due to high charging cur- \\
rent. Check pulse count \\
at coder-indicator test. \\
output jack. Refer to \\
table 5-5. High output \\
pulse count or trouble in \\
transmitter may cause \\
high charging current.
\end{tabular} \\
\hline
\end{tabular}


Figure 5-22. Low-Voltage Power Supply PP-1766/URN, Tube Socket Voltage and Resistance Diagram


NOTES
readings taken with a multimeter having a RESISTANCE OF 1000 AND 20000 -OHMS-PER-VOL FOR AC ANO DC MEASUREMENTS, RESPECTIVELY.

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kEy TO symbols
\(\checkmark\) indicates de voltage to ground UNLESS OTHERWISE SPECIFIED.
ac indicates ac voltage to ground UNLESS OTHERWISE SPECIFIED.
a indicates dC resistance to ground.
- 6. 3 Vac between pins marked WITH ONE ASTERISK.
* 12.6 V AC BE TWEEN PINS MARKEO I2.6 VAC BE TWEEN PIN
WITH TWO ASTERISKS.
*** 2.5 Y AC BETWEEN PINS MARKED WITH THREE ASTERISKS

Figure 5-23. Medium-Voltage Power Supply PP-1765/URN, Tube Socket Voltage and Resistance Diagram


Figure 5-24. High-Voltage Power Supply PP-1763/URN, Tube Socket Voltage and Resistance Diagram
(5) TROUBLESHOOTING POWER DISTRIBUTION

AND CONTROL CIRCUITS. (See figure 5-25.)-A systematic procedure for troubleshooting the power distribution and control circuits is given in the following paragraphs. This procedure is begun with the radio beacon completely deenergized. As each control circuit is energized, appropriate checks for normal operation are made. The point at which a normal indication is not obtained is the point at which detailed troubleshooting of the control circuits should start. Detailed troubleshooting consists of point-to-point voltage and resistance measurements and inspection of relays, controls, and other components in the control circuit under check.
(a) TEST EQUIPMENT AND SPECIAL TOOLS.Multimetē AN/PSM-4 is required to troubleshoot the power distribution and control circuits. No special tools are required for this procedure.
(b) CONTROL SETTINGS.- With the exception of HIGH VOLTAGE switch S1006, set all power switches as specified in table 2-1. The HIGH VOLTAGE switch is left in the OPERATE position during the performance of this procedure.
(c) TROUBLESHOOTING CHART.-Table 5-10 presents a systematic procedure for troubleshooting the power distribution and control circuits.

\section*{5-5. TYPICAL TROUBLES.}

Table 5-11 lists typical troubles which may be encountered during operation of Radio Set AN/GRN-9D.

\section*{5-6. LOCATION OF PARTS.}

The location of parts in the radio set is shown in Section 6, figures 6-1 through 6-7, 6-9 through 6-11, and 6-50 through \(6 \cdot 68\). The locating function column of the maintenance parts list (table 7-3) includes reference to the appropriate illustration on which the part is shown. This table is included in the parts list presented in Section 7.

\section*{Note}

The wiring diagrams included in Section 6 also serve as an aid for the location of parts when used in conjunction with the equipment illustrations.

TABLE 5-10. RADIO SET AN GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS. FUNCTIONAL SECTION TROUBLESHOOTING CHART
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline & Note \\
& \begin{tabular}{l} 
Before starting troubleshooting procedures described in this chart, turn off all power \\
switches. The procedures for troubleshooting in this chart are based on turning power on \\
in proper sequence and noting point at which normal indication is not obtained.
\end{tabular} \\
&
\end{tabular}
\begin{tabular}{|c|c|c|c|c|}
\hline 1 &  & *CAVITY HEATER ON lamp applies to ITT Models only & \begin{tabular}{l}
Crystal oven heater lamps DS1402 and DS1403 on front panel of frequency multiplieroscillator are on. OVEN lamp DS 1403 will remain on: however, NORMAL lamp DS 1402 will stay on until oven has reached operating temperature and then turn off and on as additional heat is required to maintain operating temperature. *CAVITY HEATER ON lamp DS 1105 on controlduplexer panel should also go on. Operation of lamp DS1 105 is similar to that for lamp DS1402. \\
Three-phase power is applied to terminals 1 , \\
2 , and 3 of terminal board TB902 (antenna spin motor; power is applied to spin motor when MASTER SWITCH S1101 and ANTENNA CONTROL SWITCH S1102 are turned to STANDBY and ON positions, respectively. \\
Power is applied to convenience outlets on receiver-transmitter cabinet, antenna control unit, and antenna pedestal. \\
Loss-of-phase relay K901 is energized.
\end{tabular} & \begin{tabular}{l}
If lamps DS1402 and DS1403 do not go on, replace lamps and check fuses F1402 and F1403, transformer T1502, and line filter FL1401 in frequency multiplieroscillator unit. Replace defective components. \\
If power is not applied to convenience outlets, check fuses F1005 and F1004. Replace blown fuse(s). \\
Check relay K901. \\
Replace if necessary.
\end{tabular} \\
\hline 2 & & Turn MASTER SWITCH S1101 on front panel of control-duplexer to STANDBY position. & Blue MAIN POWER ON lamp DS1 102 on control-duplexer should go on. & If MAIN POWER ON lamp does not go on. replace lamp and check fuses F1101, F1102, and F1106, L3-T3 contacts of primary contactor K1101, and contacts of loss-of-phase relay K901. \\
\hline
\end{tabular}

TABLE 5-10. RADIO SET AN/GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline \[
\stackrel{2}{(\text { cont })}
\] & & . & Blowers B901 and B902 in receiver-transmitter cabinet should start operating. & \begin{tabular}{l}
If all blowers fail to operate, check blower contactor K1103 and A1-A2, B1-B2 contacts of K1103. Replace defective components. \\
If blower B901 fails to operate, check fuses F901, F902, and F903. Check connections to blower motor by checking for 208 -volt 3 -phase power at terminals T1, T2, and T3 of motor B901. If voltages are present, check blower motor B901. If voltages are not present, check interconnections. Replace defective components. \\
If blower B902 fails to operate, check fuses F905, F906, and F907. Check connections to blower motor by checking for 208 -volt, 3 -phase a-c power at terminals T1, T2, and T3 of motor B902. If voltages are present, check blower motor B902. If voltages are not present, check interconnections. Replace blower motor and cabling, if necessary. \\
If blower B1001 fails to operate, check connections to blower motor by checking for 208 volts ac at terminals T1, T2, and T3 of motor B1001. If voltages are not present, check interconnections.
\end{tabular} \\
\hline
\end{tabular}

The following sequence of operation takes place when MASTER SWITCH is set to STANDBY, as directed in step 2:
(1) Primary contactor K1101 is energized, closing contacts L1-T1, L2-T2, L3-T3, L4-T4, and A1-A2, opening contacts B1-B2, applying power to control circuit bus, and energizing MAIN POWER ON lamp DS1102.

TABLE 5-10. RADIO SET AN/GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline \begin{tabular}{c} 
2 (cont) \\
(2) The 1-minute delay contactor, K1102, remains deenergized; therefore, contacts \\
\\
\\
\\
\begin{tabular}{l} 
3-4 remain closed. Blower contactor K1103 is energized through normally closed con- \\
tacts 3-4 of contactor K1102. Contacts L1-T1, L2-T2, and L3-T3 of contactor K1103 \\
close, applying power to blowers B901, B902, and B1101. Contacts A1-A2 of contactor \\
K1103 must close before contacts B1-B2 open. This transfers power from load side of \\
K1101 contacts to line side, permitting blowers to operate after MASTER SWITCH has \\
been set to OFF.
\end{tabular} \\
(3) Power is applied to ANTENNA CONTROL ON switch. Antenna control unit and \\
regulated filament bus can now be energized.
\end{tabular} \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|c|}
\hline 3 & & Set FIL ON switch S1108 on control-duplexer panel to ON position and turn MASTER SWITCH S1101 on controlduplexer panel from STANDBY to ON position. & \begin{tabular}{l}
FIL ON lamp DS1101 and MAIN POWER ON lamp DS1102 on con-trol-duplexer panel should go on. \\
Note \\
When switch S1108 is turned to ON position, all filaments are energized immediately except in radio receiver and coderindicator units of radio beacon. Amplifier-modulator, bias supply, and SAL-89 filaments are not energized until modulator filament relay K1301 is energized. (Relay K1301 is not energized until air switch S1301 is closed, indicating proper functioning of blowers B901 and B902.) \\
FILAMENT lamp DS1401 on panel of frequency multiplieroscillator should go on. \\
Note \\
FIL. SUPV. relay K1401 will be energized when primary of 2C39A filament transformer is energized (T1501). Contacts 2-4 of
\end{tabular} & \begin{tabular}{l}
Replace blower motor and cabling, if necessary. If lamps DS1101 and DS1 102 do not go on, check fuses F1102, F1108, and F1110. Also check that SUPPLY VOLTS METER M1101, with METER SELECTOR switch S1106 in REG FIL BUS position, reads 120 volts ac. If voltage is not 120 volts ac, an adjustment is provided in control-duplexer (variac T1101) for obtaining this voltage. Check variac T1101, transformer T1102, and contacts L4-T4 of primary contactor K1101. \\
Check lamps DS1101 and DS1102. Replace defective components. If lamp DS 1401 does not go on, check fuse F1401 and lamp DS1401. Replace if necessary.
\end{tabular} \\
\hline
\end{tabular}

TABLE 5-10. RADIO SET AN/GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline \[
\begin{gathered}
3 \\
\text { (cont) }
\end{gathered}
\] & & & \begin{tabular}{l}
relay K140 1 will then close, starting 1 MIN LVPS PLATE time delay relay K1605. When 1 minute has elapsed, LVPS plates are ready to be energized. \\
LV-MV READY lamp DS1605 on panel of low-voltage power supply should go on. \\
FIL lamp DS1301 on panel of amplifiermodulator should go on. \\
FILAMENT HOURS meter M1902 on panel of high-voltage power supply should be energized.
\end{tabular} & \begin{tabular}{l}
If lamp DS 1605 does not go on, check FIL. SUPV. relay K1401, 1 MIN LVPS PLATE relay K1605, air switch S1005 (DS1001 AIR SWITCH OPEN lamp will be on if air switch \(\$ 1005\) is open), and air switches S1002A, S1001A, and S903A. Replace defective components. \\
If lamp DS1301 does not go on, check air switch S1301 (if switch S1301 is defective, AIR SW OPEN lamp DS1303 on amplifier-modulator panel will go on). \\
If meter M1902 is not energized, check for 120 volts ac at terminal board TB1902. If voltage is present, check meter M1902. Replace meter, if necessary.
\end{tabular} \\
\hline 4 & & Turn ANTENNA CONTROL switch S1102 on control-duplexer panel to ON position. & \begin{tabular}{l}
ANTENNA CONTROL ON lamp DS1103 on control-duplexer panel should go on. \\
ANTENNA CONTROL lamp DS602 on coderindicator panel should go on and remain steady.
\end{tabular} & \begin{tabular}{l}
If lamp DS1103 does not go on, replace lamp and check fuses F1103 and F1104, resistor R1103, and contacts L1-T1 of relay K1101. Replace defective components and blown fuses. \\
If lamp DS602 flashes on and off, check antenna control power circuits.
\end{tabular} \\
\hline 5 & & Turn CODER INDICATOR switch 5601 on coder-indicator panel to ON position. & POWER ON lamp DS601 on coderindicator panel should go on. & If lamp DS601 does not go on, replace lamp and check fuses F601 and F602 on coderindicator panel and also \\
\hline
\end{tabular}

TABLE 5-10. RADIO SET AN/GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS,
FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|c|c|c|c|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & NEXT STEP \\
\hline \[
\begin{gathered}
5 \\
\text { (cont) }
\end{gathered}
\] & & & & resistor R601 on coderindicator video frame. Replace blown fuses and components. \\
\hline 6 & & Turn LV switch S 1601 on low-voltage power supply panel to ON position. & LV lamp DS 1603 and -375V lamp DS 1601 on low-voltage power supply should go on. & If lamp DS 1603 does not go on, replace lamp and check contacts of relay K1603 and interconnections. If lamp DS 1601 does not go on, replace lamp and check relay K1601. Replace relays and cabling, if necessary. \\
\hline 7 & & Turn MV switch S1801 on medium-voltage power supply panel to ON position. & \[
\begin{aligned}
& \text { +1000V lamp DS } 1801 \\
& \text { should go on. }
\end{aligned}
\] & If lamp DS 1801 does not go on, replace lamp and check that -375 no bias relay K1601 is energized. Refer to step 6. Check that 1kilovolt overload auxiliary relay is not energized, indicating no overload. (If an overload exists, MV OVERLOAD lamp DS 1803 on mediumpower supply panel will be on.) Check that overload reset relay K1806 is not energized, indicating no overload. \\
\hline 8 & & Turn HV switch S 1902 on panel of highvoltage power supply to ON position. & After a 5-minute time delay, HV lamp DS 1901 on highvoltage power supply panel should go on. & If lamp DS 1901 does not go on, replace lamp and check that 1kilovolt plate contactor K1804 is energized, closing contacts L4-T4, and that 2C39A filament relay K1401 is energized, closing contacts 2-4. Also check that overload reset relay K1806 is not energized, leaving its contacts in normally closed condition; that 5-minute klystron heater time delay K1606 has been allowed to run out; and that 12 -kilovolt overload auxiliary relay K1902 is not energized, indicating no overload. \\
\hline
\end{tabular}

TABLE 5-10. RADIO SET AN/GRN-9D, POWER DISTRIBUTION AND CONTROL CIRCUITS, FUNCTIONAL SECTION TROUBLESHOOTING CHART (cont)
\begin{tabular}{|c|l|l|l|l|}
\hline STEP & TEST POINT & PRELIMINARY ACTION & NORMAL INDICATION & \multicolumn{1}{c|}{ NEXT STEP } \\
\hline 9 & & \(\begin{array}{l}\text { Set receiver switch S502 } \\
\text { on receiver panel to } \\
\text { ON position. }\end{array}\) & \(\begin{array}{l}\text { POWER ON lamp DS501 } \\
\text { on receiver panel should } \\
\text { go on. }\end{array}\) & \(\begin{array}{l}\text { If lamp DS501 does not } \\
\text { go on, replace lamp } \\
\text { and check fuses F501 } \\
\text { and F502. Check re- }\end{array}\) \\
sistor R580. Replace \\
blown fuses and, if \\
necessary, replace \\
resistor R580.
\end{tabular}\(]\)

TABLE 5-11. RADIO SET AN/GRN-9D, TYPICAL TROUBLES
\begin{tabular}{|c|c|c|}
\hline TROUBLE & NATURE OF TROUBLE & SYMPTOM \\
\hline No a-c power input to both receiver-transmitter group and power supply assembly. & \begin{tabular}{l}
EMERGENCY switch S901 or MASTER SWITCH S1101 in OFF position. \\
Relay K901 or K1101 defective.
\end{tabular} & MAIN POWER ON lamp DS1102 not on. \\
\hline Blowers B901 and B902 in receiver-transmitter group cabinet inoperative. & \begin{tabular}{l}
Fuses F901 through F903 (blower B901 protection) and fuses F905 through F907 (blower B902 protection) blown. \\
Blowers defective.
\end{tabular} & \begin{tabular}{l}
Lamp in fuseholder glows. \\
AIR SW OPEN lamp DS901 on. \\
Blower motors not operating.
\end{tabular} \\
\hline Blower B1001 in power supply assembly cabinet inoperative. & \begin{tabular}{l}
Fuses F1006 through F1008 blown. \\
Blowers defective.
\end{tabular} & \begin{tabular}{l}
Lamp in fuseholder glows. \\
AIR SW OPEN lamp DS 1001 on. \\
Blower motor not operating.
\end{tabular} \\
\hline No - 1200 -volt d-c output from high-voltage power supply. & \begin{tabular}{l}
Fuses F1001 through F1003 blown. \\
Transformer T1001, switch S 1006, or relay K1001 defective. \\
High-voltage power supply failure. \\
Power distribution and control circuits failure.
\end{tabular} & \begin{tabular}{l}
Lamp in fuseholder glows. \\
HV lamp DS1901 off. \\
H. V. SUPPLY meter M1302 reads 0. \\
BEAM CURRENT meter M1301 reading other than 190 to 210 milliamperes.
\end{tabular} \\
\hline No +1000 -volt d-c output from medium-voltage power supply. & \begin{tabular}{l}
Power distribution and control circuits failure. \\
Medium-voltage power supply failure.
\end{tabular} & \begin{tabular}{l}
+1000 V lamp DS 1801 off. \\
D. C. SUPPLY VOLTAGE meter M1402 reads 0 when METER SELECTOR switch S1402 is in +1000 V SCALE \(X\) 2 position.
\end{tabular} \\
\hline No -375-volt d-c output from low-voltage power supply. & \begin{tabular}{l}
Power distribution and control circuits failure. \\
Low-voltage power supply (-375-volt d-c portion) failure.
\end{tabular} & \begin{tabular}{l}
-375V lamp DS1601 off. \\
D. C. SUPPLY VOLTAGE meter M1402 reads 0 when METER SELECTOR switch S1402 is in 375 V position.
\end{tabular} \\
\hline No +250-volt d-c output from low-voltage power supply. & \begin{tabular}{l}
Power distribution and control circuits failure. \\
Low-voltage power supply (+250-volt d-c portion) failure.
\end{tabular} & D. C. SUPPLY VOLTAGE meter M1402 reads 0 when METER SELECTOR switch S1402 is in +250 V position. \\
\hline
\end{tabular}

TABLE 5-11. RADIO SET AN/GRN-9D, TYPICAL TROUBLES (cont)
\begin{tabular}{|c|c|c|}
\hline TROUBLE & NATURE OF TROUBLE & SYMPTOM \\
\hline No a-c power input to coderindicator and radio receiver unit. & \begin{tabular}{l}
FIL ON switch S1108 in OFF position. \\
Fuse F1108 blown. \\
Variac T1101 defective.
\end{tabular} & \begin{tabular}{l}
Lamp in fuseholder glows. \\
FIL ON lamp DS1101 off.
\end{tabular} \\
\hline No a-c power input to coderindicator. & \begin{tabular}{l}
Fuses F601 and F602 blown. \\
CODER INDICATOR switch S601 in OFF position. \\
Interlock S906 or transformers T701 and T702 defective.
\end{tabular} & Lamp in fuseholder glows. POWER ON lamp DS601 off. \\
\hline No a-c power input to radio receiver. & \begin{tabular}{l}
Fuses F501 and F502 blown. \\
Receiver switch S502 in OFF position. \\
Interlock S905 or transformers T501 and T502 defective.
\end{tabular} & \begin{tabular}{l}
Lamp in fuseholder glows. \\
POWER ON lamp DS501 off.
\end{tabular} \\
\hline High or low output from high-voltage power supply. & High-voltage power supply failure. & H. V. SUPPLY meter M1302 reading other than -12 kilovolts dc. \\
\hline High or low output from medium-voltage power supply. & \begin{tabular}{l}
Potentiometer R1842 improperly adjusted. \\
Medium-voltage power supply failure.
\end{tabular} & D. C. SUPPLY VOLTAGE meter M1402 reading other than +1000 volts dc when METER SELECTOR switch S1402 is in +1000 V SCALE \(X\) 2 position. \\
\hline High or low output from low-voltage power supply. & \begin{tabular}{l}
Potentiometer R1663 (-375volt d-c adjustment) or R1623 (+250-volt d-c adjustment) improperly adjusted. \\
Low-voltage power supply failure.
\end{tabular} & D. C. SUPPLY VOLTAGE meter M1402 reading other than \(\mathbf{- 3 7 5}\) volts dc and +250 volts dc when METER SELECTOR switch S1402 is in -375V and +250 V position, respectively. \\
\hline High or low output from radio receiver power supply. & \begin{tabular}{l}
Potentiometer R507 improperly adjusted. \\
Radio receiver power supply failure.
\end{tabular} & TEST METER M501 reading other than +150 volts dc when METER SELECTOR switch S501 is in B + 200 VFS position. \\
\hline High or low output from coder-indicator power supply. & \begin{tabular}{l}
Potentiometer R710 improperly adjusted. \\
Coder-indicator power supply failure.
\end{tabular} & Multimeter connected between terminal 1 of terminal board TB701 and ground reading other than +250 volts dc. \\
\hline
\end{tabular}

TABLE 5-11. RADIO SET AN/GRN-9D, TYPICAL TROUBLES (cont)
\begin{tabular}{|c|c|c|}
\hline TROUBLE & NATURE OF TROUBLE & SYMPTOM \\
\hline Low receiver sensitivity. & \begin{tabular}{l}
Defective crystals (hybrid mixer circuit) CR201 and CR202. \\
Defective Ferris discriminator V306. \\
Defective i-f amplifier (tubes V301 through V305). \\
Defective preamplifier (tubes V201 through V203). \\
Preselector improperly adjusted.
\end{tabular} & TEST METER M501 reading other than half-scale deflection when METER SELECTOR switch S501 is in CR201 and CR202 position, respectively. \\
\hline No r-f output from transmitter. & \begin{tabular}{l}
Frequency multiplieroscillator \(\mathbf{r}\)-f circuits (tubes V1501 through V1506) defective. \\
High-voltage power supply failure. \\
Klystron improperly adjusted. \\
Klystron bias supply (transformer T1371, diodes CR1370 and CR1371, and tubes V1370 and V1371) failure. \\
Potentiometer improperly adjusted.
\end{tabular} & BEAM CURRENT meter M1301 reading other than 190 to 210 milliamperes. \\
\hline Identification call not transmitted. & \begin{tabular}{l}
Defective keyer motor B602 or keyer assembly. \\
Failure of \(1350-\mathrm{cps}\) tone generating circuit (tubes V612 and V613). \\
Switch S603, diode CR603, or tube V611 defective.
\end{tabular} & \begin{tabular}{l}
Keyer motor B602 not operating. \\
Code not heard on headset connected to TEST OUTPUT jack J607.
\end{tabular} \\
\hline
\end{tabular}



\section*{SECTION 6}

\author{
REPAIR
}

\section*{Note}

\begin{abstract}
Maintenance Standards Book NAVSHIPS 93881. 42 provides instructions for preventive maintenance e of Radio Set AN/GRN-9D. This technical manual also contains performance standards required to determine whether the equipment is operating properly and whether optimum performance of the equipment has been attained as a result of performing tuning and adjustment procedures.
\end{abstract}

\section*{6-1. FAILURE REPORT}

Report each failure of the equipment, whether caused by a defective part, wear, improper operation, or an external cause. Use ELECTRONIC FAILURE REPORT form DD787. Each pad of the forms includes full instructions for filling out the forms and forwarding them to the Bureau of Ships. However, the importance of providing complete information cannot be emphasized too much. Be sure that you include the model designation and serial number of the equipment (from the equipment identification plate), the type number and serial number of the major unit (from the major identification plate), and the type number and reference designation of the particular defective part (from the technical manual). Describe the cause of the failure completely, continuing on the back of the form if necessary. Do not substitute brevity for clarity. And remember--there are two sides to the failure report-

\section*{YOUR SIDE}

Every FAILURE REPORT is a boost for you:
1. It shows that you are doing your job.
2. It helps make your job easier.
3. It ensures available replacements.
4. It gives you a chance to pass your knowledge to every man on the team.

\section*{BUREAU SIDE}

The Bureau of Ships uses the information to:
1. Evaluate present equipment.
2. Improve future equipment.
3. Order replacements for stock.
4. Prepare field changes.
5. Publish maintenance data.

Always keep a supply of failure report forms on board. You can get them from the nearest District Publications and Printing Office.

\section*{6-2. TUNING AND ADJUSTMENT}

The tuning and adjustment procedures described in \(6-2 \mathrm{c}\) through \(6-2 \mathrm{~h}\) should be performed at the following times:

Whenever the routine checks covered in Section 3 specify that realignment and adjustments are necessary in order to ensure optimum equipment performance.

Whenever the troubleshooting charts covered in Section 5 specify that realignment and adjustments are necessary.

Whenever large scale tube replacement has been made.
Periodically, as directed by experience.

The adjustment controls are located inside the individual drawer units. To gain access to a particular control and make an adjustment, proceed as follows:

Step 1. Loosen captive screws provided on front panel of drawer unit in which control is housed.

Step 2. Pull out drawer unit until stop latch on slide assembly engages.

Step 3. Manually operate interlock provided on cabinet frame. To do so, push interlock pin gently to side and pull it out until it catches.

Step 4. Loosen hex nut which locks potentiometer shaft in adjusted position.

Step 5. Use screwdriver to make required adjustment, and tighten hex nut to secure potentiometer in desired position.

Step 6. After all adjustments have been made in drawer unit, push unit back into cabinet frame and tighten captive screws. Interlocks will be released automatically.
a. TEST EQUIPMENT AND SPECIAL TOOLS.- The test equipment required to tune and adjust the radio set for optimum performance is listed in tables \(5-1\) and 5-1a. The Original Test Equipment is referred to as Built-in Test Equipment whilst the Replacement Test Equipment is that of the TACAN Test Monitor Group MM-TMC-212A Rack. No special tools are required to perform any of the tuning and adjustment procedures.
b. CONTROL SETTINGS.- Under normal operating conditions all power switches except those of the test equipment are left in the \(0 N\) position. Refer to Section 3 for specific instructions concerning equipment turn-on procedure.

Proper adjustment of some circuits of the radio set entails the use of the test equipment. Prior to performing any of these adjustments, set up the equipment as outlined in paragraph 5-4b.

\section*{c. POWER SUPPLY ADJUSTMENTS.}

\section*{(1) LOW VOLTAGE POWER SUPPLY PP-1766/URN.}

Step 1. Turn meter selector switch S1402 (figure \(3-3\) ) to +250 V . Check that a reading between 245 and 255 volts dc is indicated on D. C. SUPPLY VOLTAGE meter M1402 (frequency multiplier-oscillator panel).

Step 2. If reading is not correct, adjust potentiometer R1623 (figure 6-1) to obtain a reading of exactly +250 volts dc.

Step 3. Turn meter selector switch S1402 to -375 V . Check that a reading between -367 and -383 volts dc is indicated on D. C. SUPPLY VOLTAGE meter M1402.

Step 4. If reading is not correct, adjust potentiometer R1663 (figure 6-1) to obtain a reading of -375 volts dc.

\section*{(2) MEDIUM VOLTAGE POWER SUPPLY PP-1765/URN.}

Step 1. Turn meter selector switch S1402 (figure \(3-3\) ) to +1000 V . Check that a reading between +980 and +1020 volts dc is indicated on D. C. SUPPLY VOLTAGE meter M1402 (frequency multiplieroscillator panel).

Step 2. If reading is not correct, adjust potentiometer R1842 (figure 6-2) to obtain a reading of exactly +1000 volts dc.
(3) RADIO RECEIVER POWER SUPPLY. Adjustment of the radio receiver power supply should be performed after receiver switch S502 (figure 3-1) has been set to ON and POWER ON lamp DS501 (radio receiver panel) has been on for at least 10 minutes. To adjust the power supply, proceed as follows:

Step 1. Turn METER SELECTOR switch S501 (figure \(3-1\) ) to \(B+200\) VFS. Check that a reading of 75 scale divisions, which is equivalent to +150 volts dc is indicated on TEST METER M501 (radio receiver panel).

Step 2. If reading is not correct, adjust potentiometer R507 (figure 6-3) to obtain a reading of exactly 75 scale divisions ( +150 volts dc).


Figure 6-1. Low Voltage Power'Supply PP-1766/URN, Right Side View

\section*{(1) LOCAL OSCILLATOR ADJUSTMENT.}

Step 1. Turn METER SELECTOR switch S501 (figure 3-1) to CR201. Check reading indicated on TEST METER M501.

Step 2. Turn METER SELECTOR switch S501 to CR202. Check reading indicated on TEST METER M501.

\section*{Note}

In each position of the switch, meter should show half-scale deflection, corresponding to 1.0 milliampere. The two readings should be nearly equal.
- Step 3. Loosen screw located on side of pick-up probe J1505 and move probe on tripler cavity V1504 (figure 6-4) in or out, as necessary, to obtain required readings. Tighten screw.
(2) SQUITTER CIRCUIT CHECK AND ADJUSTMENT.
(a) SQUITTER CONTROL VOLTAGE CHECK.

Step 1. Turn METER SELECTOR switch S501 (figure 3-1) to SQUITTER CONTROL - 10 VFS. Check reading indicated on TEST METER M501.

\section*{Note}

Meter should read about 5 volts (half-scale deflection) when local oscillator power is normal ( 1.0 milliampere). When no local oscillator power is available, squitter voltage will be about 1 volt less, or 4 volts as read on meter.

Step 2. Disconnect local oscillator input cable from jack J201 on frequency multiplier-oscillator chassis. Replace cable to local oscillator input at jack J201.
(b) SQUITTER COUNT AND ADJUSTMENT.

\section*{1. TEST EQUIPMENT AND SPECIAL} TOOLS. - The built-in test equipment is required to perform the squitter count and adjustment procedure. This equipment, comprising Power Meter-Pulse Counter TS-891/URN-3, Oscilloscope OS-54/URN-3, Pulse Analyzer-Signal Generator TS-890A/URN-3, and Pulse-Sweep Generator SG-121A/URN-3, is housed in the power supply assembly cabinet. No special tools are required to perform this procedure.
2. CONTROL SETTINGS. -Set all power switches, except those on the built-in test equipment, to the on position.
3. CONNECTIONS. - To perform this procedure, make the built-in test equipment front panel connections shown in figure 3-13.


Figure 6-3. Radio Receiver, R824/URN, Right Side View

\section*{4. INSTRUCTIONS.}

Step 1. Set MV switch S1801 on medium voltage power supply panel and HV switch S1902 on high voltage power supply panel to OFF.

\section*{CAUTION}

Variation of squitter rate adjustment may result in an extremely high squitter rate, causing high klystron beam current to trip overload relay of transmitter.

Step 2. Set METER SELECTOR switch S501 to CR201, then to CR202. Check reading indicated on TEST METER M501. Meter should indicate about 1 milliampere (half-scale deflection in each position).

Step 3. Set METER SELECTOR switch S501 to SQUITTER CONTROL - 10 VFS. This setting facilitates monitoring d-c squitter control voltage being fed back to i-f amplifiers V301 and V302.

\section*{Note}

Prior to performing the following steps, set up the built-in test equipment as specified in paragraph 5-4b.

Step 4. Turn FUNCTION SWITCH of power meterpulse counter panel to RECEIVER SENSITIVITY.

Step 5. Set COUNTER SELECTOR switch of power meter-pulse counter panel to SQUITTER.

Step 6. Set RANGE SWITCH of power meterpulse counter panel to X10. SQUITTER rate, as read on PULSE COUNT METER, should be \(2700 \pm 90\) pulses per second.

Step 7. Carefully adjust potentiometer R427 (figure 6-3) until count is \(2700 \pm 90\) pulses per second. Squitter control voltage as read on TEST METER M501 should be approximately -5 volts.

\section*{(3) 40-MICROSECOND BLANKING GATE ADJUSTMENT.}
(a) TEST EQUIPMENT AND SPECIAL TOOLS. -Oscilloscope OS-54/URN-3 is required to perform the 40 -microsecond blanking gate adjustment. No special tools are required to perform this adjustment.
(b) CONTROL SETTINGS. - Set all power switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.
(c) INSTRUCTIONS.

Step 1. Connect coaxial test lead from TEST OUTPUT jack J507 (figure 3-1) to EXT TRIGGER INPUT jack of oscilloscope panel. Set TRIGGER SELECTOR control of oscilloscope panel to +EXT.

Step 2. Connect test prod to VERT SIGNAL INPUT jack of oscilloscope panel. Connect test prod to test point TP9 (figure 6-5) and lock in signal on oscilloscope. Horizontal sweep speed should be between 50 and 100 microseconds per inch. Waveshape 17 in figure \(5-9\) should be obtained.

Step 3. Using 10 -microsecond markers, adjust potentiometer R443 (figure 6-3) to obtain a pulse width of 40 microseconds.

Step 4. Recheck squitter count, in accordance with 6-2d(2)(b).

\section*{e. CODER-INDICATOR ADJUSTMENTS.}
(1) 1350-CPS IDENTIFICATION TONE OSCILLATOR ADJUSTMENT.
(a) TEST EQUIPMENT AND SPECIAL TOOLS. -Oscilloscope OS-54/URN-3 is required to perform the \(1350-\mathrm{cps}\) identification tone oscillator adjustment. No special tools are required to perform this adjustment.
(b) CONTROL SETTINGS. -Set all power switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.

\section*{(c) INSTRUCTIONS.}

Step 1. Open coder-indicator drawer, manually set interlock on cabinet frame and set CODER INDICATOR switch S601 on coder-indicator panel to ON.


Figure 6-4. Frequency Multiplier-Oscillator CV-1171/GRN-9D, R-F Chassis, Bottom View


Figure 6-5. Radio Receiver R-824/URN, Left Side View

Step 2. Turn on antenna by setting ANTENNA CONTROL switch S1102 on control-duplexer panel to ON.

Step 3. Lower video chassis as shown in figure 6-6.

Step 4. Connect coaxial test lead from TEST OUTPUT jack J607 on coder-indicator panel to VERT SIG INPUT jack on oscilloscope panel.

Step 5. Connect coaxial test lead from SYNC OUTPUT jack J606 on coder-indicator panel to EXT TRIG INPUT jack on oscilloscope panel.

Step 6. Set switch \(\mathbf{S 6 0 3}\) (figure 6-6) to CONTINUOUS TONE.

Step 7. Lock in signal on oscilloscope with sweep speed set to 4000 microseconds per inch.

Step 8. Auxiliary reference bursts will appear as heavy pulses with tone pulse groups appearing as faint pulses evenly spaced between auxiliary reference bursts. (See waveshape 24E in figure 5-11.) Count number of tone pulse groups which occurs between auxiliary reference bursts. If \(1350-\mathrm{cps}\) identification tone oscillator is properly adjusted, nine tone pulse groups will appear between auxiliary reference bursts.

Step 9. If necessary, adjust coil L603 (figure 6-6) until nine tone pulse groups appear between auxiliary reference bursts.

Step 10. Set oscilloscope sweep speed to 100 microseconds per inch, and lock in two identification pulse pairs on oscilloscope screen.

Step 11. Adjust potentiometer R798 on coderindicator video chassis until spacing between leading edge of first pulses in each pulse pair is \(100 \pm 10\) microseconds. Adjustment of \(1350-\mathrm{cps}\) identification tone oscillator is now complete.
(2) NORTH AND AUXILIARY REFERENCE BURSTS ADJUSTMENT.
(a) TEST EQUIPMENT AND SPECIAL TOOLS. -Oscilloscope OS-54/URN-3 is required to perform the north and auxiliary reference bursts adjustment. No special tools are required to perform this adjustment.
(b) CONTROL SETTINGS. - Set all power switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.
(c) INSTRUCTIONS.

Step 1. Perform steps 1 through 5 of paragraph 6-2e(1).

Step 2. Remove plug P906 from jack J603 (figure 6-6).

Step 3. Lock in signal on oscinoscope with sweep speed set to 110 microseconds per inch. North reference burst will appear on oscilloscope screen as a series of pulse pairs. When radio set is operating properly, north reference burst consists of \(12 \pm 1\) pulse pairs. (See waveform 24A of figure 5-11.)

Step 4. Locate potentiometer R675 on coderindicator video chassis. Loosen shaft locking nut, and adjust to obtain 12 pulse-pairs on oscilloscope screen. Turning shaft clockwise decreases number of pulse pairs, turning shaft counterclockwise increases number of pulse pairs. While observing north reference burst on oscilloscope, turn shaft of potentiometer R675 clockwise to obtain 11 pulse pairs, then counterclockwise to obtain 13 pulse pairs.

The correct setting of potentiometer R675 is midway between settings which provide 11 and 13 pulse pairs. After potentiometer R675 is set correctly, carefully tighten locking screw.

Step 5. Check that spacing between leading edge of 1st pulse and leading edge of 23rd pulse is \(330 \pm 5\) microseconds ( 3 inches on oscilloscope screen with sweep speed set at 110 microseconds per inch). If spacing is correct, adjust coil L601 on coderindicator video chassis until spacing is correct.

Step 6. Replace plug P906 in jack J603, and remove plug P905 from jack J604 on coder-indicator video chassis.

Step 7. Lock in auxiliary reference bürst with sweep speed set to 40 microseconds per inch. When radio set is operating properly, auxiliary reference burst should consist of \(6 \pm 1\) pulse pairs.

Step 8. Locate potentiometer R672 on coderindicator video chassis. Loosen shaft locking nut, and adjust potentiometer R672 while observing auxiliary reference burst on oscilloscope. Turn shaft


Figure 6-6. Coder-Indicator KY382/GRN-9D, Left Side View with Video Chassis Lowered


Figure 6-7. Coder-Indicator KY-382/GRN-9D, Right Side View
clockwise until five pulse pairs are obtained, then counterclockwise until seven pulse pairs are obtained. The correct setting for potentiometer R672 is midway between settings which give five and seven pulse pairs.

Step 9. Check that spacing between leading edge of 1 st pulse and leading edge of 11 th pulse is \(120 \pm 1\) microseconds ( 3 inches on oscilloscope with sweep speed set to 40 microseconds per inch). If spacing is incorrect, adjust coil L602 on coder-indicator chassis until spacing is correct.

\section*{(3) DENTIFICATION TONE KEYER ADJUSTMENTS.}
(a) TEST EQUIPMENT AND SPECIAL

TOOLS. -A stop watch is required as a special tool to perform the identification tone keyer adjustment. No test equipment is required for this procedure.
(b) CONTROL SETTINGS. -Set all power switches, except those on the built-in test equipment, to the on position.
(c) INSTRUCTIONS.

Step 1. Open coder-indicator drawer to gain access to identification tone keyer assembly, mounted on right side of unit (figure 6-7). Operate interlocks to energize coder-indicator unit.

Step 2. Set switch \(\mathbf{S 6 0 5}\) to off position.
Step 3. Lower coder-indicator chassis as shown in figure 6-6.

Step 4. Uncouple motor B602 from code wheel assembly by loosening setscrew securing coupling end to motor shaft.

Step 5. Remove two captive screws, flat washers, and lockwashers that secure switch S 607 cover (figure 6-7) to housing. Remove cover.

Step 6. Rotate code wheel assembly until code just starts at START CODE segment (figure 6-7).

Step 7. Loosen screws located in slots of adjustable cam (figure 6-6) and position adjustable cam so that switch \(\mathbf{S 6 0 4}\) is not actuated. Tighten screws.

Step 8. Rotate code wheel assembly in counterclockwise direction until segment number 58 on the code wheel assembly actuates switch S 607 . Rotate code wheel assembly in counterclockwise direction and check that switch S004 is actuated immediately after switch \(\mathbf{S 6 0 7}\) is actuated. If it is not, loosen screws located in slots of adjustable cam, and position cam so thrat switch S 604 is actuated.

Step 9. Repeat steps 6 through 8 in order to make a fine adjustment of S 607 so that it is not actuated at the START CODE segment, but is actuated immediately after switch 5604 is actuated by the number 58 segment.

Step 10. Couple motor B602 to code wheel assembly by tightening setscrew.

Step 11. Set keyer switch S 603 (coder-indicator video chassis figure 6-6) to NORMAL KEYING.

Step 12. Connect headset to TEST OUTPUT jack J607 on coder-indicator panel.

Step 13. Set switch S 605 to on position and listen to code produced in headset. If complete code is not heard, adjust coding switch S607. To do this, unlock adjustment screw (figure 3-11). By means of adjustment screw, move switch S 607 closer to or further away from segments mounted on code wheel assembly, as required.

Step 14. Set switch S605 to off position and replace switch S 607 cover to switch housing. Set switch 5605 to on position.

Step 15. Adjust cutoff of code by using slotted cam to actuate switch S604 immediately after switch S607 actuation cycle by segment number 58 is completed.

Step 16. For fine adjustment, adjust switch S604 by loosening clamp screw and rotating switch about its pivot mounting center.

\section*{Note}

The cams are cut so that code can be trans-
- mitted for two consecutive revolutions of code wheel. Initial adjustment should be made so that the code is transmitted for one out of every five revolutions. These adjustments are independent and must be made alternately. To facilitate adjustment, it is recommended that the motor be decoupled from the drive shaft and the code wheel turned manually.

Step 17. Repeat procedures called for in step 6 with motor reconnected.
(4) SETTING THE CODE (IDENTIFICATION

CALL). - For information on setting the code, refer to paragraph 3-2c(2)(b).
(5) DELAY LINE DL601 ADJUSTMENT (ZERO DISTANCE DELAY). - The delay line is located on
video chassis of coder-indicator unit (figure 6-6). The procedure outlined below is based on checking the overall radio beacon delay of 50 microseconds and adjusting delay line DL601 as necessary to obtain that delay. The built-in test equipment is employed for this procedure.
(a) TEST EQUIPMENT AND SPECIAL

TOOLS. - The test equipment required to perform the zero distance delay adjustment is based on using the built-in test equipment. This equipment, consisting of the power meter-pulse counter, oscilloscope, pulse analyzer-signal generator, and pulse-sweep generator, is housed in the power supply assembly cabinet. No special tools are required to perform this adjustment.
(b) CONTROL SETTINGS. - Set all power switches, except those on the built-in test equipment, to the on position.
(c) CONNECTIONS. - In order to perform the zero distance delay procedure, the built-in test equipment front panel connections shown in figure 3-13 must be made.

\section*{(d) INSTRUCTIONS.}

Step 1. Set FUNCTION switches of oscilloscope panel and power meter-pulse counter panel to VIDEO DELAY.

Step 2. Set pulse-sweep generator TRIGGER SELECTOR switch to SWEEP, and PULSE CODING switch to \(11.5 \mu \mathrm{SEC}\), position 2. Set CRYSTAL SELECTOR switch to position 1.

Step 3. Adjust pulse analyzer-signal generator to provide a modulated signal. (Refer to procedure in Section 2.) Then, set MODULATION SELECTOR switch to PULSE and RF OUTPUT attenuator to - 35 DBM.

Step 4. Observe display on oscilloscope screen, and, if necessary, adjust oscilloscope controls for clear presentation. Note that two sets of pulses are displayed, the radio set output pulse and a pair of reference pulses.

Step 5. Adjust pulse-sweep generator BALANCE control so that reference pulses have slightly larger amplitude than radio set output pulses. A pattern similar to that shown in figure \(6-8\) should be obtained on oscilloscope.

Step 6. If pattern such as that shown in figure 6-8 is obtained (radio set output pulse pair to left of reference pulse pair), overall zero-distance delay is less than 50.2 microseconds and the next step should be performed. If it is to the right, the zero delay is too great; proceed to step 8.

Step 7. Change CRYSTAL SELECTOR switch on pulse-sweep generator panel to position 2. Observe that pattern is as shown in figure 6-8. If radio set output pulse pair is to left of reference pulse pair, zero-distance delay is less than 49.8 microseconds,

(B)

Figure 6-8. Overall System Delay Measurement Waveforms
and a readjustment of delay line is necessary. Proceed with step 8.

\section*{Note}

Ideally, radio set output pulses should be as much to right of reference pulse (switch position 1) as they are to left (switch position 2).

Step 8. Remove cover on delay line DL601 and loosen delay line top locking screw.

Step 9. Slide tap on delay line DL601 to right o: left, as necessary, to obtain net delay of between 49.8 and 50.2 microseconds, as determined by repeating steps 6 and 7 . Lock delay line tap in position and replace cover.

\section*{f. TRANSMITTER ADJUSTMENTS.}
(1) TRANSMITTER OUTPUT CIRCUIT

TUNING. - Refer to Section 2 for detailed instructions on overall tuning of transmitter output circuit and aging of klystron.
(2) SHAPED PULSE ADJUSTMENT.

\section*{(a) TEST EQUIPMENT AND SPECIAL}

TOOLS. -Oscilloscope OS-54/URN-3 is required to perform the shaped pulse gate adjustment. No special tools are required to perform this adjustment.
(b) CONTROL SETTINGS. -Set all power switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.
(c) INSTRUCTIONS.

Step 1. Connect coaxial test lead from SHAPED PULSE jack J1405 on frequency multiplier-oscillator panel to VERT SIG INPUT jack on oscilloscope panel. Turn FUNCTION SWITCH on oscilloscope panel to GENERAL TEST.

Step 2. Observe waveshape indicated on oscilloscope; it should be similar to waveshape 9 in figure \(5-16\). The waveshape should meet the following requirements: The shaped pulse should be symmetrical and should have a duration of \(4.5 \pm 0.5\) microseconds at half-amplitude point and 9 microseconds at base. The pulse should have an amplitude of approximately 10 volts.

Step 3. If above requirements are not met, perform steps 4 through 12.

Step 4. Connect test prod to VERT SIG INPUT jack on oscilloscope panel and connect test prod to pin 5 at V1403. The waveshape in figure 5-16, waveshape 5 , should be indicated on oscilloscope.

Step 5. Measure pulse width at half-amplitude points. If it is not \(2.6 \pm 0.1\) microseconds, adjust potentiometer R1466 on frequency multiplieroscillator video chassis (figure 6-9) to obtain this pulse width.

Step 6. Disconnect plug P917 from jack J1401 on frequency multiplier-oscillator unit. Connect Multimeter AN/PSM-4 to pin 1 at V1407.

Step 7. Adjust potentiometer R1420 on frequency multiplier-oscillator video chassis to obtain a reading of +8.0 volts dc on multimeter. After this adjustment is made, disconnect multimeter and reconnect plug P917 to jack J1401.

Step 8. Connect test prod to center tap of potentiometer R1470 on frequency multiplier-oscillator video chassis. While observing shaped pulse, adjust potentiometer R1417 on frequency multiplieroscillator video chassis for minimum reflections. See waveforms 26A and 26B in figure 5-16.

Step 9. Disconnect test prod from oscilloscope and connect coaxial test lead from VERT SIG INPUT jack on oscilloscope panel to SHAPED PULSE jack J1405 on frequency multiplier-oscillator panel.

Step 10. While observing output pulse on oscilloscope screen, adjust potentiometer R1470 to obtain maximum amplitude without limiting. See waveshape 9 B in figure 5-16 for an example of a limited shaped pulse.

Step 11. Connect coaxial test lead from VERT SIG INPUT jack to ANTENNA INCIDENT jack J1154 on control-duplexer panel. Lock in auxiliary reference burst on oscilloscope screen. Check that amplitude of pulses remains constant throughout reference burst. If reference burst appears as shown in waveshape 24 of figure \(5-16\), no further adjustment is necessary. If reference burst appears as shown in either waveshape 22 or 23 of figure 5-16, adjust potentiometer R1471 on frequency multiplieroscillator video chassis to obtain a constant amplitude for all pulses in reference burst as shown in wave-


Figure 6-9. Frequencso Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, Bottom View
shape 24. The adjustment of potentiometer R1470, as described in step 10, and the adjustment of R1471 are interdependent. If it was necessary to adjust potentiometer R1471 to minimize droop, recheck adjustment of R1470 by observing a single pulse on oscilloscope and touching up adjustment of potentiometer R1470 to obtain the maximum pulse amplitude possible without limiting.

\section*{Note}

After making adjustments on shaped pulse circuits, check peak power output and spectrum analysis as directed in paragraphs 3-6a(2) and 3-6a(5).

Step 12. Coils L1401, L1402, and L1403 (figure 6-9) are adjusted to proper value of inductance at factory and are not to be adjusted in field. Note that the inductance values are given to two decimal places on schematic diagram, figure 6-18. Replacement of these coils is a function of depot maintenance. Before replacing coil in shaper network, check its value on inductance bridge capable of measuring inductance in the range of 1 to 5 millihenrys to an accuracy of 100th of a millihenry.

\section*{(3) KEYFNG PULSE CHECKS AND ADJUSTMENTS.}
(a) KEYING PULSE WIDTH ADJUSTMENT.

\section*{1. TEST EQUIPMENT AND SPECIAL}

TOOLS. -Oscilloscope OS-54/URN-3 is required to
perform the keying pulse width adjustment. No special tools are required to perform this adjustment.
2. CONTROL SETTINGS. -Set all power switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.

\section*{3. INSTRUCTIONS.}

Step 1. Connect test prod to VERT SIG INPUT jack on ascilloscope panel. Set FUNCTION SWITCH on oscilloscope panel to GENERAL TEST.

Step 2. Connect test prod to pin 3 at V1409 on frequency multiplier-oscillator video chassis. Check that the width of the keying pulse appearing on the scope screen is \(1-+0.5-0.0\) microseconds wide at half-amplitude points.

Step 3. If requirement in step 2 is not met, adjust potentiometer R1465 on frequency multiplieroscrllator video chassis to obtain proper pulse width.

\section*{(b) CENTERING OF KEYING PULSE ABOUT THE SHAPED PULSE.}
1. TEST EQUİPMENT AND SPECIAL TOOLS. -Oscilloscope OS-54/URN-3 is required to perform the keying pulse positioning adjustment. No special tools are required to perform this procedure.

\section*{2. CONTROL SETTINGS. - Set all power} switches, except those on the built-in test equipment, to the on position. Set up and energize the oscilloscope in accordance with the instructions contained in Technical Manual NAVSHIPS 92778 supplied with the oscilloscope.

\section*{3. INSTRUCTIONS.}

Step 1. Connect coaxial test lead from VERT SIG INPUT jack on oscilloscope panel to SHAPED PULSE jack J1405 on frequency multiplier-oscillator panel and observe shaped pulse indicated on oscilloscope.

Step 2. Center shaped pulse about a vertical hairline on the scale. Note carefully positions of half-amplitude points of shaped pulse. Once these points have been determined, do not touch any of the horizontal controls of the oscilloscope.

Step 3. Disconnect coaxial test lead from oscilloscope and connect test prod to VERT SIG INPUT jack. Connect test prod to pin 3 at V1409.

Step 4. Check that two half-amplitude points of shaped pulse are centered within keying pulse.

Step 5. If not, move lead connected to tap (terminals 3, 4, 5, or 6) on delay line DL1402 (see figure 6-9), to one of the other taps as necessary to meet requirement.

\section*{Note}

Delay lines DL1401 and DL1402 are connected in series to provide enough delay to center shaped pulse on keying pulse. The entire delay of DL1401 must be used. The tap on delay line DL1402 is selected to provide additional delay if required.
g. CONTROL-DUPLEXER. -Refer to paragraphs 2-5f(2) and 2-5f(3) for instructions on adjusting preselector cavities and transmission line filter.
h. TACAN ADJUSTMENTS USING REPLACEMENT TEST EQŪIPMENT MM-TMC-212A (TABLE 5-la).- Adjustment should be made after the beacon has been turned on and allowed to warm up for at least 10 minutes, or longer where stated.
(1) SQUITTER RATE ADJUSTMENT.
(a) On the Radio Receiver, turn the METER SELECTO \(\bar{R}\) switch to the CR201 and CR202 positions in turn. The TEST METER should indicate approximately half scale in both positions. If this condition is not met, adjust the coupling from the Frequency Multiplier Oscillator as described in paragraph 6-2 \(\underline{h}\) (8) (a) 9,10 and 11 .
(b) Turn the METER SELECTOR switch to the SQUITTER CONTROL - 10 VFS position. The TEST METER should indicate approximately \(-5 \cdot 0 \mathrm{~V}\).
(c) Continue as follows:
1. On the High Voltage Power Supply, set the HV ON/OFF switch to ON.
2. Measure the squitter rate as described in para. \(\overline{3}-6 \mathrm{a}(12)(\mathrm{a})\), and adjust R427, on the right-hand side of the chassis, to obtain a squitter rate of 5400 pulses per second.
3. Return the HV ON/OFF switch to OFF.

\section*{(2) BLANKING TIME ADJUSTMENT.}
(a) On the Radio Receiver, locate TP9 on the righthand side of the video chassis. Connect a lead from TP9 to the oscilloscope CH1 INPUT jack and connect a fur ther lead from the Receiver TEST OUTPUT socket to the oscilloscope A time base TRIG IN jack.
(b) Set up the oscilloscope to observe the blanking pulse as shown in Figure 6-9a. Calibrate the markers and use them to measure the pulse. width at the half-amplitude point.
(c) Adjust R443, BLANKING TIME ADJ, on the video chassis. to obtain a pulse width of exactly \(40 \mu \mathrm{sec}\)

(3) CODER INDICATOR POWER SUPPLY.
(a) Release the four securing bolts on the Coder Indicator and draw the unit fully forward. Remove the access panel from the top of the unit.
(b) Set the Multimeter to the DC 300V range. Locate tag board TB701 on the chassis and connect the multimeter negative lead to Pin 9. Connect the positive lead to Pin 1.
(c) Manually override the interlock and adjust \(\overline{\mathrm{R}} 710\) on the power supply chassis to obtain a reading of +250 V . Disconnect the meter.
(d) Connect the positive lead to Pin 9 and the negative lead to Pin 6. Observe that the meter indicates between -100 and -110 volts. Disconnect the meter and replace the access panel.
(4) IDENTITY AND EQUALIZING PULSE SPACINGS.
(a) Measure and adjust the Identity and Equalizing pulse spacings as described in paragraph 3-6a-(12)(d).
(b) If the requirements are not met as described, adjust L603 and R798 on the Coder Indicator video chassis for an Identity pulse spacing of \(740 \mu \mathrm{sec}\) and an Equalizing pulse spacing of \(100 \mu \mathrm{sec}\) respectively.
(5) NORTH REFERENCE BURST.
(a) Perform the operations as described in paragraph 3-6a(12) (c) to count the number of pulse pairs in each burst and to measure the spacing between each pulse pair.
(b) Release the three screws securing the video chassis of the Coder Indicator, and lower the chassis. Locate R675 and loosen the locking nut. Adjust R675 to obtain twelve pulse pairs in each burst. The correct setting should be midway between the positions where 11 and 13 pulse pairs are obtained. Carefully retighten the locking nut.
(c) Locate \(L 601\) and adjust it to obtain a pulse pair spacing of \(30 \mu \mathrm{sec}\).
(6) AUXILIARY REFERENCE BURST.
(a) Perform the operations as described in paragraph 3-6a(12)(c) to count the number of pulse pairs in each burst and to measure the spacing between each pulse pair.
(b) Locate R672 and loosen the locking nut. Adjust R672 to obtain six pulse pairs in each reference burst. The correct setting is mid-way between the positions where 5 and 7 pulse pairs are obtained. Carefully re-tighten the locking nut.
(c) Locate L602 and adjust it to obtain a pulse pair spacing of \(24 \mu \mathrm{sec}\).

\section*{(7) REPLY DELAY.}
(a) Measure the Reply Delay as described in paragraph \(\overline{3-6 a}(12)(\mathrm{e})\). Locate the delay line DL601 on the video chassis and remove the cover.
(b) Loosen the locking screw and adjust the sliding tapping to obtain a reply delay of exactly \(50 \mu \mathrm{sec}\).
(c) Tighten the locking screw and replace the delay line cover. Return the video chassis to its normal position and tighten the securing screws.

\section*{(8) FREQUENCY MULTIPLIER OSCILLATOR (FMO)} ADJUSTMENTS.
(a) Tuning. - Allow sufficient time for the crystal oven to reach operating temperature. This will be shown by the intermittent lighting of the white NORMAL lamp. Release the hinged access panel covering the RF sub-chassis.
1. On the High Voltage Power Supply, ensure that the HV ON/OFF switch is set to OFF.
2. On the FMO, ensure that the DC supply voltages, as read on the DC SUPPLY VOLTAGE meter, are correct.
3. Set the TUNING meter selector S1401 to OSC and adjust L1 502 (high band) or L1513 (low band) for maximum TUNING meter reading.
4. Set S1401 to 1ST DOUBLER and adjust Ll 503 (high band) or L1514 (low band) for maximum meter reading.
5. Set S1401 to 2ND DOUBLER and adjust L1509 (high band) or L1519 (low band) for maximum reading.
6. Set S1401 to 3RD DOUBLER and adjust C1519 and C1522 (high band) or C1536 and C1537 (low band) for maximum meter reading.
7. Release the four securing bolts and draw the unit fully forward. Remove the perforated cover from the RF subchassis and manually override the interlock.

\section*{8. Set the Radio Receiver METER SELECTOR} switch to the CR201 position. Release the locking screw and adjust the tripler cavity tuning screw Z1501 (high band) or Z1504 (low band) for a maximum indication on the TEST METER.
9. Release the locking screw and adjust the local oscillator output jack J1502 (high band) or J1505 (low band) on the side of the tripler cavity untill the TEST METER indication is below mid-scale. To reduce the reading, move the jack assembly away from the cavity.
10. Repeat 8 and 9 until the TEST METER indicates a maximum reading below mid-scale. The meter should indicate between 0.6 and 1.0 mA .
11. Set the METER SELECTOR switch to CR202 and observe that the TEST METER indicates between 0.6 and 1.0 mA . If necessary, re-adjust the local oscillator output jack to meet this condition.
12. Set S1401 to AMPL. Release the locking screw and adjust Z1502 (high band) or Z1505 (low band) for a maximum indication on the TUNING meter.
13. Observe the indication on the Receiver TEST METER. If the deflection exceeds mid-scale, repeat \(\underline{9}, \underline{10}\), 11 and 12 .
14. Set S1401 to KLYSTRON INPUT INCIDENT. Release the locking screw and adjust Z1503 (high band) or Z1506 (low band) for a maximum indication on the TUNING meter.
15. Connect the Oscilloscope to the KLYSTRON INPUT INCIDENT jack and terminate the connecting lead at the oscilloscope with termination MX-554/U. Repeat 12,13 and 14 to obtain a maximum pulse amplitude on the oscilloscope. The pulse shape should be as shown in Figure 6-9b. Re-tighten all cavity locking screws and replace the perforated cover on the RF sub-chassis. Close the sub-chassis front-access plate. Measure the power output of the FMO as described in paragraph 3-6a(12(p).


Figure 6-9b
(b) Shaped pulse adjustment. - Connect the oscilloscope vertical input (Ch1 or CH2) to Pin 5 of V1404 on the video chassis.
1. Set the oscilloscope controls to observe the waveshape shown in Figure 6-9c.
2. Adjust R1466 on the video chassis to obtain a pulse width of \(2.6 \mu \mathrm{sec}\) at the half-amplitude point.


Figure 6-9c
3. Connect the oscilloscope vertical input to the centre-tapping of the potentiometer R1470 and set the oscilloscope controls to observe the waveform shown in Figure 6-9d. Ad/ust R1417 to eliminate refiections and obtain the waveshape shown in Figure 6-9e. Disconnect the oscilloscope.


Figure 6-9d


Figure 6-9e
Note
When adjustment has been made to the pulse shape, it is necessary to tune the transmitter circuits as described in paragraphs \(6-2 \underline{h}(10)(\underline{b}) \underline{1}\) to 23 inclusive.
(c) Gate Pulse Adjustment. - Connect the oscilloscope vertical input to Pin 11 on tag board TB1497 and set the controls to observe the waveshape shown in Figure 6-9f.


Figure 6-9f
Adjust R1465 to obtain a pulse width of 10 usec at the half-amplitude point. Disconnect the oscilloscope, return the unit to the rack and tighten the securing bolts.
(9) IDENTIFICATION TONE KEYER ADJUSTMENTS.For information about these adjustments, refer to paragraph 6-2e(3) and (4).
(10) ADJUSTMENT OF TRANSMITTER CIRCUITS.
(a) Amplifier Modulator Bias Adjustment.
1. Set the following switches to OFF:
a. The HV ON/OFF switch on the High Voltage Power Supply Unit.
b. The MV ON/OFF switch on the Medium Voltage Power Supply Unit.
c. The LV ON/OFF switch on the Low Voltage Power Supply Unit.
d. The ON/OFF switch on The Coder Indicator Unit.
2. Release the securing bolts on the Amplifier Modulator and draw the unit forward until the AIR SW OPEN lamp is lit. Open the klystron access panel and the hinged cathode shield.

\section*{WARNING}

The Amplifier Modulator employs lethal voltages. Before proceeding, discharge all high voltage points, including the bias channel, with the Brinkley earthing stick.
3. Set the multimeter to the DC 300 V range and connect the positive lead to the klystroncathode terminal (marked HK). Connect the negative lead to the grid terminal. Push the Amplifier Modulator into the rack until the AIR SW OPEN lamp is extinguished and observe the indication on the meter. The multimeter should indicate 125 V .
4. Adjust the bias voltage as follows:-
a. Withdraw the Amplifier Modulator fully forward.
b. Make a small adjustment of R1382 on the bias chassis.
c. Push the unit into the rack until the AIR SW OPEN lamp is extinguished.
d. Observe the multimeter indication.
e. Repeat sub-clauses a. to \(d\) inclusive, until the meter indicates 125 V .
5. Withdraw the unit until the AIR SW OPEN lamp is lit and disconnect the multimeter. Close the klystron cathode shield and front access panel. Tighten the securing screws.
6. Return the unit to the rack and tighten the securing bolts. Set the switches listed in paragraph \(\frac{1}{1}\) to ON , in the reverse order to switching off.

\section*{(b) Transmitter Tuning}

\section*{Notes}
1. The Frequency Multiplier Oscillator RF subchassis is assumed to be set up and the klystron bias voltage to be correct.
2. If the klystron is new or has been out of service for longer than three months, it must be aged as detailed in paragraph \(6-2 \mathrm{~h}(10)\) (c) 1 to 13 , inclusive, before proceeding.
3. The klystron cavity-ring spacings should be set for the correct operating frequency as shown in the chart supplied with each klystron.
4. The filter cavities in the Control Duplexer should be set for the correct frequency as shown in the table supplied with the installation.
1. Ensure that the HV ON/OFF switch on the High Voltage Power Supply is set to OFF.
2. Disconnect plug P907 from the rear of the Coder Indicator chassis.
3. Release the securing bolts on the Frequency Multiplier Oscillator and draw the unit fully forward. Manually override the interlock. Turn potentiometers R1470 and R1471, located on the video chassis, fully anti-clockwise.
4.a. Set the multimeter to the DC 10 V range. On the Frequency Multiplier Oscillator, connect the multimeter beween J 1405 (front panel) and JI 403 (rear of chassis).
b. Adjust R1420 on the video chassis for an indicaion of 8 V on the meter.
c. Disconnect the meter.
d. On the Coder Indicator, reconnect plug P907 to he rear of the chassis.
5.a. Release the securing bolts on the Control Duplexer ind draw the unit fully forward. Manually override the interock.
b. Set the Coder Indicator ON/OFF switch to ON.
c. Set the HV ON/OFF switch on the High Voltage 'ower Supply Unit, to ON.
d. Adjust R1470 on the Frequency Multiplier OscillItor clockwise until the Amplifier Modulator BEAM CURRENT meter indicates 30 mA .
e. Set the HV ON/OFF switch to OFF.
6.a. Connect the Oscilloscope CH1 vertical INPUT to he SHAPAPED PULSE jack on the Frequency Multiplier Oscillator. Terminate the connecting lead, at the oscilloscope, with lermination MX-554/U.
b. Connect the oscilloscope CH 2 vertical INPUT to the KLYSTRON INPUT INCIDENT jack.
c. Connect the A time base TRIG IN jack to the IEST OUTPUT socket on the Coder Indicator.
d. Set the oscilloscope MODE switch to CHOPPED. Using the A time base, set the oscilloscope controls to observe the waveshape shown in Figure 6.9 g .


Figure 6-9g
7. Open the RF sub-chassis access plate and adjust the tuning screw of Z1503 (high band) or Z1506 (low band) for maximum amplitude of the square pulse, while maintaining its symmetry around the shaped pulse.
8. Transfer the oscilloscope CH2 vertical INPUT to the KLYSTRON INPUT REFLECTED jack and observe the wave form shown in Figure 6-9h. Adjust the klystron input cavity for minimum amplitude of the square pulse while maintaining its symmetry around the shaped pulse.


Figure 6-9h
9. Repeat 7 and 8 until there is no further improvement and the best possible symmetry of pulses around the shaped pulse is obtained. Disconnect the oscilloscope.
10. Set the HV ON/OFF switch to ON.

\section*{Note}

In the following paragraphs, the oscilloscope vertical input is through the crystal detector and the lead is terminated at the oscilloscope with termination MX-554/U. Obtain trigger from the Coder Indicator TEST OUTPUT jack.
11. Connect the oscilloscope to the klystron centre cavity jack. Adjust the centre cavity for maximum pulse amplitude without flattening or loss of symmetry.
12. Connect the oscilloscope to the KLYSTRON OUTPUT INCIDENT jack on the Control Duplexer. Adjust the klystron output cavity and the double-slug tuner for maximum pulse amplitude without flattening or loss of symmetry.
13. Connect the oscilloscope to the KLYSTRON OUTPUT REFLECTED jack. On the Control Duplexer, adjust the front filter cavity for minimum pulse amplitude. Adjust the rear cavity for minimum pulse amplitude.
14. Connect the oscilloscope to the KLYSTRON OUTPUT INCIDENT jack.

\section*{CAUTION}

When adjusting R1470, observe the BEAM CURRENT meter on the Amplifier Modulator to ensure that the current does not exceed 10 mA .
15. Adjust R1470 for maximum pulse amplitude without limiting.
16.a. Detune the klystron centre cavity towards the high frequency side until the pulse amplitude is halved.
b. Alternately, adjust the klystron input cavity and the Frequency Multiplier Oscillator output cavity Z1503 (high band) or Z1 506 (low band) for maximum pulse amplitude.
17. Alternately adjust the klystron output cavity and the double-slug tuner for maximum pulse amplitude without flattening or loss of symmetry. Adjust the klystron centre cavity for maximum pulse amplitude without flattening or loss of symmetry.
18. Repeat paragraphs 16 and 17 until a maximum pulse amplitude is obtained, while maintaining a good pulse shape.

\section*{CAUTION}

The klystron output cavity must not be adjusted during the remainder of the tuning procedure.
19. Connect the oscilloscope to the ANTENNA INCIDENT jack on the Control Duplexer. Make the following adjustments for maximum amplitude without limiting and for the best pulse shape:-
a. Front and rear filter cavities.
b. Double-slug tuner.
c. Klystron input and centre cavities.

\section*{Note}

Slight adjustment of R1470 in the Frequency Multiplier Oscillator may also improve the shape.
20. Set the oscilloscope sweep to onserve a reference burst and adjust R1471 in the Frequency Multiplier Oscillator to eliminate droop or boost in the burst. See Figures 6-9j, 6.9 k and 6.9 l .


Pulse Boost
Figure 6-9j


Pulse Droop
Figure 6-9k


\section*{Pulse Correct}

Figure 6.9L

\section*{Note}

Interaction occurs between the adjustment of R1470 and R1471. If R1471 is adjusted, set the oscilloscope to obtain one pulse of the burst and adjust R 1470 for maximum pulse amplitude without limiting and whilst preserving a good pulse shape. The Amplifier Modulator BEAM CURRENT meter should indicate between 90 and 110 mA .
21. On the Control Duplexer, adjust the three micrometer cavity tuning heads for correct frequency as shown in TABLE 205, of Section 2.
22. Disconnect the oscilloscope and return all units to normal operation.
23.a. Measure the beacon output power as described in paragraph 2-6a(12)(n).
b. Perform a spectrum analysis as described in paragraph 3-6a(12)(m).
(c) Klystron Aging.

\section*{Notes}
1. The Frequency Multiplier Oscillator (FMO) is assumed to be correctly set up.
2. The klystron bias voltage is assumed to be correct.
1. Set the following switches to OFF:
a. The Coder Indicator ON/OFF switch.
b. The HV ON/OFF switch on the High Voltage Power Supply Unit.
c. The MASTER SWITCH on the Control Duplexer.
2. Release the securing bolts on the FMO and draw the unit fully forward. Manually override the interlock and set R1470 fully anti-clockwise.
3.a. On the Amplifier Modulator, open the klystron access door and disconnect the RF input cable from the klystron.
b. Remove the front panel from the Power Supply Cabinet transformer and blower compartment and set the BREAK IN/OPERATE switch to BREAK IN. Manually override the interlock.

\section*{4.a. Set the MASTER SWITCII to ON.}
b. When the MASTER SWITCH has been on for fifteen minutes, set the HV ON/OFF switch to ON. Allow a furthei fifteen minutes warming up time.
5. Set the Coder Indicator ON/OFF switch to ON and adjust R 1470 on the FMO for an indication of 10 mA on the BEAM CURRENT meter. Allow fifteen minutes to elapse before proceeding.
6. Observe the BEAM CURRENT meter and adjust R1470 to increase the indication by 10 mA every five minutes until the meter indicates 50 mA .
7. Set the MASTER SWITCH to OFF and the BREAK IN/OPERATE switch to OPERATE. Replace the blower compartment front panel.
8. Set the MASTER SWITCH to ON and adjust \(\mathrm{R} \overline{1} 470\) for a meter indication of 60 mA .
9. Observe the meter and adjust R1470 to increase the indication by 10 mA every five minutes until the meter indicates 90 mA . Allow five minutes to elapse before proceeding.
10. Set the HV ON/OFF switch and MASTER SWITCH to OFF.
11.a. Discharge all high voltage points in the Amplifier Modulator.
b. Reconnect the RF input cable to the klystron and close the access door.
12. Return the FMO to the rack and tighten the securing bolts. The klystron is now fully aged.
13. Tune the klystron and transmitter circuits as described in paragraph 6-2h(10)(b) \(\underline{1}\) to 23 inclusive.
(d) High Voltage Overload Relay Adjustment.

\section*{WARN ING}

The High Voltage Power Supply employs lethal voltages. Before making any adjustments in the unit, discharge all high voltage points with the Brinkley earthing stick.
1. Release the securing bolts on the Receiver and draw the unit fully forward. Manually override the interlock.
2. Observe the Amplifie'r Modulator BEAM CURRENT meter and adjust R427 in the Receiver to increase the beam current until either:-
a. The high voltage overload relay trips, or
b. The BEAM CURRENT meter indicates 125 mA .

\section*{CAUTION}

Do not allow the beam currient to exceed 125 mA .
3. Set the HV ON/OFF switch on the High Voltage Power Supply Unit to OFF. Release the securing bolts and draw the unit fully forward.
4. Locate R1912 on the power supply chassis and make a slight adjustment to the control.
5. Return the unit to the rack and tighten the securing bolts. Set the HV ON/OFF switch to ON .
6. Repeat paragraphs 2-5 inclusive, until the high voltage overload relay trips when the BEAM CURRENT meter indicates 125 mA .
7. Measure the squitter rate as described in paragraph 3-6a(12)(a) of Section 3, and set R 427 on the Receiver for a squitter rate of 5400 pulses per second.
8.a. Ensure that the BEAM CURRENT meter indicates between 90 and 110 mA .
b. Return the Receiver to the rack and tighten the securing bolts.
(e) Antenna Control Cabinet (5825-99-9325319).

\section*{Note}

For other types of antenna control cabinet, refer to their respective manuals.
1. Open the Antenna Control Cabinet door and locate TEST SWITCH 3. Depress the switch and observe on meter panel YJ:-
a. The TIME DELAY lamp is lit.
b. The SPIN MOTOR lamp is lit.
2. With the switch on the antenna speed control unit (YR) in the MOTOR LINE CURRENT position, the meter should indicate between 1.5 and 2.0 amps .

\section*{Notes}
1. Approximately one minute after depressing TEST SWITCH 3, the SPEED CONTROL indicator on the meter panel (YJ) will light. Adjustments to the ADJUST RUN UP CURRENT control must be made during the time that the TIME DELAY and SPEED CONTROL lamps are lit together, as the control becomes in-effective after the TIME DELAY lamp is extinguished. If the TIME DELAY lamp extinguishes before the adjustment is complete, depress TEST SWITCH 3 to restart the time delay period.
2. The readings on the COUPLING CURRENT and PU COIL VOLTS meters will rise just before the TIME DELAY lamp extinguishes.
3. Set the meter switch on the Speed Control Unit (YR) to the MOTOR LINE CURRENT position and check that the meter indicates between 2.0 and 4.0 amps .
4. Set the meter switch to PU COIL VOLTS and turn the ADJUST RUN UP CURRENT control clockwise until an indication of 0.6 amps is obtained on the COUPLING CURRENT meter. Locate RV3, behind the cabinet door, and adjust it for an indication of 5 V on the PU COIL VOLTS meter.
5. Check that after the TIME DELAY lamp has been extinguished:-
a. The COUPLING CURRENT meter indi-
cates 0.5A.
b. The PU COIL VOLTS meter indicates
5.0V.
c. The meter on unit \(Y R\), when switched to the MOTOR LINE CURRENT position, indicates between 1.5 and 3.5 amps .
6. Close the Antenna Control Cabinet
door.

\section*{6-3. REMOVAL,ADJUSTMENT,REPAIR AND REASSEMBEY OF PARTS AND SUBASSEMBLIES.}

\section*{a. REMOVAL OF DRAWER UNITS FROM}

CABINET. - The component units of the receivertransmitter group and power supply assembly are mounted in rack frames mounted in cabinets. To facilitate servicing, component units containing the actual transmitting, receiving, coding, timing, test,
and power supply circuits are arranged into panel-and-chassis-type drawer units. Other components of these groups, such as filament supply and blower units, are fixed-type panel-and-chassis assemblies.

The drawer-type panel-and-chassis assemblies slide in and out of the cabinet on slide rails mounted on the rack frame. When fully inserted in the frame, the drawers are secured to the frame by means of captive screws. To open a drawer, release the captive screws and pull on the panel-mounted handles. Latches on the sides of the drawer units lock the drawer in place when partly extended for inspection, adjustment or servicing. Interunit cabling connections to the drawer units are made by means of either plug-in screw-type multiconnectors, or leads fitted with terminal lugs arranged for connection to screwtype terminal boards. No solder connections exist in the interunit cabling. The interunit cabling attached to the drawer units is retractable, and long enough to permit fully extending the unit for maintenance purposes. Opening the latches and disconnecting the interunit cabling permits completely removing the drawer unit from the rack frame.

\section*{b. ADJUSTMENT OF PARTS AND SUBASSEMBLIES.}
(1) MEDIUM VOLTAGE POWER SUPPLY PP-1765/URN OVERLOAD RELAY. - Medium-voltage power supply overload relay K1803 is adjusted, by means of potentiometer R1872 (figure 6-10), to trip and actuate the overload protection circuit when a sustained overload of 225 milliamperes or more occurs. Under this condition, the relay is set to trip in less than 1 minute. The normal, full-load current provided by the power supply is 175 milliamperes. If the relay trips under normal current conditions, proceed as follows:

\section*{WARNING}

This equipment employs high voltages that are dangerous and may be fatal if contacted by operating personnel. Extreme caution should be exercised when working on this equipment. Do not depend on interlock switches or high voltage shorting switches to remove dangerous voltages. Set the MV switch to OFF before opening the medium voltage drawer and short capacitor C1802 with a grounding rod before touching components.

Step 1. Pull out medium voltage power supply unit as described in paragraph 6-3a.

Step 2. Check power supply load current. Insert a 300-milliampere d-c full-scale milliammeter, Multimeter AN/PSM-4, or equivalent, in series with terminal 4 of transformer T1801 and the lead connected to it. Turn potentiometer R1872 clockwise until overload relay does not trip. If meter reads considerably more than 175 milliamperes, shut off equipment and check power supply and load circuit for cause of overload condition. If current reading is \(\mathbf{1 7 5}\) milliamperes or less, turn potentiometer R1872 to extreme clockwise position.

Step 3. Shut equipment off; use grounding rod to discharge capacitor C1802. Connect a 20,000 -ohm 50 -watt fixed resistor between terminal E1831 and ground (do not disconnect lead from E1831).

Step 4. Turn on equipment and adjust meter current to 225 milliamperes by adjusting potentiometer R1842 (1000-volt adjustment, figure 6-2).


Figure 6-10. Medium Voltage Power Supply PP-1765/URN, Right Side View

Step 5. Slowly turn potentiometer R1872 (overload adjustment) counterclockwise until overload relay trips at 225 milliamperes. Remove 20,000 -ohm resistor, and if necessary, recheck +1000 -volt output as outlined in paragraph 6-2c(2).
(2) HIGH VOLTAGE POWER SUPPLY PP-1763/URN OVERLOAD RELAY ADJUSTMENT.

\section*{WARNING}

This equipment employs high voltages that are dangerous and may be fatal if contacted by operating personnel. Extreme caution should be exercised when working on this equipment. Do not depend on interlock switches or high voltage shorting switches to remove dangerous voltages. Set the HV switch to OFF before opening the high voltage drawer and short capacitors C1901 and C1902 with a grounding rod before touching components.

High voltage power supply overload relay K1904 (figure 6-11) is set to trip at 125 milliamperes. Normal full-load current is approximately 90 milliamperes as observed on BEAM CURRENT meter M1301. If the output current is normal but the relay still trips, current relay K1904, or capacitor C1906, or resistor R1906, R1911, or R1912 is defective, and should be replaced. If any of these parts are replaced, readjust the overload relay by trial and error, turning potentiometer R1912 very slightly with the
power off. Replace the unit in the cabinet and observe whether the relay trips. (The relay should trip in less than 1 minute.)

The 125-milliampere overload current can be obtained by changing the squitter control voltage of the radio receiver to obtain a higher than normal pulse rate. To do this, pull the radio receiver and manually close interlock S905. Carefully turn resistor R427 (figure 6-3) clockwise until 125 milliamperes is obtained on meter M1301.
(3) RADIO RECEIVER SUBASSEMBLIES. - In addition to the built-in test equipment, special test equipment is required for the proper alignment of some of the circuits of the radio receiver. These circuits are the receiver preamplifier, i-f amplifier, and Ferris discriminator circuits. The circuits are prealigned at the factory, and normally require no further alignment or adjustment in the field. No attempt should be made, therefore, to tamper with these circuits, unless it has been definitely established that realignment is necessary. Furthermore, alignment should not be attempted without the proper test equipment. The alignment procedure described in the following subparagraphs may be performed only with the test equipment specified or their electrical equivalent.

\section*{(a) TEST EQUIPMENT REQUIRED.}
1. Signal Generator AN/USM-44A, or equivalent.


Figure 6-11. High Voltage Power Supply PP-1763/URN, Left Side View
2. High-frequency Vacuum Tube Voltmeter, Genēral Radio Model 1800A, or equivalent.
3. Frequency Meter TS-323/UR, or equivalent cāpable of measuring at 63.0 megacycles per second.
4. Vacuum Tube Voltmeter, AN/USM-116, or equivalent.
5. Crystal detector, arranged as shown in figure 6-12.
6. Multimeter AN/PSM-4, or equivalent.
7. Components shown in test setup of
(b) PREAMPLIFIER ALIGNMENT (CONTINŪOUS WAVE METHOD). - Before proceeding with the alignment, make the filament and plate voltage measurements listed in table 6-1. With no signal input to the radio receiver, the voltages, measured from the points indicated to ground, should be as shown in the table.

\section*{1. ALIGNMENT PROCEDURE.}

Step 1. Pull out radio receiver unit as described in paragraph 6-3a. Remove crystal mixers CR201 and CR202.

Step 2. Connect equipment as shown in figure 6-13.


Figure 6-12. Crystal Detector for Use in Preamplifier \({ }^{\text {a }}\) lignment

TABLE 6-1. PREAMPLIFIER ALIGNMENT VOLTAGE CHART
\begin{tabular}{|l|c|}
\hline \multicolumn{1}{|c|}{ CHECK POINT } & REQUIRED INDICATION \\
\hline C223 & \(150 \pm 5\) volts dc \\
Pin 3 at V201 & \(6.3 \pm 0.3\) volts dc \\
Pin 4 at V202 & \(6.3 \pm 0.3\) volts dc \\
Pin 3 at V203 & \(6.3 \pm 0.3\) volts dc \\
Pins 6 and 5 V 201 & \(110 \pm 10\) volts dc \\
Pin 7 at V202 and & \(120 \pm 10\) volts dc \\
at C216 & \(120 \pm 10\) volts dc \\
Pins 5 and 6 at V203 & \(1.0 \pm 0.3\) volts dc \\
Pins 2 and 7 at V201 & \(1.2 \pm 0.3\) volts dc \\
Pin 2 at V202 & \(2.0 \pm 0.4\) volts dc \\
Pins 2 and 7 at V203 & \\
\hline
\end{tabular}

\section*{Nofe}

If the voltages obtained are within tolerances, the alignment may then be started. If they are not, refer to troubleshooting procedure for circuit involved.

Step 3. Set signal generator to \(63 \pm 0.1\) megacycle.

Step 4. Apply plate and filament power. Allow 5 -minute warmup time.

Step 5. Increase signal generator output level to a value that will cause approximately 0.3 volt rms to be indicated in output voltmeter.

Step 6. Adjust coils L206, L209, L210, and L211 on preamplifier chassis for maximum output on output meter. If output voltage increases beyond 0.4 volt, lower input signal level to effect 0.4 volt or less, and readjust inductances listed above for maximum output on meter.

Step 7. Repeat adjustments of step 6. Note that coil L206 is a low \(Q\) circuit and must be adjusted slowly while the output meter is carefully observed for a maximum indication.

Step 8. Set signal generator on 63 megacycles with full output, and temporarily connect a \(60 \pm 5\) micromicrofarad capacitor that is physically small (Elmenco or equivalent) from pin 7 of tube V202 to tube socket XV202, center shield and carefully adjust coil L210 for maximum output. Adjust coil L211 carefully for maximum output; however, do not allow output voltage to exceed 0.4 volt (lower input signal as required). Make these adjustments with tube shield securely in place.


Figure 6-13. Test Circuit for Alignment Preamplifier

Step 9. Remove 60-micromicrofarad capacitor from pin 7 of tube V202 and connect 75 -micromicrofarad capacitor to pin 1 of tube V203; use tube socket XV202 center shield, and carefully adjust coil L209 for maximum output. Check that signal generator is still at 63 megacycles. Make this adjustment with tube shield securely in place. Remove capacitor from pin 1 of tube V203 when adjustment is completed.

Step 10. Repeat steps 8 and 9 , then fasten preamplifier shield securely, with captive screws, to preamplifier.

Step 11. Tune signal generator from low frequency ( 61 megacycles) to high frequency of passband (about 65 megacycles). The response should not vary from a nominal output voltage of 0.40 volt rms by more than \(\pm 0.60\) volt from about 6.10 to 65 megacycles. If this condition does not exist, proceed to steps 12 and 13.

Step 12. If passband slopes upward (output increases as frequency increases, with input constant), tune slug of coil L211 clockwise (increasing inductance) very slightly (about one-half turn at a time) to flatten response to specifications in step 11. Do not tune any other adjustment to accomplish this result. Repeat this adjustment and measure flatness indicated in step 11 until passband has slope of 1 db or less. Do not allow output to exceed 0.4 volt rms for this test. If amplitude decreases markedly when tuning coil L211, tuning is probably being staggered; avoid this condition.

Step 13. If passband slopes downward (output decreases as frequency increases, with input constant), tune slug of coil L211 counterclockwise (decreasing inductance) very slightly (about one-half turn at a time) to flatten response to specifications of step 11. Do not tune any other adjustment to accomplish this result. Repeat this adjustment and measure passband flatness as indicated in step 11 until passband has slope of 1 db or less. Do not allow output to exceed 0.4 volt rms for this test. If amplitude decreases markedly when tuning coil L211, tuning is probably being staggered; avoid this condition.

\section*{2. PREAMPLIFIER CHARACTERISTICS} AFTER CON̄TINUOUS WAVE ALIGNMENT. - An input of 20,000 to 40,000 microvolts (continuous wave) single phase is sufficient to yield an output of 0.4 volt across a 50 -ohm load at 63 megacycles. The bandwidth at half-power points should be between 5.5 to 7 megacycles; at 26 db down, the width should be 18 to 21 megacycles. The response should be flat from 61 to 65 megacycles to within 1 db . At 63 megacycles (within passband) the output should be linear within 2 db to at least 2 volts rms output into 50 ohms as measured with the high-frequency vacuum tube voltmeter. The preamplifier response should be centered about \(63 \pm 0.5\) megacycles. Symmetry should be measured from the half-power points for this width measurement.
(c) I-F AMPLIFIER ALIGNMENT. -Before
proceeding with the alignment make the voltage measurements listed in table 6-2. With no signal input to the radio receiver, the voltages, measured from the points indicated to ground, should be as shown in table 6-2. Also check all i-f amplifier tubes and filament and plate supply voltages.

Step 1. Connect signal generator as shown in figure 6-13. Remove tee UG-274/U and connect cable RG-58/U from jack J203 on preamplifier to plug P303 on i-f amplifier.

Step 2. Set signal generator to \(63 \pm 0.1\) megacycles.

Step 3. Apply filament and plate power and variable negative bias supply to squitter control of i-f amplifier. Adjust this bias to -5.0 volts dc.

Step 4. Connect Voltmeter AN/PSM-4 from test point TP2 to ground. Also connect 1000 -micromicrofarad capacitor from test point TP2 to ground.

\section*{Note}

All shields must be fastened securely in place.

Step 5. Increase signal generator output to level that will effect approximately 0.5 -volt d-c output on Voltmeter AN/PSM-4.

Step 6. Adjust core of coils L302, L303, L304, L305, L306, and L308 on i-f chassis for maximum indication on output voltmeter. If output voltage increases beyond 1 volt at any time during alignment, reduce input signal level to effect 1 volt or less and readjust above inductances for maximum output on output vacuum tube voltmeter.

Step 7. Repeat adjustments in step 6. Note that coil L302 is a medium Q circuit and must be adjusted slowly while output meter is carefully observed for maximum indication.

Step 8. Set signal generator on 60.7 megacycles and adjust coil L303 for maximum output at this frequency. Do not allow output voltage to exceed 1 volt dc during alignment. Adjust generator output attenuator to keep output below 1 volt.

\section*{Nofe}

Make sure squitter bias is set at -5.0 volts for adjustments described in steps 8 through 10.

Step 9. Set signal generator on 65.4 megacycles and adjust coil L304 for maximum output at this frequency. Do not allow output voltage of test point TP2 to exceed 1 volt de during alignment.

Step 10. Set signal generator on 63 megacycles and adjust coils L302, L3C5, L306, and L308 (see step 6

TABLE 6-2. RADIO RECEIVER, I-F AMPLIFIER VOLTAGE CHART
\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multirow[b]{2}{*}{TYPE NO.} & \multirow[b]{2}{*}{TUBE TYPE} & \multicolumn{9}{|c|}{SOCKET PIN NUMBER*} \\
\hline & & 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 \\
\hline V301 & 5654/6AK5W & 0 & 2.2 & 6.3 ac & 0 & 125 & 125 & 2.2 & - & - \\
\hline V302 & 5654/6AK5W & 0 & 2.3 & 6.3 ac & 0 & 130 & 131 & 2.3 & - & - \\
\hline V303 & 5654/6AK5W & 0 & 2.3 & 6.3 ac & 0 & 130 & 134 & 2.3 & - & - \\
\hline V304 & 5654/6AK5W & 0 & 2.5 & 6.3 ac & 0 & 115 & 129 & 2.5 & - & - - \\
\hline V305 & 5654/6AK5W & 0 & 2.4 & 6.3 ac & 0 & 100 & 129 & 2.4 & - & - \\
\hline \multicolumn{11}{|c|}{CAUTION} \\
\hline \multicolumn{11}{|l|}{Make these measurements with jack J303 disconnected and jack J301 shorted to ground. Keep small shield over tubes V306 and V307 while making measurements; otherwise i-f amplifier will feed back and cause erroneous results.} \\
\hline V306 & 5726/6AL5W & 0.15 & 0 & 6.3 ac & 0 & 0.15 & 0 & 0 & - & - \\
\hline V307 & 12AT7WA & 140 & 0. 2 & 1.75 & 0 & 0 & 150 & -. 15 & 2.8 & 6.3 ac \\
\hline \multicolumn{11}{|c|}{Note} \\
\hline \multicolumn{11}{|l|}{Keep large shield over tubes V301, V302, V303, V304 and V305 while making measurements on these circuits; otherwise i-f amplifier will feed back.} \\
\hline
\end{tabular}
*All measurements made between ground and point indicated.
All d-c measurements made with \(20,000-\mathrm{ohm} /\) voltmeter.
All a-c measurements made with \(1000-\mathrm{ohm} /\) voltmeter.
and 7) for maximum output at this frequency. Do not allow output voltage to exceed 1 volt dc during alignment.

Step 11. Repeat steps 8, 9, and 10. This completes i-f alignment up to Ferris discriminator.
(d) FERRIS DISCRIMINATOR ALIGNMENT.Connect the test equipment as instructed in 6-3b(3)(c) for alignment of the i-f amplifier.

\section*{1. ALIGNMENT PROCEDURE.}

Step 1. Set signal generator to 63 megacycles; check this frequency with frequency meter. Set squitter bias at -5.0 volts.

Step 2. Remove Voltmeter AN/PSM-4 from test point TP2 and remove 1000-micromicrofarad capacitor from test point TP2 at same time.

Step 3. Connect Voltmeter AN/PSM-4 to test point TP3; connect meter to read negative voltage with respect to ground. (Use 1000-micromicrofarad capacitor from test point TP3 to ground.)

Step 4. Adjust coil L309 until reading on Voltmeter AN/PSM-4 at test point TP3 reads maximum negative. Generator must be set to 63 megacycles. Never allow this voltage to exceed -0.8 volt during alignment. If voltage exceeds this specified amount,
reduce output of signal generator to lower output to desired amount, then adjust coil L309 for maximum output.

Step 5. Tune generator from 63 megacycles to low frequency side. Observe that output at test point TP3 will fall from negative to zero volts and then reverse polarity as frequency is lowered. Keep tuning and observe maximum positive output on low frequency side. Do not allow voltage out of discriminator to exceed 1 volt on positive side during tests. Reduce generator input to effect this condition, if necessary. Keep generator output at this value for step 6, and record positive amplitude observed.

Step 6. Maintaining constant output from generator, tune signal generator toward high frequency side. Polarity will become negative before 63 megacycles and then reverse polarity again somewhere beyond 63 megacycles. With same signal generator input as in step 5 , record maximum positive voltage output on high frequency side of discriminator.

Step 7. Compare amplitudes of voltage peaks measured in step 5 and 6. Amplitudes should be within 5 percent at a nominal level of 1.0 volt. If they are not within this tolerance, check whether high frequency or low frequency side is lower. If low frequency positive peak is too low, turn coil L308 clockwise slightly; this will increase amplitude of positive low frequency side of the discriminator. If
low frequency positive peak is too large, turn coil L308 counterclockwise for correction.

Step 8. Repeat step 4.
Step 9. Tune signal generator through discriminator characteristic and observe heights of positive maxima of discriminator. If heights are not yet within 5 percent of each other at a level of \(\pm 1.0\) volt dc, repeat steps 7 and 8, and recheck until desired characteristic is obtained.

Step 10. Set signal generator to 63 megacycles with frequency meter and check step 4. This completes tuning of i-f amplifier and Ferris discriminator.

Step 11. Replace crystal mixers CR201 and CR202 and restore equipment to original condition.

\section*{2. CHARACTERISTICS OF I-F}

AMPLIFIER INCLUDING FERRIS DISCRIMINATOR.The response of the i-f amplifier at test point TP2 should approximate that of the response shown in figure 6-14. The crossover points of the negative lobe (high and low frequency points that pass through zero voltage), measured with the frequency meter,
should be symmetrically placed about \(63 \pm 0.001\) megacycles. If this is not so, readjust coil L 309 , using extreme care; remeasure the crossover frequencies with the frequency meter. Note that 180degree rotation of the slug on coil L309 will shift the center frequency of the negative lobe approximately 1 megacycle.

\section*{c. REASSEMBLY OF DRAWER UNITS. -The} reassembly of the equipment comprising the receiver-transmitter group and the power supply assembly is accomplished in the reverse order of the disassembly procedure given in paragraph 6-3a.

\section*{6-4. ILLUSTRATIONS.}
a. SCHEMATIC DIAGRAMS. - Figures 6-15 through 6-28 are the schematic diagrams for Radio Set AN/GRN-9D.
b. WIRING DIAGRAMS. -Figures 6-29 through 6-49 are the wiring diagrams for all the units of the radio set.
c. PARTS LOCATION. - Figures 6-1 through 6-7, 6-9 through 6-11, and 6-50 through 6-68 show the location of parts in the radio set.


Figure 6-14. Receiver Response Characteristics




 of Table 5.1, the mains
and 166 are not susd.





Figure 6-16. Control Duplexer C-2226A/GRN-9,


Figure 6-16a. Control Duplexer C-2226A/GRN-9. Schematic Diagram
(Replacement Test Equipment. Table 5-la)


Figure 6-17. Radio Receiver R-824/URN.
Schematic Diagram (Sheet lof 2)

Figure 6-17 (Table)
\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline REF DESIG & LOCATION & RE F DESIG & LOCATION & REF DESIG & LOCATION & REF DESIG & LOCATION & REF DESTG & LOCATION & REF DESIG & LOCATION \\
\hline C201 & 4 B & C345 & 28B & J201 & 3C & P303(J203) & 13C & R411 & 32D & S502 & 18E \\
\hline C202 & 4C & C346 & 10G & J202 & 3 C & P304 & 10G & R412 & 32B & T201 & 5B \\
\hline C203 & 5B & C347 & 9G & J203(P303) & 11B & P401 & 28 n & R413 & 32C & T401 & 32G \\
\hline \multirow[t]{2}{*}{\[
\begin{aligned}
& \text { C204 thru } \\
& \text { C206 }
\end{aligned}
\]} & \multirow[t]{2}{*}{5C} & C348 & 8F & J204(P204) & 13D & \multirow[t]{2}{*}{P403
P404} & 35 C & R414 & 32 C & T501 & 21E \\
\hline & & \multirow[t]{2}{*}{C349
C350} & \multirow[t]{2}{*}{7 F
5 F} & \multirow[t]{2}{*}{\[
\begin{aligned}
& \mathrm{J} 301 \\
& \mathrm{~J} 304
\end{aligned}
\]} & \multirow[t]{2}{*}{28D} & & \multirow[t]{2}{*}{35 C} & \multirow[t]{2}{*}{R415
R416} & \multirow[t]{2}{*}{33C} & \multirow[t]{2}{*}{T502} & \multirow[t]{2}{*}{21F} \\
\hline C208 & 3B & & & & & P404
P405 & & & & & \\
\hline C209 & 3B
3 D & C351 & 4 F & J305 & 210 & P406 & 30 D & R417 & 33B & TP1 & 21D \\
\hline C210 & 6B & \multirow[t]{2}{*}{C352} & 3F & J306 & 24 C & P407 & 35B & R418 & 33 D & TP2 & \multirow[t]{2}{*}{24C} \\
\hline C211 & 7 C & & \multirow[t]{2}{*}{20C} & \multirow[t]{2}{*}{J307
J492} & \multirow[t]{2}{*}{\(25 B\)
28 C} & \multirow[t]{2}{*}{P508
R201} & 2C & \multirow[t]{2}{*}{R419
R420} & \multirow[t]{2}{*}{33 D
34 B} & \multirow[t]{2}{*}{TP3} & \\
\hline C212 & 6 D & C354 & & & & & 4 B & & & & 25B \\
\hline C213 & 7C & C355 & 15B & J403 & 35C & R202 & 4C & R421 & 34D & TP5 & 28B \\
\hline C214 & 7B & C356 & \multirow[t]{2}{*}{17B} & J404 & 35C & \multirow[t]{2}{*}{R 205
R 29} & 6B & R422 & 34 D & TP6 & \multirow[t]{2}{*}{35C} \\
\hline C215 & 7 D & C357 & & J405 & 27 G & & 6B & R423 & 34 D & TP7 & \\
\hline C216 & 8 C & C358 & 20B & J406 & 390 & R 207 & 9 C & R424 & 35D & TP8 & 34B \\
\hline C217 & 8B & C359 & \multirow[t]{2}{*}{22B} & J407 & 35 B & R208 & \(\bigcirc \mathrm{C}\) & \multirow[t]{2}{*}{R425} & 29 D & TP9 & 29 C \\
\hline C218 & 10 C & C369 & & \multirow[t]{2}{*}{\begin{tabular}{l} 
J408 \\
\\
\hline 409
\end{tabular}} & 2811 & \multirow[t]{2}{*}{R 212
R 213} & \multirow[t]{2}{*}{80
100} & & \multirow[t]{2}{*}{34 G
32 H} & \multirow[t]{2}{*}{V201} & \multirow[t]{2}{*}{6 C
8 C} \\
\hline C219 & 8 V & C361 & 28 C
27 C & & \multirow[t]{2}{*}{288
\(35 C\)} & & & R426
R427 & & & \\
\hline C220 & 10 C & C362 & 26 I & 1410 & & \[
\begin{aligned}
& 1213 \\
& R 214
\end{aligned}
\] & 7 C & R429 & 32G & V203 & 9 C \\
\hline C221 & 10 C & C363 & \multirow[t]{2}{*}{25 D
29 C} & \multirow[t]{2}{*}{J411
J412} & 35B & R3n1 & 14 C & R430 & \multirow[t]{2}{*}{33 G
32 H} & V321 & \multirow[t]{2}{*}{14C} \\
\hline C222 & 11 C & C401 & & & 34B & R3n2 & 14D & \multirow[t]{2}{*}{R431
R432} & & \multirow[t]{2}{*}{V302} & \\
\hline C223 & 9 O & C 402 & 30 C & J413 & \multirow[t]{2}{*}{29
20} & \multirow[t]{2}{*}{R304
R305} & 150 & & 32 H
31 G & & 16 C
18 C \\
\hline C224 & 9 E & C 403 & \multirow[t]{2}{*}{31 C
32 C} & J5?1 & & & 15 C & \[
\begin{aligned}
& \mathrm{R} 432 \\
& \mathrm{R} 433
\end{aligned}
\] & 32G & \[
\begin{aligned}
& \text { V303 } \\
& \text { V304 }
\end{aligned}
\] & 19 C \\
\hline C225 & 4 B & \(\mathrm{C} 4 \mathrm{CH}_{4}\) & & J502 & \multirow[t]{2}{*}{3 E
35 C} & R306 & 14 B & \multirow[t]{2}{*}{R434} & \multirow[t]{2}{*}{\(28 \%\)
290} & V305 & \multirow[t]{2}{*}{21C
24B. 24 D} \\
\hline C226 & 4 C & C195A & 32 D & T503 & & \multirow[t]{2}{*}{R307
R30\%} & 14B & & & \multirow[t]{2}{*}{V306} & \\
\hline C227 & 10 D & C405B & 31 B & J594 & 35 C & & 16 B & R436
R437 & \[
29 \mathrm{G}
\] & & \[
\begin{aligned}
& 24 \text { B. } 24 \mathrm{D} \\
& 26 \text { B. } 27 \mathrm{~B}
\end{aligned}
\] \\
\hline C228 & 10 E & C495C & 33 r & J505 & 17E & R309 & 16B & R438 & 30 F & V308 & 26D 27D \\
\hline C229 & 5B & C+06 & 33 C & J 506 & 31D & R310 & 16 C & R439 & 29 T & V401 & 30 C \\
\hline C301 & 13 C & C407 & 33C & J507 & 35B & R312 & 18 C & R440 & 29 F & V402-1 & 29 C \\
\hline C302 & \(1 \div \mathrm{D}\) & C408 & 34 C & J508 & 2 C & R31: & 18B & R441 & 29 G & V402-2 & 31C \\
\hline C303 & 27E & C 409 & 345) & L201 & 4 B & R314 & 18B & R442 & 28G & V403 & 32 C \\
\hline C304 & 13 C & C 110 & 33H & L. 202 & 4 C & R315 & 19D & R443 & 28G & V404 & 33 C \\
\hline C305 & 15 C & CH11 & 35C & L203 & 5B & R316 & 19C & R444 & 30 C & V405 & 34 C \\
\hline C306 & 16D & C412 & 35 C & L204 & 5D & R317 & 19 B & R445 & \(30 \cdot\) & V406 & 29G \\
\hline C 307 & 17 C & C414 & 31 r & L205 & 6 B & R318 & 19 B & R447 & 32II & V407-1 & 33G \\
\hline C308 & 16 D & C415 & 32 G & L206 & 7 C & R319 & 20 D & R446 & 30G & V407-2 & 30G \\
\hline C309 & 15 C & C416 & 31 F & L207 & 7 D & R320 & 211) & R448 & 34 B & V408 & 31G \\
\hline C310 & 15 C & C. 417 & 28 E & L209 & 71) & R321 & 21 C & R44? & 34 B & V409A & 34G \\
\hline C312 & 153 & C+18 & 29 S & L, 200 & 8B & R322 & 21B & R450 & 33 C & V409B & 33G \\
\hline C313 & 163 & C419 & 285 & L210 & 9 B & R325 & 25 C & R451 & 29 G & V501 & 21F \\
\hline C315 & 17 C & C420 & 29 C & L211 & 10 B & R326 & 25 C & R452 & 30D & V502 & 21H \\
\hline C316 & 17 C & C121 & 29 F & L21? & 8 C & R327 & 25B & R453 & 35B & V503 & 24 E \\
\hline C318 & \(181)\) & C427 & 32 B & L213 & 10 C & R329 & 26 B & R454 & 34 B & V504 & 25 F \\
\hline C319 & 18 C & \(\mathrm{C}+8\) & 30 C & L217 & 4 B & R32n & 260 & R455 & 29 D & V505 & 26 H \\
\hline C329 & 18 n & C501 & 23 E & L218 & 4 C & R330 & 24 C & R456 & 310 & V506 & 2411 \\
\hline C321 & 19 C & C 52 & 25 E & L21: & 53 & 18331 & 27 C & R457 & 310 & XV501A & 18E \\
\hline C323 & 18 C & CHCO & 25 C & L220 & in & P 332 & 27 C & R458 & 33B & XF501B & 18G \\
\hline C324 & 20 B & (504 & 220 & L301 & 14C & R334 & 14 C & R459 & 33 C & XF503 & 18G \\
\hline C326 & 20 C & (505 & 226 & L,302 & 14 C & R335 & 16 C & R501 & 24 E & Z201 & 9 E \\
\hline C327 & 20 C & (506 & 23F & L. 303 & 15 C & 183336 & 17 C & R502 & 24 F & Z202 & 8E \\
\hline C328 & 20 n & (12201 & 313 & L304 & 17 C & R337 & 19 C & R503 & 24 E & Z203 & 6 E \\
\hline C32) & 21 C & Chi401 & 291) & L. 305 & 19 C & R338 & 20 C & R504 & 24 F & Z204 & 10 D \\
\hline C331 & 22 B & Ch401 & 201 & L306 & 20 C & R339 & 21B & R505 & 25 E & Z205 & 10 E \\
\hline C332 & 22B & CR402 & 3017 & L308 & 22 C & R341 & 27 B & R506 & 26 E & Z301 & 15B \\
\hline C333 & 21 C & cru03 & 301) & L. 309 & 23 C & R342 & 26 C & R 507 & 26 F & Z302 & 17 B \\
\hline C334 & 23 C & Cilla & 3111 & L310 & 18 C & R343 & 25 C & R508 & 26 F & Z303 & 19B \\
\hline C335 & 23 C & (12405 & \(31{ }^{\circ}\) & L311 & 24 C & R491 & 29 C & R509 & 23 F & Z304 & 20B \\
\hline C336 & 23 B & \(1 \times 510\) & \(20^{\circ}\) & L312 & 23D & R402 & 29 B & R510 & 22G & Z305 & 22B \\
\hline C337 & 24 C & \(\mathrm{DI}^{1} 401\) & 318 & L313 & 15B & R403 & 30 B & R511 & 23G & Z306 & 24B \\
\hline C338 & 24 C & US501
US502 & 18 F & L501 & 23 E & R404 & 30 B & R512 & 23 G & Z307 & 4F \\
\hline C339 & 25 C & E345 & 285 & M501 & 14G & R405 & 29 C & R513 & 23G & Z308 & 5 F \\
\hline C340 & 25 C & E346 & \(13{ }^{\circ}\) & P201 & 3 C & R406 & 29 C & R515 & 16 F & Z309 & 6 F \\
\hline C341 & 26B & E435 & \(28{ }^{\circ}\) & P202 & 2C & R407 & 30 D & R516 & 16G & Z310 & 7 F \\
\hline C343 & 27 B & (E503) & \(3{ }^{3}\) & P204(J204) & 11D & R408 & 30 C & R517 & 14G & Z311 & 8 F \\
\hline C344 & 27B & F501 & 18 F & P302 & 28 C & R409 & 31B & R518 & 25G & Z312 & 9 F \\
\hline & & F502 & 18 E & & & R410 & 31 C & R519 & 24 G & Z501 & ii) \\
\hline & & F503 & 18H & & & & & 8520
\(R 521\) & 18 F
17 E & & \\
\hline & & & & & & & & S501 & 15 F & & \\
\hline
\end{tabular}


\(\underset{\substack{\text { Ant/CRn-9D }}}{\text { REPR }}\)
AP16c-0701-146A (2nd Edition)

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Ref desig & Location & ref desig & location & Ref desig & Location & Ref desig & location \\
\hline \({ }^{\text {C1501 }}\) & 1 C & C1542 & 7 K & L1507 & \({ }^{68}\) & R1518 & 2 G \\
\hline \({ }^{C 1502}\) & \(4 \mathrm{4B}\) & \({ }^{\text {C1543 }}\) & \({ }^{75}\) & L1508 & \({ }^{5 C}\) & R1519 & 15 \\
\hline \({ }^{\text {c1503 }}\) & 1 B & \({ }^{\text {C1544 }}\) & 8.5 & \({ }^{\text {L1509 }}\) & \({ }^{6 \mathrm{C}}\) & \({ }_{\text {R1520 }}\) & \({ }_{3} 3\) \\
\hline \(\mathrm{Cl1504}^{\text {c }}\) & \({ }_{3 C}^{3 C}\) & \({ }^{\mathrm{C} 1545}\) & \({ }^{85}\) & \({ }^{\text {L1510 }}\) & \({ }^{7}\) & \({ }_{\text {R1522 }}\) & \({ }^{31}\) \\
\hline C1505 & \({ }^{3 C}\) & \({ }^{\text {C1546 }}\) & \({ }^{9 E}\) & \({ }^{\text {L1511 }}\) & 7 & \({ }^{\text {R1522 }}\) & \({ }^{41}\) \\
\hline \({ }^{\text {C1506 }}\) & \({ }^{2 \mathrm{D}}\) & \({ }^{\text {C1547 }}\) & 9 D & \({ }^{\text {L1512 }}\) & \({ }^{1 \mathrm{H}}\) & \({ }^{\text {R1523 }}\) & 51 \\
\hline C1507 & \({ }^{2 \mathrm{E}}\) & \({ }^{C 1548}\) & 11 E & \({ }^{\text {L1513 }}\) & \({ }^{2 H}\) & \({ }^{\text {R1524 }}\) & il \\
\hline \({ }^{\text {C1508 }}\) & \({ }^{18}\) & \({ }^{\text {C1549 }}\) & 11D & \({ }^{\text {L1514 }}\) & \({ }^{2 H}\) & R1535 & 31 \\
\hline C1509 & 3 E & C1550 & \({ }^{12 \mathrm{E}}\) & L1515 & 21 & R1536 & 41 \\
\hline C1510 & \(4 \mathrm{4E}\) & \({ }^{\text {C1551 }}\) & \({ }^{13 \mathrm{D}}\) & \({ }^{\text {L1516 }}\) & \({ }^{5 G}\) & \({ }^{\text {R1537 }}\) & \({ }^{3} \mathrm{~J}\) \\
\hline \(\mathrm{C}^{1511}\) & 4 E & \({ }^{\text {C1552 }}\) & \(9{ }^{9}\) & L1517 & \({ }^{6 G}\) & V1501 & \({ }^{\text {c }}\) \\
\hline \({ }^{\text {C1512 }}\) & \({ }^{4 \mathrm{D}}\) & \({ }^{\text {C1553 }}\) & 9 J & \({ }^{\text {L1518 }}\) & \({ }^{5 H}\) & V1502 & \({ }^{5}\) \\
\hline \({ }^{\text {C1513 }}\) & 5D & \({ }^{\text {C1554 }}\) & \({ }^{115}\) & L1519 & \({ }^{6}\) & v1503 & \({ }^{\text {7 }}\) \\
\hline C1514 & 5B & \({ }^{\text {C1555 }}\) & \({ }^{111}\) & L1520 & 7 H & V1504 & \({ }^{\text {c }}\) \\
\hline C1515 & 6D & \({ }^{\text {C1556 }}\) & \({ }^{135}\) & L1521 & 61 & v1505 & 11 C \\
\hline \({ }^{\text {C1516 }}\) & \({ }^{6 D}\) & \({ }^{\text {C1557 }}\) & \({ }^{131}\) & \({ }^{\text {L1522 }}\) & \({ }^{6 E}\) & \({ }^{\mathrm{V} 1506}\) & \({ }^{13 \mathrm{C}}\) \\
\hline C1517 & \({ }_{7}^{78}\) & \({ }^{\text {C1558 }}\) & \({ }^{8 C}\) & \({ }^{\text {L1523 }}\) & \({ }_{\text {7E }}\) & V1507 & : \\
\hline \({ }^{C 1518}\) & 7 C & \({ }^{\text {C1560 }}\) & \({ }^{15}\) & \({ }^{\text {L524 }}\) & \({ }_{8}^{8 E}\) & V1508 & ¢ \\
\hline C1519 & \({ }^{8 C}\) & \({ }^{\text {C1561 }}\) & 2 J & \({ }^{\text {L1525 }}\) & \({ }^{7}\) & V1509 & \({ }^{\text {\% }}\) \\
\hline \({ }^{\text {C1520 }}\) & \(7{ }^{7}\) & \({ }^{\text {C1562 }}\) & \({ }^{35}\) & \({ }^{\text {L1526 }}\) & \({ }_{8}^{85}\) & V1510 & \({ }^{\text {¢ }}\) - \({ }^{\text {H }}\) \\
\hline \({ }^{\text {C1521 }}\) & \({ }^{6 \mathrm{E}}\) & \({ }^{C 1563}\) & \({ }_{4}^{4 J}\) & \({ }^{\text {L1527 }}\) & \({ }_{45}^{85}\) & \(\mathrm{V}^{\mathrm{V} 511}\) & \({ }_{1}^{11 \mathrm{H}}\) \\
\hline \({ }^{\text {C1522 }}\) & 9 D & \({ }^{\text {C1564 }}\) & \({ }_{4 J}^{45}\) & \({ }^{\text {L1528 }}\) & \({ }_{68}^{4 \mathrm{E}}\) & \({ }^{\mathrm{V} 1512}\) & \({ }^{1: 4}\) \\
\hline \({ }^{\text {C1523 }}\) & \({ }^{16}\) & \({ }^{\text {C1565 }}\) & \({ }^{65}\) & \({ }^{\text {L1529 }}\) & \({ }^{6 \mathrm{E}}\) & \({ }_{\text {Y1501 }}\) & \({ }^{1 /}\) \\
\hline \({ }^{1} 1524\) & \({ }^{4 \mathrm{G}}\) & \({ }^{\text {C1566 }}\) & \({ }^{1 \mathrm{H}}\) & \({ }^{\text {L1530 }}\) & \({ }_{4}^{4 E}\) & Y1502 & \({ }_{98}^{21}\) \\
\hline C1525 & \({ }_{3}^{3 \mathrm{H}}\) & \({ }_{\text {E } 1510}\) & \({ }_{88}^{8 \mathrm{C}}\) & \({ }_{\text {L1535 }}\) & 4 J & & \({ }_{9}^{9 B}\) \\
\hline \({ }_{\text {C1526 }}^{\text {C1527 }}\) & \({ }_{2 \mathrm{l}}^{3 \mathrm{H}}\) & \(\underset{\text { E1511 }}{\text { E1512 }}\) & \({ }_{8 \mathrm{BH}}^{8 \mathrm{C}}\) & \({ }_{\text {L1536 }}^{\text {L1537 }}\) & & \({ }_{\text {Z1502 }}^{\text {Z1503 }}\) & 11 B \\
\hline \({ }_{\substack{C 1527 \\ \text { C1528 }}}\) & ¢ \({ }_{5}^{21}\) & \(\underset{\substack{\text { E1512 } \\ \text { E1513 }}}{ }\) & \({ }_{8 \mathrm{BI}}^{8 \mathrm{H}}\) & \({ }_{\text {L1538 }}^{\text {L1537 }}\) & \({ }_{118}^{6 J}\) & Z1503
Z 1504 & \(\underset{\substack{13 \mathrm{H}}}{ }\) \\
\hline C1529 & 51 & J1502 (P1406) & 108 & L1539 & 12B & 21505 & \({ }^{11 \mathrm{H}}\) \\
\hline \({ }^{C 1530}\) & \({ }_{51}^{61}\) & J1503 (P1401) & \({ }^{13 \mathrm{C}}\) & \({ }^{\text {L1540 }}\) & \({ }_{12 \mathrm{G}}^{11 \mathrm{G}}\) & \({ }_{21506}\) & \({ }^{13 \mathrm{H}}\) \\
\hline \({ }^{\text {C1531 }}\) & \({ }_{5}^{5 H}\) & J1505(P1406) & \({ }^{10 \mathrm{H}}\) & \({ }^{\text {L1541 }}\) & 12 G & \({ }^{21507}\) & \({ }^{8 \mathrm{C}}\) \\
\hline \({ }^{\text {C1532 }}\) & \({ }^{61}\) & J1506(P1401) & 13H & R1501 & 2 B & Z1508 & \({ }_{8} 8\) \\
\hline \({ }^{\text {C1533 }}\) & 7 G & J1507(P1503) & 12B & R1502 & \(1{ }^{10}\) & Z1509 & 12B \\
\hline \({ }^{\text {C1534 }}\) & \({ }_{7}^{7}\) & J1508(P1503) & \({ }^{12 \mathrm{G}}\) & \({ }_{\text {R1503 }}\) & 3 D & \({ }^{21510}\) & \({ }^{12 \mathrm{G}}\) \\
\hline \({ }^{\text {C1535 }}\) & 71 & \(\mathrm{JISO9}^{\text {(P1504) }}\) & -13F & \({ }^{\text {R1504 }}\) & \({ }_{3}^{3 C}\) & \({ }_{71511}\) & 9 D \\
\hline \({ }^{\text {C1536 }}\) & \({ }^{8 \mathrm{H}}\) & J1510(P1504) & \({ }^{13 \mathrm{~K}}\) & R1505 & 3 D & \({ }^{2} 1512\) & \\
\hline C1537 & \({ }_{7 \mathrm{~F}}^{9 \mathrm{~F}}\) & \({ }_{\text {L1502 }}^{\text {L1501 }}\) & \({ }_{2 B}^{1 C}\) & R1507
R 1508 & \({ }_{4 \mathrm{~L}}^{4 \mathrm{D}}\) & Z1513
\(\mathrm{Z1514}\) & \({ }_{9!}^{91}\) \\
\hline \({ }^{\text {C1539 }}\) & \({ }_{7 \mathrm{E}, 8 \mathrm{f}}\) & \({ }_{\text {L1503 }}\) & \({ }_{28}^{28}\) & \({ }_{\text {R1510 }}\) & 5D & \({ }_{\text {Z }}\) & \({ }_{21}^{91}\) \\
\hline \({ }_{\text {Cl }}^{1540}\) & \({ }_{8 \mathrm{e}}^{8 \mathrm{E}}\) & \({ }_{\substack{\text { L1504 } \\ \text { L1506 }}}\) & \({ }_{58}^{2 \mathrm{D}}\) & \({ }_{\text {R1511 }}\) & \({ }_{68}^{60}\) & Z1516 & \({ }_{2}{ }^{\text {D }}\) \\
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Ref pesil & L & Ref Dessic & Locarom & Ref pesic & Locaton & nef pest & Locatrom \\
\hline  & \({ }_{\substack{220}}^{\substack{30}}\) & cires & 8 & Ress & \({ }_{\text {dex }}\) &  & \({ }_{\text {l }}^{121}\) \\
\hline coict & sc & （eitio & \(\underset{\substack{160 \\ 2024}}{\substack{2}}\) &  & \({ }_{\substack{198 \\ 198}}\) &  &  \\
\hline ceic &  &  &  &  & cose &  & \(\substack{\begin{subarray}{c}{150 \\ 180 \\ 180} }} \end{subarray}\) \\
\hline coid & － & coicien & \(\underset{\substack{2 c \\ 12 c \\ 120}}{2 c}\) &  &  &  & \({ }_{\substack{211 \\ 211}}^{210}\) \\
\hline ctic &  &  & cic &  & coin &  & cien \\
\hline  & citic & Sois &  &  &  &  & 旡辰 \\
\hline cick & ， & （ras） & cic &  & \({ }_{\substack{3, \\ \text { 3k } \\ \text { 3k }}}\) & \(\underbrace{}_{\substack{\text { cram } \\ \text { Rrat } \\ \text { Rrat }}}\) & cidy \\
\hline  &  & citiol & \({ }_{\text {a }}^{\text {2．7 }}\) &  & ， &  & 樃 \\
\hline  &  &  & cick &  &  &  &  \\
\hline  &  &  & \({ }_{38}^{28}\) &  &  &  & \(\underbrace{}_{\substack { \text { and } \\ \begin{subarray}{c}{248 \\ 208{ \text { and } \\ \begin{subarray} { c } { 2 4 8 \\ 2 0 8 } }\end{subarray}}\) \\
\hline  &  &  & \％ &  & \％\({ }_{\text {\％}}^{66}\) &  & coick \\
\hline cicicio & cion & cimo &  &  & ¢ & cion & cin \\
\hline  &  &  &  &  & \％ & \(\underset{\substack{\text { Prpa } \\ \text { Tra }}}{\text { a }}\) &  \\
\hline \({ }_{\text {coicle }}^{\text {cisi }}\) &  &  & cic &  &  &  &  \\
\hline  & \(\underset{\substack { \text { and } \\ \begin{subarray}{c}{231 \\ 214{ \text { and } \\ \begin{subarray} { c } { 2 3 1 \\ 2 1 4 } }\end{subarray}}{2}\) & \(\substack{\text { foic } \\ \text { notic }}\) &  &  &  & coick & cosme \\
\hline cicicio & ， &  & \(\substack { \text { coid } \\ \begin{subarray}{c}{\text { log } \\ \text { lob }{ \text { coid } \\ \begin{subarray} { c } { \text { log } \\ \text { lob } } } \end{subarray}\) &  &  & cois & cic，ac \\
\hline  &  &  & （10ic &  &  &  & coiction \\
\hline  &  &  &  &  &  &  & ， \\
\hline coiccis &  &  &  &  &  & cis &  \\
\hline  & \(\substack{\begin{subarray}{c}{\text { aif } \\ \text { lit } \\ \text { lic }} }} \end{subarray}\) & \(\substack{\text { noid } \\ \text { noid }}\) &  &  &  &  &  \\
\hline  & ， & \(\substack{\text { Reas } \\ \text { Rest } \\ \text { Reat }}\) &  &  &  &  &  \\
\hline  & \(\underset{\substack{188 \\ 88}}{18}\) &  &  &  & \(\underset{\substack{\text { lin } \\ 123}}{121}\) & Veis & （100 \\
\hline
\end{tabular}


hotes: 1. all resistors are in ohms ano \(1 / 2\) wati unless otherwise specified
2. ALI CAPACITORS ARE II MICROFARAD D UMIISS OTHERWISE SPECLFIED
tiol PIN NUMEERS CORRECTEO BY AMOT. 4


Figure 6-23. Coder-Indicator KY-382/GRN-9D. Video Frame. Schematic Diagram


Figure 6-24. Low Voltage Power Supply PP-1766/URN,


Figure 6-24a. Low Voltage Power Supply PP-1766/URN, Schematic Diagram








Figure 6-29a. Control-Duplexer C-2226A/GRN-9,
(Replacement Test Equipment, Table 5-la)



Figure 6-31. Radio Receiver R-824/URN, Preamplifier and Mixer Subassembly. Wiring Diagram



Figure 6-33. Radio Receiver R-824/URN, Video Chassis,


Figure 6-34. Radio Receiver R-824/URN,
Power Supply Chassis, Wiring Diagram


Figure 6-35. Frequency Multiplier Oscillator CV-II7I/GRN-9D. Frame,

(DISPLACED FOR CLARITY)


Figure 6-36. Frequency Multiplier-Oscillator CV-II7I/GRN-9D. Video Chassis, Wiring Diagram



Figure 6-38. Frequency Multiplier-Oscillator




Figure 6-4I. Coder-Indicator KY-382/GRN-9D, Frame, Wiring Diagram





Figure 6-45a. Low Voltage Power Supply PP-1766/URN, Wiring Diagram
(Replacement Test Equipment, Table 5-la)

AN/GRN-9D REPAIR






6-95/6-96
Figure 6-48. Cabinet CY-3163/GRN-9D. Wiring Diagram (Sheet 2 of 2)



Figure 6-50. Radio Receiver R-824/URN, Overall View


Figure 6-51. Coder-Indicator KY-382/GRN-9D, Overall View


Figure 6-52. Coder-Indicator KY-382/GRN-9D, Left Side View


Figure 6-53. Coder-Indicator KY-382/GRN-9D, Top View


Figure 6-54. Frequency Multiplier-Oscillator CV-1171/GRN-9D, Overall View


Figure 6-55. Frequency Multiplier-Oscillator CV-1171/GRN-9D, Video Chassis, Top View


Figure 6-56. Frequency Multiplier-Oscillator R-F Chassis, Bottom View


Figure 6-57. Amplifier-Modulator AM-1701/URN


Figure 6-58. Amplifier-Modulator AM-1701/URN, Right Side View


Figure 6-59. Amplifier-Modulator AM-1701/URN, Top View


Figure 6-60. Control-Duplexer C-2226A/GRN-9


Figure 6-61. Control Duplexer C-2226A/GRN-9, Left Side View


Figure 6-62. Low Voltage Power Supply PP-1766/URN, Overall View


Figure 6-63. Low Voltage Power Supply PP-1766/URN, Top View


Figure 6-64. Low Voltage Power Supply PP-1766/URN, Rear Front View


Figure 6-65. Medium Power Supply PP-1765/URN, Overall View


Figure 6-66. Medium Voltage Power Supply PP-1765/URN, Left Side View


Figure 6-67. High Voltage Power Supply PP-1763/URN, Overall View


Figure 6-68. High Voltage Power Supply PP-1763/URN, Top View

\title{
SECTION 7 \\ PARTS LIST
}

\section*{7-1. INTRODUCTION.}

Reference designations (previously referred to as circuit symbol, reference symbol, etc.) have been assigned to identify all maintenance parts of the equipment. They are used for marking the equipment (adjacent to the part they identify) and are included on drawings, diagrams and the parts list. The letters of a reference designation indicate the kind of part (generic group) such as resistor, amplifier, electron tubes, etc. The number differentiates between parts of the same generic group. Parts of the first major unit are numbered from 201 to 599; parts of the second 601 to 799, etc. Two or more consecutive series of numbers have been assigned to major units in which there are more than one hundred parts of the same generic group. Sockets associated with a particular plug-in device, such as an electron tube or a fuse, are identified by reference designation which includes the reference designation of the plug-in device. For example, the socket for fuse F501 is designated XF501.

\section*{7-2. LIST OF MAJOR UNITS.}

Table 7-1 is arranged by the groups of reference designations that apply to a major unit. Thus, if you know a part's reference designation, this table will give you a ready reference to the major unit it is in. The table also gives the following information for each major unit: (1) its common name (see column 5), as well as its official nomenclature (see columns 3 and 4); (2) quantity in one equipment and which equipment it is part of; and (3) location of its parts in Table 7-3.

\section*{7-3. LIST OF MAJOR UNITS BY COLLOQUIAL NAME.}

Table 7-2 is arranged by the common name of major units. All major units are listed but the common name is only included when it differs from the official nomenclature. The table also locates the major unit's parts description in Table 7-3.

\section*{7-4. MAINTENANCE PARTS LIST.}

Table 7-3 lists all major units and their maintenance parts. Each major unit's parts are grouped together. Column 1 lists the reference series of each major unit followed by the reference designations of the various parts in alphabetical and numerical order. Column 2 nor mally lists the applicable government stock numbers or supporting notes. New

\begin{abstract}
Stock Number Identification Tables (SNIT) issued by the Electronic Supply Office include Federal Stock Nu mbers and Source, Maintenance and Recoverability Codes. Therefore, reference shall be made to the SNIT for this infor mation. Column 3 gives the name and describes the various parts. Complete information is given for all key parts (parts differing from any part previously listed in this table) and sub-key parts (parts identical with a key part but appearing for the first time for a major unit). The name and description are omitted for other parts. However, reference is made to the key part or sub-key part for the data. The manufacturer is listed by a five digit code nurber. For example, "21964 dwg \#" means manufactured by ITT etc. Column 4 indicates how the part is used, gives its functional location in the equipment, and lists the figure number on which it is illustrated or called out.
\end{abstract}

\section*{7-5. LIST OF MANUFACTURERS.}

Table 7-4 lists manufacturers of parts used in the equipment. The five digit numerical codes are those used in the Federal Supply system to identify the manufacturers.

\section*{7-6. NOTES.}

The following provide additional information about items listed in Table 7-3.
1. Fabricate locally from bulk material having the stock number listed in SNIT.
2. Manufacture in a Navy Shop.
3. Will be procured on demand by the nearest Naval Shore Supply Activity.
4. Non-replaceable in this application. Listed for reference only,
5. Replace by adapting or modifying the standard item having the stock number lister in SNIT. Modify as indicated in the descrin tion.
6. Replace with the substitute part having the stock number listed in SNIT.
7. Low failure item; if required, requisition from ESO, referencing NAVSHIPS 900, 180C.
8. Assemble from component parts.

TABLE 7-1. RADIO SET AN/GRN-9D, LIST OF MAJOR UNITS
\begin{tabular}{|c|c|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF. } \\
& \text { DESIGNA- } \\
& \text { TION }
\end{aligned}
\] & QUANTITY
AN/GRN-9D & NAME OF MAJOR UNIT & DESIGNATION & COLLOQUIAL NAME & PAGE \\
\hline & 1 & RECEIVER-TRANSMITTER GROUP & OA-3352/GRN-9D & & 7-5 \\
\hline 201-599 & 1 & Radio Receiver & R-824/URN & Receiver & 7-5 \\
\hline 601-799 & 1 & Coder-Indicator & KY-382/GRN-9D & & 7-35 \\
\hline 1101-1199 & 1 & Control-Duplexer & C-2226A/GRN-9D & & 7-71 \\
\hline 1301-1399 & 1 & Amplifier-Modulator & AM-1701/URN & & 7-82 \\
\hline 1401-1599 & 1 & Frequency Multiplier-Oscillator & CV-1171/GRN-9D & & 7-90 \\
\hline 901-999 & 1 & Electrical Equipment Cabinet & CY-3163/GRN-9D & & 7-58 \\
\hline & 1 & POWER SUPPLY ASSEMBLY & OA-1537A/GRN-9A & & 7-5 \\
\hline 1601-1799 & 1 & Power Supply & PP-1766/URN & Low Voltage Power Supply & 7-121 \\
\hline 1801-1899 & 1 & Power Supply & PP-1765/URN & Medium Voltage Power Supply & 7-133 \\
\hline 1901-1999 & 1 & Power Supply & PP-1763/URN & High Voltage Power Supply & 7-144 \\
\hline 1001-1099 & 1 & Electrical Equipment Cabinet & CY-3164/GRN-9D & & 7-65 \\
\hline
\end{tabular}

TABLE 7-2. RADIO SET AN/GRN-9D, LIST OF MAJOR UNTS BY COLLOQUIAL NAME
\begin{tabular}{|c|c|c|}
\hline COLLOQUIAL NAME & NOMENCLATURE & PAGE \\
\hline \begin{tabular}{l}
Receiver \\
Low Voltage Power Supply \\
Medium Voltage Power Supply \\
High Voltage Power Supply
\end{tabular} & \begin{tabular}{l}
RECEIVER-TRANSMITTER GROUP, OA-3352/GRN-9D \\
Radio Receiver R-824/URN \\
Coder-Indicator, KY-382/GRN-9D \\
Control-Duplexer, C-2226A/GRN-9 \\
Amplifier-Modulator AM-1701/URN \\
Frequency Multiplier-Oscillator, CV-1171/GRN-9D \\
Electrical Equipment Cabinet, CY-3163/GRN-9D \\
POWER SUPPLY ASSEMBLY, OA-1537A/GRN-9A \\
Power Supply PP-1766/URN \\
Power Supply PP-1765/URN \\
Power Supply PP-1763/URN \\
Electrical Equipment Cabinet, CY-3164/GRN-9D
\end{tabular} & \[
\begin{array}{r}
7-5 \\
7-5 \\
7-35 \\
7-71 \\
7-82 \\
7-90 \\
7-58 \\
7-5 \\
7-121 \\
7-133 \\
7-144 \\
7-65
\end{array}
\] \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline & & \begin{tabular}{l}
RADIO SET, AN/GRN-9D: major components c/o 1, ReceiverTransmitter Group, 1, Power Supply Assembly, 21964 \#B1068498 \\
RECEIVER-TRANSMITTER GROUP OA-3352/GRN-9D: major components c/o 1, Radio Receiver, R-824/URN; 1, Coder-Indicator, 1, Control-Duplexer, 1, Amplifier-Modulator, AM-1701/URN; 1, Frequency Multiplier-Oscillator, Electrical Equipment Cabinet, 21964 A+O \#A1068487G1
\end{tabular} & \begin{tabular}{l}
Figure 1-1 \\
Part of Radio Set \\
AN/GRN-9D \\
Figure 1-2
\end{tabular} \\
\hline & & POWER SUPPLY ASSEMBLY OA-1537A/GRN-9A: major components c/o 1, Power Supply, PP-1766/URN (Low Voltage); 1, Power Supply PP-1765/URN (Medium Voltage); 1, Power Supply PP-1763/URN (High Voltage); 1, Electrical Equipment Cabinet, 21964 \#A1068706G1 & Part of Radio Set AN/GRN-9D Figure 1-3 \\
\hline 201-599 & & RECEIVER, RADIO R-824/URN: reception, Ref Dwg Group 5, frequency data, 1025 to 1150 mc for channel center frequency ( 1024.5 mc to 1150.5 mc including channel width) 126 channels, each channel 1 mc apart from 1025 mc to 1150 mc inclusive; operating power requirements AC 117 vor 120 v ; 60 cycles, single phase, 200 watts: rack mounting, with pull-out slides, front access only; overall dim. 27" lg. , 17-1/2" wide, 9-1/2" high; 26 electron tubes plus 7 crystal diodes; superheterodyne circuit; no plug-in coils; frequency of the local oscillator controlled by direct crystal multiplication; local oscillator located externally; generates random noise pulses which triggers the transmitter in the absence of interrogation pulses; adjacent channel rejection by means of Ferris Discriminator; drives the Coder-Indicator with 2700 pulses per second and provides an isolated output of the same information for future air-toground services; 21964 dwg H2060002 and A2060002 & Part of ReceiverTransmitter Group Figure 6-50 \\
\hline C201 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(1000 \mu \mu \mathrm{f}, \pm 20 \%\); 500 v DC working; variable temp coef; MIL type CK70A102M per MIL-C-11015; 21964 dwg \#A9010576-1 & Bypass \\
\hline C202 & & Same as C201 & Bypass \\
\hline C203 & & Same as C201 & Bypass \\
\hline C204 & & Same as C201 & Bypass \\
\hline C205 & & Same as C201 & Bypass \\
\hline C206 & & Same as C201 & Bypass \\
\hline C207 & & Not Used & \\
\hline C208 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(15 \mu \mu \mathrm{f} \pm 10 \%\); 300 v DC -100 to \(+100 /\) Million \(/{ }^{\circ} \mathrm{C}\); MLL type CB11RD150K, per spec MIL-C10950A; 21964 dwg \#A9010542-2 & RF bypass \\
\hline C209 & & Same as C208 & RF bypass \\
\hline C210 & 6 & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(680 \mu \mu \mathrm{f}+100-20\) tolerance; \(500 \vee\) DC variable temp coef; MIL type CK21W681Z per spec MIL-C-11015A; 21964 dwg \#A9010573-1 & Coupling \\
\hline C211 & 6 & CAPACITOR, FLXED, CERAMIC DIELECTRIC: \(1000 \mu \mu \mathrm{f} \pm 20 \%\); 500 v DC variable temp coef; 323-04-S; MIL-C-11015A for electrical performance only; 21964 dwg \#A2060351-1 & Bypass \\
\hline C212 & & Same as C211 & Bypass \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J201 & & CONNECTOR, RECEPTACLE ELECTRICAL: 1 contact, female, right angle; series N; MIL type UG-997A/U per Navy dwg; REB 49245; 21964 *A21330-30 & LO input \\
\hline J202 & & Same as \(\mathbf{J 2 0 1}\) & Signal Input \\
\hline J203 & & CONNECTOR, RECEPTACLE ELECTRICAL: 1 round female contact; MIL type UG-1094/U BNC Series, "D" hole mounting, per Navy dwg REB 49063; 21964 dwg \#A2131937 & IF output \\
\hline \begin{tabular}{l}
\[
\mathbf{J} 204
\] \\
Cont See J301
\end{tabular} & & CONNECTOR, RECEPTACLE ELECTRICAL: 14 female contacts, straight type; current up to \(5 \mathrm{amp} ; 81312 \mathrm{MRE}-14 \mathrm{SG}\) per spec MIL-C-8384; 21964 dwg *A9010581 & IF pre-amp power Figure 6-3 \\
\hline L201 & & COIL, INTERMEDIATE FREQUENCY: single winding, single layer, close wound; 60 turns, \#34E wire; 3.0 uh \(\pm 10 \%\) at \(7.9 \mathrm{mc} \pm 0.5 \%\); o/a 1/2" lg. , 0. 125" dia. , per spec MIL-C-15305A; 21964 \#A9010281-1 & IF filter \\
\hline L202 & & Same as L201 & IF filter \\
\hline L203 & & Same as L201 & IF filter \\
\hline L204 & & Same as L201 & IF filter \\
\hline L205 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound; 56 turns; of \#34E wire, 4.55 uh \(\pm 5 \%\) at \(7.9 \mathrm{mc} \pm 0.5\); o/a dim. 1/2" lg. , 0. 156" dia, per spec MIL-C-15305A; 21964 \#A9010281-2 & Neutralizing \\
\hline 1206 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 6-3/4 turns of 26E wire; iron powered core, adjustable; 0.27 uh \(\pm 5 \%\) with no slug, 0.28 uh min to 0.38 uh max. with slug at \(40 \mathrm{mc} \pm 0.5 \%\); per spec MIL-C-15305A; 21964 \#A9010283-1 & Tuning \\
\hline L207 & & Coil, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 28 turns of \#30E wire; . 67 uh \(\pm 10 \%\) at \(40 \mathrm{mc} \pm 0.5 \%\); o/a dim. 3/8" lg. , 0. 170" dia; per spec MIL-C-15305A; 21964 \#A9010281-3 & IF choke \\
\hline L208 & & Same as L207 & IF choke \\
\hline L209 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound; 12 turns, \(\# 28 \mathrm{E}\) wire, iron powdered core adjustable, \(58 \mathrm{uh} \pm 5 \%\) with no slug, 0.68 uh min. to 1.03 uh max. with slug at \(40 \mathrm{mc} \pm 0.5 \%\) per spec MIL-C-15305A; 21964 \#A9010283-3 & IF tuning series arm tee \\
\hline L210 & & Same as L209 & IF tuning series arm tee V203 \\
\hline L211 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 16-1/2 turns, \#30E wire, adjustable powdered iron core; 1. 05 uh \(\pm 5 \%\) with no slug, 1.20 uh min. to 1.9 uh max. with slug at \(30 \mathrm{mc} \pm 0.5 \%\); per spec MIL-C-15305A; 21964 \#A9010283-4 & IF tuning series arm of tee \\
\hline L212 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, space wound, 8 turns; \#26E wire, 0.125 uh \(\pm 10 \%\) at \(60 \mathrm{mc} \pm 0.5 \% ;\) o/a dim. 3/8" lg. , 0. 107" dia. ; per spec MIL-C-15305A; 21964 \#A9010234-1 & Shunt arm of tee \\
\hline 1213 & & COIL, INTERMEDLATE FREQUENCY: 1 winding, single layer, space wound, 4 turns of \#22E wire; 0.55 uh \(\pm 10 \%\) at \(84 \mathrm{mc} \pm 0.5 \%\); o/a dim. 3/8' lg. , 0. 107' dia. ; per spec MIL-C-15305A; 21964 \#A9010234-3 & Shunt arm of tee \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DES'G
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline L214 thru L216 & & Not Used & \\
\hline L217 & & Same as L201 & IF filter \\
\hline L218 & & Same as L201 & IF filter \\
\hline L. 219 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 46 turns of \#32E wire; \(3.2 \mathrm{uh} \pm 10 \%\) at \(7.9 \mathrm{mc} \pm 0.5 \%\); o/a dim. 1/2" lg. , 0. 156" dia, per spec MIL-C-15305A; 21964 \#A9010281-4 & IF choke \\
\hline \begin{tabular}{l}
L220 \\
Cont \\
See L301
\end{tabular} & & Same as L2I9 & IF choke \\
\hline MP201 & 1 & GASKET: synthetic rubber, MIL-R-900A, class 2 ; cross-sectional style no. 7, Ref Dwg Group 74; 1/8' wide, 5/32" high w/1/16" radius, approx 42" Ig; 21964 "A9140800 & Panel sealing \\
\hline MP202 & & BOOT, DUST AND MOISTURE SEAL: silicon rubber bonded to a brass, nickel plated hex nut 15/32-32 thd; \(3 / 4 \mathrm{in}\). across flats, 7/8 in. lg; 97539 \#1030; 21964 \#A2132649-1 & Covers toggle switch on receiver panel \\
\hline MP203 & 7 & SPRING, HELICAL, COMPRESSION: cylindrical shape, Ref Dwg Group 65; 2 active coil ends squared and closed; beryllium copper wire per spec MIL-C-947; 5/32 in. lg, 5/32 in. OD; 21964 \#A9010155 & p/o clamp in mixer assy \\
\hline MP204 & & Same as MP203 & p/o clamp in mixer assy \\
\hline \begin{tabular}{l}
MP205 \\
Cont See MP301
\end{tabular} & 1 & GASKET: synthetic rubber, MIL-R-900C; 2-15/64 in. dia aperture in. center three \(1 / 8 \mathrm{in}\). dia holes spaced 120 deg apart on 2-7/16 in. dia; 2-11/16 in. dia OD, \(1 / 16\) in. thk; 21964 \#B2060910 & Sealer \\
\hline P201 & & CONNECTOR, PLUG, ELECTRICAL: 1 round male contact; one connector mating end; BNC series; 50 ohms nom impedance, 500 v peak voltage; accommodated RG-55/U and RG-58/U cables; 74868 \#85000; MLL type UG-88C/U per Sig dwg \#SC-D-72235: BuShips dwg \#REB49064; 21964 \#A2131456 & Mixer LO input \\
\hline P202 & & CONNECTOR, PLUG ELECTRICAL: 1 contact, male round, straight type; MIL type UG-21D/U per MIL STD dwg \#MS-91236; 21964 \#A2132719 & Mixer signal input \\
\hline P203 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline \begin{tabular}{l}
P204 \\
Cont \\
See P301
\end{tabular} & & Same as J304 & Power input \\
\hline R201 & 6 & RESISTOR, FIXED, COMPOSITION: 100 ohms, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF101K, per spec MIL-R-11; 21964 \#504219 & Meter shunt \\
\hline R202 & & Same as R201 & Meter shunt \\
\hline R203 & & Not Used & \\
\hline R204 & & Not Used & \\
\hline R205 & 6 & Same as R201 & Cathode bias for V202 \\
\hline R206 & 6 & RESISTOR, FIXED, COMPOSITION: 68 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF680K per spec MIL-R-11; 21964 \#504217 & Cathode bias for V201 \\
\hline R207 & 6 & RESISTOR, FIXED, COMPOSITION: 2,200 ohms \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF222K per spec MLL-R-11; 21964 \#504235 & Damping \\
\hline R208 & 6 & RESISTOR, FIXED, COMPOSITION: 220 ohms \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF221K per spec MIL-R-11; 21964 \#504223 & Bias V203 \\
\hline \[
\begin{gathered}
\text { R209 } \\
\text { thru } \\
\text { R2I }
\end{gathered}
\] & & Not Used & \\
\hline R212 & 6 & RESISTOR, FIXED, COMPOSITION: 2700 ohms; \(\pm 10 \%\); 1 watt; MIL type RC32GF272K per spec MIL-R-11; 21964 \#503923 & Plate dropping
\[
\text { V } 202
\] \\
\hline R213 & & Same as R212 & Screen resistor V203 \\
\hline \begin{tabular}{l}
R214 \\
Cont \\
See R301
\end{tabular} & 6 & RESISTOR, FIXED, COMPOSITION: 2700 ohms; \(\pm 10 \%\); 2 watt; MIL type RC42GF272K per spec MIL-R-11; 21964 \#501246 & \[
\begin{aligned}
& \text { Voltage dropping } \\
& \text { V201 }
\end{aligned}
\] \\
\hline \begin{tabular}{l}
T201 \\
Cont \\
See T401
\end{tabular} & & TRANSFORMER, INTERMEDIATE FREQUENCY: 63 mc peak frequency; phase inverter; shielded; MIL type LT8F per spec M1L-C-15305A; 21964 dwg \#A2060627G1 & Phase inverter \\
\hline V201 & & ELECTRON TUBE: pentode; MIL type 5654/6AK5W per spec MIL-E-1C; 21964 \#700561 & IF amplifier Figure 6-3 \\
\hline V202 & & ELECTRON TUBE: triode; MIL type 6J4WA, per spec MIL-E-1 (Navy); 21964 \#A2133316 & IF amplifier Figure 6-3 \\
\hline V203 Cont See V301 & & Same as V201 & IF a mplifier Figure 6-3 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOGATING FUNCTION \\
\hline XV201 & & SOCKET, ELECTRON TUBE: 7 contacts, beryllium silver plated, miniature type; JAN type TS102C01, per spec. JAN-S-28A; 21964 *740003 & Socket for V201 \\
\hline XV202 & & Same as XV201 & Socket for V202 \\
\hline \[
\begin{aligned}
& \text { XV203 } \\
& \text { Cont } \\
& \text { See XV301 }
\end{aligned}
\] & & Same as XV201 & Socket for V203 \\
\hline Z200 & & AMPLIFIER, INTEGRATOR: incoming frequencies, range 1, 1025 mc to 1087 mc (local oscillator frequency range \(1,962 \mathrm{mc}\) to 1024 mc ; range \(2,1151 \mathrm{mc}\) to 1213 mc ) resultant frequency 63 mc ; \(6.3 \mathrm{v}, 60\) cycles, single phase, \(+150 \mathrm{v} \mathrm{DC}, 50\) ohms input impedance, 21964 \#C2060282G1, (less tubes \& tube shields) & Mix incoming RF signal with output of local oscillator and amplify the resultant IF \\
\hline Z201 & & SUPPRESSOR, PARASITIC: coil 19 turns of \({ }^{26 E}\) wire, wound on \(470 \mathrm{ohm} .1 / 2\) watt resistor, (RC20GF471K), 21964 dwg \#A9010279-1 & Filament decoupling \\
\hline Z202 & & Same as Z201 & Filament decoupling \\
\hline Z203 & & Same as Z201 & Filament decoupling \\
\hline Z204 & & SUPPRESSOR, PARASITIC: coil 30 turns of \#30E wire wound on \(1000 \mathrm{ohm}, 1 / 2\) watt resistor (RC20G F102K); 21964 \#A 9010279-2 & Plate decoupling \\
\hline \begin{tabular}{l}
Z205 \\
Cont \\
See Z300
\end{tabular} & & Same as z201 & Filament decoupling \\
\hline C301 & & Same as C210 & Grid coupling \\
\hline C302 & & Same as C211 & Bypass squitter control filter \\
\hline C303 & & Same as C211 & Tank ckt grounding L303 \\
\hline C304 & & Same as C221 & Trans primary tuning \\
\hline C305 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(820 \mu \mu \mathrm{f}+100 \%-20 \%\); 500 v DC working; MIL type CK60Y821Z; per spec MIL-C-11015A; for electrical performance only; MS90128; 21964 part \#625020H821 & Cathode bypass V301 \\
\hline C306 & & Same as C211 & Bypass squitter control filter \\
\hline C307 & & Same as C305 & Cathode bypass V302 \\
\hline C308 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(68 \mu \mu \mathrm{f} \pm 10 \%\); 300 v DC working; -100 to +100 Parts/Million Deg. C; MIL type CB21PD680K; per spec MIL-C-10950A, dwg MS-91105; 21964 \#A9010543-8 & Tank circuit grounding L303 \\
\hline C309 & & Same as C211 & Screen bypass V301 \\
\hline C310 & & Same as C217 & IF coupling V301 to V302 \\
\hline C311 & & Not Used & \\
\hline C312 & & Same as C211 & IF filter V301 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C313 & & Same as C211 & IF filter V302 \\
\hline C314 & & Not Used & \\
\hline C315 & & Same as C217 & IF coupling V302 to V303 \\
\hline C316 & & Same as C211 & Screen bypass V302 \\
\hline \(\mathrm{C317}\) & & Not Used & \\
\hline C318 & & Same as C305 & Cathode bypass V303 \\
\hline C319 & & Same as C211 & Screen bypass V303 \\
\hline C320 & & Same as C308 & Tank circuit grounding L305 \\
\hline C321 & & Same as C217 & IF coupling V303 to V304 \\
\hline C322 & & Not Used & \\
\hline C323 & & Same as C201 & IF bypass plate circuit decoupling \\
\hline C324 & & Same as C211 & IF bypass \\
\hline C325 & & Not Used & \\
\hline C326 & & Same as C305 & Cathode bypass V304 \\
\hline C327 & & Same as C211 & Screen bypass V304 \\
\hline C328 & & Same as C308 & Tank circuit grounding L306 \\
\hline C329 & & Same as C305 & Cathode bypass V305 \\
\hline C330 & & Not Used & \\
\hline C331 & & Same as C201 & IF bypass \\
\hline C332 & & Same as C210 & IF coupling V305 to L308 \\
\hline C333 & & Same as C211 & Screen bypass V305 \\
\hline C334 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(82 \mu \mu \mathrm{f} \pm 2 \%\); 300 v DC working \(\mathbf{- 1 0 0}\) to +100 Parts/Million Deg C; MIL type CB21PD820G per spec MIL-C-10950A; 21964 \#A9010542-3. & Trans primary tuning \\
\hline C335 & 6 & CAPACITOR, FIXED, GLASS DIELECTRIC: \(100 \mu \mu \mathrm{f} \pm 2 \%\) tolerance; 500 v DC working; +115 to +165 Parts/Million Deg C; MIL type CY13C111G per spec MIL-C-11272A and MS15826; 21964 dwg *A9010534-1 & Trans primary tuning \\
\hline C336 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(1.0 \mu \mu \mathrm{f} \pm 0.25 \mathrm{mmf}\), 500 v DC working; JAN type CC21CK010C per spec JAN-C-20A; 21964 \#A9010900 & Coupling L308 to L309 \\
\hline C337 & 6 & CAPACITOR, FIXED, GLASS DIELECTRIC: \(100 \mu \mu \mathrm{f} \pm 2 \%\) tolerance; 500 v DC working; +115 to +165 Parts/Million Deg C; MIL type CY13C101G per spec MIL-C-11272A and MS15826; 21964 dwg *A9010534-2 & Trans secondary tuning \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline C338 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(110 \mu \mu \mathrm{f} \pm 2 \%\) tolerance; 500 v DC \(150 \mu \mu \mathrm{f} / \mu \mathrm{f}\) DEG. C NEG \(+10 \mu \mu \mathrm{f} / \mu \mathrm{f}\) DEG C to 4 . 56289/B02-110 \(\mu \mu \mathrm{f} / \mu \mathrm{f}-500 \mathrm{v} / 21964 / \mathrm{A} 9010535-1\) & Trans secondary tuning \\
\hline C339 & & Same as C334 & IF bypass \\
\hline C340 & & Same as C217 & IF bypass \\
\hline C341 & & Same as C201 & IF bypass plate circuit decoupling \\
\hline C342 & & Not Used & \\
\hline C343 & 6 & CAPACITOR, FLXED, CERAMIC DIELECTRIC: \(1000 \mu \mu \mathrm{f} \pm 20 \%\); 500 v DC working temp coef. var. per spec MIL-C-11015A; for electrical performance only; 72982 GP2L1000 \(\pm 200 ; 21964\) dwg \#A9010537-1 & Coupling V307A to V307B \\
\hline C344 & & CAPACITOR, FEXED, PAPER DIELECTRIC: . \(1 \mu \mathrm{f} \mu \mu \mathrm{f} \pm 10 \%\); 400 v DC working; MIL type CP11A3KE104K per spec MIL-C-25A; 21964 dwg \#A9010541 & Plate bypass V307 \\
\hline C345 & & CAPACITOR, FIXED, PAPER DIELECTRIC: . \(1 \mu \mu \mathrm{f} \pm 10 \%\); 200 v DC working; MIL type CP05A1KC104K per spec MIL-C-25A; 21964 dwg \#A9010536-1 & Coupling V307B to line \\
\hline C346 & & Same as C201 & Filament bypass V306 \\
\hline C347 & & Same as C201 & Filament bypass \\
\hline C348 & & Same as C211 & Filament bypass V306 \\
\hline C349 & & Same as C211 & Filament bypass V304 \\
\hline C350 & & Same as C211 & Filament bypass V303 \\
\hline C351 & & Same as C211 & Filament bypass V302 \\
\hline C352 & & Same as C211 & Filament bypass
V301 \\
\hline C353 & & Same as C217 & Coupling V304 to V305 \\
\hline C354 & & Same as C211 & Plate circuit bypass \\
\hline C355 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: . \(01 \mu \mathrm{f}+100 \%-20 \%\), 500 v DC working; MIL type CK63Y103Z; per MIL-C-11015A; 21964 part \#625023H103 & Bypass \\
\hline C356 & & Same as C355 & Bypass \\
\hline C357 & & Same as C355 & Bypass \\
\hline C358 & & Same as C355 & Bypass \\
\hline C359 & & Same as C355 & Bypass \\
\hline C360 & & Same as C355 & Cathode bypass V307B \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C361 & & Same as C355 & Cathode bypass V307A \\
\hline C362 & & Same as C305 & Coupling V306 to V307A \\
\hline \[
\begin{aligned}
& \text { C363 } \\
& \text { Cont } \\
& \text { See C401 }
\end{aligned}
\] & & Same as C337 & IF bypass \\
\hline E301 & & Same as E201 & Shield for V301 \\
\hline E301A & & Same as E201A & Insert for E301 \\
\hline E302 & & Same as E201 & Shield for V302 \\
\hline E302A & & Same as E201A & Insert for E302 \\
\hline E303 & & Same as E201 & Shield for V303 \\
\hline E303A & & Same as E201A & Insert for E303 \\
\hline E304 & & Same as E201 & Shield for V304 \\
\hline E304A & & Same as E201A & Insert for E304 \\
\hline E305 & & Same as E201 & Shield for V305 \\
\hline E305A & & Same as E201A & Insert for E305 \\
\hline E306 & & Same as E201 & Shield for V306 \\
\hline E306A & & Same as E201A & Insert for E306 \\
\hline E307 & 6 & SHIELD, ELECTRON TUBE: JAN type TS103U02 per spec JAN-S-28A, modified; 21964 \#A2132986-5 & Shield for V307 \\
\hline E307A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U02; MIL-STD-242A type \#902; 21964 \#A2132886-5 & Insert for E307 \\
\hline E308 & & Same as E201 & Shield for V308 \\
\hline \[
\begin{aligned}
& \text { E308A } \\
& \text { J301 }
\end{aligned}
\] & & \begin{tabular}{l}
Same as E201A \\
Same as J203
\end{tabular} & ```
Insert for E308
Squitter control
    input
``` \\
\hline J302 & & Not Used & \\
\hline J303 & & Not Used & \\
\hline J304 & & CONNECTOR, PLUG ELECTRICAL: 14, male, round contacts; polarized, straight type; 81312 \#MRE-14PG per spec MIL-C-8384; 21964 dwg \#A9010571 & Power input \\
\hline J305 & & CONNECTOR, RECEPTACLE ELECTRICAL: single female round contact; straight type; phone type connector, max operating voltage 1,500 v peak; 74868 \#225-B; MIL type MS16108-3 per MLL-STD242A; 21964 \#A2141949-1 & Test point for echo suppressor no. 3 \\
\hline J306 & & Same as J305 & Test point for primary discriminatory transformer \\
\hline \[
\begin{aligned}
& \mathrm{J} 307 \\
& \text { Cont } \\
& \text { See J402 }
\end{aligned}
\] & & Same as J305 & Test point discriminator output \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline L301 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, space wound, 6 turns of \(\# 26 \mathrm{E}\) wire, 0.075 uh \(\pm 10 \%\) at 84 mc \(\pm 0.5 \%\); o/a dim. 3/8" lg, \(0.107^{\prime \prime}\) dia. ; per spec MIL-C-15305A; 21964 \#A9010234-2 & Part of 50 ohm input transformer \\
\hline L302 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, space wound, 12-1/2 turns of "28E wire; iron powdered core, adjustable 0.620 uh \(\pm 5 \%\) with no slug, 0.74 uh min., 1.15 uh max. with slug at \(40 \mathrm{mc} \pm 0.5 \%\); per spec MIL-C-15305A; 21964 \#A9010283-6 & Part of 50 ohm line to grid of V301 transformer \\
\hline L303 & & Same as L209 & Interstage IF trans. V301 to V302 \\
\hline L304 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, \(10-1 / 4\) turns of \#26E wire; iron powdered core, adjustable \(0.42 \mathrm{uh} \pm 5 \%\) with no slug. 0.45 uh min ., 0.72 uh max with slug at \(40 \mathrm{mc} \pm 0.5 \%\) per spec MIL-C-15305A; 21964 \#A9010283-5 & Interstage IF trans. V302 to V304 \\
\hline L305 & & Same as L304 & Interstage IF trans. V303 to V304 \\
\hline L306 & & Same as L304 & Interstage IF trans. V304 to V305 \\
\hline L307 & & Not Used & \\
\hline L308 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 4-1/2 turns of \(0.0325^{\prime \prime}\) dia wire, silver plated, adjustable iron powdered core; 0.112 uh \(\pm 5 \%\) with no slug, 0.112 uh min. to 0.152 uh max. with slug at \(63 \mathrm{mc} \pm 0.5 \%\); 21964 \#A9010331-1 & Ferris discriminator primary \\
\hline L309 & & Same as L308 & Ferris discriminator secondary \\
\hline L310 & & Same as L219 & Choke plate feed V303 \\
\hline L311 & & COIL, INTERMEDIATE FREQUENCY: 1 winding, single layer, close wound, 35 turns of \#32E wire: 1.05 uh \(\pm 10 \%\) at \(40 \mathrm{mc} \pm 0.5 \%\); o/a dim. 3/8" lg. , \(0.107^{\prime \prime}\) dia, per spec MIL-C-15305A; 21964 \#A9010281-8 & Diode DC return V306A \\
\hline L312 & & Same as L311 & Diode DC return V306B \\
\hline \begin{tabular}{l}
1,313 \\
Cont \\
See L401
\end{tabular} & & Same as L219 & Choke plate feed V301 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP301 & 7 & CLAMP, ELECTRICAL: brass, silver plated; designed to hold \(0.195^{\prime \prime}\) nominal o/a dia. cables 74868 1025; type MX-1684/U per 21964 \#A914239 & Secures cable \\
\hline \begin{tabular}{l}
MP302 \\
Cont \\
See MP401 \\
P301
\end{tabular} & & Same as MP301
Not Used & Secures cable \\
\hline P302 & & Same as P201 & IF chassis output \\
\hline P303 & & Same as P201 & IF amp input Figure 6-3 \\
\hline \begin{tabular}{l}
P304 \\
Cont \\
See P401
\end{tabular} & & Same as J204 & IF amp power \\
\hline R301 & 6 & RESISTOR, FIXED, COMPOSITION: 1800 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF182K per spec MIL-R-11; 21964 \#504234 & Input transformer damping L302 \\
\hline R302 & 6 & RESISTOR, FIXED, COMPOSITION: 330 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF331K per spec ML-R-11; 21964 \#504225 & Squitter control decoupling \\
\hline R303 & & Not Used & \\
\hline R304 & 6 & RESISTOR, FIXED, COMPOSITION: 220,000 ohms; \(\pm 10 \% ; 1 / 2\) watt; ML type RC20G F224K per spec MIL-R-11; 21964 \#504259 & Squitter control decoupling \\
\hline R305 & & Same as R203 & Bias V301 \\
\hline R306 & & RESISTOR, FIXED, COMPOSITION: 6200 ohms; \(\pm 5 \% ; 1 / 2\) watt; MLL type RC20GF622J per spec MIL-R-11; 21964 \#504122 & Damping L203 \\
\hline R307 & 6 & RESISTOR, FIXED, COMPOSITION: 2200 ohms; \(\pm 10 \%\); 1 watt; MIL type RC32GF222K per spec MIL-R-11; 21964 \#503922 & Plate dropping
V301 \\
\hline R308 & & Same as R307 & Plate dropping V302 \\
\hline R309 & 6 & RESISTOR, FIXED, COMPOSITION: 2700 ohms; \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF272K per spec MIL-R-11; 21964 \#504236 & Damping L309 \\
\hline R310 & & Same as R208 & Bias V302 \\
\hline R311 & & Not Used & \\
\hline R312 & & Same as R208 & Bias V303 \\
\hline R313 & & Same as R306 & Damping L305 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

\section*{RADIO RECEIVER R-824/URN}
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION . & LOCATING FUNCTION \\
\hline R314 & & Same as R307 & Plate dropping V303 \\
\hline R315 & & Same as R304 & Echo suppressor V304 \\
\hline R316 & & Same as R208 & Bias V304 \\
\hline R317 & & Same as R301 & Damping L306 \\
\hline R318 & & Same as R307 & Damping L306 \\
\hline R319 & & Same as R207 & Echo suppressor V305 \\
\hline R320 & 6 & RESISTOR, FIXED, COMPOSITION: 100,000 ohms: \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF104K per spec MIL-R-11; 21964 \#504255 & Decoupling J305 \\
\hline R321 & & Same as R208 & Bias V305 \\
\hline R322 & & Same as R307 & Plate dropping V305 \\
\hline R323 & & Not Used & \\
\hline R324 & & Not Used & \\
\hline R325 & & RESISTOR, FIXED, COMPOSITION: 8200 ohms; \(\pm 5 \%\); \(1 / 2\) watt; MIL type RC20GF822J per spec MIL-R-11; 21964 \#504125 & Diode load V306B \\
\hline R326 & & RESISTOR, FIXED, COMPOSITION: \(33,000 \mathrm{ohms} ; \pm 5 \% ; 1 / 2\) watt; MIL type RC20GF333id per spec MIL-R-11; 21964 \#504139 & Diode load V306A \\
\hline R327 & & Same as R207 & Decoupling J307 \\
\hline R328 & 6 & RESISTOR, FIXED, COMPOSITION: 4700 ohms; \(\pm 10 \%\); 1 watt; MIL type RC32GF472K per spec MIL-R-11; 21964 \#503926 & Plate load V307A \\
\hline R329 & & Same as R320 & Grid return V307A \\
\hline R330 & & Same as R207 & Decoupling to J306 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R331 & & Same as R320 & Grid return V307B \\
\hline R332 & & Same as R207 & Bias V307B \\
\hline R333 & & Not Used & \\
\hline R334 & 6 & RESISTOR, FIXED, COMPOSITION: 10 ohms; \(\pm 10 \% ; 1 / 2\) watt; ML type RC20GF100K per spec MLL-R-11; 21964 \#504207 & Parasitic suppressor V301 \\
\hline R335 & & Same as R334 & Parasitic suppressor \\
\hline R336 & & Same as R334 & Parasitic suppressor V303 \\
\hline R337 & & Same as R334 & Parasit suppressor V304 \\
\hline R338 & & Same as R334 & Parasitic suppressor V305 \\
\hline R339 & 6 & RESISTOR, FIXED, COMPOSITION: 4,700 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF472K per spec MIL-R-11; 21964 \#504239 & Damping L308 \\
\hline R340 & & Not Used & \\
\hline R341 & 6 & RESISTOR, FIXED, COMPOSITION: 1000 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20G F102K per spec MLL-R-11; 21964 \#504231 & Plate decoupling
V307B \\
\hline R342 & & Same as R341 & Cathode bias V307A \\
\hline \begin{tabular}{l}
R343 \\
Cont \\
See R401
\end{tabular} & & RESISTOR, FIXED, COMPOSITION: 22,000 ohms; \(\pm 5 \%, 1 / 2\) watt; MIL type RC20GF223J per MIL-R-11; 21964 \#504135 & Diode load \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

RADIO RECEIVER R-824/URN


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES \({ }^{\text {- }}\) & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline Z300 & 4 & AMPLIFIER, INTERMEDIATE FREQUENCY: 63 mc operating frequency; \(2.7 \pm 0.3 \mathrm{mc}\) band width 3 db down; 80-90 db at zero AGC overall gain; 50 ohms input impedance, \(6.3 \mathrm{v} \mathrm{AC}, 60\) cycles, single phase, +150 v DC; 21964 \#D2060812G1 (less tubes \& tube shields) & ```
IF amplifier,
    detector and
    video amplifier
``` \\
\hline Z301 & & Same as \(\mathbf{Z 2 0 4}\) & Plate decoupling V301 \\
\hline Z302 & & Same as Z204 & Plate decoupling
V302 \\
\hline Z303 & & Same as Z204 & Plate decoupling V303 \\
\hline C401 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(330 \mu \mu \mathrm{f} \pm 10 \%\), 500 v DC working; MIL type CM20B331K per spec MIL-C-5; 21964 part *600122 & Coupling V402A to V401 \\
\hline C402 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(100 \mu \mu \mathrm{f} \pm 10 \%\), 500 v DC working; MIL type CM20B101K per spec MIL-C-5; 21964 part \#600116 & Coupling V40. to V402B \\
\hline C403 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(1000 \mu \mu \mathrm{f} \pm 10 \%\), 500 v DC working; MIL type CM30B102K per spec MIL-C-5; 21964 dwg \#A2133222-07 & Coupling V401 to V402B \\
\hline C404 & & Same as C403 & Coupling V403 to V404 \\
\hline C405 & & CAPACITOR, FLXED, PAPER DIELECTRIC: 3 sections . \(1 \mu \mathrm{f}+20 \%\) \(-10 \%\) each section; 600 v DC working; MIL type CP69B5EF104V per spec MIL-C-25A; 21964 \#A9010539 & \begin{tabular}{l}
Bypass \\
Figure 6-3
\end{tabular} \\
\hline C405A & & p/o C405 & V403 cathode bypass \\
\hline C405B & & p/o C405 & +150 v bypass \\
\hline C405C & & p/o C405 & DC filter V407A \\
\hline C406 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(220 \mu \mu \mathrm{f}+10 \%\); 500 v DC working; MIL type CM20B221K per spec MIL-C-5; 21964 part \#600120 & Coupling V404 \\
\hline C407 & & Same as C403 & Coupling V404 \\
\hline C408 & & Same as C403 & Coupling V405 \\
\hline C409 & & Same as C403 & Coupling V405 \\
\hline C410 & & Same as C344 & Video bypass R427 \\
\hline C411 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(.01 \mu \mathrm{f} \pm 10 \%\); 300 v DC working; -200 to +200 ppm per deg C load current \(\mathrm{N} / \mathrm{R}\); MIL type CM35C103K per spec MIL-C-5; 21964 dwg \#A2132725-6 & Coupling to output
J403 \\
\hline C412 & & Same as C411 & Coupling to output
\[
\mathrm{J} 404
\] \\
\hline C413 & & Not Used & \\
\hline C414 & & Same as C411 & Screen filter V408 \\
\hline C415 & & Same as C337 & Filter V409B \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C416 & & Same as C411 & Coupling V404 to V408 \\
\hline C417 & & Same as C402 & \(\underset{\text { V408 }}{\text { Coupling V402 to }}\) \\
\hline C418 & & Same as C403 & Coupling V406 \\
\hline C419 & & Same as C402 & Coupling V406 \\
\hline C420 & & Same as C411 & Coupling V406 to V407B \\
\hline C421 & & Same as C411 & Coupling, V407B to V401 \\
\hline C422 & 4 & CAPACITOR, FIXED, MICA DIELECTRIC: \(56 \mu \mu \mathrm{f}, \pm 2 \%\) tolerance, 300 v DC working, 00853 M-72; 21964 A9010542-1 (p/o DL401) & Delay line capacitor \\
\hline C423 & 4 & CAPACITOR ASSEMBLY, MICA DIELECTRIC: consisting of one 56 \(\mu \mu \mathrm{f}\) capacitor, \(\pm 1.12 \mathrm{mmf}\) tolerance and five \(110 \mu \mu \mathrm{f}\) capacitors \(\pm 2.2 \mu \mu \mathrm{f}\) tolerance, characteristic \(\mathrm{X}, 300 \mathrm{DC}\) working voltage; 72982 bracket assembly \#2826-01, CER type 2826-201 bracket; electrical characteristic per spec MIL-C-10950A; 21964 \#B9010473-2 (p/o DL401) & Delay line capacitor assembly \\
\hline C424 & 4 & CAPACITOR ASSEMBLY, MICA DIELECTRIC: consisting of six \(110 \mu \mu \mathrm{f}\) capacitors \(\pm 2.2 \mu \mu \mathrm{f}\) tolerance; characteristic \(\mathrm{X}, 300 \mathrm{DC}\) working voltage; 72982 button bracket assembly \#2826-01, 72982 2826-20I bracket; electrical characteristic per spec MIL-C-10950A; 21964 \#B9010473-1 (p/o DL.401) & Delay line capacitor assy \\
\hline C425 & & Same as C424 (p/o DL401) & Delay line capacitor assy \\
\hline C426 & & Same as C424 (p/o DL401) & Delay line capacitor assy \\
\hline C427 & & Same as C411 & Decoupling \\
\hline \begin{tabular}{l}
C428 \\
Cont \\
See C501
\end{tabular} & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(3300 \mu \mu \mathrm{f} \pm 10 \%\); 500 v DC working; MIL type CM30B332K per spec MIL-C-5; 21964 dwg \#A2133222-19 & Cathode bypass \\
\hline CR401 & & SEMI-CONDUCTOR DEVICE, DIODE: JAN type IN126 per spec MIL-E-1C; 21964 part \#701174 & Limiter \\
\hline CR402 & & Same as CR401 & Positive polarity selector \\
\hline CR403 & & Same as CR401 & Limiter \\
\hline CR404 & & Same as CR401 & Limiter \\
\hline CR405 & & Same as CR401 & Limiter \\
\hline DL401 & & DELAY LINE: electromagnetic type; overall delay of 12 microseconds; 2700 cps driving frequency; consists of one \(56 \mu \mu \mathrm{f}\) capacitor, twenty three \(110 \mu \mu \mathrm{f}\) capacitors and twenty four 1.83 mh coils \(\pm 2 \%\); 21964 \#D2060730G1 & 12 m seconds delay line Figure 6-3 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E401 & & Same as E201 & Shield for V401 \\
\hline E401A & & Same as E201A & Insert for E401 \\
\hline E402 & & Same as E307 & Shield for V402 \\
\hline E402A & & Same as E307A & Insert for E402 \\
\hline E403 & & Same as E201 & Shield for V403 \\
\hline E403A & & Same as E201A & Insert for E403 \\
\hline E404 & 6 & SHIELD, ELECTRON TUBE: JAN type TS103U01 per spec JAN-S-28A, modified 21964 \#A2132988-4 & Shield for V404 \\
\hline E404A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U01; MIL-STD-242A type \#901; 21964 \#A2132886-4 & Insert for E404 \\
\hline E405 & & Same as E307 & Shield for V405 \\
\hline E405A & & Same as E307A & Insert for E405 \\
\hline E406 & & Same as E404 & Shield for V406 \\
\hline E406A & & Same as E404A & Insert for E406 \\
\hline E407 & & Same as E404 & Shield for V407 \\
\hline E407A & & Same as E404A & Insert for E407 \\
\hline E408 & 5 & SHIELD, ELECTRON TUBE: JAN type TS102U03 per spec JAN-S-28A, modified, 21964 \#A2132988-3 & Shield for V408 \\
\hline E408A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U03; MIL-STD-242A type \#703, 21964 \#A2132886-3 & Insert for E408 \\
\hline E409 & & Same as E201 & Shield for E409 \\
\hline \begin{tabular}{l}
E409A \\
Cont \\
See E502
\end{tabular} & & Same as E201A & Insert for E409 \\
\hline J401 & & Not Used & \\
\hline J402 & & Same as J203 & Video input \\
\hline J403 & & Same as J203 & Video future use output Figure 6-3 \\
\hline J404 & & Same as J203 & Video output Figure 6-3 \\
\hline J 405 & & Same as J304 & Power and metering connector Figure 6-3 \\
\hline J406 & & Same as J203 & Blanking in Figure 6-3 \\
\hline J407 & & Same as J 203 & Test output \\
\hline J408 & & Same as J305 & Test point squitter control output Figure 6-3 \\
\hline J409 & & Same as J305 & Test point video input \\
\hline J410 & & Same as J305 & Test point future use output Figure 6-3 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D. MAINT ENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J411 & & Same as J305 & Test point video output Figure 6-3 \\
\hline J412 & & Same as J305 & Test point multivibrator output \\
\hline \begin{tabular}{l}
J4 13 \\
Cont \\
See J501
\end{tabular} & & Same as J305 & Test point blanking output Figure 6-3 \\
\hline L401 & 4 & COIL ASSEMBLY: 8 windings, universal wound, 553 turns of \#38EF wire, \(1.83 \mathrm{uh}+2 \%\); 34 ohms DC resistance; o/a dim. 3-1/4" lg, 15/32" dia; p/o DL401; per spec MIL-C-15305A; 21964 \#A9010824-1 & Delay line coil assembly \\
\hline L402 & & Same as L401 (p/o DL401) & Delay line assembly \\
\hline L403 Cont See L501 & & Same as L401 (p/o DL401) & Delay line assembly \\
\hline \begin{tabular}{l}
MP401 \\
Cont \\
See MP501
\end{tabular} & & Same as MP301 & Secures Cable \\
\hline R401 & & Same as R339 & Grid return V402A \\
\hline R402 & 6 & RESISTOR, FIXED, COMPOSITION: 4700 ohms; \(\pm 10 \%\); 2 watt; MLL type RC42GF472K per spec MLL-R-11; 21964 \#501249 & Plate load resistor V401 \\
\hline P401 & & Same as P201 & Connects to J301 \\
\hline P402 & & Not Used & \\
\hline P403 & & Same as P201 & Video future use output \\
\hline P404 & & Same as P201 & Video output \\
\hline P405 & & Same as J204 & Video power \\
\hline P406 & & Same as P20I & Blanking in \\
\hline \begin{tabular}{l}
P407 \\
Cont \\
See P501
\end{tabular} & & Same as P201 & Video test output \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R403 & & Same as R339 & Plate load resistor
V401 \\
\hline R404 & 6 & RESISTOR, FIXED, COMPOSITION: 10,000 ohms; \(\pm 10 \% ; 1 / 2\) watt, MIL type RC20GF103K per spec MIL-R-11; 21964 \#504243 & Screen dropping resistor \\
\hline R405 & 6 & RESISTOR, FIXED, FILM: 10,000 ohms; \(\pm 1 \% ; 1 / 2\) watt, MIL type RC20GF103K per spec MIL-R-11; 21964 \#501253 & Grid return V401 \\
\hline R406 & 6 & RESISTOR, FIXED, FILM: 100,000 ohms; \(\pm 1 \% ; 1 / 2\) watt, MIL type RN70B1003F per spec MIL-R-10509B; 21964 \#A9010519-2 & Grid bias bleeder V401 \\
\hline R407 & 6 & RESISTOR, FIXED, COMPOSITION: 33,000 ohms; \(\pm 10 \%\); 2 watt MIL type RC42GF333K per spec MIL-R-11; 21964 \#501259 & Screen bias resistor \\
\hline R408 & & Same as R320 & Grid return V402B \\
\hline R409 & & Same as R402 & Plate load resistor V403 \\
\hline R410 & & Same as R339 & Grid return V403 \\
\hline R411 & 6 & RESISTOR, FIXED, COMPOSITION: 6800 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF682K per spec MIL-R-11; 21964 \#504241 & Cathode bias V403 \\
\hline R412 & & Same as R339 & Plate load resistor V403 \\
\hline R413 & 6 & RESISTOR, FIXED, COMPOSITION: 15, 000 ohms, \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF153K per spec MIL-R-11: 21964 \#504245 & Trigger coupling to V404 \\
\hline R414 & & RESISTOR, FIXED, COMPOSITION: 91,000 ohms; \(\pm 5 \%\); 1 watt MIL type RC32GF913J per spec MIL-R-11; 21964 \#503837 & Cathode bias bleeder V403 \\
\hline R415 & 6 & RESISTOR, FIXED, COMPOSITION: 8200 ohms; \(\pm 10 \% ; 1 / 2\) watt: MIL type RC20GF822K per spec MIL-R-11; 21964 \#504242 & Grid return V404 \\
\hline R416 & 6 & RESISTOR, FIXED, COMPOSITION: 10,000 ohms; \(\pm 10 \%\); 2 watt; MIL type RC42GF103K per spec MIL-R-11; 21964 \#501253 & Plate load resistor V404 \\
\hline
\end{tabular}

Issued June 73

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PA RTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R417 & 6 & RESISTOR, FIXED, COMPOSITION: 3300 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20G F332K per spec MIL-R-11; 21964 \#504237 & Plate load resistor V404 \\
\hline R418 & & Same as R207 & Cathode bias V404 \\
\hline R419 & 6 & RESISTOR, FIXED, COMPOSITION: 56,000 ohms; \(\pm 10 \% ; 1 / 2\) watt; MLL type RC20GF563K per spec MLL-R-11; 21964 \#504252 & Grid return V404 \\
\hline R420 & 6 & RESISTOR, FIXED, COMPOSITION: 22,000 ohms; \(\pm 10 \%\); 2 watts; MIL type RC42G F223K per spec MLL-R-11; 21964 \#501257 & Cathode bias bleeder V404 \\
\hline R421 & & Same as R320 & Grid return V405 \\
\hline R422 & & Same as R339 & Cathode load V405 \\
\hline R423 & & Same as R339 & Cathode load V405 \\
\hline R424 & & Same as R320 & Grid return V405 \\
\hline R425 & 6 & RESISTOR, FIXED, COMPOSITION: \(47,000 \mathrm{ohms} ; \pm 10 \% ; 1 / 2\) watt; MIL type RC20GF473K per spec MIL-R-11; 21964 \#504251 & Suppressor grid return V401 \\
\hline R426 & 6 & RESISTOR, FIXED, COMPOSITION: 47,000 ohms; \(\pm 10 \%\); 1 watt; ML type RC32GF473K per spec MIL-R-11; 21964 \#503938 & Cathode lead V407A \\
\hline R427 & & RESISTOR, VARIABLE: wirewound element, 1 section; 10,000 ohms \(+10 \%\) : 2 watt nominal power rating, not tapped, no switch; JAN type RA 20A1SD103AK per spec JAN-R-19; 21964 \#B9010828-1 & Pulse count set V409B Figure 6-3 \\
\hline R428 & & Not Used & \\
\hline R429 & & Same as R307 & Serefn filter V408 \\
\hline R430 & 6 & RESISTOR, FIXEN, COMPOSITION: 470,003 ohms; \(: 10 \%, 1.2\) watt; MI: type RC20GF474K per spec MIL-R-11: 21:964 \#504263 & Filter V409B \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R431 & 6 & RESISTOR, FIXED, FILM: 14,700 ohms; \(\pm 10 \% ; 1 / 2\) watt power dissipation; MIL type RN70B1472F per spec MIL-R-10509B 21964 \#A9010519-8 & Bias voltage divider for V409B \\
\hline R432 & 6 & RESISTOR, FIXED, COMPOSITION: 1 megohm; \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF105K per spec MIL-R-11; 21964 \#504267 & Grid resistor V408 \\
\hline R433 & & RESISTOR, FIXED, FILM: 511,000 ohms; \(\pm 1 \% ; 1 / 2\) watt; MIL type RN70B5113F per spec MIL-C-10509B; 21964 \#9010519 & \[
\begin{aligned}
& \text { Pulse stretcher } \\
& \text { V409B }
\end{aligned}
\] \\
\hline R434 & & Same as R320 & Trigger coupling to V406 \\
\hline R435 & & Not Used & \\
\hline R436 & 6 & RESISTOR, FIXED, COMPOSITION: 47, 000 ohms; \(+10 \%\); 2 watt MIL type RC42GF473K per spec MLL-R-11; 21964 \#50126I & Cathode bias bleeder
V406 \\
\hline R437 & 6 & RESISTOR, FIXED, COMPOSITION: 2.2 megohm; \(\pm 10 \%\); \(1 / 2\) watt; MLL type RC20GF225K per spec MIL-R-11; 21964 \#504271 & Grid return V406 \\
\hline R438 & & Same as R339 & Plate load resistor
V407B \\
\hline R439 & & Same as R339 & Plate load resistor
V406 \\
\hline R440 & & Same as R402 & Plate load resistor V406 \\
\hline R441 & & Same as R339 & Cathode load resistor V406 \\
\hline R442 & & Same as R406 & Grid return V406 \\
\hline R443 & 6 & RESISTOR, VARLABLE: composition element; 1 section, 250,000 ohms; \(+10 \%\); 2 watts nominal power rating, no switch; MIL type RV4LAVSA254A per spec MIL-R-94 and MIL-STD-242 (ships) 21964 \#A2133049-7 & Blanking time adjust V406 Figure 6-3 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R444 & & RESISTOR, FIXED, COMPOSITION: 100,000 ohms, \(\mathbf{~} 5 \%\); \(1 / 2\) watt; MIL type RC20G F104J per spec MIL-R-11; 21964 \#504151 & Grid return V407B \\
\hline R445 & & RESISTOR, FIXED, COMPOSITION: 1.5 megohms; \(\pm 5 \% ; 1 / 2\) watt; MIL type RC20G F155J per spec MIL-R-11; 21964 \#504179 & Grid bias bleeder V407B \\
\hline R446 & & Same as R339 & Cathode resistor V407B \\
\hline R447 & 6 & RESISTOR, FIXED, FILM: 2,740 ohms; \(\pm 1 \% ; 1 / 2\) watt; MIL type RN70B2741F per spec MIL-R-10509B; 21964 \#A9010519-5 & Voltage divider V407A \\
\hline R448 & & Same as R201 & Parasitic suppressor V405 \\
\hline R449 & & Same as R201 & Parasitic suppressor V405 \\
\hline R450 & & Same as R201 & Parasitic suppressor V405 \\
\hline R451 & & Same as R201 & Parasitic suppressor V404 \\
\hline R452 & 6 & RESISTOR, FIXED, COMPOSITION: 470 ohms; \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF471K per spec MIL-R-11; 21964 \#504227 & Cathode resistor V401 \\
\hline R453 & & Same as R411 & Voltage divider test output \\
\hline R454 & & Same as R309 & Voltage divider test output \\
\hline R455 & 6 & RESISTOR FIXED, COMPOSITION: 1200 ohms; \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF122K per spec MLL-R-11; 21964 \#504232 & Limiter resistor
\(V 402 \mathrm{~A}\) \\
\hline R456 & 6 & RESISTOR, VARIABLE: wirewound element 1 section; 5000 ohms; \(\pm 10 \%\); 2 watt nominal power rating; not tapped, no switch; JAN type Ra20A1SD502AK per spec JAN-R-19; 21964 \#B9010828-2 & Limter resistor V403 Figure 6-5 \\
\hline R457 & 6 & RESISTOR, FIXED, FILM: 2,150 ohms; \(\pm 1 \% ; 1 / 2\) watt; MIL type RN70B2151F per spec MIL-R-10509B; 21964 \#A9010519-10 & \[
\begin{aligned}
& \text { Limiter resistor } \\
& \text { V403 }
\end{aligned}
\] \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline \begin{tabular}{l}
R458 \\
Cont \\
See R501
\end{tabular} & & Same as R402 & Decoupling \\
\hline \begin{tabular}{l}
T401 \\
Cont \\
See T501
\end{tabular} & & TRANSFORMER, PULSE: Interstage type; 10, 000 ohms at 2700 cycle primary input impedance, 47,000 ohms at 2700 cycles secondary output impedance; direct current resistance not rated for primary or secondary; 49956 \#363-6002G2; per spec MIL-T-27A; 21964 \#A1069872 & Impedance matching between V408 and V409B Figure 6-3 \\
\hline TB401 & 2 & TERMINAL BOARD: 64 terminals; solder stud type; 21964 \#A9010398-1 & Terminal board in video chassis assy Figure 6-5 \\
\hline \begin{tabular}{l}
TB402 \\
Cont \\
See TB- \\
501
\end{tabular} & 2 & TERMINAL BOARD: 60 terminals; solder stud type; 21964 \#A9010408-1 & Terminal board in video chassis assy Figure 6-5 \\
\hline V401 & & ELECTRON TUBE: pentode, MLL type 5725/6AS6W per spec MIL-E-1C; 21964 \#700576 & Blanking gate \\
\hline V402 & & Same as V307 & \begin{tabular}{l}
V402A: 1st video a mplifier Figure 6-3 \\
V402B: 2nd video amplifier
\end{tabular} \\
\hline V403 & & Same as V401 & Decoder Figure 6-3 \\
\hline V404 & & ELECTRON TUBE: dual triode; MIL type 5670 per spec MIL-E-1C; 21964 \#700563 & Multivibrator Figure 6-3 \\
\hline V405 & & Same as V307 & Two cathode followers Figure 6-3 \\
\hline V406 & & Same as V404 & Blanking mult \({ }^{-}\) vibrator Figure 6-3 \\
\hline V407 & & Same as V404 & Phase inverter and cathode followers Figure 6-3 \\
\hline V408 & & ELECTRON TUBE: pentode; MIL type 6005/6AQ5W per spec MIL-E-1C; 21964 \#701131 & Pulse amplifier Figure 6-3 \\
\hline \[
\begin{aligned}
& \text { V409 } \\
& \text { Cont } \\
& \text { See V501 }
\end{aligned}
\] & & Same as V306 & DC clamp and pulse connector Figure 6-3 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCAIING \\
FUNCTIION
\end{tabular} \\
\hline XV401 & & Same as XV308 & Socket for V401 \\
\hline XV402 & & Same as XV307 & Socket for V402 \\
\hline XV403 & & Same as XV308 & Socket for V403 \\
\hline XV404 & & Same as XV307 & Socket for V404 \\
\hline XV405 & & Same as XV307 & Socket for V405 \\
\hline XV406 & & Same as XV307 & Socket for V406 \\
\hline XV407 & & Same as XV307 & Socket for V407 \\
\hline XV408 & & Same as XV308 & Socket for V408 \\
\hline \begin{tabular}{l}
XV409 \\
Cont \\
See XV501
\end{tabular} & & Same as XV308 & Socket for V409 \\
\hline C501 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(10 \mu \mathrm{f} \pm 10 \% ; 600 \mathrm{v}\) DC working; MIL type CP70E1EF106K per spec MIL-C-25; 21964 part \#641041 & Filter \\
\hline C502 & & CAPACITOR, FLXED, PAPER DIELECTRIC: . \(5 \mu \mathrm{f}+10 \%\); 600 v DC working: MIL type CP54B1EF504K per spec MIL-C-25; 21964 part \#640404 & Filter \\
\hline C503 & & CAPAC ITOR, FIXED, PAPER DIELECTRIC: 2 sections, each section \(0.10 \mu \mathrm{f}+20 \%-10 \%\); 600 v DC working; MIL type CP69B4EF104V per spec MIL-C-25A; 21964 \#A9010883-2 & Filter Figure 6-5 \\
\hline C504 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(2 \mu \mathrm{f} \pm 10 \%\); 600 v DC working; MIL type CP70E1EF205K per spec MIL-C-25; 21964 \#641037 & Filter Figure 6-5 \\
\hline C505 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(1.0 \mu \mathrm{f} \pm 10 \%\); 600 v DC working; CPWB1EF105K per spec MIL-C-25; \(21964 \# 640514\) & Filter Figure 6-5 \\
\hline C506 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 2 sections, each section \(0.5 \mu \mathrm{f}+20 \%-10 \%\); 600 v DC working; MLL type CP61B6EF504V per spec MIL-C-25; 21964 \#640611 & Filter Figure 6-5 \\
\hline DS501 & & LAMP, INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens, double contact bayonet base; clear, 24446 \#10C7/IDC; 21964 part \#710071 & Power on indicator Figure 3-1 \\
\hline DS502 & & LAMP, GLOW: neon gas, 0.25 watt, \(67-87 \mathrm{v}\) DC striking voltage; double contact bayonet type; MIL type NE-16 per spec MIL-L-15098; 21964 dwg \#A2060350 & Interlock open indicator \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOGATING FUNGTION \\
\hline E501 & & Not Used & \\
\hline E502 & & Same as E408 & Shield for V502 \\
\hline E502A & & Same as E408A & Insert for E502 \\
\hline E503 & & CONNECTOR, ADAPTER: 2 contacts, 1 type BNC male, 1 type N female, MIL type UG-201A/U; ASESA 49-2A SC-D-72309; 21964 \#A2120071 & Mixer LO input adapter \\
\hline E504 & & Same as E201 & Shield for V504 \\
\hline E504A & & Same as E201A & Insert for E504 \\
\hline E505 & & Same as E408 & Shield for V505 \\
\hline E505A & & Same as E408A & Insert for E505 \\
\hline E506 & & Same as E408 & Shield for V506 \\
\hline E506A & & Same as E408A & Insert for E506 \\
\hline \[
\begin{gathered}
\text { E507 } \\
\text { thru } \\
\text { E526 }
\end{gathered}
\] & & Not Used & \\
\hline E527 & & RETAINER, CAPACITOR: MIL type CP07SA4, per spec MIL-C-25; 21964 \#384067 & Mounting bracket for C504 \\
\hline E528 & & RETAINER, CAPACITOR: MIL type CP07SD3 per spec MIL-C-25; 21964 \#384082 & Mounting bracket for C501 \\
\hline \[
\begin{gathered}
\text { E529 } \\
\text { thru } \\
\text { E549 }
\end{gathered}
\] & & Not Used & \\
\hline E550 & & RETAINER, ELECTRON TUBE: 96458, similar to \#BA-20353: 21964 \#A9010812-1 & Retainer for V501 \\
\hline E551 & & RETAINER, ELECTRON TUBE: bakelite; 21964 \#A9011495-1 & Retainer for V503 \\
\hline \[
\begin{gathered}
\text { E552 } \\
\text { thru }
\end{gathered}
\] & & Not Used & \\
\hline E597 & & & \\
\hline E598 & 6 & RETAINER, CAPACITOR: MIL type CP0905A6 per spec MIL-C-25 21964/384011 & Mounts capactor C505 in power supply \\
\hline E599 & & Same as E598 & Mounts capacitor C506 in power supply \\
\hline F501 & & FUSE, CARTRIDGE: 3 amp , 125 v ; time delay, MIL type F02D3R00B per MIL-STD MS90-07827-1 and spec MIL-F-16160C; 21964 \#882237 & Power fuse Figure 3-1 \\
\hline F502
F503 & & \begin{tabular}{l}
Same as F501 \\
Same as F501
\end{tabular} & \begin{tabular}{l}
Power fuse \\
Figure 3-1 \\
Spare fuse
\end{tabular} \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J501 & 4 & CONNECTOR, RECEPTACLE ELECTRICAL: 1 contact, round; polarized, straight type; 1000 v max, voltage, 50 ohms nominal impedance, modified as follows, all cable accommodations are deleted from the commercial connector and in its place a machined body of a low pass filter is inserted, 11/16-24 thread with a set screw \(4 / 40-1 / 8^{\prime \prime} \lg\) is the holding device, MIL type UG-571/U (p/o Z501); NOT REPLACEABLE & \begin{tabular}{l}
Signal input \\
Figure 6-3
\end{tabular} \\
\hline J502 & & \begin{tabular}{l}
CONNECTOR, RECEPTACLE ELECTRICAL: BNC series; 74868 \\
\#86025; MIL type UG-909/U per BuShips dwg \#REB49058; 21964 \#A2132720
\end{tabular} & Local oscillator input Figure 6-3 \\
\hline J503 & & Same as J502 & Video future use output Figure 6-3 \\
\hline J504 & & Same as J502 & Video output Figure 6-3 \\
\hline J505 & & CONNECTOR, RECEPTACLE ELECTRICAL: 5 contacts, male, round, positive polarization; straight type; MIL type AN3102A-14S-5P per MIL-C-5015B; 21964 \#752190 & Receiver power input Figure 6-3 \\
\hline J506 & & Same as J502 & \begin{tabular}{l}
Blanking input \\
Figure 6-3
\end{tabular} \\
\hline J507 & & Same as J502 & \begin{tabular}{l}
Test output \\
Figure 3-1
\end{tabular} \\
\hline J508 & 4 & CONNECTOR, RECEPTACLE, ELECTRICAL: 1 contact, round, polarized, straight type; 50 ohms nominal imped ance, modified as follows, all cable accommodations are deleted from commercial connector and in its place a machined body of low pass filter inserted; 5/8-24 thread with set screw \(4 / 40,1 / 8\) as a holding device; MIL type UG-23B/U (p/o Z501); NOT REPLACEABLE & Low pass filter output \\
\hline L501 & & REACTOR: fixed inductance; one section, 10 henries; 200 ma DC ; 110 ohms DC resistance; MIL type TF1RX04YY; 49956 \#292-5633G1 21964 \#A1069614 & 150 v filter choke Figure 6-3 \\
\hline M501 & & AMMETER: mounted, flush mounting panel type; DC; 0 to 100 microampere graduated in increments of 5; 50 millivolt drop across terminals for full scale deflection: calibrated for use on non-magnetic panel, MIL type MR26W100DCUAR per spec MIL-M-10304A; 21964 \#A2060455-5 & \begin{tabular}{l}
Test meter \\
Figure 3-1
\end{tabular} \\
\hline MP501 & & KNOB: pointer; black, phenolic body; MS700-18S per MIL-STD-242A; 21964 \#B2137233-2 & Meter switch knob \\
\hline MP502 & & Not Used & \\
\hline MP503 & & Not Used & \\
\hline MP504 & & CAP, ELECTRICAL: brass; fits BNC female connectors; MIL type CW-123 A/U per Navy dwg; REA 49050 and MIL-C-3608; 21964 \#A2141971 & Cover for J507 \\
\hline \[
\begin{gathered}
\text { P501 } \\
\text { thru } \\
\text { P507 }
\end{gathered}
\] & & Not Used & \\
\hline P508 & & Same as P202 & Low pass filter output \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LifT
RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R501 & 6 & RESISTOR, FIXED, COMPOSITION: 47 ohms; \(\pm 10 \%\); 2 watt; MIL type RC42GF470K per spec MIL-R-11; 21964 \#501225 & Plate decoupling V503 \\
\hline R502 & & Same as R501 & Plate decoupling V503 \\
\hline R503 & & Same as R341 & Grid decoupling V503 \\
\hline R504 & & Same as R341 & Grid decoupling V503 \\
\hline R505 & & RESISTOR, FIXED, FILM: 1 megohm; \(\pm 1 \% ; 1 / 2\) watt; MIL type RN70B1004F per spec MIL-R-10509B; 21964 \#A9010519-1 & Plate resistor V504 \\
\hline R506 & 6 & RESISTOR, FIXED, FILM: 14,700 ohms; \(\pm 1 \%\); 2 watt, MIL type RN80B1472F per spec MIL-R-10509A and MLL-STD-242A; 21964 \#A9010556-1 & Divider network Figure 6-5 \\
\hline R507 & & Same as R427 & Voltage control Figure 6-3 \\
\hline R508 & & RESISTOR, FIXED, FILM: 10,000 ohms; \(\pm 1 \% ; 2\) watt, MIL type RN80B1002F per spec MIL-R-10509A and MIL-STD-242A; 21964 \#A9010556-2 & Divider network Figure 6-5 \\
\hline R509 & 6 & RESISTOR, FIXED, COMPOSITION: 2200 ohms; \(\pm 10 \%\); 2 watt; MIL type RC42GF222K per spec ML-R-11; 21964 \#501245 & Filter \\
\hline R510 & 6 & RESISTOR, FIXED, WIREWOUND: inductive winding: 1000 ohms \(\pm 5 \%\); 10 watts; not tapped; non adjustable; ML type RW31G 102 per spec MIL-R-26A; 21964 \#A9010887-1 & Filter network \\
\hline R511 & & Same as R509 & Filter \\
\hline R512 & & Same as R509 & Filter \\
\hline R513 & & Same as R509 & Filter \\
\hline R514 & & Not Used & \\
\hline R515 & & RESISTOR, FIXED, FILM: non inductive; 1.96 megohms; \(\pm 1 \%\) 1/2 watt; MIL type RN70B1964F per spec MIL-R-10509B; 21964 \#99010519-9 & Meter multiplier \\
\hline R516 & & Same as R406 & Meter multiplier \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICÁTOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R517 & 6 & \[
\begin{aligned}
& \text { RESISTOR, FIXED, FILM: non inductive; } 1000 \text { ohms; } \pm 1 \% ; 1 / 2 \text { watt; } \\
& \text { MIL type RN70B1001F per spec MIL-R-10509B; } 21964 \\
& \text { \#A9010519-3 }
\end{aligned}
\] & Meter series resistor \\
\hline R518 & & Same as R509 & Filter \\
\hline R519 & & Same as R509 & Filter \\
\hline R520 & & RESISTOR, FIXED, WIREWOUND: 280 ohms; 3 watt; MIL type RW59V281 per spec MIL-R-26C; 21964 dwg \#A2132711-01 & Voltage dropping resistor \\
\hline R521 & 6 & RESISTOR, FIXED, COMPOSITION: \(15,000 \mathrm{ohms} ; \pm 10 \%\); 1 watt; MIL type RC32GF153K per spec MIL-R-11; 21964 \#503932 & Voltage dropping resistor \\
\hline S501 & & SWITCH, ROTARY, SELECTOR, MINIATURE: 1 section, 6 positions 2 poles non-shorting contacts; 21964 \#B2060201 & Meter selector Figure 3-1 \\
\hline S502 & & SWITCH, TOGGLE: single-pole, single throw; 0.75 amp 125 v DC, 15 amp 125 v AC, JAN type ST42A, per spec JAN-S-23; 21964 \#828212 & Power on-off switch Figure 3-1 \\
\hline T501 & & TRANSFORMER, POWER, STEP-DOWN: primary winding; 120 v AC, 60 cycles single phase; 3 output windings, \#1 secondary 5.0 v , 2 amp center tapped, \#2 secondary \(6.3 \mathrm{v}, 6.5 \mathrm{amp}\), \#3 secondary \(6.3 \mathrm{v}, 3.4 \mathrm{amp}\) center tapped; MIL type TF1SX01YY per spec MIL-T-27A; 49956 \#292-5624G1 21964 \#A1069870 & Filament power Figure 6-3 \\
\hline T502 & & TRANSFORMER, POWER, STEP-UP: primary winding 120 v AC, 60 cycle, single phase, secondary winding \(\# 1770 \mathrm{v}\) center tapped at 200 ma , secondary \#2 450 v center tapped at 55 ma ; MIL type TF1SX02YY per spec MIL-T-27A; 49956 \#292-5623G1, 21964 \#1069828 & Plate power Figure 6-3 \\
\hline TB501 & & TERMINAL BOARD: 8 terminals; single row, thru type terminals; MIL type 7 TB8 per spec MIL-T-16784 and Navy dwg 9000-S6505G73214; 21964 \#A2133072-1 & Power supply terminal board Figure 6-3 \\
\hline TB502 & 2 & TERMINAL BOARD: 28 terminals, solder stud type; 21964 \#A 9010522-1 & Power supply terminal board Figure 6-5 \\
\hline V501 & 6 & ELECTRON TUBE: dual diode; type 5R4WGB per spec MLL-E-1C; (Navy) 21964 \#A2132449 & Rectifier full wave Figure 6-3 \\
\hline V502 & 6 & ELECTRON TUBE: dual diode; MIL type 6X4W per spec MIL-E-1C; 21964 \#700151 & Rectifier full wave \\
\hline V503 & & ELECTRON TUBE: dual triode; MIL type 6080WA per spec MIL-E-1C; 21964 \#701276 & Voltage regulator Figure 6-3 \\
\hline V504 & & Same as V201 & Amplifier \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D. MAINTENANCE PARTS LIST

RADIO RECEIVER R-824/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline V505 & & ELECTRON TUBE: diode; MIL type 6627/0B2WA; per spec MIL-E-1 (Navy); 21964 spec \#2133279 & Voltage reference \\
\hline V506 & & Same as V505 & Voltage reference \\
\hline W501 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, copper, stranded, \#21 AWG silvered copper wire, 7 strand, single strand, \(0.0270 \mathrm{in} . \pm 0.0010 \mathrm{in}\), overall bare wire 0.081 in dia \(\pm 0.002 \mathrm{in}\)., solid teflon dielectric, \(R G-115 / \mathrm{U}\) type; includes 2 MIL type connectors, one located on each end, P202 and P508, as per 21964 \#B2060983G1 & Meter signal input \\
\hline W502 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; incl 2 MIL type connectors J502 and P201, as per 21964 \#C2060988G4 & Connects frequency multiplier oscillator to mixer \\
\hline W503 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; incl 2 MIL type connections J 503 and P403, one located at each end, as per 21964 \#C2060988G3 & Connects video chassis to future use output \\
\hline W504 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; 2 MIL type connectors, one located at each end, incl J504 and P404, as per 21964 \#C2060988G2 & Connects video chassis to video output \\
\hline W505 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; incl 2 MIL type connectors, J507 and P407, as per 21964 \#C2060988G5 & Connects video chassis to test output \\
\hline W506 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; 2 MIL type connectors, one located each end, incl J506 and P406, as per 21964 \#C2060988G1 & Connects external blanking to video chassis \\
\hline  & & Not Used & \\
\hline W511 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG-141/U; incl 2 MIL type connectors, E346 and P303, one located at each end, as per 21964 \#A9010410-3 & IF amplr inpu: \\
\hline XDS501 & & LIGHT, INDICATOR: friction mtg lens holder; \(125 \mathrm{v}, 6\) watts; enclosed frame; steel shell; black nickel; MIL type LH63PW3 per spec MLL-L-3661, dwg MS-90286; 21964 dwg \#A2133069-5 & Holder for DS501 \\
\hline XDS502 & 6 & LAMP HOLDER: 125 v ; Military Standard la mpholders dwg MS90290; 72619 9S4634-L-46; per spec MIL-L-3661; type LH-71-XXO; 21964 dwg \#A2142519 & Holder for DS502 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

\section*{RADIO RECEIVER R-824/URN}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline XF501

XF502 & & \begin{tabular}{l}
FUSE HOLDER: extractor post type; accommodates 2 fuses 1-1/4" lg. by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type; seated; MIL type FHL-10G per BuShips dwg \#9000-S6202-74228 and MIL-F-19207 (Ships), 21964 dwg \#A2060402 \\
Not Used
\end{tabular} & Holder for F501 and F502 \\
\hline XF503 & & FUSE HOLDER: extractor post type; accommodates 1 fuse, 1-1/4" \(\lg\) by \(1 / 4^{\prime \prime}\) dia, blown fuse indicating type; sealed; MIL type FHL11-G per BuShips dwg \#9000-S6202-74229 and MIL-F-19207 (Ships); 21964 dwg \#A2060403 & Spare fuse holder \\
\hline XV501 & 6 & SOCKET, ELECTRON TUBE: 8 contacts, beryllium, silver plated; octal dual shaped; JAN type TS101P02 per spec JAN-S-28A; 21964 " 740031 & Tube socket for V501 Figure 6-5 \\
\hline XV502 & & Same as XV308 & Socket for V502 Figure 6-5 \\
\hline XV503 & & Same as XV501 & Socket for V503 Figure 6-5 \\
\hline XV504 & & Same as XV308 & Socket for V504 Figure 6-5 \\
\hline XV505 & & Same as XV308 & Socket for V505 Figure 6-5 \\
\hline XV506 & & Same as XV308 & Socket for V506 Figure 6-5 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline 601-799 & & \begin{tabular}{l}
CODER-INDICATOR KY-382/GRN-9D \\
CODER-INDICATOR KY-382/GRN-9D: data regarding input signals received, \(1,15 \mathrm{cps}\) reference trigger pulse, pulse generated each time antenna passes through north, 15 times per second; 135 cps reference trigger pulse, pulse generated each time antenna pattern passes through \(40^{\circ}, 80^{\circ}, 120^{\circ}, 160^{\circ}, 200^{\circ}, 240^{\circ}, 280^{\circ}, 320^{\circ}, 135\) times per second; 1 video pulse, pulse is either a distance interrogation pulse or random noise pulse generated by the receiver in the absence of a distance interrogation pulse; check output with cathode ray indicator; operating power requirements, AC; 177 v or \(120 \mathrm{v}, 60\) cycles single phase, 300 watts; open aluminum framework; overall dim. 13-1/2' wide, 26-7/8" \(\lg\)., 17-1/16" high; rack mounted, with pull-out slides, front access only; generates 135 cps reference bursts (triggered from antenna) which consists of six pulse-pairs spaced 24 microseconds apart; generates 15 cps reference bursts (triggered from antenna) which consists of 12 pulse-pairs spaced 30 microseconds apart; processes and delays distance interrogation pulses and random noise pulses; generates the identification call of the beacon and identity keys the transmitter; mixes the various component pulses and encodes the composite signal; built-in coding assembly, power supply chassis, provisions for adjusting the keyer-code without interrupting the distance interrogations or azimuth services; provides coded signal for transmitter; provides monitoring facilities for antenna control; 21964 \#H2060001 and A2060001
\end{tabular} & Part of ReceiverTransmitter Group Figure 6-51 \\
\hline B602 & & MOTOR, ALTERNATING CURRENT, INDUCTION TYPE: 105-132 v AC, 60 cycles, \(\pm 5\) cps; single phase, 10 watt; 1740 rpm single shaft, ccw rotation looking from shaft end; closed frame; - 54 degrees \(\mathbf{C}\) to + 85 degrees C temp, range; 3 flexible wire leads, fixed mounting base, 4 mtg. screws \(8-32\), spaced 90 degrees apart MIL-spec. MIL-M-17509 Amend 1; 89482 \#RBC-2505, per 91264 \#1054983 & Identification keyer driving motor Figure 6-6 \\
\hline C601 thru C603 & & Not Used & \\
\hline C604 & & CAPACITOR, FLXED, PAPER DIELLECTRIC: \(\mathbf{4 \mu} \boldsymbol{\mu}, \mathrm{t}^{20 \%} ; \mathbf{4 0 0} \mathrm{v}\) DC working; MIL type CH53B1-EE405M per MIL-STD-242A and per spec MIL-C-18312; 21964 dwg \#A2060302-7 & \[
\text { B }+ \text { filter, } 250 \mathrm{v}
\]
Figure 6-52 \\
\hline C605 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(\mathbf{3 3 0} \mu \mu \mathrm{f}, \pm 5 \% ; 500 \mathrm{v}\) DC working; MIL type CM20C331J per spec MIL-C-5A; 21964 \#A2133174-30 & Capacitor for V601 and V602 \\
\hline C606 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(680 \mu \mu \mathrm{f}, \pm 2 \% ; 300 \mathrm{v}\) DC working; -100 to +100 parts per million per deg C temp coefficient; MIL type CM20D681-G per spec MIL-C-5; 21964 \#A2060310-14 & 15 cps gate multivibrator coupling capacitor \\
\hline C607 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(01 \mu \mu \mathrm{f} \pm 10 \%\); 300 v DC working; MIL type CM35C103K per spec MIL-C-5; 21964; *A2132725-6; Same as C411 & Capacitor for V602 and V603 \\
\hline C608 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(6800 \mu \mu \mathrm{f} \pm 2 \% ; 500 \mathrm{~V}\) DC working; temperature coefficient \(\mathbf{- 2 0}\) to +100 parts/million/degrees C; MIL type CM35E682G, per spec MIL-C-5 21964 \#A20603080-8 & Tuned circuit capacitor for 33.333 kc ringing circuit \\
\hline C609 & & Same as C607 & Coupling capacitor for V603 and V610 \\
\hline C610 & & Same as C607 & Capacitor for V604 and V605 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
UESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C611 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(51 \mu \mu \mathrm{f}, \pm 5 \% ; 500 \mathrm{v}\) DC working; MIL type CM20C510J per spec MIL-C-5; 21964 \#600171 & Timing, V605 cathode coupled multivibrator \\
\hline C612 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(68 \mu \mu \mathrm{f}, \pm 10 \%\); 500 v DC working; MIL type CM20B680K; per spec MIL-C-5; 21964 \#600114 & Grid coupling V605, delay line blocking oscillator \\
\hline C613 & & CAPACITOR. FIXED, PAPER DIELECTRIC: 1 section, \(0.10 \mu \mathrm{f}\), \(\pm 10 \%\); 400 v DC working, MIL type CP0-5AIKE 104 K , per spec MIL-C-25A; 21964 \#A2132594-1 & Decoupling capacitor for V606 \\
\hline C614 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(3300 \mu \mu \mathrm{f}, \pm 10 \% ; 500 \mathrm{v}\) DC working; MIL type CM30B332K per spec MIL-C-5; 21964 \#A2133222-19; Same as C428 & Lowpass filter capacitor for V606 \\
\hline C615 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1 section, \(0.047 \mu\) f, \(\pm 10 \% ; 400 \mathrm{v}\) DC working, MIL type CP05A1KE 473 K , per spec MIL-C-25A; 21964 \#A2132594-5. & -105v filter capacitor \\
\hline C616 & & Same as C613 & - 105v filter capacitor \\
\hline C617 & & Same as C612 & Grid coupling V615 output multivibrator \\
\hline C618 & & Same as C607 & Grid coupling V615, output multivibrator \\
\hline C619 & & Same as C613 & Grid coupling V607-2 output cathode follower \\
\hline C620 & & Same as C612 & Synch output coupling capacitor \\
\hline C621 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(15 \mu \mu \mathrm{f}, \pm 10 \%, 500 \mathrm{v}\) DC working; MIL type CM2-0B150K per spec MIL-C-5; 21964 \#600106 & Timing V615, output multivibrator \\
\hline C622 & & Same as C607 & Coupling capacitor V608, V1350 ref. cycle oscillator \\
\hline C623 & & Same as C615 & Plate bypass, V608 \\
\hline C624 & & Same as C605 & Grid coupling, V609, 135 cps gate multivibrator \\
\hline C625 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(330 \mu \mu \mathrm{f}, \pm 2 \%\); 500 v DC MIL type CM20D331G per spec MIL-C-5; 21964 \#600227 & Timing V609, 135 cps gate multivibrator \\
\hline C626 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(3000 \mu \mu \mathrm{f} \pm 2 \%\); 500 v DC working; -20 to +100 parts/million/degree \(C\) temperature coefficient; MIL type CM30-E302G, per spec MIL-C-5; 21964 \#A2060301-18 & Tuning, V610, 41.667 kc ringing circuit \\
\hline C627 & & Same as C607 & Grid coupling V604-1, ref burst amplifier \\
\hline C628 & & Same as C607 & Input coupling, auxiliary group feed back circuit \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C629 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(390 \mu \mu \mathrm{f}, \pm 10 \%\); 500 v DC working; MIL type CM20B391K, per spec MIL-C-5; 21964 \#600123 & Output coupling, auxiliary group feedback circuit \\
\hline C630 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(200 \mu \mu \mathrm{f}, \pm 5 \% ; 500 \mathrm{v}\) DC; MIL type CM20C201-J per spec MIL-C-5A; 21964 \#A2 133174-25 & Input coupling north group feed-back circuit \\
\hline C631 & & Same as C607 & Output coupling, north group feed-back circuit \\
\hline C632 & & Same as C613 & Grid coupling V611, priority \\
\hline C633 & & Same as C613 & Grid coupling V611, priority \\
\hline C634 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(4700 \mu \mu \mathrm{f}, \pm 10 \%\) tolerance, 500 v DC working; MIL type CM35B472K per spec MIL-C-5A; 21964 \#A2060309-2 & Cathode bypass V611, priority \\
\hline C635 & & Same as C607 & Grid coupling V611, priority \\
\hline C636 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(100 \mu \mu \mathrm{f} \pm 10 \%\), 500 v DC working; MIL type CM20-B101K per spec JAN-C-15; 21964 \#600116; Same as C402 & Grid coupling V611, priority \\
\hline C637 & & Same as C613 & Filter, bias supply \\
\hline C638 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(300 \mu \mu \mathrm{f}, \pm 5 \%\); 300 v DC working; MIL type CM20C301J per spec MIL-C-5A; 21964 \#A2 133 174-29 & Grid coupling V604-2 keyer \\
\hline C639 & 6 & CAPACITOR, FIXED, PAPER DIELECTRIC: 1 section; 300 v DC working, \(.1 \mu \mathrm{f}, \pm 5 \% 56289\) \#96P10453S2; 21964 \#A2061733-2 & Coupling, feed-back V612, 1350 cycle oscillator \\
\hline C640 & & Same as C612 & Grid coupling V612, 1350 cycle oscillator \\
\hline C641 & & Same as C613 & Grid coupling V613-1, 1350 cycle amplifier \\
\hline C642 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(1000 \mu \mu \mathrm{f}, \pm 10 \%\); 300 v DC working; MIL type CM20B102K per spec MIL-C-5; 21964 \#A2060311-12 & Grid coupling V614 \\
\hline C643 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(\mathbf{4 7 0} \mu \mu \mathrm{f}, \pm 2 \% 500 \mathrm{v}\) DC working; -100 to +100 parts per million per deg. C temp. coefficient; MIL type CM20D471G per spec MIL-C-5; 21964 \#600231 & Timing, V614, 100 \(\mu \mathrm{sec}\) multivibrator \\
\hline C644 & & Same as C612 & Differentiating capacitor V614, 100 \(\mu \mathrm{sec}\) multivibrator \\
\hline C645 & & Same as C612 & Differentiating capacitor V614, 100 \(\mu \mathrm{sec}\) multivibrator \\
\hline C646 & & Same as C607 & Filter, bias supply \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C647 & & Same as C607 & Grid coupling, V610, 41.667 kc ringing circuit \\
\hline C648 & & Same as C642 & Coupling capacitor, V605 cathode coupled MV \\
\hline C649 & & CAPACITOR, FIXED, MICA DIELECTRIC: . \(01 \mu \mathrm{f}, \pm 2 \%\); 300 v DC working; temperature coefficient -20 to +100 parts/million/degrees C; MIL type CM35E I03G, per spec MIL-C-5; 21964 \#A2060308-12 & Tuned circuit capacitor for 33.333 kc ringing circuit V603 \\
\hline C650 & & Same as C649 & Tuning V610, 41.667 kc ringing circuit \\
\hline C651 & & Same as C607 & Coupling capacitor V6I2, 1350 cycle oscillator \\
\hline C652 & & CAPACITOR, FIXED, PLASTIC DIELECTRIC: 1 section; 400 v DC working, . \(047 \mu \mathrm{f}, \pm 5 \% 56289\) \#114P47354S2; 21964 \#A2060300-5 & \[
\begin{aligned}
& \text { Tuning, V612, } 1350 \\
& \text { cycle tone oscil- } \\
& \text { lator Figure 6-52 }
\end{aligned}
\] \\
\hline C653 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1 section; 300 v DC working, . \(047 \mu \mathrm{f}, \pm 5 \%\) tolerance; 56289 \#96P47353S2; 21964 \#A2061733-1 & Tuning, V612 plate 1350 cycle tone oscillator \\
\hline \[
\begin{aligned}
& \text { C654 } \\
& \text { thru } \\
& \text { C666 }
\end{aligned}
\] & & Not used & \\
\hline \begin{tabular}{l}
C667 \\
Cont. \\
See C701
\end{tabular} & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(1 \mu \mathrm{f}, \pm 20 \%\); 600 v DC working; MIL type CH53B1EF105M per MIL-STD-242A and per spec MIL-C-18312; 21964 \#A1068596 & B602 motor starting capacitor \\
\hline CR601 & & SEMI-CONDUCTOR DEVICE, DIODE: germanium type; 40 ma max. continuous forward current; 125 ma max. peak forward current; 75 v peak inverse voltage; 0.8 mmf average shunt capacitance; MIL type 1 N69 per spec MIL-E-1C; 21964 \#700030 & Mixing diode, DL601 \\
\hline CR602 & & Same as CR601 & Mixing diode, DL601 \\
\hline CR603 & & Same as CR601 & Switching diode, V604-2 keyer \\
\hline CR604 & & Same as CR601 & Isolating diode V610 \\
\hline CR605 & & Same as CR601 & Isolating diode V603 \\
\hline CR606 & & Same as CR601 & Clamping diode V602 \\
\hline DL601 & & DELAY LINE: distributed parometer type w/output inductive coupling; total delay 49 to \(53 \mu \mathrm{sec}\) nominal; 2 output coils spaced at 32 and \(44 \mu \mathrm{sec}\) approx, two locking type coil adjustments, one varying the \(32 \mu \mathrm{sec} \mathrm{w} / \mathrm{respect}\) to \(44 \mu \mathrm{sec}\) coil by \(12 \mu \mathrm{sec}\), the second to vary the o/a delay of both coils simultaneously yet keep the delay between them constant, varying the o/a delay by \(44 \pm 4 \mu \mathrm{sec}\), incl R789; 70117 \#G115; 21964 \#A9160102 & Zero distance time delay and pulse coding Figure 6-6 \\
\hline DS601 & & LAMP, INCANDESCENT: 115-125 v, 10 watts, 40 lumens, double contact bayonet base; clear, 1 filament, tungsten; 24446 \#10C7/1DC; 21964 \#710071; Same as DS501 & Coder-Indicator 'POWER ON"' Figure 3-2 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline DS602 Cont. See DS701 & & Same as DS601 & Antenna warning light Figure 3-2 \\
\hline \[
\begin{gathered}
\text { E601 } \\
\text { thru } \\
\text { E603 }
\end{gathered}
\] & & Not used & \\
\hline E604 & 6 & SHIELD, ELECTRON TUBE: copper or brass, heat dissipating black finish; JAN type TS103U02 per spec JAN-S-28A; modified; 21964 \#A2132988-5; Same as E307 & Tube shield \\
\hline E605 & & Same as E604 & Tube shield \\
\hline E606 & & Same as E604 & Tube shield \\
\hline E607 & & Same as E604 & Tube shield \\
\hline E608 & & Same as E604 & Tube shield \\
\hline E609 & & Same as E604 & Tube shield \\
\hline E610 & & Same as E604 & Tube shield \\
\hline E611 & & Same as E604 & Tube shield \\
\hline E612 & & Same as E604 & Tube shield \\
\hline E613 & 6 & SHIELD, ELECTRON TUBE: copper or brass, heat dissipating black finish; JAN type TS103U01 per spec JAN-S-28A, modified; 21964 \#A2132988-4; Same as E404 & Tube shield \\
\hline E614 & & Same as E613 & Tube shield \\
\hline E615 & & Same as E613 & Tube shield \\
\hline E616 & & Same as E613 & Tube shield \\
\hline E617 & & Same as E613 & Tube shield \\
\hline E618 & & INSERT, ELECTRON TUBE SHIELD: black cad plated brass; on shield JAN type TS103U02; MIL-STD-242A type \#902; 21964 \#A2132886-5; Same as E307A & Insert for E604 \\
\hline E619 & & Same as E618 & Tube shield insert \\
\hline E620 & & Same as E618 & Tube shield insert \\
\hline E621 & & Same as E618 & Tube shield insert \\
\hline E622 & & Same as E618 & Tube shield insert \\
\hline E623 & & Same as E618 & Tube shield insert \\
\hline E624 & & Same as E618 & Tube shield insert \\
\hline E625 & & Same as E618 & Tube shield insert \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E626 & & Same as E618 & Tube shield insert \\
\hline E627 & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U01; MIL-STD-242A type \#901; 21964 dwg \#A2132886-4; Same as E404A & Insert for E613 \\
\hline E628 & & Same as E627 & Tube shield insert \\
\hline E629 & & Same as E627 & Tube shield insert \\
\hline E630 & & Same as E627 & Tube shield insert \\
\hline E631 & & Same as E627 & 'rube shield insert \\
\hline E632 & & Same as E618 & Tube shield insert \\
\hline \begin{tabular}{l}
E633 \\
Cont. \\
See E701
\end{tabular} & & Same as E604 & Tube shield \\
\hline F 301 & & FUSE, CARTRIDGE: \(3 \mathrm{amp} ; 250 \mathrm{v}\); instantaneous type; MIL type F02G3R00A per spec MIL-R-15160A; 21964 \#882011 & Main power fuse Figure 3-2 \\
\hline F602 & & Same as F601 & Main power fuse Figure 3-2 \\
\hline F603 & & Same as F601 & Spare fuse \\
\hline J601 & & CONNECTOR, RECEPTACLE ELECTRICAL: 1 round female contact; one connector mating end; 50 ohm nom impedance, 500 v peak voltage; low loss plastic dielectric; straight shape; MIL type UG-1094/U BNC Series, ' \(D\) " hole mounting, per Navy dwg REB 49063; 21964 \#A2131837; Same as J203 & Ground receiver input Figure 6-6 \\
\hline J602 & & Same as J601 & Video output Figure 6-6 \\
\hline J603 & & Same as J601 & 135 cps trigger input Figure 6-6 \\
\hline J604 & & Same as J601 & 15 cps trigger input Figure 6-6 \\
\hline J605 & & CONNECTOR, RECEPTACLE ELECTRICAL: 47 male round contacts; polarized; straight type; MIL type AN3102A-36-7P, per spec MIL-C-5015; 21964 \#752335 & Interconnecting cable connector \\
\hline J606 & & Same as J601 & Sync. output Figure 3-2 \\
\hline J607 & & Same as J601 & Test output Figure 3-2 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J608 & & CONNECTOR, RECEPTACLE ELECTRICAL: 10 male round contacts; polarized; straight type; MIL type AN3102A-18-1P per spec MIL-C-5015B; 21964 \#752210 & Input jack for P927 \\
\hline J609 & & Same as J601 & Output jack, 1350 cycle ref output Figure 6-6 \\
\hline J610 & & Same as J601 & Tachometer v input jack Figure 6-6 \\
\hline L601 & & COIL, RADIO FREQUENCY: single universal winding, 850 turns no. 38 AWG resin coated nylon covered for each winding, 5.7 mh to 7.5 mh at 250 kc ; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#B2060052G1 & Variable coil V603 33.333 kc ringing circuit Figure 6-6 \\
\hline L602 & & Same as \(\mathbf{L 6 0 1}\) & Variable coil, V610 41.667 kc ringing circuit Figure 6-6 \\
\hline L603 & & REACTOR: mechanical adjustable inductance type; 1 coil, \(50 \mathrm{mh} \pm 10 \%\) to \(170 \mathrm{mh} \pm 5 \%, 50\) ma max. DC current; 45 ohms \(\pm 5 \%\) resistance between terminals 1 and 2,55 ohms \(\pm 5 \%\) resistance between terminals 2 and \(3 ; 500 \mathrm{v}\) DC test voltage; MLL type TF 2 SX 20 ZZ per spec MIL-T-27A; 21964 spec \#A2060070 & Variable coil, V612, 1350 cycle oscillator Figure 6-6 \\
\hline L604 cont. See L'701 & & CHOKE, RADIO FREQUENCY: 700 ma DC current rating; 47 microhenries \(\pm 10 \%\); 1.2 ohms max DC resistance; MIL type LT8K010 per spec MIL-C-15305 and MIL-STD-242A; part \#MS91189-10; 21964 \#866000H470 & Low pass filter choke \\
\hline M601 & & METER, ARBITRARY, SCALE: panel mounted; DC; scale data, red to green to red, 4 scale divisions for 3 scale arcs; round hermetically sealed metal case, \(\pm 2 \%\) accuracy; 50 microamperes DC for full scale deflection; 2000 ohms resistance across terminals; \(D^{\prime}\) Arsonval basic movement with shaded poles for expanded center point sensitivity; 8 microamperes \(\pm 10 \%\) for \(20^{\circ}\) deflection either side of center; white background; green scale \(20^{\circ}\) either side of center; remainder red; scale marked 'Normal Range"; per spec MLL-M-10304A; 21964 \#A2060762 & Error indicating meter Figure 3-2 \\
\hline MP601 & & CLAMP, ELECTRICAL: brass, nickel plated finish; 1 screw type; \(1-3 / 8^{\prime \prime} \lg , 3 / 8^{\prime \prime}\) dia, o/a dim. ; *10-32 NF-2 mounting stud w/hex nut 3/8: across flats; 3/32" max opening of locking torque; part *K10050 or equal, modified per 21964 *A2142151G1 76487 & Dial lock \\
\hline MP602 & & CAP ELECTRICAL: brass; fits BNC female connectors; MIL type CW-123/AU per Navy dwg. REA49050 and per spec MIL-C-3608; 21964 dwg \#A9152998; Same as MP504 & Protective cover for J606 \\
\hline MP603 & & Same as MP606 & Protective cover for J607 \\
\hline MP604 & 7 & WHEEL, CODING: c/o wheel with 60 adjustable stainless steel cam segments; dim. 4-7/8 in. dia, 0.203 in . thk; four 0.149 in . dia mtg holes on 0.812 in . dia centers; markings on face, 'START CODE'; 21964 \#B9151588 & p/o tone identification keyer assy \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline MP605 & 7 & CLAMP, SHAFT: band type; steel cadmium plated; one \(78-32\) thd bolt employed; dim. o/a, 13/16 in. Ig, 7/16 in. w, 0.245 in. max deep; hole dia 0.314 in . \(\max 50222\) *SP-130-5/16 clamp bore; 21964 (A2144413 & Mounts on shaft of tone identification keyer assy \\
\hline MP606 & & FITTING, LUBRICATION: steel, \(17 / 32 \mathrm{in} . \mathrm{lg}, 0.266 \mathrm{in} . \mathrm{w}, 1 / 4-28\) (NF-2) thd one end \(3 / 32 \mathrm{in}\). lg; 57733 *1792 or equivalent; military std \#MS-15002-1; 21964 \#A2132909 & Mounts on housing of tone identification keyer assy \\
\hline MP607 & & BOOT, DUST AND MOISTURE SEAL: silicone rubber bonded to a brass nickel plated hex nut 15/32-32 thd; 3/4 in. across flats, 7/8 in. lg; 97537 *1030; 21964 \#A2132649-1; Same as MP202 & Moisture and dust proof cover for S601 \\
\hline MP612 & 1 & GASKET: synthetic rubber, MIL-R-900A, class 2; cross-section style no. 7, Ref Dwg Group 74; \(1 / 8^{\prime \prime}\) wide, \(5 / 32^{\prime \prime}\) high w/1/16" radius, approx 3 ft \(\mathrm{lg} ; 21964 \mathrm{dwg}\) *A9140800; Same as MP201 & Seals front panel \\
\hline MP613 & 4 & BEARING, BALL, ANNULAR: single row; 0.2500 in. bore dia; 0.422 in flange dia, 0.1250 wide; 40920 \#SS614FCHH: 21964 \#B2132900-4 & Mounts on cam shaft in gear box \\
\hline MP614 & & Same as MPbi3 & Mounts on idler shaft in gear box \\
\hline MP615 & 4 & GEAR ASSEMBLY: corrosion resisting steel type 303 per MIL-S-853; assy c/o two gears; o/a lg 0.562 in .; gear data, gear "A", 30teeth, 0.4687 in . pitch dia, 0.500 in . OD; gear " \(B\) " 50 teeth, 1.0416 in. pitch dia, \(1.0832 \mathrm{in} .0 \mathrm{D}, 20\) deg pressure angle each; 01351 \#250-30 and \(\# 150-50 ; 21964\) \#B2145118 & p/o idler and shaft in gear box \\
\hline MP616 & 4 & BEARING, BALL, ANNULAR: single row; bore dia, \(0.1875 \mathrm{in} . ;\) flange dia, 0.422 in. , 0.1250 in. wide; 40920 *SS6632 FCHH; 21964 *B2 132900-2 & Mounts on wheel shaft in gear box \\
\hline MP617 & 4 & GEAR, SPUR: corrosion resistant steel; 25 teeth, 20 deg pressure angle; gear data, 0.5625 in . OD, 0.5208 pitch dia, 0.406 in . hub dia, 0.1785 in . bore dia; \#6-32 NC-2B tapped hole for setscrew mtg; 21964 \#A2 145770 & p/o idler and cam shaft in gear box \\
\hline MP618 & 4 & BEARING, BALL, ANNULAR: single row; bore dia 0.2500 in ; 0 /a dia 0.3750 in. , width 0.1250 in; 40920 \#SS614CHH; 21964 *B2132910-4 & Mounts on cam shaft in gear box \\
\hline MP619 & & Same as MP618 & Mounts on idler shaft in gear box \\
\hline MP620 & & Same as MP618 & Mounts on wheel shaft in gear box \\
\hline MP62 1 & 4 & GEAR, SPUR: aluminum alloy 2024-T4; 75 teeth, 20 deg pressure angle; dim. \(1.2031 \mathrm{in} . \mathrm{OD} ; 1.1718 \mathrm{in}\). pitch dia, \(0.375 \mathrm{in} . \mathrm{lg}\); one no. 6-32 NC-2B tapped hole for setscrew; 01351 *250-75; 21964 *B2 132908-1; p/o MP627 & p/o idler and cam shaft in gear box \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R628 & 6 & RESISTOR, FLXED, COMPOSITION: 100 ohms; \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF101K per spec MIL-R-11; 21964 \#504219; Same as R201 & Decoupling resistor, plate supply \\
\hline R629 & 6 & RESISTOR, FLXED, COMPOSITION: 2200 ohms, \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF222K per spec MIL-R-11; 21964 \#504235; Same as R207 & Load resistor, T602 secondary \\
\hline \(\mathbf{R 6 3 0}\) & 6 & RESISTOR, FIXED, COMPOSITION: 10 ohms; \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF100K per spec MIL-R-11; 21964 *504207; Same as R334 & Isolating resistor, V606 delay line blocking oscillator \\
\hline R631 & 6 & RESISTOR, FIXED, COMPOSITION: 330 ohms \(\pm 10 \%, 1 / 2 \mathrm{w}\) MIL type RC20GF331K; per spec MIL-R-11; 21964 \#504225; Same as R302 & Cathode resistor, V606, delay line blocking oscillator \\
\hline R632 & & RESISTOR, FIXED, COMPOSITION: 10,000 ohms, \(\pm 5 \%\) tolerance; \(1 / 2\) watt; MIL type RC20GF103J; per spec MIL-R-11; 21964 \#504127 & Grid bias divider, V606, delay line blocking oscillator \\
\hline R633 & & RESISTOR, FIXED, COMPOSITION: 33,000 ohms; \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF333J per spec MIL-R-11; 21964 \#504139; Same as R326 & Grid bias divider, V606, delay line blocking oscillator \\
\hline R634 & & RESISTOR, FIXED, COMPOSITION: 8200 ohms; \(\pm 5 \%\); \(1 / 2\) watt; MIL type RC20GF822J per spec MIL-R-11; 21964 \#504125; Same as R325 & Grid bias divider, V606, delay line blocking oscillator \\
\hline R635 & & Same as R604 & Grid resistor, V6071, delay line output amplifier \\
\hline \(\mathbf{R 6 3 6}\) & & RESISTOR, FIXED, COMPOSITION: 12,000 ohms \(\pm 5 \% ; 1 / 2\) watt MIL type RC20GF123J per spec MIL-R-11B; 21964 \#504129 & Grid bias divider, V607-1, delay line output amplifier \\
\hline \(\mathbf{R 6 3 7}\) & & RESISTOR, FIXED, COMPOSITION: 47, 000 ohms; \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF473J per spec MIL-R-11; 21964 \#504143 & Grid bias divider, V607-1, delay line output amplifier \\
\hline R638 & 6 & RESISTOR, FIXED, COMPOSITION: 33, 000 ohms; \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF333K, per spec MIL-R-11; 21964 \#504249 & Plate load V607-1 delay line out put amplifier \\
\hline \(\mathbf{R 6 3 9}\) & & RESISTOR, FIXED, COMPOSITION: 15,000 ohms; \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF153J per spec MIL-R-11; 21964 ; 504131 & Grid tuning, V615, output MV \\
\hline R640 & 6 & ```
RESISTOR, FIXED, COMPOSITION: 22, 000 ohms; \(\pm 10 \%\); 2 watts
    MIIL type RC42GF223K, per spec MIL-R-11; 21964 \#501257; Same
    as R420
``` & Plate load, V615 output MV \\
\hline \(\mathbf{R 6 4 1}\) & & Same as F640 & Plate load, V615, output MV \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline 1869 & 6 & RESISTOR, FIKED, COMPOSITION: 1000 ohms, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF102K; per spec MIL-R-11; 21964 *504231; Same as R341 & Plate Load, V815, out put MV \\
\hline \(\mathbf{R 6 4 3}\) & & Same as R 837 & Cathode stabilizing V615, output MV \\
\hline \(\mathbf{R 6 4 4}\) & & RESISTOR, FIXED, COMPOSITION: 68,000 ohms, \(\pm 5 \% ; 1 / 2\) watt MIL type RC20GF683J, per spec MIL-R-11; 21964 *504147 & Cathode stabilizing V615, output MV \\
\hline R645 & & Same as R642 & Cathode resistor, V615, output MV \\
\hline R646 & & RESISTOR, FIXED, COMPOSITION: 560, 000 ohms, \(\pm 5 \%\) tolerance; 1/2 watt MIL type RC20GF564J, per spec MIL-R-11; 21964 "504169 & Grid bias divider, V607-2, output cathode follower \\
\hline R647 & & Same as R623 & Grid bias divider, V607-2, output cathode follower \\
\hline R648 & & Same as R616 & Grid resistor, V6072, output cathode follower \\
\hline R649 & & Same as R642 & Cathode resistor, V607-2, output cathode follower \\
\hline R650 & & Same as R628 & Test output voltage divider, V607-2, cathode follower \\
\hline R651 & & Same as R637 & Grid bias divider, V611 priority \\
\hline \(\mathbf{R 6 5 2}\) & 6 & RESISTOR, FIXED, COMPOSITION: 150,000 ohms, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF154K; per spec MIL-R-11A; 21964 \#504257 & Plate load V608 \\
\hline R653 & & Same as R629 & Cathode resistor V608 \\
\hline R654 & 6 & RESISTOR, FIXED, COMPOSITION: 1.5 megohm, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF155K per spec MIL-R-11; 21964 *504269 & Plate load resistor V608 \\
\hline R655 & 6 & RESISTOR, FDXED, COMPOSTITION: 330,000 ohms; \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF334K; per spec MIL-R-11; 21964 *504261 & Grid limiting resistor V608 \\
\hline \(\mathbf{R 6 5 6}\) & 6 & RESISTOR, FIXED, COMPOSITION: 1 megohm, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF105K; per spec MIL-R-11; 21964 *504267; Same as R132 & Grid resistor V608 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOGATING FUNCTION \\
\hline R657 & & Same as R603 & Grid resistor V601-1 \\
\hline R658 & & Same as R604 & Grid limiting resistor V601-1 \\
\hline R659 & & Same as R605 & Plate load, V601-1, 135 cps trigger amplifier \\
\hline \(\mathbf{R 6 6 0}\) & & Same as R607 & Grid voltage divider, V609, 135 cps gate MV \\
\hline R661 & & Same as R606 & Grid voltage divider, V609, 135 cps gate MV \\
\hline R662 & & Same as R608 & Plate load V609, 135 cps gate MV \\
\hline R663 & & Same as R623 & Grid timing V609, 135 cps gate MV \\
\hline R664 & & Same as R610 & Plate load V609, 135 cps gate MV \\
\hline R665 & & Same as R611 & Cathode resistor V609 135 cps gate MV \\
\hline R666 & & Same as R613 & Plate load V610, 41. 667 kc ringing circuit \\
\hline R667 & & Same as R608 & Grid resistor V610, 41.667 kc ringing circuit \\
\hline R668 & & Same as R616 & Grid limiting V610, 41.667 kc ringing circuit \\
\hline R669 & & Same as R615 & Plate load V610, 41. 667 kc ringing circuit \\
\hline R670 & & Not Used & \\
\hline R671 & & Same as R604 & Voltage divider, 135 cps ref burst feedback circuit \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & locaillle FUNCTIOH \\
\hline R672 & 6 & RESISTOR, VARIABLE: composition element; 1 section, 0.10 megohm; \(\pm 10 \% ; 2\) watt nominal power rating; no switch; MIL type RV4LAVSA104A per spec MIL-R-94 and MIL-STD-242 (Ships); 21964 \#A2 133049-3 & Voltage divider, 135 cps reference burst feedback circuit Figure 6-6 \\
\hline R673 & & Same as R638 & Voltage divider, 135 cps ref burst feedback circuit \\
\hline R674 & 6 & RESSTSTOR, FIXED, COMPOSITION: 68,000 ohms, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF683K, per spec MLL-R-11; 21964 \#504253 & Voltage divider, 15 cps reference burst feedback circuit \\
\hline R675 & & Same as R672 & 15 cps feedback Figure 6-6 \\
\hline R676 & & Same as R638 & 15 cps feedback \\
\hline R677 & & Same as R614 & Isolating resistor, V611 priority \\
\hline R678 & & Same as R614 & Isolating resistor \\
\hline R679 & & Same as R656 & Grid resistor, V611, priority \\
\hline R680 & 6 & RESISTOR, FIXED, COMPOSITION: 68, 000 ohms, \(\pm 10 \%\); 1 watt MIL type RC32GF683K; per spec MLL-R-11; 21964 \#503940 & Plate load, V611, priority \\
\hline R681 & & Same as R629 & Cathode resistor, V611 priority \\
\hline R682 & & RESISTOR, FIXED, COMPOSITION: 470, 000 ohms, \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF474J, per spec MIL-R-11; 21964 \#504167 & Grid bias divider, V611 priority \\
\hline R683 & 6 & RESISTOR, FIXED, COMPOSITION: 470,000 ohms, \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF474K, per spec MIL-R-11; 21964 \#504263; Same as \(\mathrm{R430}\) & Grid resistor, V611 priority \\
\hline R684 & & Same as R614 & Cathode resistor V604-2, keyer \\
\hline R685 & & Same as R656 & Grid resistor V604-2 keyer \\
\hline R686 & & Same as R637 & Grid bais divider V604-2, keyer \\
\hline R687 & & Same as R628 & Current limiting resistor \\
\hline R688 & & RESISTOR, FDXED, COMPOSITION: 100,000 ohms \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF104J per spec MIL-R-11; 21964 \#504151; Same as R444 & Grid voltage divider, V612, 1350 cycle oscillator \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R689 & & RESTSTOR, FDXED, COMPOSITION: 39,000 ohms, \(\pm 5 \%\); \(1 / 2\) watt MIL type RC20GF393J, per spec MIL-R-11; 21964 \#504141 & Grid voltage divider, V612, 1350 cycle oscillator \\
\hline R690 & & Same as R656 & Grid resistor V612, 1350 cycle oscillator \\
\hline R691 & & Same as R656 & Grid limiting, V613-1 1350 cycle amplifier \\
\hline R692 & 6 & RESISTOR, FIXED, COMPOSITION: 3900 ohms, \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF392K per spec MIL-R-11; 21964 \#504238 & Cathode resistor V612, 1350 cycle oscillator \\
\hline R693 & & Same as R680 & Cathode resistor V612, 1350 cycle oscillator \\
\hline R694 & & Same as R614 & Grid resistor V613-1, 1350 cycle amplifier \\
\hline R695 & & Same as R614 & Plate load, V613-1 \\
\hline R696 & & Same as R620 & Grid voltage divider, V614 \\
\hline R697 & & Same as R616 & Plate load, V614 \\
\hline R698 & & Same as R633 & Grid voltage divider, V614 \\
\hline R699 Cont. See R701 & 6 & RESISTOR, FIXED, COMPOSITION: 6800 ohms; \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF682K per spec MIL-R-11; 21964 \#504241; Same as R411 & Cathode resistor V614, \(100 \mu \mathrm{sec}\) MV \\
\hline S601 & & SWITCH, TOGGLE: single pole, single throw; 0.75 amp 125 v DC., 15 amp 125 v AC. , JAN type ST42A, per spec JAN-S-23; 21964 \#82 8212 ; Same as S502 & "ON-OFF' switch Figure 3-2 \\
\hline S602 & & Not Used & \\
\hline S603 & & Same as S601 & Continuous tone on normal keying switch Figure 6-6 \\
\hline S604 & & SWITCH, SENSITIVE: single pole double throw; 125 v AC, 15 amp ; roller leaf spring type, \(0.188^{\prime \prime}\) max pre-travel, \(0.031^{\prime \prime} \mathrm{min}\). over travel; 6 oz max operating force; 0.5 oz min release force; \(0.050^{\prime \prime}\) max movement differential; 0.020 nom contact separation; momentary action; one contact normally open, one contact normally closed; 3 screw type terminals; JAN type SS05A20 per spec JAN-S-63 and MIL-STD-242A; 21964 \#2060306 & Identification keyer keying switch Figure 6-6 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline S605 & & SWITCH, TOGGLE: double pole double throw; 6 amp ; 125 จ AC; JAN type ST22N per spec JAN-S-23: 21964 \#B2061102G1 & Identification keyer "ON-OFF" switch Figure 3-11 \\
\hline S606 & & Not Used & \\
\hline S607 & & SWTTCH, SENSTITIVE: SPDT, 0.5 amp peak current, 75 v DC; not enclosed; roller leaf type momentary action, one contact normally closed; with adjusting screw and block; 3 solder type terminals; 21964 fC2061124 & Identification keyer coding switch Figure 3-11 \\
\hline T601 & & Not Used & \\
\hline T602 & & TRANSFORMER, PULSE: three windings of \(1: 1: 1\) ratio; nominal pulse width 2 usec; winding impedance 300 ohms with a rise time of .04 usec and pulse widths .5 to 5 usec; max pulse voltage 350 v , max peak power \(200 \mathrm{w} ; 800 \mathrm{v}\) DC test voltage 49956 \#363-6004G2, MIL type TF2SX35ZZ per spec MIL-T-27A; 21964 *A1069475 & Pulse transformer, blocking oscillator V606 Figure 6-52 \\
\hline T603 Cont. See T701 & & TRANSFORMER, PULSE: 2 windings of 1:3 ratio; nominal pulse width 20 usec; winding impedance \(300 / 2700\) ohms with a rise time of 0.8 usec and pulse widths 1 to 20 usec; max pulse voltage \(350 \nabla\), max peak power \(200 \mathrm{w} ; 800\) v DC test voltage; 01961 type PE2030, MIL type TF2SX36ZZ per spec MIL-T-27A; 21964 \#A1069827 & Delay line driving pulse transformer Figure 6-52 \\
\hline TB601 & & TERIINAL BOARD: 6 terminals; double screw type; barrier type; MIL type 8TB6 per spec MIL-T-16784 and Navy dwg 9000-S6505G73214; 21964 \#A2 133063-2 & Terminal board identification tone keyer chassis \\
\hline TB602 & & Not Used & \\
\hline TB603 & & TERIINAL BOARD: 2 terminals; double screw type; barrier type; MIL type 8TB2 per spec MIL-T-16784 and Navy dwg 9000-S6505B73214; 21964 \#A2133063-1 & Interlock test board \\
\hline TB604 & & TERMINAL BOARD: 12 terminals; single row, thru type terminals; MIIL type 7TB12 per spec MIL-T-16784A and Navy dwg 9000-S6505G-73214; 21964 其A2133072-2 & Terminal board, video chassis Figure 6-52 \\
\hline TB605 thru TB694 & & Not Used & \\
\hline TB695 & 2 & TERIINAL BOARD: 78 solder stud terminals; 21964 *B2060935G1 & Terminal board for video chassis assy Figure 6-52 \\
\hline TB696 & 2 & TERIMNAL BOARD: \(\mathbf{7 8}\) hollow solder stud terminals; 21964 \#B2060934G1 & Terminal board for video chassis assy Figure 6-52 \\
\hline TB697 & 2 & TERMTINAL BOARD: 78 solder stud terminals; 21964 \#B2060986G1 & Terminal board for video chassis assy Figure 6-52 \\
\hline 50 & & & Issued June 7 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & locaring FUNCTION \\
\hline TR698 & 2 & TERMINAL BOARD: 78 solder stud terminals; 21964 \#B2060985G1 & Terminal board for video chassis assy Figure 6-52 \\
\hline TB699 Cont. See TB701 & 2 & TERMINAL BOARD: 44 hollow type solder stud terminals; 21964 *B2060932G1 & Terminal board for video chassis assy Figure 6-52 \\
\hline V601 & & ELECTRON TUBE: twin triode; MIL type 12AT7WA; per spec MIL-E-1C; 21964 \#701165; Same as V307 & Reference pulse trigger amplifier Figure 6-6 \\
\hline V602 & & Same as V601 & 15 cps gate MV Figure 6-6 \\
\hline V603 & & ELECTRON TUBE: twin triode; MIL type 5670, per spec MIL-E-1C; 21964 *700563; Same as V404 & \begin{tabular}{l}
33.333 kc pulsed oscillator \\
Figure 6-6 \\
Reference burst
\end{tabular} \\
\hline V604 & & Same as V601 & amplifier keyer Figure 6-6 \\
\hline V605 & & Same as V601 & Cathode coupled MV Figure 6-6 \\
\hline V606 & & ELECTRON TUBE: twin triode; MIL type 5687WA; per spec MIL-E-1 (Navy); 21964 \# A2 133281 & Delay line blocking oscillator \\
\hline V607 & & Same as V606 & Delay line output amplifier, output cathode follower Figure 6-6 \\
\hline V608 & & Same as V601 & 1350 reference cycle oscillator Figure 6-6 \\
\hline V609 & & Same as V601 & \begin{tabular}{l}
135 cps gate MV \\
Figure 6-6
\end{tabular} \\
\hline V610 & & Same as V603 & 41.667 kc pulsed oscillator Figure 6-6 \\
\hline V611 & & Same as V601 & Priority tube Figure 6-6 \\
\hline V612 & & Same as V603 & 1350 cycle oscillator Figure 6-6 \\
\hline V613 & & Same as V603 & 1350 cycle amplifier Figure 6-6 \\
\hline V614 & & Same as V603 & \begin{tabular}{l}
100 usec MV \\
Figure 6-6
\end{tabular} \\
\hline V615 Cont. See V701 & & Same as V606 & \begin{tabular}{l}
Output MV \\
Figure 6-6
\end{tabular} \\
\hline XDS601 & & LIGHT, INDICATOR: friction mtg lens holder; accomodates style S-6 lamp; 125 v, 6 watts; MIL type LH63PW3 per spec MIL-L-3661, dwg MS-90286; 21964 \#A2133069-5; Same as XDS501 & Holder for DS601 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline \begin{tabular}{l}
XDS602 \\
Cont. \\
See XDS701
\end{tabular} & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; 125 v , 6 watts; MIL type LH63BA3 per spec MIL-L-3661, dwg MS90286; 21964 \#A2133080-3 & Holder for DS602 \\
\hline XF601 & & FUSE HOLDER: extractor post type; accommodates 2 fuses 1-1/4" lg. by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type; sealed; MIL type FHL10G per BuShips dwg \#9000-S6202-74228 and per spec MIL-F19207 (Ships); 21964 \#A2 060402 ; Same as XF501 & Fuse holder for F601 \\
\hline XF602 & & FUSE HOLDER: extractor post type; accommodates 1 fuse 1-1/4" \(\lg\) by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type; sealed; MIL type FHL11G per BuShips dwg \#9000-S6202-74229 and per spec MIL-F-19207 (Ships); 21964 \#A2060403; Same as XF503 & Fuseholder for F602 \\
\hline XV601 & & SOCKET, ELECTRON TUBE: 9 contacts, brass, nickel plated; miniature; includes metal shield base, JAN type TS103P01, per spec JAN-S-28A-1; 21964 \#740004; Same as XV307 & Tube socket for V601 \\
\hline XV602 & & Same as XV601 & Tube socket for V602 \\
\hline XV603 & & Same as XV601 & Tube socket for V603 \\
\hline XV604 & & Same as XV601 & Tube socket for V604 \\
\hline XV605 & & Same as XV601 & Tube socket for V605 \\
\hline XV606 & & Same as XV601 & Tube socket for V606 \\
\hline XV607 & & Same as XV601 & Tube socket for V607 \\
\hline XV608 & & Same as XV601 & Tube socket for V608 \\
\hline XV609 & & Same as XV601 & Tube socket for V609 \\
\hline XV610 & & Same as XV601 & Tube socket for V610 \\
\hline XV611 & & Same as XV601 & Tube socket for V611 \\
\hline XV612 & & Same as XV601 & Tube socket for V612 \\
\hline XV613 & & Same as XV601 & Tube socket for V613 \\
\hline XV614 & & Same as XV601 & Tube socket for V614 \\
\hline XV615 & & game as XV601 & Tube socket for V615 \\
\hline Y604 & & RESONATOR, TUNING FORE: fixed frequency, 1350 cycles, hermeti* cally sealed metal case; electrically equivalent to 95267 \#J-1350-E* 40-85 percent per spec Mill-5-16400A; 21964 \#A2060071 & 1350 cycle tuning fork \\
\hline
\end{tabular}

TABLE 7-3 RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C701 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(6 \mu \mathrm{f} \pm 10 \%, 600 \mathrm{v}\) DC working; MIL type CP70E1EF605K per spec MIL-C-25; 21964 \#641039 & Plate supply filter Figure 6-53 \\
\hline C702 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1 section; \(0.1 \mu \mathrm{f}\), \(\pm 10 \%, 400\) v DC working; MIL type CP09A1 KE104K per spec MIL-C-25A; 21964 \#643518 & Stabilizing V704, control tube \\
\hline C703 & & Same as C701 & Bias supply filter Figure 6-53 \\
\hline C704 & & Same as C702 & Bypass, V705, voltage regulator \\
\hline DS701 & & LAMP, GLOW: neon gas, 0.25 watt, \(67-87 \mathrm{v}\) DC striking voltage; double contact bayonet type; T4-1/2 bulb; MIL type NE-16 per spec MIL-L-1 5098, 21964 \#A2060350; Same as DS502 & \begin{tabular}{l}
"POWER ON" \\
warning light Figure 6-7
\end{tabular} \\
\hline E701 thru E703 & & Not used & \\
\hline E704 & 5 & SHIELD, ELECTRON TUBE: copper or brass, heat dissipating black finish; JAN type TS102U02 per spec JAN-S-28A, modified; 21964 \#A2132886-2; Same as E202 & Tube shield \\
\hline E705 & & INSERT, ELECTRON TUBE SHIELD: black cad plated brass; use on shield JAN type TS102U02; MIL-STD-242A type \#702, 21964 \#A2132988-2; Same as E202A & Insert for E704 \\
\hline E706 & 5 & SHIELD, ELECTRON TUBE: copper or brass, heat dissipating black finish; JAN type TSI02U03 per spec JAN-S-28A, modified; 21964 \# A2132988-3; Same as E408 & Tube shield \\
\hline E707 & & INSERT, ELECTRON TUBE SHIELD: black cad plated brass; use on shield JAN type TS102U03 per MIL-STD-242A type \#703; 21964 \#A2132886-3; Same as E408A & Insert for E706 \\
\hline E708 & & Same as E706 & Tube shield \\
\hline E709 & & Same as E707 & Insert for E708 \\
\hline E710 thru E725 & & Not used & \\
\hline E726 & & RETAINER, ELECTRON TUBE: steel, retains standard octal type tube base; clamps tube with spring action; 07387 \#926-C; 21964 \#B2141834-8 & Retainer for V701 \\
\hline E727 & & RETAINER, ELECTRON TUBE: stainless steel, type 302, c/o clip, strap and bracket; 07387 \#926 H-5; 21964 \#A9153393 & Retainer for V703 \\
\hline L701 & & REACTOR: filter choke; one section; 10 henries; 200 ma DC; 110 ohms DCR; 440 peak wv; AC drop 200 v rms, per spec MIL-T-27; Grade 1, Class R Family O4; life expectancy X; case YY; MIL type TF1RX04YY; 21964 spec \#A9010462 and dwg \#B9151068; Same as L501 & Plate supply filter choke Figure 6-6 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R701 & 6 & RESISTOR, FIXED, COMPOSITION: 33 ohms; \(\pm 10 \% ; 1 / 2\) watt MIL type RC20GF330K per spec MIL-R-11; 21964 " 504213 & Balancing resistor V703, series regulator \\
\hline R702 & & Same as R701 & Balancing resistor, V703, series regulator \\
\hline R703 & & Same as R642 & Grid balancing V703, series regulator \\
\hline R704 & & Same as R642 & Grid balancing V703, series regulator \\
\hline R705 & & Same as R674 & Plate load V'704, control tube \\
\hline R706 & & Same as R688 & Screen voltage divider, V704, control tube \\
\hline R707 & & RESISTOR, FIXED, COMPOSITION: 82, 000 ohms; \(\pm 5 \%\); I/2 watt MIL type RC20GF823J per spec MIL-R-11; 21964 \#504149 & Screen voltage divider, V704, control tube \\
\hline R708 & 6 & RESISTOR, FIXED, COMPOSITION: 390,.000 ohms; \(\pm 10 \%\); \(1 / 2\) watt MIL type RC20GF394K per spec MIL-R-11; 21964 \#504262 & Grid bias divider, V704, control tube \\
\hline R709 & & Same as R683 & Grid limiting, V704, control tube \\
\hline R710 & & Same as R672 & Power supply B+ control, V704, control tube Figure 6-53 \\
\hline R711 & & Same as R652 & Grid bias voltage divider, V704, control tube \\
\hline R712 & 6 & RESISTOR, FIXED, COMPOSITION: 3900 ohms \(\pm 10 \%\); 2 watt; MIL type RC42GF392K per spec MIL-R-11; 21964 \#501248 & Current limiting resistor, for V705, voltage regulator \\
\hline R713 & & Same as R712 & Current limiting resistor for V705 voltage regulator \\
\hline R714 & & Same as R615 & Current limiting resistor for V705 voltage regulator \\
\hline \(\mathbf{R 7 1 5}\) & & Same as R615 & Current limiting resistor for V705 voltage regulator \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCATING \\
FUNCTION
\end{tabular} \\
\hline R799 & 6 & RESISTOR, FIXED, COMPOSITION: 33,000 ohms \(\pm 10 \%\); 1 watt MIL type RC32GF333K per spec MIL-R-11; 21964 \# 503936 & Plate load, V614, \(100 \mu \mathrm{sec}\) MV \\
\hline T701 & & TRANSFORMER, POWER, STEP-DOWN: input 120 v AC, 60 cycles, single phase; output, sec no. one 5 vct at 3 amp , sec no. two 6.4 v at \(16 \mathrm{amp} ; 49956\) \#292-5625G1, MIL type no. TF1SX01YY; 21964 \#A1069871 & \begin{tabular}{l}
Filament voltage supply \\
Figure 6-6
\end{tabular} \\
\hline T702 & & TRANSFORMER, POWER, STEP-UP: input 120 v AC, 60 cycles, single phase, output, sec no. one 850 v ct at 200 ; sec no. two 450 v ct at .055 ; 49956 \# 292-5619G1; MIL type TF1SX02YY; 21964 \#A1069472 & Plate and bias voltage supply Figure 6-6 \\
\hline TB701 & & TERMINAL BOARD: 10 terminals; double screw type; barrier type; MIL type 8TB10 per spec MIL-T-16734 and Navy dwg 9000-S6505G-73214; 21964 \#A2133063-4 & Terminal board, power supply Figure 6-53 \\
\hline  & & Not Used & \\
\hline TB798 & 2 & TERMINAL BOARD: 16 Hollow solder stud terminals; 21964 \#B2060936G1 & Terminal board for power supply assy Figure 6-53 \\
\hline TB799 & 2 & TERMINAL BOARD: 20 hollow solder stud terminals; 21964 \#B2060937G1 & Terminal board in power supply assy Figure 6-53 \\
\hline V701 & 6 & ELECTRON TUBE: dual diode; MIL type 5R4WGB per spec MIL-E-1C; (Navy); 21964 \#A213449; same as V501 & Plate supply rectifier Figure 6-6 \\
\hline V702 & 6 & ELECTRON TUBE: dual diode; MIL type 6X4W per spec MIL-E-1C; 21964 \#700151; Same as V502 & Bias supply rectifier Figure 6-6 \\
\hline V703 & & \begin{tabular}{l}
ELECTRON TUBE: dual triode; MIL type 6080WA, per spec MIL-E- \\
1C; 21964 \#701276; Same as V503
\end{tabular} & Series regulator Figure 6-7 \\
\hline V704 & & ELECTRON TUBE: pentode; MIL type 6AH6; per spec MIL-E-1C; 21964 \#700116 & Control tube \\
\hline V705 & & ELECTRON TUBE: diode; MIL type 6627/OB2WA, per spec MIL-E-1 (Navy); 21964 \#A2133279; Same as V505 & Bias voltage regulator Figure 6-6 \\
\hline XDS701 & 6 & LAMP HOLDER: 125 v ; accommodates double contact bayonet base lamp; Military Standard lampholders dwg MS90290; 72619 \#9S4634-L-46; MIL type LH-71-XXO per spec MIL-L-3661; 21964 \#A9152053 or A2142519; Same as XDS502 & "POWER ON" warning light holder \\
\hline XV701 & 6 & SOCKET, ELECTRON TUBE: 8 contacts, beryllium silver plated octal, oval shaped; JAN type TS101P02 per spec JAN-S-28A; 71785 \#51B16758; 21964 \#740031; Same as XV501 & Socket for V701 plate supply rectifier Figure 6-53 \\
\hline XV702 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, brass, nickel plated; miniature; includes metal shield base, JAN type TS10-2P01, per spec JAN-S-28A-1;21964 \#740002; Same as XV308 & Socket for V702, bias supply rectifier Figure 6-53 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CODER-INDICATOR KY-382/GRN-9D
\(\left.\begin{array}{|c|c|c|c|}\hline \begin{array}{c}\text { REF } \\ \text { DESIG }\end{array} & \text { NOTES } & \text { NAME AND DESCRIPTION } & \begin{array}{c}\text { LOCATING } \\ \text { FUNCTION }\end{array} \\ \hline \text { XV703 } & & \text { Same as XV701 } & \begin{array}{c}\text { Socket for V703 } \\ \text { series regulator } \\ \text { Figure 6-53 }\end{array} \\ \text { XV705 } & & \text { Same as XV702 } & \begin{array}{c}\text { Socket for V704, } \\ \text { control tube } \\ \text { Figure 6-53 }\end{array} \\ & & \text { Same as XV702 } & \begin{array}{c}\text { Socket for V705, bias } \\ \text { voltage regulator }\end{array} \\ \text { Figure 6-53 }\end{array}\right]\)

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline 901-999 & & CABINET, ELECTRICAL EQUIPMENT CY-3163/GRN-9D: Steel color grey; overall dim. 34-1/8" lg., 25" wide, 72" high; cutout for specific equipment, qty. \(1,7-3 / 8^{\prime \prime}\) wide by \(15-15 / 16^{\prime \prime}\) high, Receiver, Radio R-824/URN; qty. 1, dim. 11-3/8" wide by 15\(5 / 16^{\prime \prime}\) high, Coder-Indicator; Qty. 1, dim. \(19-7 / 8^{\prime \prime}\) wide by 9 9/16' high, Control-Duplexer; qty. 1 , dim. \(19-7 / 8^{\prime \prime}\) wide by 205/16" high, Amplifier-Modulator AM-1701/URN; qty. 1, dim. 19-7/8' wide by \(7-9 / 16^{\prime \prime}\) high, Frequency Multiplier- Oscillator; carrying handles incl. qty. 2, eyebolts, adjacent corners on top of cabinet; dripproof; 4 shock mounts on bottom of cabinet \& 2 shock mounts on the back of the cabinet; junction box (located on back of cabinet) large enough to accommodate incoming cables; bottom portion of cabinet has built-in blowers \& filters; shock mounts are removable for equipment installation; 21964 \#J2060332 and A2060332; u/o AN/GRN-9D & Part of ReceiverTransmitter Group \\
\hline B901 & & FAN, CENTRIFUGAL: electric motor operated; non-portable; AC motor, fixed base; single unit on common shaft, direct drive connection, one rotor stage; single inlet with rectangular discharge outlet, 480 cfm at 2 in . static pressure; ccw rotation, 82877 \#AO-9293; 21964 \#A2060067 & ```
General ventilation
    (Receiver side
    cooling)
``` \\
\hline B901A & & MOTOR, ALTERNATING CURRENT: squirrel-cage induction type; AC, 208-220/440 v, 50-60 cps, \(3 \mathrm{ph} ; 3 / 4 \mathrm{hp}\), single take-off shaft, 3450 rpm , cw rotation of output shaft looking at load end; 82877 \#9293-01; p/o B901 & p/o centrifugal fan \\
\hline B902 & & FAN, CENTRIFUGAL: electric motor operated; non-portable; AC motor, fixed base; single unit on common shaft, direct drive connection; one rotor stage; single inlet with rectangular discharge outlet; 425 cfm at 3 in . static pressure; cw rotation, facing driving side; 82877 \#AO-9294; 21964 \#A20600068 & Ventilation for klystron V1304 \\
\hline B902A & & MOTOR, ALTERNATING CURRENT; squirrel-cage induction type; AC \(208-220 / 440 \mathrm{v}, 50-60 \mathrm{cps}, 3 \mathrm{ph} ; 1 / 2 \mathrm{hp}\), single take-off shaft, 3300 rpm , ccw rotation of output shaft looking at load end; 82877 \#9294-01; p/o B902 & p/o centrifugal fan \\
\hline DS901 & & LAMP, GLOW: neon gas, 0.04 watt; T-3-1/4 bulb; MLL type NE-51 per spec MIL-L-15098B; 21964 \#A2141970 & Indicator light Figure 3-6 \\
\hline E901 and E902 & & Not Used & \\
\hline E903 & 6 & INSULATOR, STANDOFF: MIL-STD-242A; 21964 \#B2061734 & HV input cable connection \\
\hline E904 and E905 & & Not Used & \\
\hline E906 & 6 & INSULATOR, STANDOFF: Steatite, grade L4A, MLL type NS4AB2016 per MIL-STD-242A; 21964 dwg \#A2133225-3 & Standoff for 700 v input \\
\hline E907 & & Same as E906 & Standoff for 1000 v input \\
\hline E908 & & Same as E906 & Standoff for 700 v internal connection \\
\hline F901 & & FUSE, CARTRIDGE: \(3 \mathrm{amp}, 125 \mathrm{v}\); time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 seconds; enclosed type; MIL type F02D3R00B per MIL-STD-MS90078-27-1 and spec MIL-F-15160C; 21964 \#882237; Same as F501; u/o AN/GRN-9D & ```
Overload protection
    for B901
    Figure 3-6
``` \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline F902 & & Same as F901; u/o AN/GRN-9D & Overload protection for B901 Figure 3-6 \\
\hline F903 & & Same as F901; u/o AN/GRN-9D & Overload protection for B901 Figure 3-6 \\
\hline F904 & & Same as F901; u/o AN/GRN-9D & Spare for F901, F902, F903 \\
\hline F905 & & FUSE, CARTRIDGE: \(2 \mathrm{amp}, 125 \mathrm{v}\), time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; ferrule type terminals; dim. \(0.250^{\prime \prime} \mathrm{lg}, 0.250^{\prime \prime}\) dia; enclosed type, glass case; one time; non-indicating; \(1-1 / 4^{\prime \prime} \mathrm{lg}\), \(0.250^{\prime \prime}\) dia, 0/a dim; MIL type F02D2R00B, per MIL-STD-MS9007-8-26-1 and spec MIL-F-15160A; 21964 \#882236; u/o AN/GRN-9D & \begin{tabular}{l}
Overload protection for B902 \\
Figure 3-6
\end{tabular} \\
\hline F906 & & Same as F905; u/o AN/GRN-9D & Overload protection for B902 Figure 3-6 \\
\hline F907 & & Same as F905; u/o AN/GRN-9D & Overload protection for B902 Figure 3-6 \\
\hline F908 & & Same as F905; u/o AN/GRN-9D & Spare for F905, F906, F907 \\
\hline FL901 & & FILTER, RADIO INTERFERENCE: 40 amps at 208 v ; \(\mathbf{6 0} \mathbf{~ c p s ; ~ h e r - ~}\) metically sealed; dim. \(2-7 / 8 \mathrm{in} . \mathrm{lg}, 2-1 / 8 \mathrm{in}\). w. \(4-5 / 16 \mathrm{in} . \mathrm{h}\); four \#10-32 NF-2A mtg studs on \(1-1 / 8 \mathrm{in}\). by \(1-7 / 8 \mathrm{in}\). centers; 2 thd terminals; 81831 \#FA1851E; 21964 \#A2060432; u/o AN/GRN-9D & External power cable \\
\hline FL902 & & Same as FL901; u/o AN/GRN-9D & External power cable \\
\hline FL903 & & Same as FL901; u/o AN/GRN-9D & Main input line noise filter \\
\hline FL904 & & FILTER, RADIO INTERFERENCE: 15 amps at 125 v ; 60 cps ; hermetically sealed; o/a dim. \(2 \mathrm{in} . \mathrm{lg}, 1-1 / 2 \mathrm{in} . \mathrm{w}, 3 \mathrm{in} . \mathrm{h}\); four \#8-32NC-2A mtg studs on \(3 / 8 \mathrm{in}\). by 1-1/4 in. centers; 2 thd ceramic terminals; 81831 \#FA2055A; 21964 \#A2060433 & Aux power line noise filter \\
\hline FL905 & & Same as FL904 & Aux power line noise filter \\
\hline FL906 & & Same as FL901; u/o AN/GRN-9D & Main input line noise filter \\
\hline J901 & & CONNECTOR, RECEPTACLE ELECTRICAL: 2 female flat contacts; not polarized; straight shape; 21964 \#A2060427 & Convenience outlet \\
\hline J902 & & Not Used & \\
\hline J903 & & CONNECTOR, ADAPTER: 2 contacts, female, round; straight type; MIL type UG-701/U per MIL std dwg \#MS90266; per 21964 \#A2141974 & 15 cps ref pulse input tocabinet, accepts P901 \& P903 \\
\hline J904 & & Same as J903 & 135 cps ref pulse input to cabinet \\
\hline *K901 & & RELAY, ARMATURE: 1A contact arrangement, 120 v AC; \(60 \mathrm{cps}, 5\) amps contact rating; 1 coil, 208 AC operating voltage, 185 v AC pick-up voltage at \(65 \mathrm{cps}, 130 \mathrm{v}\) AC drop-out voltage at \(55 \mathrm{cps}, 4\) watt; 3-11/32 in. lg, 1-31/32 in. sq; three no. 8-32 thd mtg studs located triangularly on bottom; 02116 \#RX-14-38; 21964 \#A2061031-1; u/o AN/GRN-9D & Loss of phase protection relay \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline K902 & & Same as *K901; u/o AN/GRN-9D & Loss of phase protection relay \\
\hline MP901 & & MOUNT, RESILIENT: mild steel; cadmium plated; 81860 part \#3500T10; 21964 \#B2060795 (4 each used) & Cabinet shock mounts \\
\hline MP902 & & IMPELLER, FAN, CENTRIFUGAL: multiblade type; forward curved blade; steel, cd pl; single w; 36 vanes; ccw rotation; 92172 \#610314H; 82877 \#9293-04; p/o B901 & p/o centrifugal fan \\
\hline MP903 & & IMPELLER, FAN, CENTRIFUGAL: multiblade type; forward curved blade; steel, cd pl; single w; 32 vanes; cw rotation; 95933 \#631-35-S; 82877 \#9294-04; p/o B902 & p/o centrifugal fan \\
\hline MP904 & & KNOB: oblong; phenolic; black; designed to accommodate flatted shaft, \(0.375^{\prime \prime}\) dia max, \(5 / 8^{\prime \prime}\) deep shaft hole; set screw fastened, 0.2 " dia holes; brass bushing; arrow marking; 3-1/2" lg. 7/8' wide, 1-1/8" deep ; per BuShips dwg \#9S5363-L item \#6; 21964 \#A2140920 & u/w emergency switch S901 \\
\hline MP905 & & CLAMP, ELECTRICAL: brass, silver plated; 1 clamp nut gland packing type; 21964 \#A21431-22-1 and A2143123-1 & u/w HV line goes to E903 \\
\hline MP906 & & CAP, ELECTRICAL: aluminum alloy, round; mounts by chain and 2-18NS-2A female thread; includes chain approx \(5-3 / 4^{\prime \prime} \lg\) between centers of attachments, brass, nickel pl; 02660 \#9760-32; 21964 \#A2060436 & External power cable \\
\hline MP907 & & BOLT, REDUCED SHANK: steel rod, type no. 303 per MIL-S-853, class 7, type C; passivate finish; head data not applicable to MBCA Ref Dwg Group 29; knurled thumb head socket recess, \(1 / 2^{\prime \prime}\) high, 7/8" dia, o/a dim., recess dim. , \(0.3120^{\prime \prime}\) dim. across flats, 3/8" deep; reduced shank data \(5 / 8^{\prime \prime}\) dia, \(25 / 32^{\prime \prime} \mathrm{lg} ; 3 / 8^{\prime \prime}-16 \mathrm{NC}-2\) thd, 3/8' min. lg; 2-5/32" nominal lgth; 21964 \#A9140059 (4 each used) & Used to secure unit in cabinet \\
\hline MP908 & & BOLT, REDUCED SHANK: steel rod type no. 303 per MIL-S-853 class 7, type A; electro polish; head data not applicable to MBCA Ref Dwg Group 29, knurled thumb head slotted, \(1 / 4^{\prime \prime}\) high, 1/2" dia, o/a dim., slot dim., \(1 / 16^{\prime \prime}\) wide, \(3 / 32^{\prime \prime}\) deep; reduced shank data \(0.171^{\prime \prime}\) dia, \(0.6875^{\prime \prime} \mathrm{lg}, 1 / 4^{\prime \prime}-20 \mathrm{NC}-2\) thread, \(0.3828^{\prime \prime} \mathrm{min}\). lg; 1.375' nominal lgth; 21964 \#A2141567-1 (4 each used) & u/w duct section \\
\hline MP909 & 2 & HOLDER, WRENCH: beryllium copper; nickel plated finish; holds wrench by means of two \(3 / 8^{\prime \prime}\) dia holes, one on each end, two \(0.193^{\prime \prime}\) dia mounting holes on \(1 / 4^{\prime \prime}\) by \(3 / 8^{\prime \prime}\) mounting centers; 21964 \#A2142246 & Holds wrench \\
\hline MP910 & 6 & WRENCH: Allen hexagon key type; size \(5 / 16^{\prime \prime}\); steel, cadmium plated; T handle; 70276 609T, per 21964 \#A2142269 & Used to secure unit \\
\hline MP911 & & CLEANER, AIR: round type; passivated stainless steel container; replaceable element; thumb head mounting bolt, 3 support straps equally spaced located at top; 00736 P-56, part \#C170-66; 21964 \#B2140978 (2 each used) & Air intake filter \\
\hline MP912 & & BEARING, BALL, ANNULAR: ground; single row; radial; nonloading groove; self contained; both rings flush; 0.7874 in. bore dia, 1, 8504 in. OD, 0.8125 w over-all; 2 closure shields; snap ring and groove external locating device; std internal fit-up data, ABEC-1 tolerances; high temp grease per spec MIL-G-3278; govt spec NAVY 42B5, II std; 28443 \#MRC204SFFC; p/o B901 & p/o centrifugal fan motor \\
\hline MP913 & & Same as MP912; p/o B902 & p/o centrifugal fan motor \\
\hline
\end{tabular}

\section*{ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D}
\begin{tabular}{|c|c|c|c|}
\hline REF & NOTES & \begin{tabular}{c} 
NAME AND DESCRIPTION
\end{tabular} \\
DESIG
\end{tabular}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP927 & 7 & CONDUIT ASSEMBLY, METAL FLEXIBLE: unshielded neoprene coated "Flexflyte L" outer conductor, fiberglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal band terminations; dim. o/a. 30 in . \(\mathrm{lg}, 1-1 / 16 \mathrm{in}\). OD, \(7 / 8 \mathrm{in}\). ID; 83144 FT-833; 21964 \#82143312-5 & Located in wiring harness \#3 \\
\hline MP928 & 7 & CONDUIT ASSEMBLY, METAL, FLEXIBLE: unshielded; neoprene coated "Flexflyte L" outer conductor; fiberglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal band terminations; dim. o/a. 29 in . lg, 1-1/4 in. OD, 1 in. ID; 83144 FT-834; 21964 \#B2143312-6 & Located in wiring harness \#1 \\
\hline MP929 & 7 & CONDUIT ASSEMBLY, METAL, FLEXIBLE: unshielded; neoprene coated "Flexflyte L" outer conductor; fiberglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal band terminations; dim. o/a, 25 in . lg, 1-1/4 in. OD, 1 in. ID; 83144 FT-835; 21964 \#B2143312-7 & Located in wiring harness \#4 \\
\hline MP930 & 7 & CONDUIT ASSEMBLY, METAL, FLEXIBLE: unshielded; neoprene coated "Flexflyte L" outer conductor; fiberglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal bend terminations; dim. o/a, 25 in . lg, 1-1/16 in. OD, 7/8 in. ID; 83144 FT-832; 21964 \# B2143312-4 & Located in wiring harness \#2 \\
\hline MP931 & & Same as 0913 & u/w junction box \\
\hline MP932 & 7 & COUPLING, HOSE: neoprene coated nylon; inch flange for mtg ; dim. 8 in . dia of flange, \(6-7 / 16 \mathrm{in}\). ID, \(2-5 / 16 \mathrm{in} . \mathrm{h}\); six 0.213 in . dia mtg holes equally spaced on 7.375 in . dia between centers; 98683 GWY-1 X; 21964 \#A2060954 & Couples air filter \\
\hline MP933 & 2 & RUBBER CHANNEL: synthetic medium; solid; 20-25/32 in. lg, \(1 / 4 \mathrm{in}\). \(\mathrm{w}, 1 / 8 \mathrm{in}\). thk; flanges \(3 / 16 \mathrm{in}\). deep, \(1 / 32\) in. thk; \(14370 \# 887\); 21964 \#A2061063G3 (2 each used) & Seals box in cabinet \\
\hline MP934 & 2 & RUBBER CHANNEL: synthetic medium; solid; 9-11/32 in. \(\lg , 1 / 4 \mathrm{in}\). \(w, 1 / 8\) in. thk; flanges \(3 / 16\) in. deep, \(1 / 32\) in. thk; \(14370 \# 887\); 21964 \#A2061063G4 (2 each used) & Seals air filter \\
\hline P901 & & CONNECTOR, PLUG ELECTR1CAL: 1 contact, male, round; straight type; M1L type UG-934A/U; ASESA dwg \#AS-2047 and MS90277; per 21964 \# A2131528 & 15 cps ref pulse ext cable plug, mates w/J903 \\
\hline P902 & & Same as P901 & 135 cps ref pulse ext cable plug, mates w/J904 \\
\hline P903 & 6 & CONNECTOR, PLUG ELECTR1CAL: 1 contact, male, round; straight type; M1L type UG-709A/U per MIL-STD dwg \#MS90214; per 21964 \#A2141976 & 15 cps ref pulse int cable plug, mates w/J903 \\
\hline P904 & & Same as P903 & 135 cps ref pulse int cable plug, mates w/J904 \\
\hline P905 & & CONNECTOR, PLUG, ELECTRICAL: 1 round male contact; one connector mating end; BNC series; 74868 \#85000; MIL type UG-88C/U per Sig dwg \#SC-D-72235; BuShips dwg \#REB49064; 21964 \#A2131456; Same as P201 & 15 cps ref pulse cable plug, mates w/J604 \\
\hline P906 & & Same as P905 & 135 cps ref pulse cable plug, mates w/J603 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
UESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline P907 & & CONNECTOR, PLUG, ELECTRICAL: 1 contact, male, round; straight type; MIL type UG-260B/U per Sig dwg *SC-D-72247; 21964 \#A2131518 & Video output to frequency multiplier oscillator drawer; mates w/J602 \\
\hline P908 & & Same as P905 & Dist info output to Coder-Indicator, mates w/J601 \\
\hline P909 & & Same as P905 & DME input to CoderIndicator, mates w/J504 \\
\hline P910 & & Not Used & \\
\hline P911 & & Not Used & \\
\hline P912 & & Not Used & \\
\hline P913 & & Same as P907 & Connects to J1350, modulator driver \\
\hline P914 & & Not Used & \\
\hline P915 & & Same as P905 & Connects to J1309, to klystron \\
\hline P916 & & Not Used & \\
\hline P917 & & Same as P907 & Connects to J1401, FMO \\
\hline P918 & & Same as P907 & Connects to J1402, FMO \\
\hline F919 & & Same as P905 & Connects to J1403, FMO \\
\hline P920 & & Same as P905 & Connects to J1407, FMO \\
\hline P921 & & CONNECTOR, PLUG, ELECTRICAL: 1 contact, male, round; straight type; MIL type UG-573A/U per ASESA dwg \#AS-2047; per 21964 \#A2141978 & Connects to J501 input Receiver \\
\hline P922 & & Same as P905 & Connects to \(\mathbf{J 5 0 2}\), input to local oscillator \\
\hline P923 & & CONNECTOR, PLUG, ELECTRICAL: 1 contact, male, round; N series; straight type; MIL type UG-21D/U per MIL-STD dwg \#MS-91236; 21964 \#A2132719; Same as P202 & Connects to Z1153: output to Receiver \\
\hline P924 & & Same as P905 & Connects to J1410, FMO \\
\hline P925 & & Not Used & \\
\hline P926 & & Same as P905 & Connects to \(\mathbf{J 1 5 0 6}\), FMO output low band \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

\section*{ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline P927 & 6 & CONNECTOR, PLUG, ELECTRICAL: 7 size 12,40 size 16 contacts, female round; polarized; straight type; AN3106A-36-7S, with cable clamp type AN3057-24, per spec MIL-C-5015-B; 21964 \#753077 & Connects to J605 Coder-Indicator \\
\hline P928 & 6 & CONNECTOR, PLUG, ELECTRICAL: 5 size 16 contacts, female, round; polarized; straight type; AN3106B-14S-5S, with cable clamp type AN3057-6 per spec MIL-C-5015; per 21964 \#752939 & Connects to J505 input to Power Supply \\
\hline P929 & & Not Used & \\
\hline P930 & & Same as P907 & Connects to P931 \\
\hline P931 & & CONNECTOR, PLUG, ELECTRICAL: 1 contact, female, round; straight type; BNC; MIL type UG-261B/U per MIL-STD-242A, Navy dwg \#REB49061; 21964 \#A2060428 & Connects to P930 \\
\hline P932 & & Same as P905 & Connects to P933 \\
\hline P933 & & CONNECTOR, PLUG, ELECTRICAL: 1 contact, female, round; straight type; BNC; MIL type UG-89B/U per MIL-STD-242A and MS35169, Navy dwg \#REB49132; 21964 \#A2132937 & Connects to P932 \\
\hline P934 & & CONNECTOR, PLUG, ELECTRICAL: 10 female contacts, size no. \(16 \mathrm{AWG}, 22 \mathrm{amp}\), four rated 700 v DC and six rated 250 v DC ; straight shape; MIL type AN3106A-18-1S per spec MIL-C-5015B; 21964 \#752953 & Connects to J 608 \\
\hline S901 & & SWITCH, ROTARY: 5 sections; 4 positions (two OFF and two ON) reciprocating action; non-pile up type, 5 poles, 2 throw; 60 amps , 450 v AC; 82181 type P, style 1 per 21964 \#A2141150; 21964 \#B2140975 & Emergency "ON-OFF" switch Figure 3-6 \\
\hline S902 & & SWITCH, PUSH-PULL: two single pole, double throw switches; AC, 10 amp ; 250 v ; momentary, 91929 \#4AC5 per spec MIL-S-6743; 21964 \#B2141195 & Interlock switch assembly, AmplifierModulator \\
\hline S903 & & Same as S902 & Interlock switch assembly, FMO \\
\hline S904 & 6 & SWITCH, INTERLOCK: door type; \(10 \mathrm{amp}, 110\) or 220 v AC or DC, single pole double break, female type, brass, silver pl; 21964 \#B2141184-1; This is one half of Navy type Switch \#CG-24067A or 24446 \#M-7460330-G4; (See E1317) & Interlock switch Amplifier-Modulator \\
\hline S905 & & Same as S902 & Interlock, switch assembly, Receive: \\
\hline S906 & & SWITCH, PUSH-PULL: SPDT w/actuator; AC, \(10 \mathrm{amp} ; 250 \mathrm{v}\) push to operate, momentary, actuates switch; pull to operate, maintained until reset by next push stroke; 91929 \#2AC6; MIL type MS16106A-1, per spec MIL-S-6743; 21964 \#B2141196 & Interlock switch Coder-Indicator \\
\hline S907 & & SWITCH, PRESSURE: SPDT; vane type; rotary actuated; switch assembiy shall operate at 0.50 in max static pressure (water column) and release at 01 in . min static pressure (water column); \(5 \mathrm{amp}, 250 \mathrm{v}\) AC; barrier type screw terminal board, MIL type 8TB2 per MIL-T-16784; 93652 \#113 per spec MIL-E-16400A and MIL-S-901B; 21964 \#A2061416 & Air switch for B901 \\
\hline TB901 & & TERMINAL BOARD: 12 feedthru type terminals, 24 thd studs; single row; barrier type; MIL type 5TB12, per spec MIL-T-16784; 21964 \#A21331 20-3 & External cable connection \\
\hline
\end{tabular}

TABLE 7-3, RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3163/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline TB902 & & TERMINAL BOARD: six 1/4"-20 stud type feed thru terminals w/terminal nuts; barrier type; 21964 \# B2142117 and A2142118-1 & External cable connection \\
\hline TB903 & & TERMINAL BOARD: 20 thd stud terminals in double row; barrier type; MIL type 4 TB20, per spec MIL-T-16784; 21964 \# A2133226-2 & External cable connection \\
\hline TB904 & & Same as TB903 & External cable connection \\
\hline TB905 & & Same as TB903 & External cable connection \\
\hline TB906 & & Same as TB903 & External cable connection \\
\hline TB907 & & Same as TB903 & External cable connection \\
\hline TB908 & & Same as TB903 & External cable connection \\
\hline TB909 & & TERMINAL BOARD: 10 terminals; double screw type; barrier type; voltage rating 600 v AC; MIL type 6TB10 per spec MIL-T-16784 and Navy dwg \# 9000-S6505B-73214;88223 p/o B901 & \(p / o\) centrifugal fan motor \\
\hline TB910 & & Same as TB909; p/o B902 & \(\mathrm{p} / \mathrm{o}\) centrifugal fan motor \\
\hline XDS901 & & LIGHT, INDICATOR: supplied w/lens 5/8" dia. amber, plain design, stovepipe shape, fluted, screw type holder; accommodates neon T-3-1/4, NE-51 lamp single contact miniature bayonet base; 125v, 75 watts; MIL type LH64PA5 per spec MIL-L-3661 and MS-90287; 21964 \# A2133081-2 & Lampholder for DS901 \\
\hline XF901 & & FUSE HOLDER: extractor post type; MIL type FHL10G per BuShips dwg \#9000-S6202-74228 and per spec MIL-F-19207 (Ships); 21964 \#A2060402; Same as XF501; u/o AN/GRN-9D & Fuseholder for F901 \\
\hline XF902 & & Same as XF901; u/o AN/GRN-9D & Fuseholder for F902 \\
\hline XF903 & & Same as XF901; u/o AN/GRN-9D & Fuseholder for F903 \\
\hline XF904 & & Same as XF901; u/o AN/GRN-9D & Fuseholder for F904 \\
\hline & & ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D & \\
\hline 1001-1099 & & CABINET, ELECTRICAL EQUIPMENT, CY-3164/GRN-9D: steel; color grey; overall dim. \(34-1 / 8^{\prime \prime} \lg\), \(25^{\prime \prime}\) wide, \(72^{\prime \prime}\) high; cutout for specific equipment, qty. 2 , dim. 7-1/2" wide by 13-5/8" high, space for Test Equipment; qty. 2, dim. 11-3/8" wide by 13-5/8" high, space for Test Equipment; qty. 1, dim. 7-1/2" wide by 15-1/4" high, Power Supply PP-1766/URN; qty 1, dim. 11-1/2" wide by 15-1/4" high; Power Supply PP-1765/URN; qty. 1 , dim. 21 " wide by 12-1/8" high, Power Supply PP-1763/ URN; carrying handles incl. qty. 2, eyebolts, adjacent corners on top of cabinet; dripproof; 4 shock mounts on bottom of cabinet and 2 shock mounts on the back of the cabinet; upper portion of cabinet has space for mounting future test equipment; junction box (located on back of cabinet) large enough to accommodate incoming cables; bottom portion of cabinet has built in blowers, filters and transformers; shock mounts are removable for equipment installation; 21964 \# J1069532 and A1069532; u/o AN/GRN-9D & Part of Power Supply Assembly GRN-9D \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
EI.ECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline B1001 & & FAN, CENTRIFUGAL: electrical motor operated; non-portable; AC motor, fixed base; single unit on common shaft, direct drive connection; one rotor stage; single inlet with rectangular discharge outlet; 425 cfm at 3 in. static pressure; ccw rotation; 82877 \#AO-9295; 21964 \#A2060429 & Ventilation (Power Supply side cooling) \\
\hline B1001A & & MOTOR, ALTERNATING CURRENT: squirrel-cage induction type; AC \(208-220 / 440 \mathrm{v}, 50-60 \mathrm{cps}, 3 \mathrm{ph} ; 3 / 4 \mathrm{hp}\), single take-off shaft, 3350 rpm , cw rotation of output shaft looking at load end; 82877 \#9295-01; p/o B1001 & p/o centrifugal fan \\
\hline DS1001 & & LAMP, GLOW: neon gas, 0.04 watt; T-3-1/4 bulk; ML type NE-51 per spec MIL-L-15098B; 21964 \#A2141970; Same as DS901 & Air switch "OPEN" indicator \\
\hline DS1002 & & LAMP, INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens, double contact bayonet base; clear; 24446 \#10C7/1DC; 21964 \#710071; Same as DS501 & Interlocks shorted \\
\hline E1001 & 6 & INSULATOR, STANDOFF: MIL-STD-242A; 21964 \#A2061861G2 & HV input cable connection \\
\hline E1002 thru E1009 & & Not Used & \\
\hline E1010 & 6 & INSULATOR, STANDOFF: steatite, grade L4A; MIL type NS4AB2016 per MIL-STD-242A; 21964 \#A2133225-3; Same as E906 & Standoff insulator for 700 v supply \\
\hline E1011 & & Same as E1010 & Standoff insulator for 1000 v supply \\
\hline F1001 & & FUSE, CARTRIDGE: \(15 \mathrm{amp}, 500 \mathrm{v}\); normal blowing; MIL type F60H15R0C per spec MIL-F-15160B and MIL-STD MS15249-11-1 (Ships); 21964 \#882290; u/o AN/GRN-9D & Pri protection HV plate T1001 \\
\hline F1002 & & Same as F1001; u/o AN/GRN-9D & Pri protection HV plate T1001 \\
\hline F1003 & & Same as F1001; u/o AN/GRN-9D & Pri protection HV plate T1001 \\
\hline F1004 & & Same as F1001; u/o AN/GRN-9D & Convenience outlet protection \\
\hline F1005 & - & Same as F1001; u/o AN/GRN-9D & Convenience outlet protection \\
\hline F1006 & & FUSE, CARTRIDGE: \(3.20 \mathrm{amp}, 250 \mathrm{v}\); time delay; MIL type F09G3R20B and MS90085-55-1, per spec MIL-F-15160; 21964 \#882326; u/o AN/GRN-9D & Blower protection
B1001 \\
\hline F1007 & & Same as F1006; u/o AN/GRN-9D & Blower protection
B1001 \\
\hline F1008 & & Same as F1006; u/o AN/GRN-9D & Blower protection
B1001 \\
\hline F1009 & & Same as F1001; u/o AN/GRN-9D & Spare for F1001 thru F1005 \\
\hline F1010 & & Same as F1006; u/o AN/GRN-9D & Spare for F1006. F1007. F1008 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D


ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP1009 & & CLEANER, AIR: round type; passivated stainless steel container; \(8-5 / 32^{\prime \prime} \mathrm{lg}, 8^{\prime \prime}\) dia, o/a dim.; replaceable element; thumb head mounting bolt approx \(7-1 / 4^{\prime \prime} \mathrm{lg}\) with \(3 / 8^{\prime \prime}-16 \mathrm{NC}-2\) thd at end, 3 support straps equally spaced located at top; 00736 \#P-56, part \#C17066; 21964 \#B2140978; Same as MP911 & Air intake filter \\
\hline MP1010 & & BEARING, BALL, ANNULAR: ground; single row, radial; nonloading groove; self contained; both rings flush; 8.7874 in . bore dia, 1.8504 in OD, 0.8125 in . w over-all;' 2 closures shields; snap ring and groove external locating device; std internal fit-up data, ABEC-1 tolerances; high temp grease per spec MLL-G-3278; govt spec NAVY 42B5, II std; 38443 \#MRC204FFC; Same as MP912; p/o B1001 & p/o centrifugal fan motor \\
\hline MP1011 & 2 & RUBBER CHANNEL: synthetic medium; solid \(10-3 / 32 \mathrm{in} . \mathrm{lg}, 1 / 4 \mathrm{in}\). w, \(1 / 8 \mathrm{in}\). thk; flanges \(3 / 16 \mathrm{in}\). deep, \(1 / 32 \mathrm{in}\). thk; \(14370 \# 887\); 21964 \#A2061063G1 (2 each used) & Seals box in cabinet \\
\hline MP1012 & 1 & GASKET: synthetic rubber, JAN-R-1149; class 1 ; not applicable to Ref Dwg Group 75; five \(0.290^{\prime \prime}\) dia holes for bolts on \(1-1 / 2^{\prime \prime}, 5-1 / 8^{\prime \prime}\), \(7-1 / 4^{\prime \prime}\) and \(4-3 / 4^{\prime \prime}\) respective mounting centers; o/a dim., \(20-15 / 16^{\prime \prime}\) lg, \(1^{\prime \prime}\) wide, \(1 / 16^{\prime \prime}\) thk; 21964 \#T2141114 ( 2 each used); Same as MP914 & u/w junction box \\
\hline MP 1013 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1 ; not applicable to Ref Dwg Group 75; four \(0.290^{\prime \prime}\) dia holes for bolts on \(4-3 / 4^{\prime \prime}, 4-3 / 4^{\prime \prime}\) and \(5-1 / 2^{\prime \prime}\) respective mounting centers; o/a dim., \(21-1 / 2^{\prime \prime} \mathrm{lg}, 1^{\prime \prime}\) wide, \(1 / 16^{\prime \prime}\) thk; 21964 \#T2141124; Same as MP915 & \(\mathrm{u} / \mathrm{w}\) junction box \\
\hline MP1014 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1 ; not applicable to Ref Dwg Group 75; four \(0.290^{\prime \prime}\) dia holes for bolts on 4-3/4", 4-3/4" and \(5-1 / 2^{\prime \prime}\) respective mounting centers; o/a dim., \(19-7 / 16^{\prime \prime} \mathrm{lg}, 1^{\prime \prime}\) wide, \(1 / 16^{\prime \prime}\) thk; 21964 \#T2141125; Same as MP916 & u/w junction box \\
\hline MP1015 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1 ; similar to style no. 12, Ref Dwg Group 75; 4-1/8' lg by \(2-7 / 8^{\prime \prime}\) wide aperture in center w/1/4" radius on corners; four \(0.290^{\prime \prime}\) dia holes for bolts on \(3-1 / 2^{\prime \prime}\) by \(4-3 / 4^{\prime \prime}\) mounting centers; o/a dim., \(5-1 / 4^{\prime \prime} \lg , 4^{\prime \prime}\) wide, \(1 / 16^{\prime \prime}\) thk, 1/4" radius on corners; 21964 \#B2141112 (4 each used); Same as MP917 & u/w junction box \\
\hline MP1016 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1; similar to style no. 12, Ref Dwg Group 75; 16-1/4' \(\lg\) by \(4-1 / 8^{\prime \prime}\) wide aperture in center w/1/4" radius on corners; ten \(0.290^{\prime \prime}\) dia holes for bolts on \(4-3 / 4^{\prime \prime}\) by \(16-7 / 8^{\prime \prime}\) mounting centers; o/a dim., \(17-3 / 8^{\prime \prime} \lg , 5-1 / 4^{\prime \prime}\) wide, \(1 / 16^{\prime \prime}\) thk, \(1 / 4^{\prime \prime}\) radius on corners' 21964 \#C2141113 (4 each used); Same as MP918 & u/w junction box \\
\hline
\end{tabular}

\section*{ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP1017 & 7 & COUPLING, HOSE: neoprene coated nylon; incl flange for mtg; dim., 8 in . dia of flange, 6-7/16 in. ID. 2-5/16 in. h ; six 0.213 in . dia mtg holes equally spaced on 7.375 in . dia between centers; 98683 CWY-1X; 21964 \# A2060954; Same as MP931 & Couples air filter to blower \\
\hline MP1018 & 2 & RUBBER CHANNEL: synthetic medium; solid; 9-19/32 in. lg, \(1 / 4 \mathrm{in}\). w, \(1 / 8\) in. thk; flanges \(3 / 16\) in. deep, \(1 / 32\) in. thk; 14370 ( 2 each used) no. 887; 21964 \#A2061063G2 & Seals air filter \\
\hline MP1019 & 2 & GASKET: filter; sponge rubber sheet; 8 in. OD; inside dia 6-3/8 in.; 56277; 21964 \# A2061116; Same as MP922 & Seals filter ring \\
\hline MP1020 & 2 & GASKET: synthetic rubber; dim. over-al 3-1/4 in. lg, 2-1/2 in. w, \(1 / 32\) in. thk; aperture 2-19/32 in. \(\mathrm{lg}, 1-27 / 32 \mathrm{in}\). w; eight \(3 / 16 \mathrm{in}\). dia mitg holes, four on 2-5/16 in. by 1-5/16 in. centers, four on 2-3/16 in. by \(1-1 / 2\) in. centers, 21964 \# A2061173; Same as MP920 & Seal in cabinet Receiver-Transmitter assy \\
\hline MP1021 & 2 & GASKET: synthetic rubber; 2-13/16 in. lg. 2-3/16 in. w, 1/32 in. thk; aperture 2 in . dia. four 3/16 in. dia mtg holes on 2-3/16 in. by 1-9/16 in centers; 21964 \# A2061190; Same as MP921 & Seal for bushing assy \\
\hline MP1022 & 7 & CONDUIT ASSEMBLY, METAL, FLEXIBLE: unshielded; neoprene coated "flexflyte L" outer conductor; fibreglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal band terminations; dim. o/a 23 in . lg, 1-1/16 in OD, \(7 / 8 \mathrm{in}\). ID, 83144 FT-831; 21964 \#B2143312-3 & Located in wiring harness \#2 \\
\hline MP1023 & & Same as MP1022 & Located in wiring harness \#3 \\
\hline MP1024 & & CONDUIT ASSEMBLY, METAL, FLEXIBLE: unshielded; neoprene coated, "Flexflyte L" outer conductor; fiberglass liner, covering and cord; 2-1/2 in. bending radius; cuff and metal band terminations; dim. o/a, \(25 \mathrm{in} . \lg , 1-1 / 16 \mathrm{in}\). OD, \(7 / 8 \mathrm{in}\). ID; 83144 FT-832; 21964 \#B2143312-4; Same as MP930 & Located in wiring harness \#1 \\
\hline R1001 & & RESISTOR, FIXED, WIREWOUND: 280 ohms total resistance, 3 watt power dissipation; \(350^{\circ} \mathrm{C}\) maximum continuous operating temperature; characteristic V; body dim. \(1 / 2\) ' \(\lg , 3 / 16^{\prime \prime}\) dia.; 2 wire lead terminals; MIL type RW59V281 per spec MIL-R-26C; 21964 \#A2132711-01; Same as R520 & Voltage dropping resistor \\
\hline S1001 & & SWITCH, PUSH-PULL: two single pole, double throw switches; AC, 10 amp .; 250 v push to operate, momentary, actuates one switch only, pull to operate, maintained until reset by next push stroke, both switches actuated; 91929 \#4AC5; per spec MIL-S-6743; 21964 \#B2141195; Same as S902 & Interlock switch assembly, Low Voltage Power \\
\hline S1002 & & Same as S1001 & Interlock switch assy, Medium Voltage Power Supply \\
\hline S1003 & & Same as S1001 & Interlock switch assy, transformer and blower compartment \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
HEF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline S1004 & 6 & SWITCH, INTERLOCK: door type; \(10 \mathrm{amp}, 110\) or 220 v AC or DC, single pole double break, female type, 21964 \#B2141184-1; This is one half of Navy type Switch \#CG-250A or 24446 \#M7460330G4 (see E1915); Same as S904 & Interlock switch HV power supply \\
\hline S1005 & & SWITCH, PRESSURE: SPDT; vane type rotary actuated; rotary actuated; switch assembly shall operate at 0.50 inch max, static pressure (water column), and release at 0.1 inch min static pressure (water column); \(5 \mathrm{amp}, 250 \mathrm{v}\) AC; similar to 93652 \#113 per spec M1L-S-901B; 21964 \#A2061416; Same as S907 & Air switch for B1001 \\
\hline S1006 & & SWITCH: 3 PDT, 15605 \#8795K3; 21964 \#A1069541 & \\
\hline T1001 & & TRANSFORMER, POWER. STEP-UP: encapsulated, epoxy resin; input data \(208 \mathrm{v} 60 \mathrm{cps}, 3\) phase; output data, 3 output windings 9440 v between terminals at 0.240 amp , per line; insulation to withstand 1000 v rms test on primaries and \(18,000 \mathrm{rms}\) on secondaries; maximum o/a dim. \(9-11 / 16^{\circ}\) high, \(16-3 / 4^{\prime \prime} \mathrm{lg}\). , \(9-9 /^{\prime} 16^{\prime \prime}\) wide; terminal data; for Optio. 2; 12 terminals, c/o 9 screw type terminals, 11/16" high on insulated pillars, and 3 flush mounted threaded inserts, \(8-32\) threads by \(1,4^{\prime \prime}\) deep for Option \(3 ; 12\) screw type terminals \(11 / 16^{\prime \prime} \pm i / 32^{\prime \prime}\) high on insulated pillars, four \(9,16^{\prime}\) dia. mtg holes on \(7-7,{ }^{\prime} 16^{\prime \prime}\) by \(13-5 / 8^{\prime \prime} \mathrm{mtg}\) centers; grounded electrostatic shield between the primary and secondary wincings; primary delta-connected secondaries starconnected for use with a 3 phase full-wave starconnected rectifier; 49950̈ \#292-5000Gl MIL type TF2TX02ZZ. per spec MIL-T-27A; 21964 \#A1069474; u o AN GRN-9( ) & 12 kv power supply plates \\
\hline TB1001 & & TERMINAL BOARD: 20 thd stud terminals in double row; barrier type; MIL type 4TB20, per spec MIL-T-16784; 21564 \#A2133226-2; Same as TB903 & External cable connection \\
\hline TB1002 & & Same as TB1001 & External cable connection \\
\hline TB1003 & & Same as TB1001 & External cable connection \\
\hline TB1004 & & Same as TB1001 & External cable connection \\
\hline TB1005 & & TERMINAL BOARD: 10 terminals; double screw type; barrier type; MIL type 6 TB10 per spec MIL-T-1ö784 and Navy dwg \#9000-S6505B73214; 88223; Same as TB909; p, o B1001 & p/o centrifugal fan motor \\
\hline XDS1001 & & LIGHT, INDICATOR: supplied w/lens, \(5 ; 8^{\circ}\) dia, amber plain design, stove-pipe shape: fluted, screw type holder; accommodates neon T-3-1/4, NE-51 lamp single contact miniature bayonet base; 125 v , 75 watt; brass sheil black nickel finish, enclosed; \(2-5 / 16^{\prime \prime} \mathrm{lg}, 15 / 10^{\prime \prime}\) dia o/a dim, 1 mounting hole required, \(11 / 16^{\prime \prime}\) dia., accommodates up to \(9 / 32^{\circ}\) max thick panel; horizontally mounted; lamp replaceable from front of panel; 2 terminals solder lug type. located on socket base, both insulated from shell: includes built in \(51,000 \mathrm{ohm} 1 / 3\) watt composition resistor; MIL type LH64 PA5 per spec MIL-L-3661 and MS-G0287; 21964 \#A2133081-2; Same as XDS901 & \[
\begin{aligned}
& \text { Lampholder for } \\
& \text { DS1001 }
\end{aligned}
\] \\
\hline
\end{tabular}

ELECTRICAL EQUIPMENT CABINET CY-3164/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

\section*{CONTROL-DUPLEXER C-2226A/GRN-9D}
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline CR1151 & & CRYSTAL UNTT, RECTIFYING: silicon, cartridge type; \(1,000 \mathrm{mc}\) frequency design; 8.0 db max conversion loss; 2.5 max output noise ratio; 6.5 watts burnout test; \(0.820^{\prime \prime} \mathrm{lg}, 0.294^{\prime \prime}\) dia overall dimensions; ferrule type terminals, one on each end; MIL type 1N25, per spec MIL-E-1C; 21964 \#700026 & Crystal detector assembly rectifier u/w E1152 \\
\hline DC1151 & & COUPLER, DIRECTIONAL: two end fittings, 02114 connectors, part no. CM-1013-9036B and CM-1010-9036C without bullet, for main line; two BNC type UG-185/U connector receptacles modified for indicator; 960 to \(1250 \mathrm{mc} ; 40 \mathrm{db}\) coupling; \(4.75^{\prime \prime} \mathrm{lg}, 1.46^{\prime \prime}\) wide, 2 , 34" high; incl protective end caps; type CU-430/URN-3; 21964 \#C2140826 and A2140827-1 & Klystron output monitoring \\
\hline \[
\begin{aligned}
& \mathrm{DC} 1152 \\
& \text { thru } \\
& \text { DC1155 }
\end{aligned}
\] & & Not Used & \\
\hline DC1156 & & Same as DC1151 & Antenna input monitoring \\
\hline DS1101 & & LAMP, INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens, double contact bayonet base; clear; 24446 \#10C7/1DC; 21964 \#710071, Same as DS501 & Filament lamp Figure 3-5 \\
\hline DS1102 & & Same as DS1101 & Main power Figure 3-5 \\
\hline DS1103 & & Same as DS1101 & Antenna control Figure 3-5 \\
\hline DS1104 & & Same as DS1101 & \begin{tabular}{l}
Interlock short \\
Figure 3-5
\end{tabular} \\
\hline DS1105 & & LAMP, GLOW: MIL type NE-51 per ML spec MIL-L-15098B; 21964 \#A2141970; Same as DS901 & \\
\hline \[
\begin{aligned}
& \text { E1101 } \\
& \text { thru } \\
& \text { E1151 }
\end{aligned}
\] & & Not Used & \\
\hline E1152 & & HOLDER, CRYSTAL: ML type 1 N 21 or 1 N 25 crystal diodes accommodated; 2 BNC type connector, female located on one end, male on other end; 74868 \#MS-585 per 21964 \#A2140845 & \begin{tabular}{l}
Ref detector \(u / w\) CR1151 \\
Figure 2-14
\end{tabular} \\
\hline \[
\begin{aligned}
& \text { E1153 } \\
& \text { thru } \\
& \text { E1161 }
\end{aligned}
\] & & Not Used & \\
\hline E1162 & & LINE SECTION, RADIO FREQUENCY TRANSMISSION: 50 ohms impedance, phosphor bronze, silver plated; friction mounted; cylindrical rod shaped; overall dimensions \(1-9 / 16^{\prime \prime} \mathrm{lg}, 0.341^{\prime \prime}\) dia; 02114 \#215-302C; per 21964 \#A2140636 & Connection between DC1151 and Z1156 or 21157 \\
\hline E1163 & & Same as E1162 & Connection between Z1156 or Z1157 and P1183 \\
\hline E1164 & & Same as E1162 & Connection between DS1151 and Z1156 or Z1157 \\
\hline E1165 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCATING \\
FUNCTION
\end{tabular} \\
\hline E1166 & & Not Used & \\
\hline E1167 & & Same as E1162 & Connection between P1183 and DC1156 \\
\hline E1168 & & Not Used & \\
\hline E1169 & & Not Used & \\
\hline E1170 & & Same as E1162 & Connection between DC1156 and P1157 \\
\hline E1171 & & Same as E1162 & Connection between DC1156 and P1167 \\
\hline E1172 & & Same as E1162 & Connection from P1158 to DC1151 \\
\hline F1101 & & FUSE, CARTRIDGE: \(3 \mathrm{amp}, 125 \mathrm{v}\); time delay; MIL type F02D3R00B, per spec MLL-F-15160A and MLL-STD MS90078-27-1; 21964 \#882237; Same as F501 & Transmitter start-stop circuit protection Figure 3-5 \\
\hline F1102 & & Same as F1101 & Control circuit neut bus protection Figure 3-5 \\
\hline F1103 & & FUSE, CARTRIDGE: \(15 \mathrm{amp} ; 250 \mathrm{v}\); time delay; MIL type F03G15R0B per spec MLL-F-15160A; MIL-STD MS90079-26-1; 21964 \#882263 & Deck unit protection Figure 3-5 \\
\hline F1104 & & Same as F1103 & Deck unit protection Figure 3-5 \\
\hline F1105 & & Same as F1101 & \begin{tabular}{l}
Spare for F1101. \\
F1102. and F1106
\end{tabular} \\
\hline F1106 & & Same as F1101 & Control circuit protection Figure 3-5 \\
\hline F1107 & & Same as F1103 & Regulated fil bus neut protection Figure 3-5 \\
\hline
\end{tabular}

CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline F1108 & & Same as F1103 & Regulated fil bus protection Figure 3-5 \\
\hline F1109 & & FUSE, CARTRIDGE: \(0.50 \mathrm{amp}, 250 \mathrm{v}\); time delay; MIL type F02GR500B per spec MIL-F-15160A and MIL-STD MS90078; 21964 \#882232 & Spare for F1110 \\
\hline F1110 & & Same as F1109 & M1101, DS1101 protection. Figure 3-5 \\
\hline F111 & & Same as F1103 & Unregulated plate supply bus protection Figure 3-5 \\
\hline F1112 & & Same as F1103 & \[
\begin{aligned}
& \text { Spare for F1103. } \\
& \text { F1104, F1107, F1108, } \\
& \text { F1111, F1113, F1114 }
\end{aligned}
\] \\
\hline F1113 & & Same as F1103 & \\
\hline F1114 & & Same as F1103 & \\
\hline J1101 & & JACK, TELEPHONE: accommodates 2 conductor female type plug, \(0.916^{\prime \prime}\) max. dia; contact arrangement not incl. in MBCA Ref Dwg Group 4, 2 conductor, tip and sleeve \(0.969^{\prime \prime}\) lg nose type contact; \(1-19 / 32^{\prime \prime}\) sq by \(1.718^{\prime \prime}\) deep overall dim.; four \(5 / 32^{\prime \prime}\) dia countersunk mounting holes on \(1-1 / 4^{\prime \prime}\) sq mounting centers on mounting plate; Navy type H-27A; BuShips dwg \#9000-S6501C-74120 Rev 1 modified by painting surface grey per 21964 \#A2143641 and A2143640-1 & Sound powered telephone connection Figure 3-5 \\
\hline J1102 & & CONN ECTOR, RECEPTACLE, ELECTRICAL: single female round contact; straight type; phone type connector, black nylon insulator overall dimensions \(15 / 16^{\prime \prime} \mathrm{lg}\), w/hex face nut \(5 / 16^{\prime \prime}\) across flats max operating voltage 1500 v peak; cylindrical shape, brass, nickel plated; silver plated contacts; one \(1 / 4^{\prime \prime}\) dia mounting stud w/1/4" -32 NS-2 thd, \(15 / 32^{\prime \prime} \mathrm{lg}\), one \(1 / 4^{\prime \prime}-32\) hex nut \(11 / 32^{\prime \prime}\) across flats, one lockwasher; 74868 type 225-B; MIL type MS16108-3 per MIL-STD-242A; 21964 \#A2141949-1; Same as J305 & Interlock test point at S1107A (11) Figure 2-14 \\
\hline J1103 & & Same as J1102 & Interlock test point at S1107A (1) and S1107B (9) Figure 2-14 \\
\hline J1104 & & Same as J1102 & Interlock test point at HV power supply Figure 2-14 \\
\hline J1105 thru J1151 & & Not Used & \\
\hline J1152 & & CONNECTOR, RECEPTACLE, ELECTRICAL: BNC series; 1-9/64" lg, \(0.212^{\prime \prime}\) ID; 50 ohms nom impedance; accommodates RG-58/U cables; weatherproof; 74868 \#86025; MIL type UG-909/U per BuShips dwg \#REB49058; 21964 spec \#A2132720; Same as J502 & Klystron output. reflected wave test point Figure 3-5 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J1153 & & Same as J1152 & Antenna input reflected wave test point Figure 3-5 \\
\hline J1154 & & Same as J1152 & Antenna input incident wave test point Figure 3-5 \\
\hline \(\mathbf{J 1 1 5 5}\) & & CONNECTOR, ADAPTER: 2 female contacts, round; straight type; \(2.207^{\prime \prime} \mathrm{lg}, 1-9 / 16^{\prime \prime}\) wide, \(1-9 / 16^{\prime \prime}\) high, o/a dimensions; radio frequency connector, 50 ohms nominal impedance, constant frequency impedance characteristic; cylindrical shape; brass, silver pl, polyethylene insert; mates with HN male and LC, UG-154/U or equivalent; includes mounting plate with four no. 9 (0.196") drill holes on \(1-3 / 16^{\prime \prime}\) by \(1-3 / 16^{\prime \prime}\) mounting centers; MIL type UG-259/U, per NAVY dwg \#REB49204; 21964 \#A2133206 & RF output to antenna Figure 3-5 \\
\hline \(\mathbf{J 1 1 5 6}\) & & Not Used & \\
\hline J1157 & & Same as J1152 & Klystron output incident wave test point Figure 3-5 \\
\hline K1101 & & RELAY, ARMATURE: closed type five poles normally open, one pole normally closed, 4 poles double break, 2 poles single break, double break contacts rated \(50 \mathrm{amp}, 220 \mathrm{v} \mathrm{AC}\), single break contacts rated \(10 \mathrm{amp}, 250 \mathrm{v} \mathrm{AC}\); single inductive winding, \(120 \mathrm{v} \mathrm{AC}\),60 cycles; 2 terminals on coil and each pole; continuous duty; \(6^{\prime \prime} \mathrm{lg}, 5-5 / 16^{\prime \prime}\) wide, \(4-3 / 8^{\prime \prime}\) high approx o/a dim. ; three mounting holes on \(0.228^{\prime \prime}\) dia on 2-1/2" by 4-5/8' mounting centers; one single break contact makes before other single break contact breaks per spec MIL-C2212A; similar to 04009 size 2 type "CRA" -241-U, modified per 21964 \#C2060991 and spec A2140748-5 & Primary power contactor Figure 6-61 \\
\hline K1102 & & RELAY, MOTOR DRIVEN: SPDT, 115/250 v, \(5 \mathrm{amp}, 60\) cycles; motor data AC, synchronous type, 105 to 132 v rms, 60 cycles; 2 terminals for motor, 3 terminals for contacts; 1 min time interval; resets automatically; hermetically sealed; overall dimensions 3-23/32" high, 2-23/32" dia; mounting 2-23/32" sq w/four 0.166" dia holes; 2-5/32" C to C located at bottom; time interval factory adjusted; 14907 type HT1L2M set at 1 min; 21964 \#A2142407 & Blower "OFF" time delay \\
\hline K1103 & & RELAY, ARMATURE: closed type; five poles single-throw contacts four poles normally open, one normally closed, 3 poles double break, 2 poles single break, double break contacts rated \(25 \mathrm{amp}, 220 \mathrm{v}\) AC, single break contacts rated \(10 \mathrm{amp}, 250 \mathrm{v} \mathrm{AC}\); single inductive winding, 120 v AC; 60 cycles; 2 terminals on coil and each pole; continuous duty; \(4-3 / 8^{\prime \prime} \mathrm{lg}, 3-7 / 8^{\prime \prime}\) wide, \(3-3 / 16^{\prime \prime}\) high approx \(0 / a\) dim. ; three mounting holes for \(0.190^{\prime \prime}\) dia screw, on \(2^{\prime \prime}\) by 3-1/4" mounting centers; one single break contact makes before other single break contact breaks; per spec MIL-C-2212A; similar to 04009 size 1 type 'RA"' modified per 21964 \#C2061343 and spec A2140748-6; Same as K1001 & Blower control Figure 6-61 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D. MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline M1101 & & VOLTMETER: panel mounted; AC, 60 cycles, single phase, 2 wires; marked "volts", 0 to 150 left to right graduated in increments of 5 , marked AC; round case molded thermosetting compound or metal; style no. 15, MBCA Ref Dwg Group 27; flange 2.69' dia, \(0.40^{\prime \prime}\) max. thick, \(2.21^{\prime \prime}\) body dia, \(1.36^{\prime \prime}\) body depth from mounting surface, excluding terminals; satisfactory for use on either nonmagnetic panels or magnetic steel panels \(1 / 16^{\prime \prime}\) to \(1 / 8^{\prime \prime}\) thick without additional calibration; black markings and pointer, white background; self contained; ruggedized; three \(0.125^{\prime \prime}\) dia mounting holes on \(1.22^{\prime \prime}\) radius; 2 screw stud type terminals \(1 / 4^{\prime \prime}-28\) thread, \(0.5^{\prime \prime}\) min. \(\lg\); ML type MR26W150ACVVR, per spec MIL-M-10304A; 21964 \#A2060455-1 & Monitor, regulated filament bus 120 v ac input Figure 3-5 \\
\hline MP1101 & & KNOB: oblong; phenolic; black; Navy dwg \#9000-S6202-A-74000-2; 21964 \#A2142041 & Knob for master switch, S1101 \\
\hline MP1102 & & KNOB: pointer; black; MS 700-18S per MIL-STD-242A; 21964 \#B2132733-2; Same as MP501 & Knob for interlock shorting switch S1 107 \\
\hline MP1103 & 5 & KNOB: black molded bakelite; 21964 \#B2061431G1 & Knob for T1101 Figure 2-14 \\
\hline MP1104 & & COVER, ELECTRICAL CONNECTOR: molded phenolic; includes beaded chain; u/w NAVY type H-27A jack; 21964 \#A9141291 and A9141290-1 & Covers J1101 \\
\hline MP1105 & & CAP, ELECTRICAL: brass, fits BNC female connector; includes beaded chain; 74868 \#1500 MLL type CW-123A/U; per spec MLL-C-3608 and NAVY dwg \#REA49050; 21964 \#A2141971; Same as MP504 & u/w J1152 \\
\hline MP1106 & & Same as MP1105 & u/w J1153 \\
\hline MP 1107 & & Same as MP1105 & u/w J1154 \\
\hline MP1108 & 7 & WRENCH: single open and spanner type w/two \(1 / 8^{\prime \prime} \lg , 0.113^{\prime \prime}\) dia pins; \(15 / 16^{\prime \prime}\) size opening; \(6^{\prime \prime} \mathrm{lg}, 1-9 / 16^{\prime \prime}\) wide, \(7 / 16^{\prime \prime}\) thk o/a dim.; bronze cadmium plated; straight head; flat straight handle; special for connectors; 02114 \#215-301 modified per 21964 \#B2141441 (2 each used) & Used to tighten connectors Figure 2-14 \\
\hline MP1109 & & BOLT, REDUCED SHANK: steel rod, type no. 303 per MLL-S-853 class 7, type C; passivate finish; head data not applicable to MBCA Ref Dwg Group 29, knurled thumb head socket recess, 1/2" high, \(7 / 8^{\prime \prime}\) dia, o/a dim., recess dim., \(0.3130^{\prime \prime}\) dim., across flats, \(3 / 8^{\prime \prime}\) deep; reduced shank data \(5 / 8^{\prime \prime}\) dia, \(25 / 32^{\prime \prime} \lg , 3 / 8^{\prime \prime}-16 \mathrm{NC}-2\) thd, 3/8" min, lg, 2-5/32" nominal lg; 21964 \#A9140059 (4 each used); Same as MP907 & Used to secure unit in cabinet \\
\hline MP1110 & & Same as MP1105 & u/w J1157 \\
\hline MP1111 & & Same as MP1105 & \\
\hline MP1112 & 2 & BOLT, REDUCED SHANK: steel rod type no. 303; passivate finish; rd knurled head w/screw driver slot; 21964 \#A130048A128 ( 6 each used) & Secures access door \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP1113 & & COUPLING ASSEMBLY: \(0.248^{\prime \prime}\) dia steel rod, passivated finish, with 2 " lg universal attached to each end by straight pin; accommodates round type shafts, \(0.250^{\prime \prime}\) dia bores; overall dim. \(7-3 / 8^{\prime \prime} \lg .1 / 2\) " OD; set screw mounted, four 6-32 NC-2B tapped holes; 21964 \#B2061846G1 & Connects to S1101 to panel \\
\hline MP1114 & 2 & GASKET: synthetic rubber, MIL-R-900C; 17/32 in. dia aperture in centre; three 0.144 in . dia holes spaced 120 deg apart on \(3 / 4 \mathrm{in}\). dia; 1 in OD by \(1 / 32\) in. thk; 21964 \# A2061686 & Seal for bearing on front panel \\
\hline MP1115 & & BOOT, DUST AND MOISTURE SEAL: silicone rubber bonded to a brass nickel plated hex nut 15/32-32 thd; \(3 / 4\) in. across flats, \(7 / 8 \mathrm{in}\). lg ; \#1030; 21964 \# A2132649-1; Same as MP202 & Seal for toggle switch \\
\hline MP1116 & & Same as MP1115 & Seal for toggle switch \\
\hline MP1117 & & Same as MP1 115 & Seal for toggle switch \\
\hline MP1 118 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1 ; similar to style no. 18, Ref Dwg Group 75;1-1/32" dia aperture in center; four 11/64" dia holes for bolts on 1-1/4" by 1-1/4" mounting centers; o/a dim., \(2-7 / 32^{\prime \prime} \lg , 1-9 / 16^{\prime \prime}\) wide, \(1 / 32^{\prime \prime}\) thk, \(5 / 32^{\prime \prime}\) radius on corners; 21964 \# A2141762 & Seals telephone connector plate to panel \\
\hline MP1119 & 1 & GASKET: synthetic rubber, JAN-R-1149, class 1 ; style no. 18, Ref Dwg Group 75; 1-5/32" dia aperture in center; four 11/64" dia holes for bolts on \(1-3 / 16^{\prime \prime}\) by \(1-3 / 16^{\prime \prime}\) mounting centers; o/a dim., \(1-17 / 32\) " \(\lg , 1-17 / 32\) " wide, \(1 / 32\) " thk, \(5 / 32\) '" radius on corners; 21964 \# A2141763 & \(\mathrm{u} / \mathrm{w}\) connector adapter J1155 \\
\hline MP1120 & 1 & GASKET: synthetic rubber, MIL-R-900C; 2-15/64 in. dia aperture in centre; three \(1 / 8 \mathrm{in}\). dia holes spaced 120 deg apart on 2-7/16 in dia; 2-11/16 in. dia OD, 1/16 in thk; 21964 \#B2060910; Same as MP205 & Seal for M1101 \\
\hline MP1121 & 1 & GASKET: synthetic rubber, MIL-R-900A, class 2; cross-section style no. 7, Ref Dwg Group 74; \(1 / 8^{\prime \prime}\) wide, \(5 / 32\) " high w/1/16" radius, approx \(65 " \lg ; 21964\) \#A9140800; Same as MP201 & Panel sealing \\
\hline P1101 thru P1150 & & Not used & \\
\hline P1151 & & CONNECTOR, PLUG, ELECTRICAL: 1 round male contact; one connector mating end; BNC series; 50 ohms nom impedance, 500 v peak voltage; accommodates RG-55/U and RG-58/U cables; weatherproof; 74868 \# 85000; MIL type UG-88C/U per Sig dwg \#SC-D-72235; BuShips dwg \# REB49064; 21964 \# A2131456; Same as P201 & Cable connector DC1151 (1) \\
\hline \[
\begin{aligned}
& \text { P1152 } \\
& \text { thru } \\
& \text { P1156 }
\end{aligned}
\] & & Not Used & \\
\hline P1157 & & CONNECTOR, ADAPTER: 2 female contacts; angle type; \(90^{\circ}\) angle; approx overall dim. 3 " \(\mathrm{lg}, 3^{\prime \prime}\) high, 1-13/32" dia; 50 ohms nominal impedance, constant frequency impedance characteristic; right angle shape, copper matl, commercial bright dip; brass couplings, one female coupling and one male coupling 1-1/4"-18 NEF-2 thd for \(7 / 8^{\prime \prime}\) line; to be supplied with protective end caps; 21964 \# A2061364; includes E1162 & Connects DC1 156 and P1183 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline P1158 & & Same as P1157 & Connects input cable DC1151 \\
\hline P1159 thru P1161 & & Not Used & \\
\hline P1162 & & Same as P1151 & Cable connector on DC1151 (R) \\
\hline P1163 thru P1166 & & Not Used & \\
\hline P1167 & & CONNECTOR, PLUG, ELECTRICAL: MIL type UG-1126/U; 21964 - \#B1069500 & Cable connector on W1152 \\
\hline P1168 & & CONNECTOR, FLUG, ELECTRICAL: 1 contact, male round; straight type; HN series; \(2-3 / 8^{\prime \prime} \mathrm{lg}, 7 / 8^{\prime \prime}\) dia, o/a dim.; radio frequency connector, 50 ohms nominal impedance, constant frequency impedance characteristic; cylindrical shape, brass, silver plated, gland locking type; teflon insert; 0 564" max size of cable opening; MIL type UG-494A/U per NAVY dwg *REB49217; 21964 \#A2133064 & Cable connector on N1 152 \\
\hline P1169 & 6 & CONNECTOR, ADAPTER: 2 contacts, one male, one female, round; type LC; angle type \(90^{\circ}\) angle; \(2.263^{\prime \prime} \mathrm{lg}, 1.474^{\prime \prime}\) high, \(0975^{\prime \prime}\) dia, \(0 / a\) dimensions; radio frequency connector, 50 ohms nominal impedance; constant frequency impedance; right angle shape; brass, silver pl, polyethylene insert; MLL type UG-216B/U, per spec MIL-C-3650 and NAVY dwg \#REB49158, Revision ' \({ }^{\text {D '; }} 21964\) \#A2141968 & Connects J1155 to. P1170 \\
\hline P1170 & & CONNECTOR, PLUG: 1 contact, male round; type LC; straight type; \(3^{\prime \prime} \mathrm{lg}, 1-1 / 2^{\prime \prime}\) dia. , o/a dim.; radio frequency connector, 50 ohms nominal impedance; constant frequency impedance; cylindrical shape, brass, silver pl; the insulation and center contact are provided by the dielectric and center conductor of the cable; \(0.945^{\prime \prime}\) dia max cable opening; coupling nut 1-1/2' across flats, \(1-1 / 4^{\prime \prime}-18\) NS-2 coupling nut thread; MIL type UG-154A/U, per spec MIL-C-3650 and NAVY dwg \#REB49152; 21964 \#A2141969 & Connects RG-18/U from antenna to RF output J1155 via P1169 \\
\hline P1171 & & Same as P1151 & Cable connector on DC1156 (R) \\
\hline P1172 thru P1174 & & Not Used & \\
\hline P1175 & & Same as P1151 & Cable connector on DC1156 (I) \\
\hline P1176 thru P1182 & & Not Used & \\
\hline & & & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline P1183 & & CONNECTOR, ADAPTER: 3 contacts, 2 female, 1 male; tee type; 4 in. \(\lg , 1-25 / 32 \mathrm{in}\). wide. 50 ohms impedance; constant impedance; tee shape, copper material; brass couplings, one female coupling and one male coupling \(1-1 / 4 \mathrm{in}\). thd, for \(7 / 8 \mathrm{in}\). line, one connector, male; one \#10-32 thd mtg hole tapped in block; 21964 \#C2061380G1 & Junction for P1157, Z1153 and Z1156 or Z1157 \\
\hline R1101 & & RESISTOR, FIXED, WIREWOUND: 280 ohms, 3 watt; \(350^{\circ} \mathrm{C}\) maximum continuous operating temperature; Characteristic V; MIL type RW59V281 per spec MIL-R-26C; 21964 \#A2132711-01; Same as R520 & Voltage dropping resistor, DS1101 \\
\hline R1102 & & Same as R1101 & Voltage dropping resistor, DS1102 \\
\hline R1103 & & Same as R1101 & Voltage dropping resistor, DS1103 \\
\hline R1104 & & Same as R1101 & Voltage dropping resistor, DS1104 \\
\hline S1101 & & SWITCH, ROTARY: 6 sections; 4 position reciprocating action; non "pile-up" type, 5 poles, 3 throws; 120 v AC, 60 cycles, \(10 \mathrm{amp} ;\) copper silver plated; phenolic sections between steel plates; \(2-47 / 64^{\prime \prime} \mathrm{lg}, 2-3 / 16^{\prime \prime}\) wide, \(2-1 / 8^{\prime \prime}\) high overall dim.; 4 mounting holes \#10-24 tap equally spaced on \(2-5 / 16^{\prime \prime}\) dia circle; round type shaft, \(13 / 16^{\prime \prime} \mathrm{lg}, 1 / 4^{\prime \prime}\) dia; screw type terminals; special switching sequence \(\mathrm{w} /\) both shorting and non-shorting contacts; 82121 " P ", style II or CHH type ' RP' per spec MIL-S-15291; 21964 \#B2141774 and spec A2141773 & Master unit "ON-OFF" switch Figure 3-5 \\
\hline S1 102 & & SWITCH, TOGGLE: double-pole, single throw; 0.75 amp 125 v DC; 25 amp 125 v AC., resistive load rating; plastic and metal; overall dim., excluding terminals, bushing and handle \(1-21 / 64^{\prime \prime} \mathrm{lg}, 49 / 64^{\prime \prime}\) wide, \(25 / 32^{\prime \prime}\) deep; bat type handle, \(11 / 16^{\prime \prime} \mathrm{lg}\), excluding lg of bushing; locking action 4 terminals, solder lug type, located on back; single hole mounting type, bushing \(15 / 32^{\prime \prime}-32\) NS-2 thread, 15/32" lg from mounting surface; one mounting nut assembled, other hardware packed in bulk; JAN type ST52K per spec JAN-S-23; 21964 \#828238 & Deck unit "ON-OFF" switch Figure 3-5 \\
\hline S1103 thru S1105 & & Not Used & \\
\hline S1106 & & SWITCH, TOGGLE: double-pole, double throw; 0.75 amp 125 v DC. , 15 amp 125 v AC., resistive load rating; plastic and metal, overall dim., excluding terminals, bushing and handle \(1-21 / 64^{\prime} \lg , 49 / 64^{\prime \prime}\) wide, \(25 / 32^{\prime}\) deep; bat type handle, \(11 / 16^{\prime \prime} \mathrm{lg}\), excluding If of bushing; locking action one side, other side momentarily on; 6 terminals, solder type lug located on back; single hole mounting type, bushing \(15 / 32^{\prime \prime}-32\) NS-2 thread, \(15 / 32^{\circ} \mathrm{lg}\) from mounting surface; one mounting nut assembled, other hardware packed in bulk; JAN type ST52R, per spec JAN-S-23; 21964 \#828243 & \begin{tabular}{l}
u/w M1 101 \\
Figure 3-5
\end{tabular} \\
\hline S1107 & & SWITCH, ROTARY: 2 sections; 2 positions; non pile-up type, 5 poles; solid silver alloy contacts; ceramic wafer; \(1-1 / 2^{\prime \prime} \mathrm{lg}, 1-1 / 4^{\prime \prime}\) wide, \(1-5 / 16^{\prime \prime}\) high; mounted by \(3 / 8^{\prime \prime} \mathrm{lg},-32\) thread bushing; flatted type shaft \(9 / 16^{\prime \prime} \mathrm{lg}, 0.250^{\prime \prime}\) dia, o/a dim.; solver lug type terminals; per spec MIL-S-3786; 21964 \#B2140830 & Interlock short switch Figure 3-5 \\
\hline S1108 & & Same as S1102 & Regulated filament Figure 3-5 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline T1101 & & TRANSFORMER, VARIABLE POWER: input voltage taps at 57. 5, 115 and 135 v , with respect to start of winding, \(\mathbf{6 0}\) cycles, single phase; output data 0 to 135 v range, \(6 \mathrm{amp}, 0.9 \mathrm{kva}\) rating; voltage varied by \(1-1 / 2^{\prime \prime}\) dia knob; winding and brush to frame test voltage not less than 500 v rms; air cooled; open frame, metal; overall dim , excluding terminals, 4-1/2' high, 4-1/2' wide, 3-15/16" deep; 5 terminals, solder lug type, located on top; 4 mounting holes \(0.265^{\prime \prime}\) dia \(3-3 / 4^{\prime \prime}\) by \(3-3 / 4^{\prime \prime} \mathrm{c}\) to c ; \(24655 \mathrm{~W}-5\) "Variac", as described or equal per spec MIL-T-27A; 21964 \#A2061 244 & "ON-OFF" switch Figure 2-14 \\
\hline T1102 & & TRANSFORMER, POWER STEP-DOWN: hermetically sealed, metal case; input data 70 v max. , 60 cycles, single phase; 1 output winding, \(17.5 \mathrm{v}, 14 \mathrm{amp}\); insulation to withstand 600 v rms test; dim., MBCA Ref Dwg Group 12, 3-3/4' max lg, 4-11/32' max. wide, 6-1/4' \(\max\) high; 4 terminals; solder lug type, located on top; four 5/16-18 NC-2 threaded studs on \(2-1 / 2^{\prime \prime}\) by 3-5/16" mounting centers; grounded electrostatic shield between the primary and the secondary; 49956 \#292-6017G2 MIL type TF1SX01YY per spec MIL-T-27A; 21964 \#A1069869 & p/o fil bus voltage regulation circuit \\
\hline TB1101 & & TERMINAL BOARD: 8 feedthru type terminals w/thd studs; barrier type; MIL type 5TB8, per spec MIL-T-16784; 21964 \#A2133120-1 & Incoming cable connector Figure 2-16 \\
\hline TB1102 & & TERMINAL BOARD: 12 terminals; single row, thru type terminals; voltage rating 600 v rms ; MIL type 7TB12 per spec MIL-T-16784A and Navy dwg \#9000-S6505G-73214; 21964 \#A2133072; Same as TB604 & Incoming cable connector Figure 2-16 \\
\hline TB1103 & & Same as TB1102 & Incoming cable connector Figure 2-16 \\
\hline TB1104 & & Same as TB1102 & Incoming cable connector Figure 2-16 \\
\hline W1152 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor 1/10 AWG stranded copper, type RG-119/U terminations; incl 2 MIL type connectors, P1167 and P1168, one located each end, as per 21964 \#B2061533G1 & Connects DC1156 and J1155 \\
\hline XDS 1101 & & LIGHT, INDICATOR: friction mtg lens holder: accommodates style S-6 lamp; \(125 \mathrm{v}, 6\) watts; MIL type LH63 PW3 per spec MIL-L-3661, dwg MS-90286; 21964 \#A2133069-5; Same as XDS501 & Retainer for DS1101 \\
\hline XDS1102 & & LIGHT, INDICATOR; friction mtg lens holder; accommodates style S-6 lamp; 125 v , 6 watts; MIL type LH63BB3 per spec MIL-L-3661, dwg MS-90286; 21964 \#A2133080-4 & Retainer for DS1102 \\
\hline XDS1103 & & Same as XDS1101 & Retainer for DS1103 \\
\hline XDS 1104
XDS1105 & & \begin{tabular}{l}
LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; 125 v , 6 watts; MIL type LH63BR3 per spec MIL-L-3661, dwg MS-90286; 21964 \#A2133080-1; Same as XDS1002 \\
LIGHT, INDICATOR: MIL type LH64PA5 per MIL-L-3661; MS90287; 21964 \#A2133081-2; Same as XDS901
\end{tabular} & Retainer for DS1 104 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

CONTROL-DUPLEXER C-2226A/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XF1101 & & FUSEHOLDER: extractor post type; accommodates 1 fuse; MIL type FHL10G per BuShips dwg \# 9000-S6202-74228 and per spec MIL-F19207 (Ships); 21964 \# A2060402; Same as XF501 & Holds F1101 \& F1102 \\
\hline XF1102 & & Same as XF1101 & Holds F1103 \& F1104 \\
\hline XF1103 & & Same as XF1101 & Holds F1107 \& F1108 \\
\hline XF1104 & & Same as XF1101 & Holds F1105 \& F1106 \\
\hline XF1105 & & Same as XF1101 & Holds F1109 \& F1110 \\
\hline XF1106 & & Same as XF1101 & Holds F1111 \& F1112 \\
\hline XF1107 & & Same as XF1101 & Holds F1113 \& F1114 \\
\hline Z1153 & & FILTER ASSEMBLY, ELECTRICAL: c/o three band pass filters on a common mtg plate; frequency data, 12 mc approx band width, 1024 to 1151 mc frequency range; 50 ohms input, 50 ohms output; dim. o/a, 8-3/4 in. lg, 2-1/8 in. w, 7-1/2 in. high; ceased, rectangular shape, metal; mounts by four thd inserts on mtg angle and by a \#8-32 screw in bottom of each cavity; type N modified series connector used as output loop; three cavities each w/micrometer adjustment; 21964 \# A2061359 & Receiver filter \\
\hline Z1154 & & Not Used & \\
\hline 21155 & & Not Used & \\
\hline Z1156 & & FILTER, BAND PASS: 400 kc approx band width, 960 to 1025 mc frequency range; 50 ohms input, 50 ohms output, 93341 \# 20B8400-L. 21964 \#C106585 & Transmitter band pass filter for spectrum control low band Figure 6-60 \\
\hline Z1157 & & FILTER, BAND PASS: 340 kc approx band width, 1150 to 1215 mc frequency range; 50 ohms input, 50 ohms output; 93341 \# 20B8900-H 21964 \#C1068586 & Transmitter band pass filter for spectrum control high band Figure 6-60 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline 1301-1399 & & \begin{tabular}{l}
AMPLIFIER-MODULATOR, AM-1701/URN \\
AMPLIFIER-MODULATOR, AM-1701/URN: class "A" radio frequency amplifier; 7 kw amplifier power output, 1 channel, 500 ohms impedance; AC; \(120 \mathrm{v}, 60\) cycles \(\pm 2\) cycles, single phase; DC; 12000 v ; aluminum cabinet; overall dim. \(26-25 / 32^{\prime \prime} \mathrm{lg}\). 23-1/16" wide, 21-13/32" high; rack mounted; 21964 \#J2060340 and "A2060340; u/o AN/GRN-9( )
\end{tabular} & Part of Receiver-Transmitter/GRN9D Figure 6-57 \\
\hline \[
\begin{aligned}
& \text { C1301 } \\
& \text { thru } \\
& \text { C1307 }
\end{aligned}
\] & & Not Used & \\
\hline C1308 & 6 & CAPACITOR, FIXED, MICA DIELECTRIC: \(.01 \mu \mathrm{f} \pm 10 \% ; 300 \mathrm{v}\) DC working; -200 to 200 parts/million/degree \(C\) temperature coefficient; MLL type CM35C-103K per spec MIL-C-5A; 21964 \#A2142279-1; same as C411 & Bypass M1301 \\
\hline C1309 & & Sarne as C1308 & Bypass M1302 \\
\hline C1370 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1000 v DCW, \(10 \mu \mathrm{f}\) \(\pm 10 \%\); MIL type CP70E1EG106K, per spec MIL-C-25A; 21964 \#641050 & Coupling to T1372 \\
\hline C1371 & & Same as C1370 & Coupling T1372 \\
\hline C1372 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(10 \mu \mathrm{f} \pm 10 \%\); 600 v DC working, MIL type CP70E1EF106K per spec MIL-C-25; 21964 "641041; Same as C501 & Bias supply filter Figure 6-58 \\
\hline C1373 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 400 v DCW, \(.1 \mu \mathrm{f}\) \(\pm 10 \%\); ML type CP05A1EE104K, per spec MIL-C-25A; 21964 \#A2133046-5 & Bias supply ripple filter \\
\hline C1374 & & Same as C1372 & Bias supply output filter Figure 6-58 \\
\hline CR1370 & & SEMICONDUCTOR DEVICE, DIODE: silicon; diode; MIL type 1N256 per spec MIL-E-1C; 21964 \#A2133078 & Bias rectifier Figure 6-59 \\
\hline CR1371 & & Same as CR1370 & Bias rectifier \\
\hline DS1301 & & LAMP INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens, double contact bayonet base; clear, 24446 \#10C7/1DC; 21964 *710071; Same as DS501 & \begin{tabular}{l}
T1303 'ON' indicator \\
Figure 2-7
\end{tabular} \\
\hline DS1302 & & Not Used & \\
\hline DS1303 & & LAMP, GLOW: neon gas, 0.04 watt; 120 v ; T-3-1/4 bulb; miniature bayonet base; MLL type NE-51 per spec MIL-L-15098B; 21964 \#A2141970; Same as DS901 & \begin{tabular}{l}
S1301 "OPEN" \\
Figure 2-7
\end{tabular} \\
\hline DS1304 & & LAMP, GLOW: neon gas, 0.25 watt, \(67-87\) v DC striking voltage; double contact bayonet type; T4-1/2 bulb; MIL type NE-16 per spec MIL-L-15098; 21964 \#A2060350; Same as DS502 & M1302 protector \\
\hline DS1305 & & Same as DS1301 & Illumination of klystron compartment \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1311 & & LINE SECTION, RADIO FREQUENCY TRANSMISSION: 50 ohms impedance, phosphor bronze, silver plated; friction mounted; cylindrical rod shaped; overall dimensions \(1-9 / 16^{\prime \prime} \mathrm{lg}, 0.341^{\prime \prime}\) dia; 02114 \#. 215-302C; 21964 \#A2140636; Same as E1162 & P1311 center conductor \\
\hline E1312 thru E1316 & & Not Used & \\
\hline E1317 & 6 & CONTACT, ELECTRICAL: \(u / w\) interlock switch; furnished conducting surface for switch; one brass contact, silver pl, rd. approx \(7 / 16^{\prime \prime}\) dia; \(1-7 / 8^{\prime \prime} \lg .1-1 / 2^{\prime \prime}\) wide, \(11 / 16^{\prime \prime}\) thk, approx o/a dim.; \(10 \mathrm{amp}, 110\) or 220 v AC or DC; two \(0.154^{\prime \prime}\) dia mounting holes on \(1-1 / 4^{\prime \prime}\) mounting center, recessed \(5 / 8^{\prime \prime}\) deep to clear \#6 hex nut; 21964 \#B2141184-2, this is one half of NAVY type switch \#2444624067A or 24446 \#M7460330-G3 (See S904) & u/w interlock switch \\
\hline E1318 thru E1321 & & Not Used & \\
\hline E1322 & & Same as E1311 & P1312 center conductor \\
\hline E1323 & & Same as E1311 & Z1303 input center conductor \\
\hline E1324 & & Same as E1311 & Z1303 output center conductor \\
\hline E1325 & & Same as E1311 & P1309 center conductor \\
\hline E1326 & & INSULATOR, STANDOFF: "Mycalex 410", grade L-4B, white glazed; square pillar; style no. 42 , section M, Ref Dwg Group 9; 3/4 in. lg, 1 in. sq; two 6-32 NC-2 thd insert 9/32 in. lg , located on bottom; one 1/4-20 NC-2 thd insert \(3 / 8 \mathrm{in}\). lg , located on top 21964 \#A2143188 & Standoff insulator \\
\hline E1327 & & Same as E1326 & Standoff insulator \\
\hline E1328 & & Same as E1326 & Standoff insulator \\
\hline E1329 & & Same as E1326 & Standoff insulator \\
\hline E1370 & 6 & SHIELD, ELECTRON TUBE: JAN type TS-102U01 per spec JAN-S-28A, modified; 21964 \#A2132988-1; Same as E201 & Shield for V1370 \\
\hline E1370A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U01; MIL-STD-242A type \#701; 21964 \#A2132886-1; Same as E201A & \[
\begin{aligned}
& \text { Insert for shield } \\
& \text { E1370 }
\end{aligned}
\] \\
\hline E1371 & 6 & SHIELD, ELECTRON TUBE: JAN type TS102U02 per spec JAN-S28A, modified; 21964 \#A2132988-2; Same as E202 & Shield for V1371 \\
\hline E1371A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U02; MIL-STD-242A type \#702; 21964 \#A2132886-2; Same as E202A & Insert for shield E1371 \\
\hline E1372 & 6 & SHIELD, ELECTRON TUBE: JAN type TS103U02 per spec JAN-S-28A modified; 21964 \#A2132988-5; Same as E307 & Shield for V1372 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1372A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U02; MLL-STD-242A type \#902; 21964 \#A2132886-5; Same as E307A & Insert for shield E1372 \\
\hline F1301 & & Not Used & \\
\hline F1302 & & FUSE, CARTRIDGE: \(3 \mathrm{amp}, 125 \mathrm{v}\) time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; ferrule type terminals, silver plated; dim. , \(1 / 4^{\prime \prime} \mathrm{lg}\), \(1 / 4^{\prime \prime}\) dia; enclosed type, glass case; one time; non-indicating; \(1-1 / 4^{\prime \prime} \lg , 0.25^{\prime \prime}\) dia, o/a dim. ; MIL type F02D3R00B, per spec MLL-F-15160C and MLL-STD MS90078-27-1; 21964 \#882237; Same as F501 & ```
Primary T1301
    protection
    Figure 2-7
``` \\
\hline F1303 and F1304 & & Not Used & \\
\hline F1305 & & Same as F1302 & \begin{tabular}{l}
Spare fuse \\
Figure 2-7
\end{tabular} \\
\hline J1309 & & CONNECTOR, RECEPTACLE: BNC series; \(1-9 / 64^{\prime \prime} \mathrm{lg}, 0.212^{\prime \prime}\) ID; 50 ohms nom impedance; accommodates RG-55 and RG-58/U cables; weather-proof; 74868 \#86025; MIL type UG-909/U per BuShips dwg \#REB49058; 21964 \#A2132720, Same as J502; p/o W1307 & RF input V1304 Figure 6-58 \\
\hline J1370 & & CONNECTOR, RECEPTACLE: 1 round female contact; one connector mating end; 50 ohm nom impedance, 500 v peak voltage; low loss plastic dielectric; straight shape; 1-3/64" \(\lg\) o/a; w/inclosing shell; proof; MIL type UG-1094/U BNC Series, ' \(\mathrm{D}^{\prime}\) ' hole mounting, per Navy dwg REB49063; 21964 \#A2131837; Same as J203 & Shaped pulse in from FMO Figure 6-58 \\
\hline K1301 & & RELAY, ARMATURE: contact arrangement 2 form C type, DPDT, MBCA Ref Dwg Group 4, break-make, AC, 120v, \(10 \mathrm{amp} ; 1\) winding, inductive winding; AC, 132 v , max continuous operation, operating current not rated, 60 cycles; 6 terminals for contacts, 2 terminals for coil; continuous duty; hermetically sealed; 2-5/8' high, \(1-25 / 32^{\prime \prime}\) wide, \(1-21 / 32^{\prime \prime}\) deep, o/a dim.; four no. 6-32 mounting studs spaced \(1.218^{\prime \prime}\) c to c located on bottom; 70309 PBH ; per spec MLL-R-5757C; 21964 \#A2060235 & \begin{tabular}{l}
T1370 primary delay \\
Figure 6-59
\end{tabular} \\
\hline M1301 & & AMMETER: panel mounted; DC; milliamperes, \(0-200\) left to right graduated in increments of 5, marked ' \(D C\) '', round, molded thermosetting compound or metal; style no. 15, MBCA Ref Dwg Group 27; flange \(2.69^{\prime \prime}\) dia. \(0.40^{\prime \prime}\) max thick, \(2.21^{\prime \prime}\) body dia, \(1.85^{\prime \prime}\) body depth from mounting surface, excluding terminals, \(2 \%\) accuracy at full scale reading; 150 millivolts drop across terminals; satisfactory for use on either non-magnetic panels or magnetic steel panels \(1 / 16^{\prime \prime}\) to \(1 / 8^{\prime \prime}\) thick without additional calibration; black markings and pointer, white background, self contained; ruggedized, three \(0.125^{\prime \prime}\) dia mounting holes on \(1.22^{\prime \prime}\) radius; 2 screw stud type terminals \(1 / 4-28\) thread, \(0.5^{\prime \prime} \mathrm{min} \lg ; \mathrm{MLL}\) type MR26W200DCMAR, per spec MLL-M-10304A; 21964 \#A2060455-6 & V1304 beam current meter Figure 2-7 \\
\hline M1302 & & VOLTMETER: panel mounted; kilovolts, 0.15 left to right, graduated in increments of 0.2 marked ' DC '; round, molded thermosetting compound or metal; style no. 15, MBCA Ref Dwg Group 27; flange 2. \(69^{\prime \prime}\) dia, \(0.40^{\prime \prime}\) max thick, \(2.21^{\prime \prime}\) body dia, \(1.86^{\prime \prime}\) body depth from mounting surface, excluding terminals, \(2 \%\) accuracy at full scale reading; 1 milliampere \(\pm 5 \%\) with 150 millivolts max terminal drop; satisfactory for use on either nonmagnetic panels or magnetic steel panels \(1 / 16^{\prime \prime}\) to \(1 / 8^{\prime \prime}\) thick without additional calibration; black markings and pointer, white background; used with external resistor; ruggedized \(0.125^{\prime \prime}\) dia. mounting holes on \(1.22^{\prime \prime}\) radius; 2 screw stud type terminals \(1 / 4-28\) thread, \(0.5^{\prime \prime}\) min lg; ML type MR26W0-15DCKVR; per spec MIL-M-10304A; 21964 \#A2060455-3 & High voltage indicator Figure 2-7 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline MP1301 & & WRENCH, OPEN END, FIXED: steel, 4-1/2 in. \(\mathrm{lg}, 5 / 32 \mathrm{in}\). thk; double ended type; \(1 / 2 \mathrm{in}\). opening, one end \(15^{\circ}\) angle opening, other end \(75^{\circ}\) angle opening; 65814 "1132; 21964 \#A2142701 & Mounted on cabinet \\
\hline MP1302 & 7 & PLUNGER, QUICK RELEASE: steel type B-1113, cadmium plated finish; \(5 / 8 \mathrm{in}\). overall Ig , thd insert \#8-32 NC-2, plunger extends \(3 / 32 \mathrm{in}\). from body, dia of plunger 0.080 in . max; 92214, "S-50; 21964 \#A2142321-1 & Mounted in cabinet frame \\
\hline MP1303 & & Same as MP1302 & Mounted in cabinet frame \\
\hline MP 1304 & 1 & GASKET: synthetic rubber, MIL-R-900 A, class 2; cross sectional style no. 7, Rel Dwg Group 74; \(1 / 8^{\prime \prime}\) wide, \(5 / 32^{\prime \prime}\) high \(w / 1 / 16^{\prime \prime}\) radıus, approx 65" lg; 21964 "A9140800; Same as MP201 & Panel sealing \\
\hline MP 1305 & 1 & GASKET: synthetic rubber, MIL-R-900C, class 1; styie no. 10 , MBCA Ref Dwg Group 75; 2-15/64" dia aperture in center; three \(1 / 8^{\prime \prime}\) dia holes spaced 120 deg apart on 2-7/16" dia; 2-11/16" outside dia. 1/16" thk; 21964 \#B2060910; Same as MP1120 & Sealing for meters \\
\hline MP1306 & & Same as MP1305 & \\
\hline P1308 & & CONNECTOR, PLUG, ELECTRICAL: 1 round male contact; one connector mating end; BNC series; 50 ohms nom impedance, 500 v peak voltage; accommodates RG-55/U and RG-58/U cables; 74868 \#85000; MIL type UG-88C/U per Sig dwg \#SC-D-72235; SuShips dwg \#REB49064; 21964 \#A2131456; Same as P201, p/o W1307 & RF input connector for V1304 \\
\hline P1309 & & CONNECTOR, PLUG: 1 round female inner conductor, 1 round 02114 \#CM-1013-9036B female coupling on end; radio frequency connector, 50 ohms nominal impedance, constant frequency; cylindrical shape, brass body; 9/16" dia max cable opening; ML type UG-1126/U; 21964 *B1069500; p/o W1301; Same as P1167 & Connector on W1301 \\
\hline P1310 & & Same as P1309; p/o W1301 & \\
\hline P1311 & & COUPLER, TRANSMISSION LINE: coaxıal line type; 950 to 1225 mc frequency range; 50 ohms nominal impedance; copper material; mounts to transmission line by two \(7 / 8 \mathrm{in}\). female brass couplings, 1-1/4-18 NEF thd; \(90^{\circ}\) bend; 1-3/4 in. distance from center of one end to contact surface of other end; 2.375 in . distance from center of second end to contact surface of other end; 02114 \#PA-8-11-2; 21964 "B2061800, \#A2061788 & Connects V1304 to P1312 \\
\hline P1312 & & COUPLER, TRANSMISSION LINE: coaxıal line type; \(950-1225 \mathrm{mc}\) frequency range; 50 ohms nominal impedance; copper material; mounts to transmission line by one \(7 / 8 \mathrm{mn}\). male coupling with nut and one \(7 / 8\) in. female coupling; male coupling nut \(1-1 / 4-18\) NEF-2B thd, female couphing 1-1/4-18 NEF thd; \(180^{\circ}\) bend; \(2-1 / 2 \mathrm{in}\). distance from center of one end to contact surface of other end; 02114 \#PA-8-12-1; 21964 *B2061777G1, \#A2061789 & Connects Z1303 to P1311 \\
\hline P1313 & & Same as P1312 & Connects Z1303 to P1309 \\
\hline R1390 & & \[
\begin{array}{cl}
\text { Resistor Set, Fixed, Wirewound. Selected from: } \\
10 \mathrm{~W} / 5905-99-720-2849, & 10 \mathrm{~W} / 5905-99-720-2851 \\
10 \mathrm{~W} / 5905-99-720-2853, & 10 \mathrm{~W} / 5905-99-720-2855 \\
10 \mathrm{~W} / 5905-99-720-2857, & 10 \mathrm{~W} / 5905-99-720-2859 \\
10 \mathrm{~W} / 5905-99-720-2860, & 10 \mathrm{~W} / 5905-99-720-2862 \\
10 \mathrm{~W} / 5905-99-720-2864, & 10 \mathrm{~W} / 5905-99-720-2867
\end{array}
\] & \begin{tabular}{l}
Klystron \\
filament \\
shunt resistor
\end{tabular} \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1306 & & RESISTOR, FIXED, WIREWOUND: inductive winding: 7.5 megohms, \(+0.5 \% ; 1 \mathrm{kv}\) per megohm of resistance voltage rating; \(150^{\circ} \mathrm{C}\) max continuous operating temp; tempered glass case, \#MFA type EX-59; 21964 \# A2142549-1 & High voltage metering multiplier, M1302 Figure 2-8 \\
\hline R1307 & & Same as R1306 & High voltage metering multiplier, M1302 Figure 2-8 \\
\hline R1314 & & RESISTOR, FIXED, FILM (HIGH STABILITY): 1000 ohms, \(\pm 5 \%\); 55 watt, \(225^{\circ} \mathrm{C}\) hot spot temperature; glass insulated, excellent high frequency properties; 14674 \# RW-37 pe I MIL-R-11804A; 21964 \# A2141186-2 & High voltage bus discharge Figure 6-59 \\
\hline R1319 & & RESISTOR, FIXED. WIREWOUND: 280 ohms, 3 watt; \(350^{\circ} \mathrm{C}\) maximum continuous operating temp; characternstic V; MIL type RW59V-281 per MIL-R-26C; 21964 \# A2132711-01; Same as R520 & DS 1301 voltage dropping resistor \\
\hline R1370 & & RESISTOR. FIXED, WIREWOUND: 14 watts; 350 deg C continuous operating temp; MIL type RW31 V501, per spec MIL-R-26B; 21964 \#A2133346G3 & T1302 loading \\
\hline R1371 & & RESISTOR, FIXED, COMPOSITION: \(\mathbf{8 2 , 0 0 0}\) ohms, \(\pm 5 \% ; 1\) watt MIL type RC32GF823J; per spec MIL-R-11; 21964 \# 503836 & T1371 voltage divider \\
\hline R1372 & & RESISTOR, FIXED, COMPOSITION: 150,000 ohms, \(\pm 5 \% ; 1.0\) watt, MIL type RC32GF154J, per spec MIL-R-11; 21964 \#503842 & T1371 voltage divider \\
\hline R1373 & & RESISTOR, FIXED, COMPOSITION: 68,000 ohms; \(\pm 5 \%\) : 1 watt; MIL type RC32GF683J; per spec MIL-R-11; 21964 \# 503834 & V1370 screen voltage divider \\
\hline R1374 & & RESISTOR, FIXED, COMPOSITION: 39,000 ohms, \(\pm 5 \%\); 1 watt, MIL type RC32GF393J, per sper MIL-R-11; 21964 \# 503828 & V1370 screen voltage divider \\
\hline R1375 & & \begin{tabular}{l}
RESISTOR, FIXED, COMPOSITION: 100,000 ohms; \(\pm 10 \% ; 1 / 2\) \\
watt; MIL type RC20GF104K per spec MIL-R-I1; 21964 \# 504255; Same as R320
\end{tabular} & V1370 plate load \\
\hline R1376 & & RESISTOR, FIXED, COMPOSITION: 470 ohms; \(\pm 5 \%\); 2 watt MIL type RC42GF471J, per spec MIL-R-11; 21964 \# 501105 & V1372 grid parasitic suppressor \\
\hline R1377 & & Same as R1376 & V1372 grid parasitic suppressor \\
\hline R1378 & & RESISTOR, FIXED, COMPOSITION: 33 ohms, \(\pm 5 \% ; 2\) watt; MIL type RC42GF330J, per spec MIL-R-11; 21964 \# 501077 & V1372 cathode parasitic suppressor \\
\hline R1379 & & Same as R1378 & V2372 cathode parasitic suppressor \\
\hline R1380 & & Same as R1378 & VI370 grid parasitic suppressor \\
\hline R1381 & & RESISTOR, FIXED, COMPOSITION: 100,000 ohms, \(\pm 5 \%\); I/ 2 watt; MIL type RC20GF104], per spec MIL-R-1IA; 21964 \# 504151; Same as R444 & Bias supply voltage divider \\
\hline R1382 & 6 & RESISTOR, VARIABLE: composition; 100,000 ohms \(\pm 10 \%\); one section; 2 watt; std A taper; MIL type RV4LAVSA104A per spec MIL-R-94A; 21964 \# A2133049-3; Same as R672 & Bias supply voltage divider Figure 6-59 \\
\hline R1383 & & RESISTOR, FIXED, COMPOSITION: 220,000 ohms; \(\pm 5 \% ; 1 / 2\) watt; MIL type RC20GF224J per spec MIL-R-11; 21964 \# 504159 & Bias supply voltage divider \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1384 & & RESISTOR, FIXED, WIREWOUND: 4,000 ohms; 14 watts; MIL type RW31V40-2, per spec MIL-R-26C; 21964 \#A2133346G2 & Bias supply load \\
\hline R1385 & & RESISTOR, FIXED, WIREWOUND: inductive winding; 20 ohms, \(\pm 5 \%\); 113 watts; MIL type RW37V200 per spec MIL-STD-242A; 21964 \#A2061920 & Klystron surge protection \\
\hline S1301 & & SWITCH, PRESSURE: SPDT; vane type rotary actuated; switch assembly shall operate at 0.50 inch max static pressure (water column) and release at 0.1 inch min static pressure (water column); \(5 \mathrm{amp}, 250 \mathrm{v}\) AC; barrier type screw terminal board; MIL type 8TB2 per MIL-T-167-84; located on top; 5/8" mounting stud omitted, mounted by \(5 / 8^{\prime \prime}-18 \mathrm{NF}-2\) tapped hole; similar to 93652 \#113 per spec MIL-E-16400A and MIL-S-901B; 21964 \#A2061416 & Air pressure switch \\
\hline \[
\begin{gathered}
\mathrm{S} 1302 \\
\text { thru }
\end{gathered}
\] & & Not Used & \\
\hline S1304 & & SWITCH, TOGGLE: SPDT: \(0.75 \mathrm{amp}, 125\) v DC., \(15 \mathrm{amp}, 115\) v AC, resistive load rating; JAN type ST42A, per spec JAN-S-23; 21964 \#828212; Same as 5502 & Trouble light switch \\
\hline S1370 & & SWITCH, SHORTING: high voltage discharge, DC; SPST, normally closed, double break, 21964 \#C2140529 and A2140528-1 & High Voltage discharge Figure 6-59 \\
\hline S1371 & & SWITCH, SENSITIVE: SPDT: \(115 \mathrm{v}, 0.4 \mathrm{amps}\); plunger type actuator; per spec JAN-S-63, part \#SS03A20; 21964 \#A2133423G1 & Filament compartment interlock \\
\hline T1370 & & TRANSFORMER, POWER, STEP DOWN AND STEP UP: open frame; input 120 v AC, 60 cycles, single phase; 2 output windings, no. 1 secondary 120 v at 1 amp , no. 2 secondary 4.2 v at 43 amp ; insulation to withstand 600 v rms test on primary and \(23,400 \mathrm{v}\) rms test on secondaries; 6 screw type terminals; grounded electrostatic shield between primary and all secondaries, 49956 \#292-6006G2 per spec MIL-T-27A; 21964 \#1069476 & V1304 filament transformer and bias chassis power transformer Figure 2-8 \\
\hline T1371 & & TRANSFORMER, POWER, STEP DOWN AND STEP UP: encapsulated, epoxy resin; input 120 v AC, 60 cycles, single phase; 2 output windings, no. 1 secondary 225 v at 0.1 amp , no. 2 secondary \(6.3 \mathrm{v} / \mathrm{CT}\) at 1 amp ; insulation to withstand 600 v rms test on primary, 1680 v rms test on HV secondary and 980 v rms test on LV secondary; 8 solder lug terminals; grounded electrostatic shield between primary and all secondaries; 49956 \#292-6007G2 per spec MIL-T-27A; 21964 \#A1069477 & Bias chassis transformer Figure 6-58 \\
\hline T1372 & & TRANSFORMER, PULSE: hermetically sealed, metal case; 500 ohms impedance at \(7200 \pm 180 \mathrm{pps} ; 800 \mathrm{v}\) operating voltage on primary, voltage transformation \(1: 1 \mathrm{w} / 500 \mathrm{ohm}\) secondary load; 2400 v rms primary, 18.5 kv rms secondary insulation test voltages; dim. o/2 4-7/8 in. lg, 3-7/16in. w, 2-29/32in. h; 4 solder lug pillar type terminals, two \(25 / 32 \mathrm{in}\). h , other two 2-7/8 in. h from surface of case; mounts by 4 thd studs on 2-5/8 in. by 2-1/8 in. mtg centers; 49956 \#363-6009G2 per spec MIL-T-27A, part \#TF1RX36JA; 21964 \#A1069478 & T1304 grid pulse transformer Figure 6-59 \\
\hline TB1301 & & TERMINAL BOARD: 8 terminals; thru type terminal ; voltage rating 600 v rms; MIL type 7TB8 per spec MIL-T-1,\(~ 84 \mathrm{~A}\) and NAVY dwg 9000-S6505G-73214; 21964 \#A2133072-1; Same as TB501 & Power input Figure 6-58 \\
\hline TB1302 & & Same as TB1301 & \begin{tabular}{l}
Power input \\
Figure 6-58
\end{tabular} \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
AMPLIFLER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline TB1370 & & TERMINAL BOARD: 6 feedthru type terminals, barrier type; MIL type 11TB6, spec MLL-T-16784; 21964 *A2133380-G2 & Bias chassis connections Figure 6-59 \\
\hline TB1398 & & TERMINAL BOARD: (For Reference Only) & Resistor mtg board \\
\hline TB1399 & 2 & TERMINAL BOARD: 25 solder stud type terminals; 21964 \#B2061636 & Resistor mtg board, bias chassis \\
\hline V1304 & & ELECTRON TUBE: klystron cavity; metal envelope, non-standard envelope, cylindrical shape, top 6-7/8" sq, 17-1/4" min. 19" max. lg o/a dim. excluding terminals; 7 terminals, two rigid leads from base of tube and grid connection, one BNC radio frequency input and one monitor fitting, one \(7 / 8^{\prime \prime}\) coaxial radio frequency output fitting, all located at side of envelope, ceramic output connector seal; one ground connection located at top of envelope; test power output 7-5 kw; cascade amplifier klystron, control grid modulated; 56232 \#SAL-89 per spec MIL-E-1; 21964 \#A. 2061964 & Power amplifier \\
\hline V1370 & & ELECTRON TUBE: pentode; MIL type 5654/6AK5W per spec MIL-E-1C; 21964 \#700561; Same as V201 & Regulator a mplifier bias chassis Figure 6-59 \\
\hline V1371 & & ELECTRON TUBE: diode; glass envelope; RMA envelope T-5-1/2; 7 terminations, pin type, located on bottom; miniature voltage regulator; USN type 5651 WA; per spec MIL-E-1C; (Navy); 21964 \#A2133280 & Voltage reference, bias chassis Figure 6-59 \\
\hline V1372 & & ELECTRON TUBE: twin triode; glass envelope; RMA type T6-1/2; 9 terminations; pin type; located on bottom mfg class, amplifier; USN type 5687 WA ; per spec MIL-E-1C (Navy); 21964 \#A2133281; Same as V606 & Bias chassis, series regulator Figure 6-59 \\
\hline W1301 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, MIL type no. RG-87A/U, 50 ohms nominal impedance, 7 strands no. 20 AWG silver coated copper wire, dielectric teflon \(0.290^{\prime \prime}\) nominal dia, double braid copper shield, round shape, \(0.440^{\prime \prime}\) o/a crosssection dia, fibreglas silicone impregnated jacket; assembly \(63^{\prime \prime} \pm 1 / 4^{\prime \prime}\) long overall cable 56-3/4" lg excluding terminations; connector plugs P1309 and P1310, 21964 \#B2061559 located one on each end; insulation stripped \(5 / 8^{\prime \prime}\) and tinned, shield stripped 7/8', jacket stripped 1-1/8'; 21964 \#B2061540 & RF output cable assembly, V1304 \\
\hline W1307 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, tefion dielectric, single silver coated copper shield, outermost covering teflon-tape seal, fiberglas braid jacket; 0.195 in . dia o/a cross section of cable; MIL type RG-141/U; assembly is approx 43-1/4 in. Ig incl terminations; incl two MIL type connectors, P1308 and J1309, one located each end, as per 21964 \#B2061204 & Cable connects J1309 to V1304 input \\
\hline XDS1301 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; MBCA Ref Dwg Group 7, double contact bayonet candelabra; 125 v 6 watts; enclosed frame; steel shell; black nickel, overall dim., 3-1/32" lg., \(1-1 / 8^{\prime \prime}\) dia; panel mounted, 1 in . hole required; horizontally mounted; white jewel, plain design, torpedo shape, MIL type LH63PW3 per spec MLL-L-3661, dwg MS-90286; 21964 \#A2133069-6; Same as XDS501 & Holder for DS1301 \\
\hline
\end{tabular}

AMPLIFIER-MODULATOR AM-1701/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REf \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XDS1303 & & LIGHT, INDICATOR: supplied w/lens, \(5 / 8^{\prime \prime}\) dia, amber, plain design, stovepipe shape, fluted, screw type holder; accommodates neon T-3-1/4 NE-51 lamp single contact miniature bayonet base; \(125 \mathrm{v}, 75\) watt; brass shell black nickel finish, enclosed; 2-5/16" lg , \(15 / 16^{\prime \prime}\) dia o/a dim. , 1 mounting hole required, \(11 / 16^{\prime \prime}\) dia., accommodates up to \(9 / 32^{\prime \prime}\) max thick panel; horizontally mounted; lamp replaceable from front of panel; 2 terminals, solder lug type, located on socket base; both insulated from shell; includes built in 51,000 ohm \(1 / 3\) watt composition resistor; MIL type LH64PA5 per spec MIL-L-3661 and MS-90287; 21964 \#A2133081-2; Same as XDS901 & Holder for DS1303 \\
\hline XDS 1304 & 6 & LAMP HOLDER: 125 v ; accommodates double contact bayonet base lamp; MBCA Ref Dwg Group 7; molded bakelite body; body dim \(1-9 / 16 \mathrm{in} . \lg , 1 \mathrm{in}\). wide, \(1-1 / 8 \mathrm{in}\). high; 2 screw type terminals; two \(3 / 16 \mathrm{in}\). dia holes on \(1-3 / 16 \mathrm{in}\). mtg centers; Military Standard lamp-holders dwg MS90290; 72619 \#9S4634-L-46; MIL spec no. MIL-L-3661; type \#LH-71-XXO; 21964 \#A9152053 or \#A2142519; Same as XDS502 & Holder for DS 1304 \\
\hline XDS 1305 & & Same as XDS1304 & Holder for DS1305 \\
\hline XF1301 & & FUSE HOLDER: extractor post type; accommodates 2 fuses \(1-1 / 4^{\prime \prime}\) \(\lg\) by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type sealed; MIL type FHL10G per BuShips Dwg \#9000-S6202-74228 and MIL-F-19207 (Ships); 21964 \#A2060402; Same as XF501 & Holder for F1302 and F1305 \\
\hline XV1370 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, brass, nickel plated; miniature; includes metal shield base, \(0.800^{\prime \prime}\) dia, \(0.611^{\prime \prime}\) high; includes center shield, \(0.125^{\prime \prime}\) ID; oval; \(1-1 / 8^{\circ} \mathrm{lg}, 0.800^{\prime \prime}\) wide, \(25 / 32^{\prime \prime}\) high o/a dimensions, excluding terminals; molded thermosetting plastic body; one piece saddle mounting, \(5 / 8^{\prime \prime}\) dia. chassis hole required, 2 mounting holes, \(0.125^{\prime \prime}\) dia., \(0.875^{\prime \prime}\) c to c; JAN type TS102P01, per spec JAN-S-28A-1; 21964 \#740002; Same as XV308 & Socket for V1370 \\
\hline XV1371 & & Same as XV1370 & Socket for V1371 \\
\hline XV1372 & & SOCKET, ELECTRON TUBE: 9 contacts; brass, nickel plated; miniature; includes metal shield base, \(0.940^{\prime \prime}\) dia, \(0.611^{\prime \prime}\) high; includes center shield, \(0.125^{\prime \prime}\) ID oval; \(1-3 / 8^{\circ} \mathrm{lg}, 0.940^{\prime \prime}\) wide, 25/32" high, o/a dimensions, excluding terminals; molded thermosetting plastic body; one piece saddle mounting, \(3 / 4^{\prime \prime}\) dia. chassis hole required, 2 mounting holes, \(0.125^{\prime \prime}\) dia., \(1.125^{\prime \prime} \mathrm{c}\) to c ; JAN type TS103P01, per spec JAN-S-28A; 21964 \#740004; Same as XV307 & Socket for V1372 \\
\hline Z1301 & & Not Used & \\
\hline Z1302 & & Not Used & \\
\hline Z1303 & & TUNER, TRANSMISSION LINE: 960 to 1250 mc frequency tuning range; u/w 50 ohms line; \(13-1 / 8^{\prime \prime} \mathrm{lg}, 1-7 / 8^{\prime \prime}\) wide, \(3-3 / 8^{\prime \prime}\) high, overall dim.; 27 cm range scale \(\mathrm{w} /\) sliding pointers, slug tuned; one coupling nut on each end \(1-1 / 4^{\prime \prime}-18\) NEF-2 thd, for \(7 / 8^{\prime \prime}\) line; two mounting brackets each \(w /\) two 6-32 tapped holes one near each end; 21964 \#A2141750G2 & Matches klystron output impedance Figure 2-20 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline 1401-1599 & & FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D: frequency data, final multiplier output, 961.5 to \(1024.5 \mathrm{mc}, 1150.5\) to 1213.5 mc ; operating power requirements, AC: \(120 \mathrm{v}, 60 \pm 5\) cycles, single phase, 150 va, DC; \(-375 / 250 / 1000 \mathrm{v}, 04 / .20 / .055\) amps; impedance data, 50 ohms output; crystal oscillator tubes 5670 with crystal type CR-32/U with special tolerance on initial frequency accuracy; open aluminum framework; overall dim. 26-25/32" lg. , 23-1/16" wide, 8-21/32" high; rack mounted with pull-out slides, front access only; to provide a crystal controlled pulsed RF signal to excite the Amplifier-Modulator; 21964 \#A1068944 u/o AN/GRN-9D & \begin{tabular}{l}
GRN-9D \\
Figure 6-54
\end{tabular} \\
\hline C1401 & & Not Used & \\
\hline C1402 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(0.10 \mu \mathrm{f}+10 \%\); 900 v DC working, MIL type CP05A1KE104K, per spec MIL-C-25A; 21964 dwg \#A2132594-1; Same as C613 & \[
\begin{aligned}
& \text { Coupling, V1401 } \\
& \text { to V1402 } \\
& \text { Figure 6-9 }
\end{aligned}
\] \\
\hline C1403 & & Not Used & \\
\hline C1404 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(1 \mu \mathrm{f}, \pm 10 \%\) tolerance; 400 v DC working, MIL type CP05A1KE105K per spec MIL-C-25A; 21964 dwg \#A2132594-3 & \[
\begin{aligned}
& \text { Coupling, V1402 } \\
& \text { to V1403, V1404 } \\
& \text { and V1405 } \\
& \text { Figure 6-9 }
\end{aligned}
\] \\
\hline C1405 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(2 \mu \mathrm{f}, \pm 10 \%\); 2000 v DC working; MIL type CP70E1EJ205K per spec MIL-C-25; 21964 part \#641068 & Plate bypass, V1403 V1404, V1405 Figure 6-55 \\
\hline C1406 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(910 \mu \mu \mathrm{f} \pm 5 \%\); 2,500 v DC working; MIL type CM45B911J, per spec MIL-C-5A; 21964 part \#603192; u/o AN/GRN-9A & Filter, p/o shaper network \\
\hline C1407 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(510 \mu \mu \mathrm{f} \pm 5 \%, 2,500 \mathrm{v}\) DC working; MIL type CM45B511J, per spec MIL-C-5A; 21964 part "603186; u/o AN/GRN-9 & Filter, p/o shaper network \\
\hline C1408 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(300 \mu \mu \mathrm{f} \pm 5 \%\); 2,500 v DC working; MIL type CM45B301J per spec MIL-C-5A; 21964 part \#603180; u/o AN/GRN-9 & Filter, p/o shaper network \\
\hline C1409 & & Not Used & \\
\hline C1410 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1,000 v DCW \(0.1 \mu \mathrm{f}\) \(\pm 10 \%\); MIL type CP53B1EG-104K per spec MIL-C-25A; 21964; part \#640351: Same as C1301 & Coupling, shaper network to V1407 Figure 6-55 \\
\hline C1411 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(0.01 \mu \mathrm{f} \pm 10 \% ; 400 \mathrm{v}\) DC working, MIL type CP05A1KE103K, per spec MIL-C-25A; 21964 part \#A2132594-4 & \[
\begin{aligned}
& \text { Bypass, grid bias } \\
& \text { to V1403, V1404, } \\
& \text { V1405 }
\end{aligned}
\] \\
\hline C1412 & & Same as C1404 & Bypass, screen grid V1407 Figure 6-9 \\
\hline C1413 & & Same as C1411 & Coupling, DL1401
to V1408 \\
\hline C1414 & & Same as C1402 & Coupling. V1408 to V1409 Figure 6-9 \\
\hline C1415 & & Same as C1404 & Coupling, Receiver blanking output Figure 6-9 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1416 & & CAPACITOR, FIXED, MCA DIELECTRIC: \(27 \mu \mu \mathrm{f}, \pm 5 \% \mathrm{v}\) DC working; MIL type CM20C270J per spec MIL-C-5A; 21964 part \#600164 & \[
\begin{aligned}
& \text { Bypass, cathode } \\
& \text { V1408 }
\end{aligned}
\] \\
\hline C1417 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(68 \mu \mu \mathrm{f}+5 \% ; 2,500 \mathrm{v}\) DC working; MIL type CM45B680J, per spec MIL-C-5A; 21964 part \#603165; u/0 AN/GRN-9A & Filter, p/o shaper network \\
\hline C1418 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(10 \mu \mathrm{f} \pm 10 \%\); 100 v DC working; MIL type CP54B1 FB106K per MIL-C-25; 21964 part \#643645; u/o AN/GRN-9A & Bypass R1457 to ground Figure 6-9 \\
\hline C1419 & & CAPACTTOR, FIXED, MICA DIELECTRIC; \(22 \mu \mu \mathrm{f}, \pm 5 \% 500 \mathrm{v}\) DC working; MIL type CM20C220J per spec MIL-C-5A; 21964 part \#600162 & Coupling, V1401 \\
\hline C1420 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(4 \mu \mathrm{f}, \pm 20 \% ; 400 \mathrm{v}\) DCW; MIL type CH53B1EE405M per MIL-STD-242A and MIL spec MIL-C-18312; 21964, dwg \#A2060302-7; Same as C604 & Bypass +250 v supply Figure 6-9 \\
\hline C1421 & & CAPACITOR, FIXED, MICA DIELECTRIC: 300 v DC working, \(10 \mathrm{f} \pm 10 \%\); MIL type CM15B100K per spec MIL-C-5A; 21964 part \#603959 & Coupling, V1402 \\
\hline C1422 & & Not Used & \\
\hline C1423 & & CAPACITOR, FIXED, MICA DIELECTRIC: 300 v DC working, \(33 \mathrm{f} \pm 5 \%\); MIL type CM15C330J per spec MIL-C-5A; 21964 part \#604031 & Coupling, V1402 \\
\hline C1424 Cont. See C1501 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(02 \mu \mathrm{f}, \pm 10 \% ; 1000 \mathrm{v}\) DC working; MIL type CP26A1EG203K per MIL-C-25A and MIL-STD-242A; 21964 dwg A2061919; u/o AN/GRN-9A & p/o compensating network Figure 6-55 \\
\hline CR1401 & & SEMI-CONDUCTOR, DEVICE, DIODE: germanium type; 40 ma max continuous forward current; 125 ma max peak forward current; 75 v peak inverse voltage; 0.8 mmf average shunt capacitance; MIL type 1N69, per spec MIL-E-1B; 21964 part \#700030; Same as CR601 & Clamping Diode, grid V1408 \\
\hline
\end{tabular}

TABLE7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF
DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline CR1402 & & Same as CR1401 & Clamping diode, grid V1402 \\
\hline CR1403 & & SEMI-CONDUCTOR DEVICE, DIODE: silicon. cartridge type; \(1,000 \mathrm{mc}\) frequency design; 8.0 db max conversion loss; 2.5 max output noise ratio; 6.5 watts burnout test; MIL type 1N25, per spec MIL-E-1C; 21964 part \#700026; Same as CR1151 & \[
\begin{aligned}
& \text { Rectifier p/o } \\
& \text { detector E1401 }
\end{aligned}
\] \\
\hline CR1404 & & Same as CR1403 & Rectifier, p/o detector E1402 \\
\hline DC1401 & & COUPLER, DIRECTIONAL: two end fittings, BNC type UG-89/U connector jacks modified for main line, two BNC type UG-185/U connector receptacles modified for indicator; 480 to 1215 mc frequency range; 25 db at 1100 mc coupling loss; less than 1.06 voltage standing wave ratio at 1000 mc ; CU-431/URN-3; 21964 dwg \#C2090962 and A2090963-1 & Directional coupler between V1506 or V1512 and klystron Figure 6-54 \\
\hline DL1401 & & DELAY LINE: distributed parameter type; output taps provided at \(0.9,1.0,1.1,1.2,1.3\) and \(1.4 \mu \mathrm{sec}\) time delay; 1.3 mc bandwidth; characteristic impedance 2,500 ohms \(\pm 5 \% ; 500 \mathrm{v}\) rms test voltage; 21964 dwg \#A2061302 & Delay line input of V1408A Figure 6-9 \\
\hline DL1402 & & Same as DL1401; u/o AN/GRN-9D & Delay line input of V1408A Figure 6-9 \\
\hline DL1403 & & Not Used & \\
\hline DS1401 & & LAMP, INCANDESCENT: 115-125 v, 10 watts, 40 lumens, double contact bayonet base; clear, 24446 \#10C7/1DC; 21964 part \#710071; Same as DS501 & Filaments "ON" Figure 3-3 \\
\hline DS1402 & & LAMP, INCANDESCENT: \(6.8 \mathrm{v}, 0.15 \mathrm{amp}\), single contact miniature bayonet base; NAVY type \#TB-14, MIL type MS15571-2 per MIL-STD-242A; 21964 dwg \#A2141961 & Oven heater booster Figure 3-3 \\
\hline DS1403 & & Same as DS1402 & Oven heater normal Figure 3-3 \\
\hline E1401 & & HOLDER, CRYSTAL: MIL types IN21 or 1N25 crystal diodes accommodated; 2 BNC type cónnectors, female located on one end, male on other end, cylindrical body; 74868 part no. MS-585 per 21964 dwg \#A2140845; Same as E1152 & Crystal detector reflected wave V1506 or V1512 output \\
\hline E1402 & & Same as E1401 & Crystal detector, klystron input; reflected wave \\
\hline E1403 & & Not Used & \\
\hline E1404A & 5 & SHIELD, ELECTRON TUBE: 98978 \#T-12-1030; \#A2132699 modified 21964 \#B2061847G1 & Shield for V1403 \\
\hline E1404B & & \[
\begin{aligned}
& \text { RETAINER, ELECTRICAL SHIELD: } 98978 \text { part \#T-12-1001; } \\
& 21964 \text { \#A2132698 }
\end{aligned}
\] & Base for E1404A \\
\hline E1405A & & Same as E1404A & Shield for V1404 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline E1405B & & Same as E1404B & Base for E1405A \\
\hline E1406A & & Same as E1404A & Shield for V1405 \\
\hline E1406B & & Same as E1404B & Base for E1406A \\
\hline E1407A & & Same as E1404A & Shield for V1407 \\
\hline E1407B & & Same as E1404B & Base for E1407A \\
\hline E1408A & 6 & SHELD, ELECTRON TUBE: JAN type TS103U02 per JAN-S-28A, modified; 21964 \#A2132988-5; Same as E307 & Shield for V1401 \\
\hline E1408B & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U02; MIL-STD-242A type \#902; 21964 \#A2132886-5; Same as E307A & Insert for shield E1408 \\
\hline E1409A & & Same as E1408A & Shield for V1402 \\
\hline E1409B & & Same as E1408B & Insert for shield E1409 \\
\hline E1410A & & Same as E1408A & Shield for V1408 \\
\hline E1410B & & Same as E1408B & Insert for shield E1410 \\
\hline E1411A & & Same as E1408A & Shield for V1409 \\
\hline E1411B & & Same as E1408B & Insert for shield E1411 \\
\hline E1412 & 7 & CLAMP, ELECTRICAL: brass, silver plated; 74868 \#1025 MIL type MX-1684/U per 21964 "A9142339; Same as E345 & Outer conductor ground, output cable from El402 \\
\hline E1413 & & Same as E1412 & Outer conductor ground, output cable from E1401 \\
\hline E1414 & & SHIELD, ELECTRON TUBE: 98978 \#TR6-6025; 21964 \#A2133276-6 & Shield for V1406 \\
\hline E1415 thru E1419 & & Not Used & \\
\hline E1420A & & Same as E1408A & Shield for V1410 \\
\hline E1420B & & Same as E1408B & Insert for shield E1420 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCATING \\
FUNCTION
\end{tabular} \\
\hline E1421 & & INSULATOR, BUSHING: ceramic grade L-5A; Ref Dwg Group no. 9 style, no. 174; MIL type NS5AW4 103 per JAN-I-8; 21964 \#A2133203-3; Same as E1318 & Ceramic feedthru insulator, 700 v DC \\
\hline E1422 & & INSULATOR, BUSHING: ceramic grade L-5A; MIL type NS5AW4203 per JAN-I-8; 21964 \#A2133204-3; Same as E1320 & Ceramic feedthru insulator 1000 v DC \\
\hline E1423 & & CLIP, ELECTRICAL: beryllium copper; silver plated; 76487 \#36002-B; 21964 dwg \#A2133216 & Plate clip for V1403 \\
\hline E1424 & & Same as E1423 & Plate cap for V1404 \\
\hline E1425 & & Same as E1423 & Plate cap for V1405 \\
\hline E1426 & & Same as E1423 & Plate cap for V1407 \\
\hline E1427 & & CLIP, ELECTRICAL: phosphor bronze cadmium plated; 01009 \#90 1SL-2BC; 21964 dwg \#A2133343 & Plate clip for V1406 \\
\hline E1428 & & Same as E1423; u/o AN/GRN-9D & Plate cap for V1411 \\
\hline E1429 & & RETAINER, ELECTRON TUBE: beryllium copper, 21964 \#A2060132-1 & Retainer for V1504 \\
\hline E1430A & & Same as E1404A; u/o AN/GRN-9D & Shield for V1411 \\
\hline E1430B & & Same as E1404B; u/o AN/GRN-9D & Base for E1430A \\
\hline E1431 & & Same as E1429 & Retainer for V1506 \\
\hline E1432 & & Same as E1429 & Retainer for V1510 \\
\hline E1433 & & Same as E1429 & Retainer for V1511 \\
\hline E1434 & & Same as E1429 & Retainer for V1512 \\
\hline \begin{tabular}{l}
E1435 \\
Cont \\
See E1501
\end{tabular} & & Same as E1429 & Retainer for V1505 \\
\hline F1401 & & FUSE, CARTRIDGE: \(2 \mathrm{amp}, 250 \mathrm{v}\); time delay, \(135 \%\) for 0.1 hour and \(300 \%\) for 6 sec ; enclosed type; MIL type F02G2500A per spec MIL-F-15160A and MIL-STD MS90078; 21964 \#882221 & Protection primaries T1403 and T1501 Figure 3-3 \\
\hline F1402 & & Same as F1401 & Protection primary T1502 Figure 3-3 \\
\hline F1403 & & Same as F1401 & Protection primary T1502 Figure 3-3 \\
\hline F1404 & & Same as F1401 & Spare \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9L
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline FL1401 & & FILTER, RADIO INTERFERENCE: capacitor-coil type; 150 v DC, 5 amp ; enclosed in case, 00656 \#1N-151; 21964 \#A2 142586 & Filter, lowpass for HR1501 and HR1.002 Figure 2-17 \\
\hline J1401 & & CONNECTOR, RECEPTACLE: 1 round female contact; one connector mating end; \(\mathbf{5 0} \mathbf{~ o h m}\) nom impedance, 500 v peak voltage; MIL type UG-1094/U BNC Series "D" hole mounting, per Navy dwg REB 49063; 21964 \#A2131837; Same as J203 & Video pulse input to V1401 Figure 6-55 \\
\hline J1402 & & Same as J1401 & Beam pulse output from V1409 Figure 6-55 \\
\hline J1403 & & Same as J1401 & Receiver blanking pulse output from V1409 Figure 6-55 \\
\hline J1404 & & Same as J1401 & Video pulse input test point V1401 Figure 3-3 \\
\hline J1405 & & Same as J1401 & Shaped pulse test point V1407 Figure 3-3 \\
\hline J1406 & & Not Used & \\
\hline J1407 & & CONNECTOR, RECEPTACLE: BNC series; 50 ohms nom impedance; accommodates RG-55 and RG-58/U cables; 74868 \#86025; MIL type UG-909/U per BuShips dwg \#REB49058; dwg \#A2132720; Same as J502 & DC1401 output to klystron \\
\hline J1408 & & Same as J1401 & Klystron input reflected wave test point Figure 3-3 \\
\hline J1409 & & Same as J1401 & Klystron input incident wave test point Figure 3-3 \\
\hline \begin{tabular}{l}
J1410 \\
Cont \\
See J1501
\end{tabular} & & Same as J1407 & V1504 or V1510 output to receiver Figure 6-55 \\
\hline K1401 & & RELAY, ARMATURE: contact arrangement 2 form C type, DPDT, break-make, \(A C, 120 \mathrm{v}, 10 \mathrm{amp} ; 1\) winding, inductive winding; \(A C, 132 \mathrm{v}\) max continuous operation, operating current not rated, 60 cycles; 6 terminals for contacts, 2 terminals for coil; continuous duty; hermetically sealed; 70309 type PBH per spec MIL-R-5757C; 21964 dwg \#A2060235; Same as K1301 & Relay, supervisor for T1403 and T1501 Figure 6-55 \\
\hline L1401 & & COIL, RADIO FREQUENCY: 1 pie universal winding, 575 turns no. \(5 / 41\) litz copper wire, 6.5 mh inductance \(\pm 2 \%\); ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#C2060141G4; u/o AN/GRN-9() & Filter p/o shaper network Figure 6-9 \\
\hline L1402 & & COIL, RADIO FREQUENCY: 1 pie universal winding, 460 turns no. \(5 / 41\) litz copper wire, 4.3 mh inductance \(\pm 2 \%\); ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#C2060141G5; u/o AN/GRN-9() & Filter, p/o shaper network Figure 6-9 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
FREQUENCY/MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline L1403 Cont See L1501 & & COIL, RADIO FREQUENCY: 1 pie universal winding, 350 turn no. \(5 / 41\) litz copper wire, 2.0 mh inductance \(\pm 2 \%\); ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#C2060141G6; u/o AN/GRN-9(') & Filter, p/o shaper network Figure 6-3 \\
\hline M1401 & & AMMETER: DC 0 to \(\mathbf{1 0 0}\) micro-ampere graduated in increments of 5 ; overall dim. 50 millivolt drop across terminals for full scale deflection; calibrated for use on nonmagnetic panel; self contained, MIL type MR26W 100DCUAR per spec MIL-M-10304A; 21964 \#A2060455-5; Same as M501 & Tuning indicator Figure 3-3 \\
\hline M1402 & & VOLTMETER: DC; marked kilovolts, 0 to 1 left to right, graduated in increments of 20; round molded thermosetting compound or metal, style no. 15, MBCA Ref Dwg Group 27; 2\% accuracy at full scale reading; 1 milliampere \(\pm 5 \%\) with 150 millivolts max terminal drop; MIL type \#MR26W001DCKVR, per spec MIL-M-10304; 21964 \#A2060455-2 & DC supply voltage indicator Figure 3-3 \\
\hline MP1401 & & KNOB: pointer; black, phenolic body; MS700-18S per MIL-STD242A; 21964 \#B2132733-2; Same as MP501 & Knob for S1401 \\
\hline MP1402 & & Same as MP1401 & Knob for \(\mathbf{S 1 4 0 2}\) \\
\hline MP1403 & & CAP ELECTRICAL: brass; fits BNC female connectors; MIL type CW-123A/U per Navy dwg REA49050 and MIL-C-3608; 21964 no. A2141971; Same as MP504 & Cover, cap and chain for J1404 \\
\hline MP1404 & & Same as MP1403 & Cover, cap and chain for J1405 \\
\hline MP1405 & & Same as MP1403 & Cover, cap and chain for J1408 \\
\hline MP1406 & & Same as MP1403 & Cover, cap and chain for J1409 \\
\hline MP1407 & & ALIGNMENT TOOL; combination screwdriver and wrench type, 2 working ends; \(0.050^{\prime \prime}\) screwdriver slot; 7/32" hex socket; 21964 \#B2061316G1 & Mounted in cover of cabinet \\
\hline MP1408 & 1 & GASKET: synthetic rubber, MIL-R-900C, class 1 ; style no 10 , MBCA Ref Dwg Group 75; 2-15/64" dia aperture in center; three \(1 / 8^{\prime \prime}\) dia holes spaced 120 deg apart on 2-7/16" dia; 2-11/16" outside dia, 1/16" thk; 21964 *B2060910; Same as MP205 & Sealing for meter M1401 \\
\hline MP1409 & & Same as MP1408 & Sealing for meter M1402 \\
\hline P1401 & & CONNECTOR, PLUG, ELECTRICAL: 1 round male contact; one connector mating end: BNC series; 50 ohms nom impedance, 500 v peak voltage; accommodates RG-55/U and RG58/U cables; 74868 \#85000 MIL type UG-88C/U per Sig dwg \#SC-D-72235; BuShips dwg \#REB-49064; 21964 \#A2131456; Same as P201 & Cable connector on J1503 or J1506, p/o W1403 \\
\hline P1402 & & Same as P1401; p/o W1403 & Cable connection on DC1401 input \\
\hline P1403 & & Same as P1401 & Cable connection on DC1401 output \\
\hline P1404 & & Same as P1401; p/o W1401 and W1402 & Cable cornection on E1401 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNGTION \\
\hline R1415 & & Same as R1411 & Screen grid dropping resistor, V1405 \\
\hline R1416 & & RESISTOR, FIXED, WIREWOUND: 25,000 ohms \(\pm 3 \%\); 30 watt MIL type RH50G253H per spec MIL-R-18546A (Ships); 21964 \#A2132948-6 & Damping resistor T1402 secondary Figure 6-9 \\
\hline R1417 & & RESISTOR, VARIABLE: composition element; 1 section, 500 ohms \(\pm 10 \%\); 2 watt nom power rating; linear taper MIL type RV4LAVSA501A per MIL-R-94 and MIL-STD-242 (Ships) 21964 \#580004H501 & Output termination, p/o shaper network Figure 2-17 \\
\hline R1418 & & RESISTOR, FIXED, WIREWOUND: 3500 ohms; \(\pm 3 \%\); 30 watt; MIL type RH50G352H per spec MIL-R-18546A (Ships); 21964 \#A2133519G2 & Output termination p/o shaper network Figure 6-9 \\
\hline R1419 & & RESISTOR, FIXED, WIREWOUND: 2000 ohms \(\pm 3 \%\); 30 watt; MIL type RH50G202H per spec MIL-R-18546A (Ships) 21964 \#A2132948-8 & Plate load V1402 \\
\hline R1420 & 6 & RESISTOR, VARLABLE: composition element; 1 section, 250,000 ohms \(\pm 10 \%\); 2 watt nominal power rating; linear taper; MIL type RV4LAVSA254A per MIL-R-94 and MIL-STD-242 (Ships); 21964 \#580004H254; Same as R443 & Grid bias adjust, V1407 Figure 2-17 \\
\hline R1421 & - & Same as R1409 & Grid leak resistor, V1407 \\
\hline R1422 & & Same as R1410 & Grid blocking resistor, V1407 \\
\hline R1423 & & Same as R1408; u/o AN/GRN-9D & Screen grid V1407, V1411 \\
\hline R1424 & 6 & RESISTOR, FIXED, COMPOSITION: 470,000 ohms \(\pm 10 \%\); 2 watt; MIL type RC42GF474K, per spec MIL-R-11; 21964 \#501273 & p/o screen grid voltage divider, V1407 \\
\hline R1425 & & RESISTOR, FIXED, WIREWOUND: 2000 ohms \(\pm 5 \%\); 10 watt; MIL type RW56G202 per spec MIL-R-26B; 21964 \#535070 & Cathode load V1407 \\
\hline R1426 & 6 & RESISTOR, FIXED, COMPOSITION: \(47 \mathrm{ohms}+10 \%\); \(1 / 2\) watt; MIL type RC20GF470K per spec MIL-R-11, 21964 \#504215 & Shaped pulse monitoring, V1407 \\
\hline R1427 & & Same as R1405 & Voltage divider V1408 \\
\hline R1428 & & RESISTOR, FIXED, COMPOSITION: 1.5 megohm \(\pm 5 \%\); \(1 / 2\) watt; MIL type RC20GF155J per spec MIL-R-11; 21964 \#504179; Same as R445 & Voltage divider V1408 \\
\hline R1429 & & RESISTOR, FIXED, COMPOSITION: 150, 000 ohms \(\pm 5 \%\); \(1 / 2\) watt; MIL type RC20GF154J, per spec MIL-R-11; 21964 \#504155 & Voltage divider grid V1408 \\
\hline R1430 & & RESISTOR, FIXED, COMPOSITION: 68,000 ohms \(\pm 5 \% ; 1 / 2\) watt; MIL type RC20GF683J, per spec MIL-R-11; 21964 \#504147; Same as R644 & Voltage diviaer grid V1408 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1431 & & Same as R1419 & Plate load, V1408B Figure 6-55 \\
\hline R1432 & 6 & RESISTOR, FIXED, COMPOSITION: 1 megohm \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF105K per spec MIL-R-11; 21964 \#504267; Same as R432 & Grid bias voltage divider, V1409 \\
\hline R1433 & 6 & RESISTOR, FIXED, COMPOSITION: 100,000 ohms \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF104K per spec MIL-R-11A; 21964 *504255; Same as R320; \(u\) /o AN/GRN-9D & Grid leak resistor, V1409 \\
\hline R1434 & & Not Used & \\
\hline R1435 & 6 & RESISTOR, FIXED, COMPOSITION: 3300 ohms \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF332K per spec MIL-R-11; 21964 \#504237; Same as R417 & Grid blocking, V1409A \\
\hline R1436 & & Same as R1430 & Grid leak, V1409 \\
\hline R1440 & & Same as R1435 & Grid blocking, V1409B \\
\hline R1441 & & RESISTOR, FIXED, FILM: 1.47 megohm \(\pm 1 \%\); 1 watt; MIL type RN-75B1474F, per spec MIL-STD-242A and MIL-R-10509; 21964 \#A2060501-1 & 1000 v DC metering shunt \\
\hline R1442 & & Same as R1441 & 1000 v DC metering shunt \\
\hline R1443 & & RESISTOR, FIXED, WIREWOUND: 1 megohm \(\pm 0.5 \%\); JAN type MFC105, per spec JAN-R-29; 21964 \#A2142503-1 & Meter multiplier M1402 Figure 2-17 \\
\hline R1444 & 6 & RESISTOR, FIXED, COMPOSITION: 2700 ohms \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF272K per spec MIL-R-11; 21964 *504236; Same as R309 & Delay line termination: DL1401 \\
\hline R1445 & & RESISTOR, FIXED, FILM: 750,000 ohms \(\pm 1 \%\); 1 watt; MIL type RN75B7503F per MIL-STD-242A and MIL-R-10509; 21964 *A2060501-2 & 1000 v DC meter multiplier \\
\hline R1446 & & Same as R1419 & Plate load V1402B Figure 6-9 \\
\hline R1448 & & RESISTOR, FIXED, FILM: 464, 000 ohms \(\pm 1 \%\); 1 watt; MIL type RN75B4643F per MIL-STD-242A and MIL-R-10509; 21964 \#A2060501-3 & Voltage divider, V1410 grid \\
\hline R1449 & & RESISTOR, FIXED, FILM: 649, 000 ohms \(\pm 1 \%\); 1 watt; MIL type RN75B6493F per MIL-STD-242A and MIL-R-10509; 21964 \#A2060501-4 & Voltage divider, V1410 grid \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1465 & & Same as R1420 & \begin{tabular}{l}
Grid resistor V1401 \\
Figure 2-17
\end{tabular} \\
\hline R1466 & 6 & RESISTOR, VARIABLE: composition element; 1 section, 0.10 megohms, \(\pm 10 \%\); 2 watt nominal power rating; no switch MIL type RV4LAVSA104A per MIL-R-94 and MIL-STD-242 (Ships); 21964 \#580004H104; Same as R672 & Grid leak V1402 Figure 2-17 \\
\hline R1467 & 6 & RESISTOR, FIXED, COMPOSITION: 47,000 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF473K, per spec MIL-R-11; 21964 \# 501261 u/o AN/GRN-9D & Shaper network termination \\
\hline R1468 & & RESISTOR, FIXED, WIREWOUND: 3,100 ohms total resistance \(\pm 3 \%\); 30 watt; MIL type RH50G312H per spec MIL-R-18546B (Ships); 21964 \# A2133519G1 & Plate load V1402 Figure 6-9 \\
\hline R1469 & & Same as R1430 & Voltage divider grid V1402 \\
\hline R1470 & 6 & RESISTOR, VARIABLE: composition element; 1 section \(\mathbf{5 0 , 0 0 0}\) ohms, \(\pm 10 \% ; 2\) watt nominal power rating; no. switch; MIL type RV4LAVSA503A per spec MIL-R-94 and MIL-STD-242 (Ships); 21964 \#580004H503; Same as R1310; u/o AN/GRN-9D & Shaper network termination Figure 2-17 \\
\hline R1471 & & Same as R1470 of AN/GRN-9D 1; u/o AN/GRN-9D & p/o compensating network Figure 2-17 \\
\hline R1472 & & Same as R1410; u/o AN/GRN-9D & Parasitic suppressor grid V1411 \\
\hline R1473 & & Same as R1408; \(\mathbf{u} / \mathrm{o}\) AN/GRN-9D & Screen voltage divider V1411 \\
\hline \begin{tabular}{l}
R1474 \\
Cont \\
See R1501
\end{tabular} & & Same as R1447; \(\mathbf{u} / \mathrm{o}\) AN/GRN-9D & Blanking pulse output termination V1409 \\
\hline S1401 & - & SWITCH ROTARY: 2 sections; 1 pole, 9 positions each section; 2 rotor contacts, 20 fixed contacts; rotor and fixed contacts solid non-shorting type; 76854 type DHC per 21964 \#B2060222 & Selector for M1401 Figure 3-3 \\
\hline S1402 & & SWITCH, ROTARY: 2 sections; 1 pole, 5 positions each section; 2 rotor contacts, 12 fixed contacts; non-shorting type; 76854 type DHC per 21964 \#B2060034 & \begin{tabular}{l}
Selector for M1402 \\
Figure 3-3
\end{tabular} \\
\hline T1401 & & Not Used & \\
\hline T1402 & & TRANSFORMER, PULSE: 2 windings; primary, negative rectangular pulse 2.5 microseconds wide and 800 v amplitude at \(2 \%\) duty cycle from source impedance of 500 ohms ; secondary, 1350 v positive pulse across 1400 ohm load when 800 v negative pulse is impressed on primary; primary inductance \(15.8 \mathrm{mh} \pm 2 \%\), secondary inductance \(45.5 \mathrm{mh} \pm 2 \%\), primary 2.5 ohms; secondary 10.2 ohms; 49956 \#363-2372G1 MIL type TF1SX32YY per MIL-T-27A; 21964 \#A1069956 & Pulse transformer, plates of V1403, V1404, V1405 to shaper network Figure 6-55 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline T1403 & & TRANSFORMER, POWER STEPDOWN: 120 v AC, 60 cycles, single phase; 1 output winding, secondary 6.4 v \(10.5 \mathrm{amp} ; 49956\) *2925620G1 MIL type TF1SX01JB per spec MIL-R-27A; 21964 *A1069615 & Filament supply, V1401, V1402, V1403, V1405, V1406, V1408, V1409 Figure 6-55 \\
\hline \begin{tabular}{l}
T1404 \\
Cont \\
See T1501
\end{tabular} & & TRANSFORMER, PULSE: interstage type; 75 v DC primary operating voltage, \(19 \mathrm{ma} ; 25 \mathrm{v} \mathrm{DC}\) secondary operating voltage, \(25 \mathrm{ma} ; 1000 \mathrm{v}\) DC insulation voltage; 49956 \#363-2098GI; MIL type TF1RX36YY per spec MIL-R-27; 21964 \#A2061755; u/o AN/GRN-9D only & Pulse transformer plate load for V1409 Figure 6-55 \\
\hline TB1 & & TERMINAL BOARD: 9 terminals; single row, solid studs; per 21964 \#B1069957G1 & Component board \\
\hline TB2 & & TERMINAL BOARD: 9 terminals; single row, solid studs; per 21964 "B1069957G2 & Component board \\
\hline TB1401 & & TERMINAL BOARD: 8 terminals; single row, thru type terminals; MIL type 7TB8 per MIL-T-16784A and NAVY dwg 9000-S6505G73214; 21964 \#A2133072-1; Same as TB501 & AC power input \\
\hline TBI402 & & Same as TB1401 & DC power input \\
\hline TB1403 & 6 & TERMINAL BOARD: 18 terminals; double screw type; barrier type; 18 studs; MIL type \(10 \mathrm{~T}-\mathrm{B} 18\) per MIL-T-16784; and NAVY dwg 9000-S6505G732 14; 21964 \#A2 133248-3 & Terminal board for video assy Figure 6-9 \\
\hline \[
\begin{gathered}
\text { TB1404 } \\
\text { thru } \\
\text { TB1493 }
\end{gathered}
\] & & Not Used & \\
\hline TB1494 & 2 & TERMINAL BOARD: 12 solder stud type terminals; 21964 \#B2061873G1 & Mounted in video assy \\
\hline TB1495 & 2 & TERMINAL BOARD: 8 hollow solder stud type terminals; 00781 \#12856; 21964 \#355637 & Mounts resistors R1535, R1536 \\
\hline TB1496 & 2 & TERMINAL BOARD: 10 solder stud type terminals; 21964 \#B2060776G1 & Mounted in video assy \\
\hline TB1497 & 2 & TERMINAL BOARD: 26 solder stud type terminals; 21964 \#B2061718G1; u/o AN GRN-9D & Mounted in video assy Figure 6-9 \\
\hline TB1498 & 2 & TERMINAL BOARD: 26 solder stud type terminals; 21964 \#B2060773G1 & Mounted in video assy Figure 6-9 \\
\hline TB1499 & 2 & TERMINAL BOARD: 12 solder stud type terminals; 21964 \#B2060722G1 & \begin{tabular}{l}
Mounted in video \\
assy \\
Figure 6-9
\end{tabular} \\
\hline V1401 & & \[
\begin{aligned}
& \text { ELECTRON TUBE: MIL type 5814A per spec MIL-E-1C; } \\
& 21964 \# 701164
\end{aligned}
\] & p/o gate pulse multivibrator Figure 6-55 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINT ENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline V1402
V1403 & & \begin{tabular}{l}
ELECTRON TUBE: twin triode; MIL type 5687WA per MIL spec \\
MLL-E-1 (Navy); 21964 \#A2133281; Same as V606 \\
ELECTRON TUBE: MIL type 6293 per spec MIL-E-1C; \\
21964 \#701259
\end{tabular} & \begin{tabular}{l}
Pulse widener \\
Figure 6-55 \\
Pulse amplifier \\
Figure 2-17
\end{tabular} \\
\hline V1404 & & Same as V1403 & Pulse amplifier Figure 6-55 \\
\hline V1405 & & Same as V1403 & Pulse amplifier Figure 6-55 \\
\hline V1406 & & ELECTRON TUBE: high vacuum half wave rectifier; RMA type T6-1/2; MIL type 6 V3A per spec MIL-E-1C; 21964 \#A2132479 & Pulse undershoot damper Figure 6-55 \\
\hline V1407 & & Same as V1403 & Cathode follower Figure 2-17 \\
\hline V1408 & & Same as V1402 & p/o gate pulse multivibrator Figure 6-55 \\
\hline V1409 & & Same as V1402 & Cathode follower Figure 6-55 \\
\hline V1410 & & Same as V1402 & Voltage divider Figure 6-55 \\
\hline \begin{tabular}{l}
V1411 \\
Cont See V1501
\end{tabular} & & Same as V1403; \(u\) /o AN/GRN-9D & Voltage divider Figure 2-17 \\
\hline W1401 & & Not Used & \\
\hline W1402 & - & Not Used & \\
\hline W1403 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield, type RG141/U; incl 2 MLL type connectors, P1401 and P1402, one located on each end, per 21964 dwg \#B2060996G1 & \[
\begin{aligned}
& \text { Connects J1503 } \\
& \text { to P1403 }
\end{aligned}
\] \\
\hline W1404 thru W1407 & & Not Used & \\
\hline W1408

W 1409 & 8 & \begin{tabular}{l}
CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric, single silver coated copper shield type RG141/U; incl 2 MIL type connectors, P1403 and J1407, one located on each end, per 21964 \#B2061035G1 \\
Not Used
\end{tabular} & \[
\begin{aligned}
& \text { Connects P1402 } \\
& \text { to P920 }
\end{aligned}
\] \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline  & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline W1410 & 8 & CABLE ASSEMBLY, RADIO FREQUENCY: coaxial, 50 ohms nom impedance, inner conductor no. 19 AWG copper covered steel, teflon dielectric single silver coated copper shield, type RG141/U; incl 2 MLL type connectors, P1406 and J1410, one locatedon each end, per 21964 dwg \#B2060879G1 & Connects output of Coder-Indicator to video assy \\
\hline XDS1401 & & LIGHT, INDICATOR: friction mtg lens holder; \(125 \mathrm{v}, 6\) watts; enclosed frame; steel shell; black nickel; MIL type LH63PW3 per MIL-L-3661, dwg MS-90286; 21964 dwg \#A2133069-5; Same as XDS501 & Holder for DS1401 \\
\hline XDS 1402 & & LIGHT, INDICATOR: supplied w/lens, nominal voltage rating 28 v ; MIL type LH62PW2 per MIL-L-3661 and MS90287; 21964 \#A2133051-2 & Holder for DS1402 \\
\hline XDS1403 & & Same as XDS1402 & Holder for DS1403 \\
\hline XF1401 & & FUSEHOLDER: extractor post type; accommodates 2 fuses, \(1-1 / 4^{\prime \prime} \lg\) by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type; sealed; MIL type FHL10G per BuShips dwg \#9000-S6202-74228 and MIL-F-19207 (Ships); 21964 \#A2060402; Same as XF501 & \[
\begin{aligned}
& \text { Holder for F1401, } \\
& \text { F1404 }
\end{aligned}
\] \\
\hline XF1402 & & Same as XF1401 & Holds F1402 and F1403 \\
\hline XV1401 & & SOCKET, ELECTRON TUBE: 9 contacts, brass, nickel plated; miniature; JAN type \#TS103P01, per spec JAN-S-28A-1; 21964 \#740004; Same as XV307 & Socket for V1401 \\
\hline XV1402 & & Same as XV1401 & Socket for V1402 \\
\hline XV1403 & 6 & SOCKET, ELECTRON TUBE: 8 contacts, copper base, silver plated, small body, JAN type TS101P01 per spec JAN-S-28A; 21964 \#740000 & Socket for V1403 \\
\hline XV1404 & & Same as XV1403 & Socket for V1404 \\
\hline XV1405 & & Same as XV1403 & Socket for V1405 \\
\hline XV1406 & & Same as XV1401 & Socket for V1406 \\
\hline XV1407 & & Same as XV1403 & Socket for V1407 \\
\hline XV1408 & & Same as XV1401 & Socket for V1408 \\
\hline XV1409 & & Same as XV1401 & Socket for V1409 \\
\hline XV1410 & & Same as XV1401 & Socket for V1410 \\
\hline XV1411
Cont
See XV1501 & & Some as XV1403; u/o AN/GRN-9D & Socket for V1411 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline  & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCATING \\
FUNCTION
\end{tabular} \\
\hline Z1401 & 2 & SUPPRESSOR, PARASTTIC: network; \(1.9 \mu \mathrm{~h} \pm 10 \%\) at 7.9 mc ; coil 24 turns of \#22 wire, wound on \(10 \mathrm{ohm}, 2\) watt resistor (RC42GF100K); 21964 \#B2060124 & \begin{tabular}{l}
Parasitic suppressor \\
V1403 \\
Figure 6-55
\end{tabular} \\
\hline Z1402 & & Same as Z1401 & \begin{tabular}{l}
Parasitic suppressor V1404 \\
Figure 6-55
\end{tabular} \\
\hline Z1403 & & Same as Z1401 & \begin{tabular}{l}
Parasitic suppressor \\
V1405 \\
Figure 6-55
\end{tabular} \\
\hline Z1404 & & Same as Z1401 & \begin{tabular}{l}
Parasitic suppressor V1407 \\
Figure 6-55
\end{tabular} \\
\hline \[
\begin{aligned}
& \text { Z1405 } \\
& \text { Cont } \\
& \text { See Z1501 }
\end{aligned}
\] & & Same as Z1401; u/o AN/GRN-9() & Parasitic suppressor V1411 Figure 6-55 \\
\hline C1501 & 6 & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(1000 \mu \mu \mathrm{f} \pm \mathbf{5 0 \%}\); -20\% tolerance, 500 v DC working; 72982 2443-01-000 with hex nut; 21964 \#B2132685-1 & Feedthru bypass
\[
150 \text { v DC }
\] \\
\hline C1502 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(820 \mu \mu \mathrm{f}+100 \%\) \(-20 \% 500\) v DC working; Temp Coef N/R; MIL type CK60Y821Z, per MIL-C-11015A; for electrical performance only: 21964 part *625020H821; Same as C305 & Bypass, plate supply, V1501B \\
\hline C1503 & & Same as C1502 & Bypass, plate supply, V1501A. \\
\hline C1504 & & Same as C1502 & Coupling, V1501A plate to V1501B grid \\
\hline C1505 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(47 \mu \mu \mathrm{f}, \pm 2 \%\), 500 v DC working: JAN CC21UJ470G per JAN-C-20A; 21964 dwg \#A9142374-5; Same as C217 & \[
\begin{aligned}
& \text { Coupling, V1501B } \\
& \text { to V1502 }
\end{aligned}
\] \\
\hline C1506 & & Same as C1502 & DC blocking between cathode of V1501 \\
\hline C1507 & & Same as C1501 & Feedthru bypass, to DS1403 \\
\hline C1508 & & Same as C1501 & Feedthru bypass, 24 v AC \\
\hline C1509 & & Same as C1501 & Feedthru bypass, to DS1402 \\
\hline C1510 & & Same as C1501 & Feedthru bypass, V1501A metering \\
\hline C1511 & & Same as C1501 & Feedthru bypass, V1501B metering \\
\hline C1512 & & Same as C1502 & Bypass V1502 cathode \\
\hline C1513 & & Same as C1502 & Bypass V1502 cathode \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1514 & & Same as C1502 & \[
\begin{aligned}
& \text { Coupling, V1502 } \\
& \text { to V1503 }
\end{aligned}
\] \\
\hline C1515 & & Same as C1502 & Screen grid bypass, V1502 \\
\hline C1516 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(15 \mu \mu \mathrm{f} \pm 2 \% ; 500 \mathrm{v}\) DC working; temp coefficient SH; JAN type CC21-SH150G per JAN-C-20A; 21964 dwg \#A2132736-03 & Plate neutralizing, V1502 \\
\hline C1517 & & CAPACITOR, FIXED, MICA DIELECTRIC: \(1000 \mu \mu \mathrm{f} \pm 20 \% 300 \mathrm{v}\) DC working; -100 to +100 parts/million Deg. C; MIL type CB11RB102M per MIL-C-10950A; 21964 part \#615361 & Feedthru bypass, plate supply, V1503 \\
\hline C1518 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(22 \mu \mu \mathrm{f}, \pm 2 \%\), 500 v DC working; JAN type CC21UJ220G per JAN-C-20A; 21964 dwg \#A2132735-06 & \[
\begin{aligned}
& \text { Coupling, V1503 } \\
& \text { to Z1507 }
\end{aligned}
\] \\
\hline C1519 & & CAPACITOR, VARIABLE, AIR DIELECTRIC: plate meshing type, 1 section, \(5.1 \mu \mu \mathrm{f} \pm 20 \% \max\), \(1.5 \mu \mu \mathrm{f} \pm 20 \%\) min.; each section straight line capacity; 1250 v AC peak voltage; screwdriver adjustment; \(180^{\circ} \mathrm{CW}\) rotation; CEJ type 5M11, per JAN-C-92; 21964 dwg \#A2060185 & Plate tuning V1503 Figure 2-18 \\
\hline C1520 & & Same as C1502 & Cathode bypass V1503 \\
\hline C 1521 & & Same as C1501 & Feedthru bypass V1502 metering \\
\hline C1522 & & CAPACITOR, VARIABLE, CERAMIC DIELECTRIC: rotary type, single section; 7 to \(45 \mu \mu \mathrm{f} ; 500 \mathrm{v}\) DC working; screwdriver slot adjustment; MIL type CV11C450 per MIL-C-81; 21964 part \#670006 & Trimmer V1504 input Figure 2-18 \\
\hline C1523 & & Same as C1502 & Bypass, V1507A plate supply \\
\hline C1524 & & Same as C1502 & Bypass, V1507B plate supply \\
\hline C1525 & & Same as C1502 & Coupling, V1507A to V1507B \\
\hline C1526 & & Same as C1505 & \[
\begin{aligned}
& \text { Coupling, V1507 } \\
& \text { to V1508 }
\end{aligned}
\] \\
\hline C1527 & & Same as C1502 & DC blocking between cathodes of V1507 \\
\hline C1528 & & Same as C1502 & Cathode bypass V1508 \\
\hline C1529 & & Same as C1502 & Cathode bypass
V1508 \\
\hline C1530 & & Same as C1502 & Bypass screen grid V1508 \\
\hline C1531 & & Same as C1502 & Coupling, V1508 to V1509 \\
\hline C1532 & - & Same as C1516 & Plate neutralizing V1508 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D. MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1533 & & Same as C1517 & Feedthru pybass V1509 plate supply \\
\hline C1534 & & Same as C1505 & Coupling, V1509 to Z1508 \\
\hline C1535 & & Same as C1502 & Cathode bypass
V1509 \\
\hline C1536 & & Same as C1519 & Plate tuning V1509 Figure 2-18 \\
\hline C1537 & & Same as C1522 & \begin{tabular}{l}
Trimmer V1510 \\
Figure 2-18
\end{tabular} \\
\hline C1538 & & Same as C1501 & \[
\begin{aligned}
& \text { Feedthru bypass } \\
& 6.3 \mathrm{v} \mathrm{AC}
\end{aligned}
\] \\
\hline C1539 & & Same as C1502 & Filament bypass V1501 \\
\hline C1540 & & Same as C1502 & \(\underset{\text { V1502 }}{\text { Filament bypass }}\) \\
\hline C1541 & & Same as C1502 & Filament bypass V1503 \\
\hline C1542 & & Same as C1501 & Feedthru bypass
6.3 v AC \\
\hline C1543 & & Same as C1502 & \(\underset{\text { V1507 }}{\text { Filament bypass }}\) \\
\hline C1544 & & Same as C1502 & \(\underset{\text { V1508 }}{\substack{\text { Filament }}}\) \\
\hline C1545 & & Same as C1502 & Filament bypass
V1509 \\
\hline C1546 & & Same as C1517 & Feedthru bypass V1504 filament \\
\hline C1547 & & Same as C1517 & Feedthru bypass V1504 filament \\
\hline C1548 & & Same as C1517 & Feedthru bypass V1505 filament \\
\hline C1549 & & Same as C1517 & Feedthru bypass V1505 filament \\
\hline C1550 & & Same as C1517 & Feedthru bypass V1506 filament \\
\hline C1551 & & Same as C1517 & Feedthru bypass V1506 filament \\
\hline C1552 & & Same as C1517 & Feedthru bypass V1510 filament \\
\hline C1553 & & Same as C1517 & Feedthru bypass V15 10 filament \\
\hline C1554 & & Same as C1517 & Feedthru bypass V1511 filament \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1555 & & Same as C1517 & Feedthru bypass V1511 filament \\
\hline C1556 & & Same as C1517 & Feedthru bypass V1512 filament \\
\hline C1557 & & Same as C1517 & Feedthru bypass V1512 filament \\
\hline C1558 & & Same as C1505 & Coupling Z1507 to V1504 \\
\hline C1559 & & Same as C1505 & Coupling Z1508 to V1510 \\
\hline C1560 & & Same as C1501 & Feedthru bypass
\[
24 \text { v AC }
\] \\
\hline C1561 & & Same as C1501 & Feedthru bypass to DS1403 \\
\hline C1562 & & Same as C1501 & Feedthru bypass to DS1402 \\
\hline C1563 & & Same as C1501 & Feedthru bypass V1507A metering \\
\hline C1564 & & Same as C1501 & Feedthru bypass V1507B metering \\
\hline C1565 & & Same as C1501 & Feedthru bypass V1508 metering \\
\hline C1566 & & Same as C1501 & Feedthru bypass
150 v DC \\
\hline C1567 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(1 \mu \mathrm{f}, \pm 10 \% ; 200 \nabla\) DC working; MIL type CP05A1KC104K per spec MIL-C-25/A; 21964 part \#644149; Same as C345 & Cathode bypass V1510 \\
\hline C1568 & & CAPACITOR, FIXED, CERAMIG DIELECTRIC: \(1000 \mu \mu \mathrm{f}, \pm 20 \%\), 500 vdc , per MIL-C-19321, 21964 \#A1068959; Same as C201 & Bypass for RF choke V1504 plate supply \\
\hline C1569 & & Same as C1568 & Bypass for RF choke V1504 plate supply \\
\hline C1570 & & Same as C1568 & Bypass for RF choke V1501A metering \\
\hline C1571 & & Same as C1568 & Bypass for RF choke V1501B metering \\
\hline C1572 & & Same as C1568 & Bypass for RF choke V1502 metering \\
\hline C1573 & & Same as C1568 & Bypass for filament choke V1506 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1574 & & Same as C1568 & Bypass for filament choke V1506 \\
\hline C1575 & & Same as C1568 & Bypass for filament choke V1505 \\
\hline C1576 & & Same as C1568 & Bypass for filament choke V1505 \\
\hline C1577 & & Same as C1568 & Bypass for filament choke V1504 \\
\hline C1578 & & Same as C1568 & Bypass for filament choke V1504 \\
\hline C1579 & & Same as C1568 & Bypass for filament choke V1501. V1502. V1503 \\
\hline C1580 & & Same as C1568 & Bypass for filament supervisory choke \\
\hline C1581 & & Same as C1568 & Bypass for filament supervisory choke \\
\hline C1582 & & Same as C1568 & Bypass for RF choke crystal heater \\
\hline C1583 & & Same as C1568 & Bypass for RF choke crystal heater \\
\hline C1584 & & Same as C1568 & Bypass for RF choke crystal heater \\
\hline C1585 & & CAPACITOR, FIXED, CERAMIC DIELECTRIC: \(100 \mu \mu \mathrm{f}\), \(+80 \%-20 \%, 1000\) v DC; per MIL-C-19321, 21964 \#A1068960 & RF bypass \\
\hline E1501 & 5 & SHIELD, ELECTRON TUBE: JAN type TS103U01 per JAN-S-28A, modified; 21964 \#A2132988-4; Same as E404 & Shield for V1501 \\
\hline E1501A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103U01; MIL-STD-242A type \#901; 21964 \#A2132886-4; Same as E404A & Insert for shield E1501 \\
\hline E1502 & 5 & SHIELD, ELECTRON TUBE: JAN type TS-102U01 per JAN-S-28A, modified 21964 \#A2132988-1; Same as E201 & Shield for V1502 \\
\hline E1502A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U01; MIL-STD-242A type \#701; 21964 \#A2132886-1; Same as E201A & Insert for shield E1502 \\
\hline E1503 & 6 & SHIELD, ELECTRON TUBE: JAN type TS102U02 per JAN-S28A, modified 21964 \#A2132988-2; Same as E202 & Shield for V1503 \\
\hline E1503A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U02; MIL-STD-242A type \#702 21964 \#A2132886-2; Same as E202A & Insert for shield E1503 \\
\hline E1504 & & Same as E1501 & Shield for V1507 \\
\hline E1504A & & Same as E1501A & Insert for shield E1504 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1505 & & Same as E1502 & Shield for VI508 \\
\hline E1505A & & Same as E1502A & Insert for shield E1505 \\
\hline E1506 & & Same as E1503 & Shield for V1509 \\
\hline E1506A & & Same as E1503A & Insert for shield E1506 \\
\hline HR1501 & & OVEN, CRYSTAL: for crystal unit MIL type CR-32/U in MIL type \(\mathrm{HC}-6 / \mathrm{U}\) holder; oven temperature \(75^{\circ} \mathrm{C}\), ambient temperature ranges \(-54^{\circ} \mathrm{C}\) to \(+75^{\circ} \mathrm{C} \pm 5^{\circ} \mathrm{C}\) tolerance and \(-25^{\circ} \mathrm{C}\) to \(+75^{\circ} \mathrm{C} \pm 2^{\circ} \mathrm{C}\) tolerance, 24 v AC, 60 cycles, single phase, 36 volt-amperes 84678 \#HOD 0-2, 21964 \#1068981 (p/o Z1516) & Oven for Y 1501 RF assy high band \\
\hline HR1502 & & Same as HR1501; (p/o Z1515) & Oven for Y 1502 RF assy low band \\
\hline J1501 & & Not Used & \\
\hline J1502 & & CONNECTOR, RECEPTACLE: 1 contact, round female straight type, metal, polarized; RF connector, 50 ohms nom impedance, MIL type UG-1094/U BNC series, Navy dwg REB49063, modified 21964 \#B2060628G-1 & V1504 local oscillator freq. output Figure 6-56 \\
\hline J1503 & & CONNECTOR, RECEPTACLE ELECTRICAL: 1 contact, round female \(90^{\circ}\) type, 21964 \#B2060086 & To P1401 Figure 6-4 \\
\hline J1504 & & Not Used & \\
\hline J1505 & & Same as J1502 & V1510 local oscillator freq. output Figure 6-56 \\
\hline J1506 & & Same as J1503 & \begin{tabular}{l}
To P1401 \\
Figure 6-4
\end{tabular} \\
\hline J1507 & & CONNECTOR, RECEPTACLE, ELECTRICAL: contains parasitic suppressor assembly, sealed c/o two uninsulated RF chokes (Z1509) ntd on board assy, plug, insulator and probe; coil data, 10 uh at \(40 \mathrm{mc}, 0.60\) ohms DC resistance, \(750 \mathrm{ma} ; 21964\) \#B2060814G1 & To P1503 \\
\hline J1508 & & CONNECTOR, RECEPTACLE, ELECTRICAL: Same as J1507 except for reference symbol marking on case; 21964 \#B2060814G2 & To P1503 \\
\hline J1509 & & CONNECTOR, RECEPTACLE, ELECTRICAL: 24 male contacts; one connector mating end; \(5 \mathrm{amps}, 800 \mathrm{v}\) DC; 02660 \#26-4401-24P; 21964 *B2132197-14 & Power cable connector high band RF chassis Figure 6-56 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline J1510 & & Same as J1509 & Power cable connector, low band RF chassis Figure 6-56 \\
\hline L1501 & & COIL, RADIO FREQUENCY: 2,000 ma DC current rating; 0.22 microhenries \(\pm 20 \%\); 0.04 max \(D C\) resistance; wire lead type; B2142 \#10100-22; 21964 \#A2130069-6 & RF choke +150 v DC \\
\hline L1502 & & COIL, RADIO FREQUENCY: single layer close wound, winding 14 turns no. 30R2 AWG wire, \(0.86 \mu \mathrm{~h}\) to \(1.15 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment 21964 \#C2060131G1 & Plate tuning V1501A Figure 2-18 \\
\hline L1503 & & COIL, RADIO FREQUENCY: single layer close wound winding, 6 turns no. 27R2 AWG wire, \(0.237 \mu \mathrm{~h}\) to \(0.295 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 "C2060131G2 & Plate tuning V1501B Figure 2-18 \\
\hline L1504 & & COIL, RADIO FREQUENCY: 1000 ma DC current rating; 1.0 uh \(\pm 20 \%\); 0.3 ohms max DC resistance; cylindrical shape; wire lead type; 82142 \#10100-30; 21964 \#A2132611-3 & Parasitic suppressor in cathode circuit of V1501 \\
\hline L1505 & & Not Used & \\
\hline L1506 & & Same as \(\mathbf{L 1 5 0 1}\) & RF choke V1502 screen grid supply \\
\hline L1507 & & Same as L1501 & RF choke V1503 plate supply \\
\hline L1508 & & COIL, RADIO FREQUENCY: 550 ma DC current rating; 2.2 \(\mu \mathrm{h}, \pm 20 \%\) tolerance; 1.10 max DC resistance; wire lead type; B2142 \#10100-34; 21964 \#A2130069-9 & RF choke in screen circuit of V1502 \\
\hline L1509 & & COIL, RADIO FREQUENCY: single layer close wound winding, 4 turns no. 23R2 AWG wire, \(0.129 \mu \mathrm{~h}\) to \(0.150 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#C2060131G3 & Plate tuning V1502 Figure 2-18 \\
\hline L1510 & & Same as L1504 & RF choke V1503 plate supply \\
\hline L1511 & & Same as L1508 & RF choke V1503 cathode \\
\hline \(\mathbf{L 1 5 1 2}\) & & Same as L1501 & RF choke +150 v DC \\
\hline 1513 & & COIL, RADIO FREQUENCY: single layer close wound winding; 17 turns no. 30R2 AWG wire, \(1.12 \mu \mathrm{~h}\) to \(1.42 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment 21964 C2060131G4 & Plate tuning V1507A Figure 2-18 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline L1514 & & COIL, RADIO FREQUENCY: single layer close wound winding; 8 turns no. 27R2 AWG wire, \(0.345 \mu \mathrm{~h}\) to \(0.43 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment; 21964 \#C2060131G5 & Plate tuning V1507B Figure 2-18 \\
\hline \(\mathbf{L 1 5 1 5}\) & & Same as L1504 & Spurious oscillator suppressor V1507 \\
\hline L1516 & & Same as L1501 & RF choke V1508 screen grid supply \\
\hline L1517 & & Same as L1501 & RF choke V1509 plate supply \\
\hline L1518 & & Same as L1508 & RF choke V1508 plate supply \\
\hline L1519 & & COIL, RADIO FREQUENCY: single layer close wound winding, 6 turns no. 23R2 AWG wire, \(0.198 \mu \mathrm{~h}\) to \(0.237 \mu \mathrm{~h}\) inductance; ceramic coil form; adjustable tuning, powdered iron slug, screwdriver adjustment 21964 *C2060131G6 & Plate tuning V1508 Figure 2-19 \\
\hline L1520 & & Same as L1504 & RF choke V1509 plate supply \\
\hline L1521 & & Same as L1508 & RF choke V1509 cathode \\
\hline L1522 & & Same as L1501 & Filament choke V1501 \\
\hline L1523 & & Same as L1501 & Filament choke V1502 \\
\hline L1524 & & Same as L1501 & Filament choke V1503 \\
\hline L1525 & & Same as L1501 & Filament choke V1507 \\
\hline L1526 & & Same as L1501 & Filament choke V1508 \\
\hline L1527 & & Same as L1501 & Filament choke V1509 \\
\hline L1528 & & Same as L1508 & RF choke V1501A metering \\
\hline L1529 & & Same as L1504 & RF choke V1502 metering \\
\hline L1530 & & Same as L1508 & RF choke V1501B metering \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline L1531 thru L1534 & & Not Used & \\
\hline L1535 & & Same as L1508 & RF choke V1507A metering \\
\hline 15156 & & Same as L1508 & RF choke V1507B metering \\
\hline \(\mathbf{L 1 5 3 7}\) & & Same as L1508 & RF choke V1508 metering \\
\hline \(\mathbf{L 1 5 3 8}\) & 4 & COIL, RADIO FREQUENCY: \(10 \mu \mathrm{~h}\) inductance; p/o z1509 & p/o Z1509 \\
\hline \(\mathbf{L 1 5 3 9}\) & & Same as L1538; p/o Z1509 & p/o Z1509 \\
\hline L1540 & & Same as L1538; p/o Z1510 & p/o Z1510 \\
\hline L1541 & & Same as L1538; p/o Z1510 & p/o Z1510 \\
\hline L1542 & & COIL, RADIO FREQUENCY: 2100 ma DC current rating; \(22 \mu \mathrm{~h}\), \(\pm 20 \%\); . 04 max DC resistance; MIL type LT7K126, per MIL-C15305A and MS75008; 21964 \#866001H228 & RF choke V1506 plate supply \\
\hline L1543 & & Same as L1542 & RF choke V1504 plate supply \\
\hline L1544 & & Same as L1542 & RF choke +150 v DC \\
\hline L1545 & & Same as \(\mathbf{L 1 5 4 2}\) & ```
RF choke V1501A
    metering
``` \\
\hline L1546 & & Same as L1542 & RF choke V1501B metering \\
\hline L1547 & & Same as \(\mathbf{L 1 5 4 2}\) & RF choke V1502 metering \\
\hline L1548 & & Same as L1542 & Filament choke V1506 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline \(\mathbf{L 1 5 4 9}\) & & Same as L1542 & Filament choke V1506 \\
\hline L1550 & & Same as L1542 & Filament choke V1505 \\
\hline \(\mathbf{L 1 5 5 1}\) & & Same as L1542 & Filament choke V1505 \\
\hline L1552 & & Same as L1542 & Filament choke V1504 \\
\hline L:553 & & Same as L1542 & Filament choke V1504 \\
\hline L1554 & & Same as L1542 & \[
\begin{aligned}
& \text { Filament choke V1501, } \\
& \text { V1502, V1503 }
\end{aligned}
\] \\
\hline L1555 & & Same as L1542 & Filament supervisory choke \\
\hline L1556 & & Same as L1542 & Filament supervisory choke \\
\hline L1557 & & Same as L1542 & RF choke crystal heater \\
\hline L1558 & & Same as L1542 & RF choke crystal heater \\
\hline L1559 & & Same as L1542 & RF choke crystal heater \\
\hline P1501 & & Not Used & \\
\hline P1502 & & Not Used & \\
\hline P1503 & & CLIP, ELECTRICAL: \#2, over all length 1 ", width \(3 / 8^{\prime \prime}\), phosper bronze, nickel plate, 72307 \#2, 21964 \#A2140562 & \[
\begin{aligned}
& \text { To J1507 or } \\
& \mathrm{J} 1508
\end{aligned}
\] \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline P1504 & & CONNECTOR, PLUG, ELECTRICAL: 24 female contacts; one connector mating end; \(5 \mathrm{amps}, 800 \mathrm{v}\) DC; 0.5625 " dia max cable accommodated; 02660 \#26-4301-24S; 21964 \#B2132687-2 & Main power plug for RF chassis \\
\hline R1501 & 6 & RESISTOR, FIXED, COMPOSITION: 22,000 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF223K per MIL-R-11; 21964 \#504247; Same as R604 & Voltage dropping V1501A plate \\
\hline R1502 & & Same as R1411 & Cathode bias, V1501A \\
\hline R1503 & 6 & RESISTOR, FIXED, COMPOSITION: 220 ohms, \(\pm 10 \%\) tolerance; 1/2 watt; ML type RC20GF221K per spec MIL-R-11; 21964 *504223; Same as R208 & Cathode bias, V1501B \\
\hline R1504 & 6 & RESISTOR, FIXED, COMPOSITION: \(4,700 \mathrm{ohms}, \pm 10 \% ; 1 / 2\) watt; MIL type RC20GF472K per spec MLL-R-11; 21964 \#504239; Same as R339 & Grid leak V1501B \\
\hline R1505 & & Same as R1410 & Meter shunt V1501A \\
\hline R1506 & & Not Used & \\
\hline R1507 & 6 & RESISTOR, FIXED, COMPOSITION: 47,000 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF473K, per spec MIL-R-11; 21964 \#504251; Same as R425 & Grid leak, V1502 \\
\hline R1508 & 6 & RESISTOR, FIXED, COMPOSITION: 2, \(200 \mathrm{ohms}, \pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF222K per spec MLL-R-11; 21964 \#504235; Same as R207 & \[
\begin{aligned}
& \text { Metering shunt, } \\
& \text { V1501B }
\end{aligned}
\] \\
\hline R1509 & & Not Used & \\
\hline R1510 & & Same as R1503 & Cathode bias, V1502 \\
\hline R1511 & & Same as R1410 & Cathode bias, V1503 \\
\hline R1512 & & Not Used & \\
\hline R1513 & 6 & RESISTOR, FIXED, COMPOSITION: 22 ohms, \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF220K per spec MLL-R-11; 21964 \#504211 & Metering shunt, V1502 \\
\hline R1514 thru R1517 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline R1518 & & Same as R1501 & Voltage dropping V1507A plate \\
\hline R1519 & & Same as R1411 & Cathode bias, V1507A \\
\hline R1520 & & Same as R1503 & Cathode bias, V1507B \\
\hline R1521 & & Same as R1504 & Grid leak V1507B \\
\hline R1522 & & Same as R1507 & Grid leak, V1508 \\
\hline R1523 & & Same as R1503 & Cathode bias, V1508 \\
\hline R1524 & & Same as R1410 & Cathode bias, V1509 \\
\hline  & & Not Used & \\
\hline R1528 & & Same as R1410 & Cathode bias, V1504 or V1510 \\
\hline R1529 & & Not Used & \\
\hline R1530 & & Same as R1426 & Cathode bias, V1505 or V1511 \\
\hline R1531 & & Not Used & \\
\hline \(\mathbf{R 1 5 3 2}\) & 6 & RESISTOR, FIXED, COMPOSITION: 10 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF100K per spec MIL-R-11; 21964 \#504207; Same as R334 & Cathode bias, V1506 or V1512 \\
\hline R1533 & 6 & RESISTOR, FIXED, COMPOSITION: 220, 000 ohms, \(\pm 10 \%\); \(1 / 2\) watt; MIL type RC20GF224K per spec MIL-R-11; 21964 \#504259: Same as R304 & Meter multiplier, V1504 or V1510 tuning \\
\hline R1534 & 6 & RESISTOR, FIXXED, COMPOSITION: 10,000 ohms, \(\pm 10 \%, 1 / 2\) watt; MIL type RC20GF103K per spec MIL-R-11; 21964 *504243; Same as R404 & Meter multiplier V1505 or V1511 tuning \\
\hline R1535 & & Same as R1410 & Meter multiplier V1501 or V1507 tuning \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1536 & & Same as R1508 & ```
Meter multiplier
    V1502 or V1508
    tuning
``` \\
\hline R1537 & & Same as R1513 & Cathode resistor V1509 \\
\hline T1501 & & TRANSFORMER, POWER, STEPDOWN: 120 v AC, 60 cycles, single phase; \#1 secondary 6.4 v 1.5 amp , 2 secondary 6.4 v 1.0 amp , \#3, \#4, and \#5 secondary 5.5 v 1.1 amp each; 49956 \#292-5621G1; MIL type TF1SX01KA per MIL-T-27A; 21964 \#A1069535 & \begin{tabular}{l}
Filament supply, V1407, V1501, V1502, V1503, V1504, V1505, V1506, V1507, V1508, V1509, V1510, V1511, V1512 \\
Figure 2-17
\end{tabular} \\
\hline T1502 & & TRANSFORMER, POWER, STEPDOWN: 120 v AC, 60 cycles, single phase; secondary 24 v \(1.6 \mathrm{amp} ; 49956\) \#292-6020G2; MIL type TF1SX01GA per MIL-T-27A; 21964 \#A1069537 & Heater supply, HR1501, HR1502 Figure 2-17 \\
\hline T1503 & & TRANSFORMER, POWER STEPDOWN: primary 120 v AC, 60 cycles, single phase; secondary \(6.3 \mathrm{v}, 2.5 \mathrm{amps} ; 49956\) \#292-5622G1 MIL type TF1SXO1FA per spec MIL-T-27A; 21964 \#A1069867 u/0 AN/GRN-9D & Filament supply Figure 2-17 \\
\hline V1501 & & ELECTRON TUBE: dual triode; MIL type 5670 per spec MIL-E-1C; 21964 \#700563; Same as V404 & Oscillator, frequency doubler Figure 2-18 \\
\hline V1502 & & ELECTRON TUBE: pentode; MIL type \#5654/6AK5W per spec MIL-E-1C; 21964 \#700561; Same as V201 & Frequency doubler Figure 2-18 \\
\hline V1503 & & ELECTRON TUBE: triode; MIL type \#6J4WA, per spec MIL-E-1 (Navy) 21964 \#A2133316; Same as V202 & Frequency doubler Figure 2-18 \\
\hline V1504 & & ELECTRON TUBE: triode; MLL type 2C39A per MIL-E-1C; 21964 \#700043 & Frequency tripler Figure 2-18 \\
\hline V1505 & & Same as V1504 & \begin{tabular}{l}
RF amplifier \\
Figure 2-18
\end{tabular} \\
\hline V1506 & & Same as V1504 & \begin{tabular}{l}
RF amplifier \\
Figure 2-18
\end{tabular} \\
\hline V1507 & & Same as V1501 & Oscillator, frequency doubler Figure 2-18 \\
\hline V1508 & & Same as V1502 & Frequency doubler Figure 2-18 \\
\hline V1509 & & Same as V1503 & Frequency doubler Figure 2-18 \\
\hline V1510 & & Same as V1504 & Frequency tripler Figure 2-18 \\
\hline V1511 & & Same as V1504 & \begin{tabular}{l}
RF amplifier \\
Figure 2-18
\end{tabular} \\
\hline V1512 & & Same as V1504 & \begin{tabular}{l}
RF amplifier \\
Figure 2-18
\end{tabular} \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XHR1501 & 6 & SOCKET, ELECTRON TUBE: 8 contacts, beryllium, silver plated; octal dual shaped, JAN type TS101P02 per spec JAN-S-28A; CMG 51B16758; 21964 \#740031; Same as XV501 & Socket for HR1501 \\
\hline XHR1502 & & Same as XHR \({ }^{1501}\) & Socket for HR 1502 \\
\hline \[
\begin{aligned}
& \text { XR1501 } \\
& \text { thru } \\
& \text { XR1568 }
\end{aligned}
\] & & Not Used & \\
\hline XR1569 & & CLIP, ELECTRICAL: ferrule style no. 5, MBCA Ref Dwg Group 37; beryllium copper, nickel plated; similar to 95114 13-16-CN; 21964 \#A2 141510 & Holder for R1569 \\
\hline XR 1570 & & Same as XR1569 & Holder for R1569 \\
\hline XR1571 & & Same as XR1569 & Holder for R1443 \\
\hline XR1572 & & Same as XR1569 & Holder for R1443 \\
\hline XV1501 & & Same as XV1401 & Socket for V1501 Figure 6-4 \\
\hline XV1502 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, brass, nickel plated; miniature; JAN type \#TS102P01 per spec JAN-S-28A-1; 21964 *740002; Same as XV308 & Socket for V1502 Figure 6-4 \\
\hline XV1503 & & Same as XV1502 & Socket for V1503 Figure 6-4 \\
\hline \[
\begin{gathered}
\text { XV1504 } \\
\text { thru } \\
\text { XV1506 }
\end{gathered}
\] & & Not Used & \\
\hline XV1507 & & Same as XV1401 & Socket for V1507 Figure 6-4 \\
\hline XV1508 & & Same as XV1502 & Socket for V1508 Figure 6-4 \\
\hline XV1509 & & Same as XV1502 & Socket for V1509 Figure 6-4 \\
\hline Y1501 & & * CRYSTAL UNIT, QUARTZ: 1 crystal plate; MIL crystal holder type no. HC-6/U, MIL type \#CR-65/U per spec MIL-C-21240 21964 \#A 1068962-1; (p/o Z1516) & Crystal oscillator, frequency determining; RF assy high band Figure 6-4 \\
\hline Y1502 & & * Same as Y1501; (p/o Z1515) & Crystal oscillator frequency determining; RF assy low band \\
\hline & & * Frequency depends upon channel assignment. Requisition must state channel or crystal frequency and reference crystal type and equipment application. & Figure 6-4 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCTY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline Z1501 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1501A and Z1501B (For Reference Only) & Figure 6-56 \\
\hline Z1501A & &  output frequency 1151 mc to 1213 mc ; brass, silver plated, rhodium finish; power take-off from coupling loop; manual tuning by dielectric slug; lower section, high band; c/o C1546, C1547, Z1511, Z1512; 21964 dwg \#B2060127-1 & Tripler (high band) lower section \\
\hline Z1501B & & CAVITY, TUNED: c/o plunger, electron tube type 2C39A (V1504), tube retainer, anode clamp, anode contact, and an insulator cap; upper section; high band; 21964 \#A2061886G1 & Tripler, (high band) upper section \\
\hline Z1502 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1502A and Z1502B (For Reference Only) & Figure 6-56 \\
\hline Z1502A & & CAVITY, TUNED: coaxial; input and output frequency range, 1151 mc to 1213 mc ; brass, silver plated, rhodium finish; power takeoff from coupling loop; manual tuning by dielectric slug; lower section; high band 21964 dwg \#A2060039-1 & 1st amplifier (high band) lower section \\
\hline Z1502B & & CAVITY, TUNED: c/o plunger, electron tube type 2X39A (V1505), tube retainer, anode clamp, anode contact, insulator cap; upper section; high band; 21964 \# A2061886G2 & 1st amplifier, (high band) upper section \\
\hline Z1503 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1503A and Z1503B (For Reference Only) & Figure 6-56 \\
\hline Z1503A & & Same as Z1502A & Final amplifier (high band) lower section \\
\hline Z1503B & & CAVITY, TUNED: c/o plunger, electron tube type 2C39A (V1506), tube retainer, anode clamp, anode contact, insulator cap; upper section; high band; 21964 dwg \#A2061886G3 & Final amplifier (high band) upper section \\
\hline Z1504 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1504A and Z1504B (For Reference Only) & Figure 6-56 \\
\hline Z1504A & & CAVITY, TUNED: coaxial; input frequency 321.4 mc to 343.3 mc , output frequency 962 to 1024 mc ; brass, silver plated, rhodium finish; power take-off from coupling loop, manual tuning by dielectric slug; lower section; low band; c/o C1552, C1553, Z1514; 21964 \#B2060127-2 & Tripler, (low band) lower section \\
\hline Z1504B & & CAVITY, TUNED: c/o plunger, electron tube type 2C39A (V1510), tube retainer, anode clamp, anode contact, insulator cap; upper section; low band; 21964 \#A2061886G4 & Tripler, (low band) upper section \\
\hline Z1505 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1505A and Z1505B (For Reference Only) & Figure 6-56 \\
\hline Z1505A & & CAVITY, TUNED: coaxial; input and output frequency range 962 mc to 1024 mc ; brass, silver plated, rhodium finish; power take-off from coupling loop; manual tuning by dielectric slug; lower section; low band; 21964 dwg \#A2060039-2 & 1st amplifier (low band) lower section \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
FREQUENCY MULTIPLIER-OSCILLATOR CV-1171/GRN-9D
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline Z1505B & - & CAVITY, TUNED: c/o plunger, electron tube type 2C39A (V1511), tube retainer, anode clamp, anode contact, insulator cap; upper section; low band 21964 \#A2061886G5 & 1st amplifier, (low band) upper section \\
\hline Z1506 & 8 & CAVITY ASSEMBLY, TUNED: c/o Z1506A and Z1506B (For Reference Only) & Figure 6-56 \\
\hline Z1506A & & Same as Z1505A & Final amplifier (low band) lower section \\
\hline Z1506B & & CAVITY, TUNED: c/o plunger, electron tube type 2C39A (V1512), tube retainer, anode clamp, anode contact, insulator cap; upper section; low band; 21964 \#A2061886G6 & Final amplifier (low band) upper section \\
\hline Z1507 & & FREQUENCY MULTIPLIER, COAXIAL TUNED CAVITY: \(1 / 4\) wavelength stub; brass, silver plated; c/o \(47 \mathrm{mmf} \pm 5 \%\), fixed glass capacitor (MIL type CY10C470J) and RG141/U coaxial cable assy with 2 connectors; 21964 \#B2060761G1 & Couples RF energy from V1503 to V1504 Figure 2-18 \\
\hline Z1508 & & FREQUENCY MULTIPLIER, COAXIAL TUNED CAVITY: \(1 / 4\) wavelength stub; brass, silver plated; c/o \(47 \mathrm{mmf} \pm 5 \%\), fixed glass capacitor (MIL type CY10C470J) and RG141/U coaxial cable assy with two connectors; 21964 \#B2060761G2 & Couples RF energy from V1509 to V1510 Figure 2-18 \\
\hline Z1509 & & SUPPRESSOR ASSEMBLY, PARASITIC: sealed assy c/o two uninsulated RF chokes mtd on board assy, plug, insulator and probe; coil data, \(10 \mu \mathrm{~h}\) at \(40 \mathrm{mc}, \mathbf{0 . 6 0}\) ohms DC resistance, 750 ma ; 21964 \#B2060814G1 & ```
Parasitic suppressor
    between Z1502 and
    Z1503
    Figure 6-56
``` \\
\hline Z1510 & 6 & Same as Z1509 except for ref symbol marking on case; 21964 *B2060814G2 & Parasitic suppressor between Z1505 and Z1506 Figure 6-56 \\
\hline Z1511 & 2 & CHOKE, RADIO FREQUENCY: 2000 ma DC current rating; \(1.0 \mu \mathrm{~h}\) \(\pm 20 \%\); 21964 \#B2061344G1 & Filament choke V1504 \\
\hline Z1512 & & Same as Z1511 & Filament choke V1504 \\
\hline Z1513 & & Same as Z1511 & Filament choke V1510 \\
\hline Z1514 & & Same as Z1511 & Filament choke V1510 \\
\hline Z1515 & 8 & OVEN ASSEMBLY, CRYSTAL: c/o HR1502, Y1502, 21964 *B1068990 & Crystal oven assy for RF assy low band Figure 2-18 \\
\hline Z1516 & 8 & OVEN ASSEMBLY, CRYSTAL: c/o HR1501, Y1501 21964 *B1068990 & Crystal oven assy for RF assy high band Figure 2-18 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline & & POWER SUPPLY PP-1766/URN & \\
\hline 1601-1799 & & POWER SUPPLY PP-1766/URN: rectification data, electronic type, 5R4WGB full wave; output data, DC; \(300 \mathrm{v}, 0.010 \mathrm{amp}\), regulated; \(250 \mathrm{v}, 0.285 \mathrm{amp}\), regulated; \(-215 \mathrm{v}, 0.006^{\prime \prime} \mathrm{amp}\), regulated; -375 v , 0.065 amp , regulated; \(-400 \mathrm{v}, 0.05 \mathrm{amp}\), regulated; input data, AC: \(120 \mathrm{v}, 60\) cycles; single phase; over-all dim. \(26-25 / 32^{\prime \prime} \mathrm{lg}\), 13-1/2" wide, \({ }^{15-31 / 32^{\prime \prime}}\) high; filter incl; rack-mounted with pullout slides, front access only; housed in an open aluminum framework, provides low-voltage for the system 21964 \#A2060008 and 2060008 & Part of Power Supply Assembly. OA-1537/GRN-9A Figure 6-62 \\
\hline C1601 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 10 uf, \(\pm 10 \% ; 1500 \mathrm{v}\) DC working; MIL type \#CP70B1EH106K, per spec MIL-C-25; 21964 \#641501 & \[
\begin{aligned}
& \text { Filter for }+250 \mathrm{v} \text {; } \\
& +300 \mathrm{v} \text { power supply }
\end{aligned}
\]
Figure 6-64 \\
\hline C1602 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 0.5 uf, \(+20-10 \%\), 1000 v DC working; MIL type \#CP55B4EG504V, per spec MIL-C-25; 21964 \#643695 & Filter \& cathode bypass Figure 6-1 \\
\hline C1603 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 0.1 uf, \(\pm 10 \%, 600 \mathrm{v}\) DC working; MIL type \#CP55B1EF104K, per spec MIL-C-25; 21964 \#640459 & Grid bypass V1605 Figure 6-1 \\
\hline C1604 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 0.5 uf, \(\pm 10 \%\), 600 v DC working; MIL type \#CP55B1EF504K, per spec MIL-C-25; 21964 \#640461 & \begin{tabular}{l}
Cathode bypass V1605 \\
Figure 6-1
\end{tabular} \\
\hline C1605 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(2 \mathrm{uf}, \pm 10 \%, 600 \mathrm{v}\) DC working; MIL type \#CP70E1EF205K per spec MIL-C-25; 21964 \#641037; Same as C504 & Output filter for
\[
+250 \mathrm{v}
\] \\
\hline \[
\begin{gathered}
\text { C1606 } \\
\text { thru } \\
\text { C1609 }
\end{gathered}
\] & & Not Used & \\
\hline C1610 & & Same as C1601 & Filter for - 375 v power supply Figure 6-1 \\
\hline C1611 & & Same as C1602 & Filter, V1612, one section not used Figure 6-1 \\
\hline C1612 & & Same as C1603 & Grid bypass V1612 Figure 6-1 \\
\hline C1613 & & Same as C1604 & \begin{tabular}{l}
Cathode bypass V1612 \\
Figure 6-1
\end{tabular} \\
\hline C1614 & & Same as C1605 & Output filter - 375 v power supply Figure 6-63 \\
\hline \[
\begin{gathered}
\text { C1615 } \\
\text { thru } \\
\text { C1019 }
\end{gathered}
\] & & Not Used & \\
\hline C1620 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCF PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline C1621

C1622 & 6 & \begin{tabular}{l}
CAPACITOR, FIXED, MICA DIELECTRIC: 510 uuf, \(\pm 5 \%\); 500 v DC working; \(-55^{\circ} \mathrm{C}\) to \(85^{\circ} \mathrm{C}\) operating temperature range; MIL type \#CM20C511J per spec MIL-C-5A; 21964 \#A2133174-35 \\
Not Used
\end{tabular} & Feedback, V1605 \\
\hline C1623 & & Same as C1621 & Feedback, V1612 \\
\hline DS1601
DS1602 & & \begin{tabular}{l}
LAMP, INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens, double contact bayonet base; clear, 24446 \#10C7/1DC; 21964 \#710071; Same as DS501 \\
Not Used
\end{tabular} & -375 v, "ON" Figure 3-7 \\
\hline DS1603 & & Same as DS1601 & \begin{tabular}{l}
LVPS "ON" \\
Figure 3-7
\end{tabular} \\
\hline DS1604 & & LAMP, GLOW: neon gas, 0.25 watt, \(67-87 \mathrm{v}\) DC striking voltage; double contact bayonet type; MIL type NE-16 per MLL-L-15098; 21964 \#A2060350; Same as DS502 & \begin{tabular}{l}
LV "ON" \\
Figure 6-63
\end{tabular} \\
\hline DS1605 & & Same as DS1601 & Ready for LV, MV Figure 3-7 \\
\hline E1601

E1602 & 7 & \begin{tabular}{l}
RETAINER, ELECTRON TUBE: stainless steel; clamps tube with spring action; \(2-1 / 4^{\prime \prime}\) high, \(3-7 / 32^{\prime \prime}\) wide; holds material \(2.04^{\prime \prime}\) dia; two slots for \#10 screw on 2-25/32" mounting center, CAIS type 926-Q7, bracket \#195-07-35; 21964 \#A2140766 (3 each used) \\
Not Used
\end{tabular} & Tube clamp \\
\hline E1603 & & Not Used & \\
\hline E1604 & & Not Used & \\
\hline E1605 & 5 & SHIELD, ELECTRON TUBE: JAN type \#TS103U02 per JAN-S-28A, modified; 21964 \#A2132988-5; Same as E307 & Shield for V1605 \\
\hline E1605A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type \#TS103U02; MIL-STD-242A type \#902; 21964 \#A2132886-5; Same as E307A & Insert for E1605 \\
\hline E1606 & 5 & SHIELD, ELECTRON TUBE: JAN type \#TS102U02 per JAN-S-28A, modified; 21964 \#A2132988-2; Same as E202 & Shield for V1606 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

POWHR SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOGATING FUNCTION \\
\hline E1606A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type *TS102U02; MIL-STD-242A type *702; 21964 *A2132886-2; Same as E202A & Insert for E1606 \\
\hline \[
\begin{gathered}
\text { E1607 } \\
\text { thru } \\
\text { E1611 }
\end{gathered}
\] & & Not Used & \\
\hline E1612 & & Same as E1605 & Shield for V1612 \\
\hline E1612A & & Same as E1605A & Insert for E1612 \\
\hline E1613 & & Same as E1606 & Shield for V1613 \\
\hline E1613A & & Same as E1606A & Insert for E1613 \\
\hline \[
\begin{gathered}
\text { E1614 } \\
\text { thru } \\
\text { E1620 }
\end{gathered}
\] & & Not Used & \\
\hline E1621 & & CLIP, ELECTRICAL: beryllium copper; silver plated finish; 21964 \#A2141702 & Plate clip, V1603 \\
\hline E1622 & & Same as E1621 & Plate clip, V1603 \\
\hline E1623 & & Same as E1621 & Plate clip, V1604 \\
\hline E1624 & & Same as E1621 & Plate clip, V1604 \\
\hline E1625 & & Not Used & \\
\hline E1626 & & Not Used & \\
\hline E1627 & & Same as E1621 & Plate clip V1611 \\
\hline E1628 & & Same as E1621 & Plate clip, V1611 \\
\hline E1629 & & Not Used & \\
\hline E1630 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1631 & & RETAINER, CAPACITOR: for mounting capacitor; MIL type \#CP07SG4, per spec MIL-C-25 modified; 21964 *B2143620-2 & Mounts C1601 \\
\hline E1632 & & Same as E1631 & Mounts C1601 \\
\hline E1633 & & Same as E1631 & Mounts C1610 \\
\hline E1634 & & Same as E1631 & Mounts C1610 \\
\hline E1635 & & Not Used & \\
\hline E1636 & & Not Used & \\
\hline E1637 & & RETAINER, CAPACITOR: for mounting capacitor; MIL type\#CP07SA4, per spec MIL-C-25 modified; 21964 \#B2143620-1; Same as E527 & Mounts C1605 \\
\hline E1638 & & Not Used & \\
\hline E1639 & & Not Used & \\
\hline E1640 & & Same as E1637 & Mounts C1605 \\
\hline E1641 & & Not Used & \\
\hline E1642 & & Not Used & \\
\hline E1643 & & Same as E1637 & Mounts C1614 \\
\hline E1644 & & Same as E1637 & Mounts C1614 \\
\hline F1601 & & FUSE, CARTRIDGE: \(0.75 \mathrm{amp}, 250 \mathrm{v}\); time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type, MIL type \#F02GF750B, per spec MIL-F-15160A and MIL std MS90078-23-1; 21964 \#882233 & Protection, fil. transformer T1603 Figure 3-7 \\
\hline F1602 & & FUSE, CARTRIDGE: \(1 \mathrm{amp}, 250 \mathrm{v}\), time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type; MIL type \#F02G1 R00B, per spec MIL-F-15160A and MIL std MS90078-24-1; 21964 \#882234; Same as F1303 & Protection, fil. transformer T1604 Figure 3-7 \\
\hline
\end{tabular}

TABLE 7-3, RADIO SET AN/GKN-9D, MAIITTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline F1603 & & FUSE, CARTRIDGE: \(2 \mathrm{amp}, 125 \mathrm{v}\) time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type; MIL type \#F02D2R00B, per spec MIL-F-15160A and MIL std MS90078-26-1; 21964 \#882236; Same as F905 & Protection plate transformer T1601 Figure 3-7 \\
\hline F1604 & & Same as F1602 & Protection plate transformer T1602 Figure 3-7 \\
\hline F1605 & & Same as F1601 & Spare \\
\hline F1606 & & Same as F1602 & Spare \\
\hline F1607 & & Same as F1603 & Spare \\
\hline F1608 & & Same as F1602 & Spare \\
\hline H1601 & & CAP, ELECTRICAL: moulded phenolic; u/w NAVY type H-27A jack; 21964 \# A9141290-1 and \# A9141291; Same as H1101 & Covers J1609 \\
\hline H1602 & & BOLT, REDUCED SHANK: steel rod, type no. 303 per MIL-S-853 class 7, type C; passivate finish; 21964 \# A9140059 (4 each used) Same as H903 & Used to secure unit in cabinet \\
\hline J1601 & & CONNECTOR, RECEPTACLE: single female round contact; straight type; phone type connector, black nylon insulator, max operating voltage \(1,500 \mathrm{v}\) peak; silver plated contacts, 74868 type 225-B; MIL type MS16108-3 per MIL-STD-242A; 21964 \# A2141949-1; Same as J305 & Metering, 250/300 v \\
\hline J1602 & & Not Used & \\
\hline J1603 & & Same as J1601 & Metering, -375v \\
\hline J1604 & & CONNECTOR, RECEPTACLE: single female round contact; straight type; phone type connector, red nylon insulator; max operating voltage 1,500 v peak; silver plated contacts, 74868 type 225-A; MIL type MS16082 per MIL-STD-242A; 21964 \# A2141949-3 & Metering, +250 v \\
\hline \[
\begin{gathered}
\mathrm{J} 1605 \\
\text { thru } \\
\mathrm{J} 1607
\end{gathered}
\] & & Not Used & \\
\hline J1608 & & CONNECTOR, RECEPTACLE: single female round contact; straight type; phone type connector, green nylon insulator; mac operating voltage \(1,500 \mathrm{v}\) peak; silver plated contacts; 74868 type 225-D; MIL type MS16108-5 per MIL-STD-242A; 21964 \# A2141949-2 & Metering, -375 v \\
\hline J1609 & & JACK, TELEPHONE: accommodates 2 conductor female type plug, \(0.916^{\prime \prime}\) max dia; Navy type H-27A; BuShips dwg \#9000-S6501C-74120 modified by painting surface grey per 21964 \#A2143641 and A2143640-1; Same as J1 101 & Sound powered telephone connection \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline K1601 & & \begin{tabular}{l}
RELAY, ARMATURE: contact arrangement 2C, MBCA Ref Dwg Group 4, DPDT, single break, 2 amp, 115 v AC; one inductive winding; coil resistance 8000 ohms, operating current 3 ma , pickup current 2.3 ma; 6 terminals on contacts, 2 terminals on coil; continuous duty; 78277 \#22RFCC-90510, per spec MIL-R-5757C; 21964 \#A2140533 \\
Not Used
\end{tabular} & -375 v supervisory \\
\hline K1603 & & RELAY, ARMATURE: closed type; four poles single-throw contacts, normally open, double break, \(A C, 220 \mathrm{v}, 10 \mathrm{amp}\); single inductive winding, 120 v AC, 60 cycles; 8 contact terminals, 2 coil terminals; per spec MIL-C-2212A; similar to 04005 size 0U type "CRA"; 21964 \#C2141272-1 and spec \#A2140748-1 & \begin{tabular}{l}
LVPS plate contactor \\
Figure 2-12
\end{tabular} \\
\hline K1604 & & RELAY, ARMATURE: contact arrangement 2 form \(C\) type, DPDT, \(A C, 120 \mathrm{v}, 10 \mathrm{amp} ; 1\) winding, inductive winding; AC, 123 v ; max continuous operating, operating current not rated, 60 cycles, 6 terminals for contacts, 2 terminals for coil; continuous duty; hermetically sealed; 70309 type PBH, per spec MIL-R-5757C; 21964 \#A2060235; Same as K1301 & \begin{tabular}{l}
B+ protector \\
Figure 6-63
\end{tabular} \\
\hline K1605 & & RELAY, MOTOR DRIVEN: SPDT, \(115 / 250 \mathrm{v}, 5 \mathrm{amp}, 60\) cycles; motor data AC, synchronous type, 105 to 132 v rms. 60 cycles; 2 terminals for motor 3 terminals for contacts; 1 min time interval; resets automatically: hermetically sealeu: time interval factory adjusted; 14907 \# 430 H set at 1 min ; per 21964 \# A2142407; Same as K1102 & ```
Blower "OFF" time
    delay B901, B902.
    B1001
    Figure 6-1
``` \\
\hline K1606 & & RELAY, MOTOR DRIVEN: SPDT, \(115 ; 250 \mathrm{v}, 5 \mathrm{amp}, 60\) cycles motor data AC, synchronous type, 105 to 132 v rms, 60 cycles; 2 terminals for motor; 3 terminals for contacts; 5 min time interval; resets automatically; hermetically sealed; time interval factory adjusted; 14907 \#430H set at 5 min ; per 21964 \#A2142405 & V1304, Klystron heater time delay Figure 6-1 \\
\hline MP1601 & & BOOT, DUST AND MOISTURE SEAL: silicone rubber bonded to a brass nickel plated hex nut \(15 / 32-32\) thd; \(3,4^{\circ}\) across flats, \(7 / 8^{\prime \prime} \mathrm{lg}\); 97539 part \#1030; 21964 \#A213264G-1; Same a; MP202 & Seal for switch, on panel \\
\hline MP1602 & 1 & GASKET: synthetic rubber, MIL-R-900A, class 2; cross-sectional style no. 7, Ref Dwg Group 74; \(1 ; 8^{\prime \prime}\) wide, \(5,32^{\prime \prime}\) high w/1/16"' radius, approx 44-9/32* 1 g ; 21964 \#A9140800; Same as MP201 & Panel sealing \\
\hline MP1603 & 2 & GASKET: synthetic rubber; dim. \(1-9 / 16^{\prime \prime}\) w \(1-9,16^{\prime \prime} \mathrm{h}, 1 / 32^{\prime \prime}\) thk; aperture \(1-1 / 32^{\prime \prime}\) hole dia; four \(11 / 64^{\circ}\) uia mtg holes on \(1-1 / 4^{\prime \prime}\) by 1-1/4" centers; 21964 \#A2141718 & Seals telephone jack \\
\hline R1601 & 6 & RESISTOR, FIXED, COMPOSITION: 150,000 ohms, \(\pm 10 \%\); 2 watt; MIL type RC42GF154K, per spec MIL-R-11; 21964 \#501267 & Divider, V1605 \\
\hline R1602 & & Same as R1601 & Divider, V1605 \\
\hline R1603 & & RESISTOR, FIXED, COMPOSITION: 75, 000 ohms, \(\pm 5 \%\); 2 watt; MIL type \#RC42GF753J, per spec MIL-R-11; 21964 \#501158 & Divider, V1605 \\
\hline R1604 & 6 & RESISTOR, FIXED, COMPOSITION: 1.0 megohm, \(\pm 10 \%\); 1 watt; MIL type \#RC32GF105K, per spec MIL-R-11; 21964 \#503954 & Decoupling, V1605 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1605 & 6 & RESISTOR, FLXED, COMPOSITION: 47 ohms, \(\pm 10 \% ; 1\) watt; MIL type *RC32GF470K, per spec MIL-R-11; 21964 \#503902 & Damping, V1604 \\
\hline R1606 & & Same as R1605 & Damping, V1604 \\
\hline R1607 & & Same as R1605 & Damping, V1604 \\
\hline R1608 & & Same as R1605 & Damping, V1603 \\
\hline R1609 & & Same as R1605 & Damping, V1603 \\
\hline R1610 & & Same as R1605 & Damping, V1603 \\
\hline R1611 & 6 & RESISTOR, FIXED, COMPOSITION: 470 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type *RC 20GF471K, per spec MIL-R-11; 21964 \(\boldsymbol{\$ 5 0 4 2 2 7 ; ~ S a m e ~}\) as R452 & Damping, V1603 \\
\hline R1612 & & Same as R1611 & Damping, V1603 \\
\hline R1613 & & Same as R1611 & Damping, V1604 \\
\hline R1614 & & Same as R1611 & Damping, V1604 \\
\hline R1615 & 6 & RESISTOR, FIXED, COMPOSITION: 10,000 ohms, \(\pm 10 \%\); 2 watt; MIL type \#RC42GF103K, per spec MIL-R-11; 21964 \#501253; Same as R416 & Voltage divider cathode V1605 \\
\hline R1616 & 6 & RESISTOR, FIXED, COMPOSITION: 9100 ohms, \(\pm 5 \%\); 2 watt; MIL type \#RC42GF912J, per spec MIL-R-11; 21964 \# 501136 & Voltage divider cathode V1605 \\
\hline R1617 & & Same as R1615 & Voltage divider cathode V1605 \\
\hline R1618 & 6 & RESISTOR FIXED, COMPOSITION: 220,000 ohms, \(\pm 10 \%\); 1 watt; MIL type \#RC32GF224K, per spec MIL-R-11; 21964 \#503946 & Plate, V1605 \\
\hline R1619 & & Same as R1618 & Plate, V1605 \\
\hline R1620 & 6 & RESISTOR, FIXED, COMPOSITION: 12,000 ohms, \(\pm 10 \%\); 2 watt; immersion; 2 wire lead terminals; MIL type \#RC42GF123K, per spec MIL-R-11; 21964 \#501254; Same as R613 & Voltage divider cathode V1605 \\
\hline R1621 & 6 & RESISTOR, FIXED, COMPOSITION: 6800 ohms, \(\pm 10 \% ; 2\) watt; MIL type \#RC42GF682K, per spec MIL-R-11; 21964 \#501251 & Voltage divider cathode V1605 \\
\hline R1622 & & Same as R1615 & Voltage divider cathode V1605 Figure 6-63 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

\section*{POWER SUPPLY PP-1786/URN}
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1623 & 6 & RESISTOR, VARIABLE: composition element; 1 section, 5,000 ohms \(\pm 10 \%\); 2 watt nom power rating; no switch, MIL type RV4LAVSA502A per MIL-R-94 and MIL-STD-242 (Ships); 21964 \#A2133049-4; Same as R1364 & Output voltage control \(+250 \mathrm{v}\) Figure 2-12 \\
\hline R1624 & 6 & RESISTOR, FIXED, COMPOSITION: 47, 000 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20G F473K, per spec MIL-R-11; 21964 \#504251; Same as R425 & Decoupling, V1605 Figure 6-1 \\
\hline R1625 & 6 & RESISTOR, FIXED, COMPOSITION: 82,000 ohms, \(\pm 10 \%\); 1 watt; MIL type RC32GF823K, per spec MIL-R-11; 21964 \#503941 & \begin{tabular}{l}
Plate, V1606 \\
Figure 6-1
\end{tabular} \\
\hline R1626 & & Same as R1620 & Voltage divider cathode V1605 \\
\hline R1627 & & Same as R1618 & Plate, V1605 \\
\hline R1628 & & Not Used & \\
\hline R1629 & 6 & RESISTOR, FIXED, COMPOSITION: 2.7 megohm, \(\pm 10 \%\); 1 watt; MIL type RC32GF275K, per spec MIL-R-11; 21964 \#503959 & Feedback, V1605 \\
\hline \[
\begin{aligned}
& \text { R1630 } \\
& \text { thru } \\
& \text { R1646 }
\end{aligned}
\] & & Not Used & \\
\hline R1647 & & Same as R1601 & Divider, V1612 \\
\hline R1648 & & Same as R1601 & Divider, V1612 \\
\hline R1649 & & Same as R1603 & Divider, V1612 \\
\hline R1650 & & Same as R1604 & Decoupling, V1012 Figure 6-1 \\
\hline R1651 & & Same as R1605 & Damping, V1611 \\
\hline R1652 & & Same as R1605 & Damping, V1611 \\
\hline R1653 & & Same as R1605 & Damping, V1611 \\
\hline R1654 & & Same as R1611 & Damping, V1611 \\
\hline R1655 & & Same as R1611 & Damping, V1611 \\
\hline R1656 & 6 & RESISTOR, FIXED, COMPOSITICN: 18, 000 ohms, \(\pm 10 \%\); 2 watt; MIL type RC42GF183K, per spec MIL-R-11; 21904 \#501256 & Voltage divider cathode V1612 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
HEF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTI ON \\
\hline R1657 & & Same as R1656 & Voltage divider cathode V1612 \\
\hline R1658 & 6 & RESISTOR, FIXED, COMPOSITION: 330,000 ohms, \(\pm 10 \%\); 2 watt; MIL type RC42GF334K, per spec MIL-R-11; 21964 \#501271; Same as R1408 & Plate, V1612 \\
\hline R1659 & & Same as R1620 & Voltage divider cathode V1612 \\
\hline R1660 & & Same as R1615 & Voltage divider cathode V1612 \\
\hline R1661 & 6 & RESISTOR, FIXED, COMPOSITION: 220, 000 ohms, \(\pm 10 \%\); 2 watt; MIL type RC42GF224K, per spec MIL-R-11; 21964 \#501269; Same as R1423 & Plate, V1612 \\
\hline R1662 & 6 & RESISTOR, FIXED, COMPOSITION: 470, 000 ohms, \(\pm 10 \% ; 2\) watt; MLL type RC42GF474K, per spec MIL-R-11; 21G64 \#501273; Same as R1424 & Plate, V1612 \\
\hline R1663 & & RESISTOR, VARIABLE: composition element; 1 section, 15,000 ohms, \(\pm 10 \%\), 2 watt nominal power rating; no switch; MIL type RV4LAVSA153A per MIL-R-94 and MIL-STD-242 (Ships); 21964 \#A2133049-5 & \begin{tabular}{l}
Output voltage control, -375 v \\
Figure 2-12
\end{tabular} \\
\hline R1604 & & RESISTOR, FIXED, COMPOSITION: 12,000 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF123J, per spec MIL-R-11; 21964 \#501139 & Voltage divider cathode V1612 \\
\hline R1665 & & Same as R1664 & Voltage divider cathode V1612 \\
\hline R1666 & & RESISTOR, FIXED, COMPOSITION: 10,000 ohms; \(\pm 5 \%\); 2 watt; MIL type RC42GF103J, per spec MIL-R-11; 21964 \#501137; Same as R1353 & Voltage divider cathode V1612 \\
\hline R1667 & & Same as R1624 & Decoupling, V1612 Figure 6-1 \\
\hline R1668 & & Same as R1601 & \begin{tabular}{l}
Plate, V1613 \\
Figure 6-1
\end{tabular} \\
\hline R1669 & & RESISTOR, FIXED, COMPOSITION: 1000 ohms; \(\pm 5 \%\); 2 watt; MIL type RC42GF102J, per spec MIL-R-11; 21964 \#501113 & Voltage divider cathode V1612 \\
\hline R1670 & 6 & RESISTOR, FIXED, COMPOSITION: 1.8 megohm, \(\pm 10 \%\); 1 watt; MIL type RC32GF185K, per spec MIL-R-11; 21964 \#503957 & Feedback, V1612 \\
\hline Cont. See R1701 & & & \\
\hline S1601 & & SWITCH, TOGGLE: single pole, single throw; 0.75 amp 125 v DC, 15 amp 125 v AC; JAN type ST42A, per spec JAN-S-23; 21964 \#828212; Same as S502 & Air switch for LVES Figure 3-7 \\
\hline T1601 & & TRANSFORMER, POWER STEP-UP: 120 v AC, 60 cycles, single phase; 1 output winding, center tapped, 520-0-520 vat 04 amp ; 49956 \#292-3676G1 MIL type no. TF1SX02YY per spec MIL-T-27A; 21964 \# A1 069534 & ```
250/300 v plate
    supply
    Figure 6-64
``` \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER BUPPLY PP-1766/URN


POWRR 8UPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XDS 1601
XDS1602 & & \begin{tabular}{l}
LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; \(125 \mathrm{v}, 6\) watts; MIL type LH63BG3 per MIL-L-3661, dwg MS-90286; 21964 \#A2133080-2 \\
Not Used
\end{tabular} & Holds DS1601 \\
\hline XDS 1603 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; 125 v , 6 watts; MIL type LH63BR3 per MIL-L-3661, dwg MS-90286; 21964 \#A2133080-1; Same as XDS1002 & Holds DS1603 \\
\hline XDS1604 & 6 & LAMPHOLDER: 125 v accommodates double contact bayonet base lamp; Military Standard lampholders dwg MS90290; 72619 \#9S4634-L-46; MIL spec no. MIL-L-3661; type \#LH-71-XXO; 21964 \#A9152053 or A2142519; Same as XDS502 & Holds DS1604 \\
\hline XDS1605 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; \(125 \mathrm{v}, 6\) watts; MIL type LH63BB3 per MIL-L-3661, dwg MS-90286; 21964 \#A2133080-4; Same as XDS1102 & Holds DS1605 \\
\hline XF1601 & & FUSEHOLDER: extractor post type; accommodates 2 fuses \(1-1 / \mathbf{4}^{\prime \prime} \mathbf{l g}\), 1/4" dia; blown fuse indicating type; sealed; MLL type FHL10G per BuShips Dwg \#9000-S6202-74228 and MIL-F-19207 (Ships); 21964 \#A2060402; Same as XF501 & Holds F1601 \& F1605 Figure 6-64 \\
\hline XF1602 & & Same as XF1601 & Holds F1602 \& F1606 Figure 6-64 \\
\hline XF1603 & & Same as XF1601 & Holds F1603 \& F1607 Figure 6-64 \\
\hline XF1604 & & Same as XF1601 & Holds F1604 \& F1608 \\
\hline XV1601 & 6 & SOCKET, ELECTRON TUBE: 8 contacts, beryllium, silver plated; octal dual shaped; MLL type TS101P02 per JAN-S-28A; 71785 51B16758; 21964 \#740031; Same as XV501 & Socket for V1601 Figure 6-1 \\
\hline XV1602 & & Same as XV1601 & Socket for V1602 Figure 6-1 \\
\hline XV1603 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, phosphor bronze and beryliium copper, silver plated; 74970 \#122-101-200; 21964 \#B2141950 & Socket for V1603 \\
\hline XV1604 & & Same as XV1603 & Socket for V1604 \\
\hline XV1605 & & SOCKET, ELECTRON TUBE: 9 contacts, brass, nickel plated; miniature; includes metal shield base; JAN type TS103P01, per spec JAN-S-28A-1; 21964 \#740004; Same as XV307 & Socket for V1605 Figure 6-1 \\
\hline XV1606 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, brass, nickel plated, miniature; includes metal shield base; JAN type TS102P01, per spec JAN-S-28A-1; 21964 \#740002; Same as XV308 & Socket for V1606 Figure 6-1 \\
\hline \[
\begin{gathered}
\text { XV1607 } \\
\text { thru. } \\
\text { XV1609 }
\end{gathered}
\] & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XV1610 & & Same as XV1601 & Socket for V1610 Figure 6-1 \\
\hline XV1611 & & Same as XV1603 & Socket for V1611 \\
\hline XV1612 & & Same as XV1605 & Socket for V1612 Figure 6-1 \\
\hline XV1613 & & Same as XV1606 & \begin{tabular}{l}
Socket for V1613 \\
Figure 6-1
\end{tabular} \\
\hline R1701 & & Not Used & \\
\hline R1702 & & Not Used & \\
\hline R1703 & & RESISTOR, FIXED, COMPOSITION: 5100 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF512J, per spec MIL-R-11; 21964 \#501130 & Voltage divider cathode V1605 \\
\hline R1704 & 6 & RESISTOR, FIXED, COMPOSITION: 56,000 ohms, \(\pm 10 \%\); 1 watt; MIL type RC32GF563K, per spec MIL-R-11; 21964 \#503939 & Voltage dropping K1601 \\
\hline R1705 & & RESISTOR, FIXED, COMPOSITION: 62, 000 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF623K, per spec MIL-R-11; 21964 \#501156 & Voltage dropping K1601 \\
\hline R1706 & & Not Used & \\
\hline R1707 & & Not Used & \\
\hline R1708 & 6 & RESISTOR, FDXED, COMPOSITION; 47 ohms, \(\pm 10 \% ; 2\) watt; MIL type RC42GF470K, per spec MIL-R-11; 21964 \#501225; Same as R501 & Current balancing V1603 \\
\hline R1709 & & Same as R1708 & Current balancing V1604 \\
\hline R1710 & & RESISTOR, FIXED, WIREWOUND: 280 ohms, 3 watt; MIL type RW59V281 per MIL-R-26C; 21964 \#A2132711-01; Same as R520 & Voltage dropping resistor for V1601 \\
\hline R1711 & & Not Used & \\
\hline R1712 & & Same as R1710 & Voltage dropping resistor for V1603 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1766/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1713 & 6 & RESISTOR, FIXED, COMPOSITION: 15,000 ohms, \(\pm 10 \%\) tolerance; 1 watt; MIL type RC32GF153K, per spec MIL-R-11; 21964 \#503932; Same as R521 & Voltage dropping resistor for V1604 \\
\hline R1714 & & Same as R1710 & Voltage dropping resistor for V1605 \\
\hline \[
\begin{gathered}
\text { TB1701 } \\
\text { thru } \\
\text { TB1796 }
\end{gathered}
\] & & Not Used & \\
\hline TB1797 & 2 & TERMINAL BOARD: 12 brass solder stud terminals; 21964 \#B2060111G1 & Mounts in LVPS \\
\hline TB1798 & 2 & TERMINAL BOARD: 24 brass solder stud terminals; 21964 \#C2060108 & Mounts in LVPS \\
\hline TB1799 & 2 & TERMINAL BOARD: 24 brass solder stud terminals; 21964 *C2060109 & Mounts in LVPS \\
\hline & & POWER SUPPLY PP-1765/URN & \\
\hline 1801-1899 & & POWER SUPPLY, PP-1765/URN: rectification data, electronic type, 2 type 836 tube, full-wave; output data, DC; \(1000 \mathrm{v}, 0.090 \mathrm{amp}\), regulated; \(700 \mathrm{v}, 0.085 \mathrm{amp}\), unregulated; input data; \(\mathrm{AC} ; 120 \mathrm{v}\), 60 cycles, single phase; over-all dim. \(26-25 / 32^{\prime \prime} \mathrm{lg}, 9-1 / 2^{\prime \prime}\) wide, 15-31/32" high; filter incl; rack-mounted with pullout slides, front access only; housed in an open aluminum frame work; provides medium voltage for the system; 21964 \#J2060009 & ```
Part of Power Supply
    Assembly
    OA-1537/GRN-9A
    Figure 6-65.
``` \\
\hline C1801 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 6 uf, \(\pm 10 \%\); 2500 v DC working; MIL type \#CP70E1EK605K, per spec MIL-C-25; 21964 \#641081 & \begin{tabular}{l}
Input filter \\
Figure 6-66
\end{tabular} \\
\hline C1802 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 2 uf, \(\pm 10 \%\); 2000 DC working; MIL type CP70E1EJ205K, per spec MIL-C-25; 21964 \#641068; Same as C1405 & \begin{tabular}{l}
Output bypass 1000 v \\
Figure 6-10
\end{tabular} \\
\hline \[
\begin{gathered}
\mathrm{C} 1803 \\
\text { thru } \\
\text { C1809 }
\end{gathered}
\] & & Not Used & \\
\hline C1810 & & CAPACITOR, FLXED, PAPER DIELECTRIC: 0.5 uf, \(\pm 10 \%\); 2000 v DC working; MIL type CP70E1EJ504K, per spec MIL-C-25; 21964 \#641066 & 829B screen bypass Figure 6-10 \\
\hline C1811 & & Not Used & \\
\hline C1812 & & CAPACITOR, FIXED, PAPER DIELECTRIC: \(2 \mathrm{mf}, \pm 10 \%\); 600 v DC working; MIL type CP70E1EF205K, per spec MIL-C-25; 21964 \#641037; Same as C504 & Overload circuit \\
\hline C 1813 & & Same as C1812 & Overload circuit \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline DS1801 & & LAMP, INCANDESCENT: \(115-125 \mathrm{v}, 10\) watts, 40 lumens double contact bayonet base; clear, 1 filament, tungsten; 24446 \#10C7/1DC; 21964 *710071; Same as DS501 & Indicator med voltage "ON" Figure 3-9 \\
\hline DS1802 & & LAMP, GLOW: neon gas, 0.25 watt, \(67-87 \mathrm{v}\) DC striking voltage; double contact bayonet type; MIL type NE-16 per MIL-L-15098; 21964 *A2060350; Same as DS502 & \begin{tabular}{l}
MV "ON" \\
Figure 2-13
\end{tabular} \\
\hline DS1803 & & LAMP, GLOW: neon gas, 0.04 watt; 120 v ; miniature bayonet base; MIL type NE-51 per MIL-L-15098B; 21964 \#A2141970; Same as DS901 & Medium voltage overload Figure 3-9 \\
\hline E1801 & & CLIP, ELECTRICAL: beryllium copper; cadmium plated finish; 42498 dwg \#SD-D198 part 4; 21964 \#A2141723 & Plate clip for V1901 \\
\hline E1802 & & Same as E1801 & Used w/V1802 \\
\hline E1803 thru E1807 & & Not Used & \\
\hline E1808 & 5 & SHIELD, ELECTRON TUBE: JAN type TS103U02 per JAN-S-28A, modified; 21964 \# A2132988-5; Same as E307 & Shield for V1808 \\
\hline E1808A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS103 U02; MIL-STD-242A type \#902; 21964 \#A2132886-5; Same as E307A & Insert for E1808 \\
\hline E1809 & & Not Used & \\
\hline E1810 & 5 & SHIELD, ELECTRON TUBE: JAN type TS102U03 per JAN-S-28A, modified; 21964 \#A2132988-3; Same as E408 & Shield for V1810 \\
\hline E1810A & & INSERT, ELECTRON TUBE SHIELD: use on shield JAN type TS102U03; MIL-STD-242A type \#703; 21964 dwg \#A2132886-3; Same as E408A & Insert for E1810 \\
\hline E1811 & & Same as E1810 & Shield for V1811 \\
\hline E1811A & & Same as E1810A & Insert for E1811 \\
\hline E1812 & & Same as E1810 & Shield for V1812 \\
\hline E1812A & & Same as E1810A & Insert for E1812 \\
\hline E1813 & & Same as E1810 & Shield for V1813 \\
\hline E1813A & & Same as E1810A & Insert for E1813 \\
\hline E1814 & & Same as E1810 & Shield for V1814 \\
\hline E1814A & & Same as E1810A & Insert for E1814 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1815 thru E1820 & & Not Used & \\
\hline E1821 & & CLIP, ELECTRICAL: beryllium copper; silver plated finisn; 21964 *A2141702; Same as E1621 & u/w V1803 \\
\hline E1822 & & Same as E1821 & u/w V1803 \\
\hline E1823 & & Same as E1821 & u/w V1804 \\
\hline E1824 & & Same as E1821 & u/w V1804 \\
\hline E1825 & & Same as E1821 & u/w V1805 \\
\hline E1826 & & Same as E1821 & u/w V1805 \\
\hline E1827 & & Same as E1821 & u/w V1806 \\
\hline E1828 & & Same as E1821 & u/w V1806 \\
\hline E1829 & & Same as E1821 & u/w V1807 \\
\hline E1830 & & Same as E1821 & u/w V1807 \\
\hline E1831 thru E1838 & & Not Used & \\
\hline E1839 & & RETAINER, CAPACITOR: MLL type CP07FB2, per spec MIL-C-25; 21964 \#380019 & Mounts C1810 \\
\hline E1840 & & Same as E1839 & Mounts C1810 \\
\hline E1841 & & RETAINER, CAPACITOR: MIL type CP07SA4, per spec MIL-C-25; modified, 21964 \#B2143620-1; Same as E527 & Holds C1812 \\
\hline E1842 & & Same as E1841 & Holds C1812 \\
\hline E1843 & & Same as E1841 & Holds C1813 \\
\hline E1844 & & Same as E1841 & Holds C1813 \\
\hline F1801 & & FUSE, CARTRIDGE: 5 amp ; 250 v time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type; MIL type F03G5R00B, per spec MIL-F-15160A and MIL STD MS90079-22-1; 21964 \#882259; Same as F1301 & \begin{tabular}{l}
Primary T1801 \\
protection \\
Figure 3-9
\end{tabular} \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline F1802 & & FUSE, CARTRIDGE: \(1 \mathrm{amp}, 250 \mathrm{v}\); time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type; MIL type F02G1R00B, per spec MIL-F-15160A and MIL STD MS90078-24-1; 21964 \#882234; Same as F1303 & Primaries T1802, T1804 protection Figure 3-9 \\
\hline F1803 & & Same as F1802 & Primary T1803 protection Figure 3-9 \\
\hline F1804 & & Same as F1801 & Spare \\
\hline F1805 & & Same as F1802 & Spare \\
\hline F1806 & & Same as F1802 & Spare \\
\hline J1801 & & CONNECTOR, RECEPTACLE, ELECTRICAL: single female round contact; straight type; phone type connector; 74868 \#225-B; MLL type MS16108-3 per MIL-STD-242A; 21964 \#A2141949-1; Same as J305 & Metering, ground \\
\hline J1802 & & Not Used & \\
\hline J1803 & & CONNECTOR, RECEPTACLE, ELECTRICAL: single female round contact; straight type; phone type connector; 74868 \#225-A; MLL type MS-10108-2 per MLL-STD-242A; 21964 \#A2141949-3; Same as J1604 & Metering, +1000 v \\
\hline K1801 & & RELAY, ARMATURE: contact arrangement 2C, DPDT, single break, \(2 \mathrm{amp}, 115 \mathrm{v} \mathrm{AC}\); 1 inductive winding; coil resistance 8000 ohm , operating current 3 ma , pick-up current \(2.3 \mathrm{ma} ; 6\) terminals on contacts, 2 terminals on coil; continuous duty; hermetically sealed; 78277 \#22RJCC-90510, per spec MLL-R-5757C; 21964 \# A2140533; Same as K1601 & 1000 v supervisory \\
\hline K1802 & & RELAY, ARMATURE: contact arrangement 2A1B, single break, 5 amp 115 v AC; single winding, 120 v AC, 60 cycles; 6 terminals on contacts, 2 terminals on coil; continuous duty; hermetically sealed; 71482 \#SG36015 type "GAC'' per spec MIL-R-5757C; 21964 \#A2140532 & Overload auxiliary 1000 v Figure 6-66 \\
\hline K1803 & & RELAY, ARMATURE: contact arrangement 1 C , single break, 2 amp , \(115 \mathrm{v} \mathrm{AC} ; 1\) inductive winding, \(\mathrm{DC} ; 16,000\) ohms resistance, 12.8 v operating voltage, 0.8 ma continuous operating current; 3 terminals on contacts, 2 terminals on coil, continuous duty; hermetically sealed; per spec MIL-R-5757C; 78277 \#5RJ90764-SLL; 21964 \#A2143385 & Overload 1000 v \\
\hline K1804 & & RELAY, ARMATURE: open type; four poles single-throw contacts, normally open, double break, AC, \(220 \mathrm{v}, 10 \mathrm{amp}\); single inductive winding; 120 v AC, 60 cycles; 8 contact terminals, 2 coil terminals; per spec MIL-C-2212A; similar to \(04009{ }^{\text {'CRA" }}\) ' size 00; 21964 \#C2141272-1 and spec A2140748-1; Same as K1603 & \begin{tabular}{l}
Plate contactor \\
Figure 6-10
\end{tabular} \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline K1805 & & RELAY, MOTOR DRIVEN: four SPDT contacts, \(115 / 250 \mathrm{v}, 5 \mathrm{amp}\), 60 cycles; motor data AC, synchronous type, \(120 \mathrm{v}, 60\) cycles; 2 terminals for motor; 4 terminals for contacts; three reclosures \(1 / 20 \mathrm{sec}\) duration of each impulse, 3 sec interval between impulses; automatically resets after each reclosure if successive trips are at least \(1 / 5 \mathrm{sec}\) apart, requires electrical reset by external switching circuit after three reclosure trials; hermetically sealed; 14907 HHR3, 21964 \#A2142406 & Overload reset circuit reclosing relay Figure 6-10 \\
\hline K1806 & 6 & RELAY, ARMATURE: closed type; four poles single-throw contacts. normally closed, double break, AC, \(220 \mathrm{v}, 10 \mathrm{amp}\); single inductive winding, 120 v AC 60 cycles; 8 contact terminals, 2 coil terminals; per spec MIL-C-2212A; similar to 04009 size 00 type "CRA"; 21964 \#C2141272-2 and spec A2140748-2 *See note below & Overload reset supervisory Figure 6-10 \\
\hline MP1801 & 7 & INSULATOR, WASHER: silicon resin glass cloth, type GSG; natural color; round shape; code no. 76 MBCA Ref Dwg Group; \(1 / 4^{\prime \prime}\) thk, \(5 / 8^{\prime \prime}\) dia \(0.169^{\prime \prime}\) dia hole centered; shank \(1 / 8^{\prime \prime}\) thk by \(1 / 4^{\prime \prime}\) dia; \(10,000 \mathrm{psi}\); special resistance to heat and flame; 21964 \#A2141686 (2 each used) & \(u / w\) wirewound resistor \\
\hline MP1802 & 7 & INSULATOR, WASHER: silicon resin glass cloth, type GSG; natural color; round shape; code no. 76 MBCA Ref Dwg Group; \(1 / 4^{\prime \prime}\) thk, \(1^{\prime \prime}\) dia. \(0.196^{\prime \prime}\) dia hole centered; shank \(1 / 8^{\prime \prime}\) thk by \(15 / 32^{\prime \prime}\) dia; \(10,000 \mathrm{psi}\); special resistance to heat and flame; 21964 \#A2141683-2 (3 each used) & \(u / w\) wirewound resistors \\
\hline MP1803 & 7 & INSULATOR, WASHER: silicon resin glass cloth, type GSG; natural color; round shape; code no, 76 MBCA Ref Dwg Group; 1/4" thk, \(1^{\prime \prime}\) dia, \(0.196^{\prime \prime}\) dia hole centered, shank \(1 / 8^{\prime \prime}\) thk by \(15 / 32^{\prime \prime}\) dia; \(10,000 \mathrm{psi}\); special resistance to heat and flame; 21964 \#A2141683-1 (3 each used) & \(\mathrm{u} / \mathrm{w}\) wirewound resistors \\
\hline MP1804 & & INSULATOR, BUSHING: ceramic grade L-5A; Ref Dwg Group no. 9, style \#174; MIL type NS5AW4103 per JAN-I-8; 21964 \#A2133203-3; Same as E1318 & Mounts C1801 \\
\hline MP1805 & & Same as MP1804 & Mounts C1801 \\
\hline MP1806 & & INSULATOR, BUSHING: ceramic grade L-5A; MIL type NS5AW4203 per JAN-I-8; 21964 \#A2133204-3; Same as E1320 & Mounts C1802 \\
\hline MP1807 & & Same as MP1806 & Mounts C1802 \\
\hline MP1808 & & BOLT, REDUCED SHANK: steel rod, type no. 303 per MIL-S-853, class 7, type C; passivate finish; head data not applicable to MBCA Ref Dwg Group 29, knurled thumb head socket recess, 1/2" high, 7/8' dia, o/a dim., recess dim. , \(0.3130^{\prime \prime}\) dim. across flats, 3/8' deep; reduced shank data \(5 / 8^{\prime \prime}\) dia, \(25 / 32^{\prime \prime} \lg ; 3 / 8^{\prime \prime}-16 \mathrm{NC}-2\) thd, 3/8' min lgth; 2-5/32" nominal lgth; 21964 \#A9140059 (4 each used); Same as H903 & Used to secure unit in cabinet \\
\hline MP1809 & 1 & GASKET: synthetic rubber, MIL-R-900A, class 2; cross sectional style no. 7, Ref Dwg Group 74; \(1 / 8^{\prime \prime}\) wide, \(5 / 32^{\prime \prime}\) high w/1/16" radius, approx 40-9/32" 1 g ; 21964 \#A9140800; Same as MP201 & Panel sealing \\
\hline MP1810 & & \begin{tabular}{l}
BOOT, DUST AND MOISTURE SEAL: silicon rubber bonded to a brass nickel plated hex nut \(15 / 32-32\) thd; \(3 / 4^{\prime \prime}\) across flats, 7/8' lg ; 97539 \#1030; 21964 \#A2132649-1; Same as MP202 \\
* For field replacement use same spare as provided for K1603, reversing fixed contacts to give the desired NC contact combination.
\end{tabular} & Seal for switch on panel \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN


TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1865 & & RESISTOR, FIXED, COMPOSITION: 82,000 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF823J per spec MIL-R-11; 21964 *501159 & Relay voltage divider \\
\hline R1866 & & Same as R1865 & Relay voltage divider \\
\hline R1867 & & Same as R1865 & Relay voltage divider \\
\hline R1868 & & Same as R1865 & Relay voltage divider \\
\hline R1869 thru R1871 & & Not Used & \\
\hline R1872 & & RESISTOR, VARIABLE: composition element; 1 section, 25, 000 ohms, \(\pm 10 \%\); 2 watt; no switch; MIL type RV4LAVSA253A per MIL-R-94 and MIL-STD-242 (Ships); 21964 \#A2133049-1; Same as R1470 & Over-load adjustment Figure 6-10 \\
\hline R1873 & 6 & RESISTOR, FIXED, WIREWOUND: 180 ohms, \(\pm 5 \%\); 18 watt; MIL type RW33G181, per spec MIL-R-26A; 21964 \# 531003 & Over-load relay shunt \\
\hline R1874 & & RESISTOR, FIXED, WIREWOUND: 12,000 ohms, \(\pm 5 \% ; 38\) watt; MIL type RW35G123, per spec MIL-R-26; 21964 *530399 & \begin{tabular}{l}
Plate V1810 \\
Figure 6-10
\end{tabular} \\
\hline R1875 & & RESISTOR, FIXED, WIREWOUND: 1400 ohms, \(\pm 5 \%\); 38 watt; MIL type RW35G142, per spec MIL-R-26; 21964 *531112 & 700 volt series Figure 6-10 \\
\hline R1876 & & Same as R1875 & 700 volt series dropping Figure 6-10 \\
\hline R1877 thru R1879 & & Not Used & \\
\hline R1880 & & RESISTOR, FIXED, COMPOSITION: 2200 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF222J, per spec MÍL-R-11; 21964 \#501121 & Screen dropping for 829B tube \\
\hline R1881 & & Same as R1880 & Screen dropping for 829B tube \\
\hline R1882 & & Same as R1880 & Screen dropping for 829B tube \\
\hline R1883 & 6 & RESISTOR, FIXED, COMPOSITION: 10,000 ohms, \(\pm 10 \% ; 1 / 2\) watt; MIL type RC20GF103K, per spec MIL-R-11; 21964 \#504243; Same as R404 & Parasitic suppressor V1808 \\
\hline R1884 thru R1886 & & Not Used & \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTEṄANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline R1887 & 6 & RESISTOR, FIXED, COMPOSITION: 120 ohms, \(\pm 10 \%\); 2 watt; MIL type RC42GF121K, per spec MIL-R-11; 21964 \#501230 & Cathode current balancing V1803 Figure 6-10 \\
\hline R1888 & & Same as R1887 & Cathode current balancing V1804 Figure 6-10 \\
\hline R1889 & & Same as R1887 & Cathode current balancing V1805 Figure 6-10 \\
\hline R1890 & & Same as R1887 & Cathode current balancing V1806 Figure 6-10 \\
\hline R1891 & & Same as R1887 & Cathode current balancing V1806 Figure 6-10 \\
\hline R1892 & & Not Used & \\
\hline R1893 & & RESISTOR, FIXED, COMPOSITION: 27, 000 ohms, \(\pm 5 \%\); 2 watt; MIL type RC42GF273J, per spec MIL-R-11; 21964 \#501147; Same as R1362 & Overload circuit \\
\hline R1894 & 6 & RESISTOR, FIXED, COMPOSITION: 6800 ohms, \(\pm 10 \% ; 2\) watt; MIL type RC42GF682K, per spec MIL-R-11; 21964 \#501251; Same as R1621 & Overload circuit \\
\hline R1895 & & RESISTOR, FLXED, WIREWOUND: 280 ohms, 3 watt; MIL type RW59V281, per MIL-R-26C; 21964 \#A2132711-01; Same as R520 & \[
\begin{aligned}
& \text { Voltage dropping } \\
& \text { resistor for } \\
& \text { DS1801 }
\end{aligned}
\] \\
\hline R1896 & 6 & RESISTOR, FIXED, COMPOSITION: 15,000 ohms, \(\pm 10 \%\); 1 watt; MIL type RC32GF153K, per spec MIL-R-11; 21964 \#503932; Same as R521 & \[
\begin{aligned}
& \text { Voltage dropping } \\
& \text { resistor for } \\
& \text { DS1802 }
\end{aligned}
\] \\
\hline S1801 & & SWITCH, TOGGLE: single-pole, single-throw; \(0.75 \mathrm{amp}, 125 \mathrm{v}\) DC, \(15 \mathrm{amp}, 125 \mathrm{v}\) AC, resistive load rating; JAN type ST42A, per spec JAN-S-23; 21964 \#828212; Same as S502 & 1 kv 'ON' switch Figure 3-9 \\
\hline S1802 & & SWITCH, TOGGLE: double-pole, double throw; \(0.75 \mathrm{amp}, 125 \mathrm{v}\) DC, \(15 \mathrm{amp}, 125 \mathrm{v}\) AC, resistive load rating; JAN type \#ST52R, per spec JAN-S-23; 21964 \#828243; Same as S1106 & Overload reset for MVPS Figure 3-9 \\
\hline T1801 & & TRANSFORMER, POWER STEP UP: 120 v AC, 60 cycles, single phase; 1 output winding, center tapped, \(1260-0-1260 \mathrm{v}\) at 0.28 amp ; 49956 \#292-3697G1B MIL type TC1SX02YY per MIL-T-27A; 21964 *A1069829 & Rectifier plate Figure 6-10 \\
\hline T1802 & & TRANSFORMER, POWER, STEPDOWN: 120 v AC, 60 cycles, single phase; 1 output winding, 2.6 v center tapped, \(10 \mathrm{amp} ; 49956\) *292-6009G2 MIL type TF1SX01YY per MIL-T-27A; 21964 dwg \#A1069868 & Rectifier heater Figure 6-66 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline REF DESIG & NOTES & NAME AND DESCRIPTION & LOCAT ING FUNCTION \\
\hline T1803 & & TRANSFORMER, POWER, STEPDOWN: 120 v AC, 60 cycles, single phase; 4 output windings, secondary \(\$ 1\) is 12.7 v at 2.3 amp , secondary \(\$ 2\) is 12.7 v at 3.5 amp , secondaries \(\# 3\) and \(\geqslant 4\) are 6.4 v at \(0.3 \mathrm{amp} ; 49956\) *292-5632G1 MIL type TF1SX01JA per MIL-T-27A; 21964 \#A1069536; Same as T1604 & Regulator \& amplifier heaters \\
\hline TB1801 & & TERMINAL BOARD: 10 terminals; double screw type; barrier type; MIL type 8TB10 per MIL-T-16784 and NAVY dwg \({ }^{\boldsymbol{*} 9000-S 6505 G-}\) 73214; 21964 A2133063-4; Same as TB701 & Terminal board Figure 2-13 \\
\hline TB1802 & & Same as TB1801 & Terminal board Figure 2-13 \\
\hline \[
\begin{gathered}
\text { TB1803 } \\
\text { thru } \\
\text { TB1897 }
\end{gathered}
\] & & Not Used & \\
\hline TB1898 & 2 & TERMINAL BOARD: 24 terminals; hollow solder stud type; 21964 *B2060870G1 & Mounts R1867, R1868 Figure 6-66 \\
\hline TB1899 & 2 & TERMINAL BOARD: 25 terminals; hollow solder stud type; 21964 *A2140479-1 & Mounts in cabinet \\
\hline V1801 & & \[
\begin{aligned}
& \text { ELECTRON TUBE: diode; MIL type 836, per spec MIL-E-1C; } \\
& 21964 * 700178
\end{aligned}
\] & \begin{tabular}{l}
Rectifier \\
Figure 6-66
\end{tabular} \\
\hline V1802 & & Same as V1801 & \begin{tabular}{l}
Rectifier \\
Figure 6-66
\end{tabular} \\
\hline V1803 & & ELECTRON TUBE: twin pentode; MIL type \(\# 829 \mathrm{~B}\), per spec MIL-E-1C; 21964 \#700176; Same as V1603 & Series regulator Figure 2-13 \\
\hline V1804 & & Same as V1803 & Series regulator Figure 2-13 \\
\hline V1805 & & Same as V1803 & Series regulator Figure 2-13 \\
\hline V1806 & & Same as V1803 & Series regulator Figure 2-13 \\
\hline V1807 & & Same as V1803 & Series regulator Figure 2-13 \\
\hline V1808 & & ELECTRON TUBE: twin triode; MIL type \(112 \mathrm{AT7WA}\), per spec MIL-E-1C; 21964 \#701165; Same as V307 & Regulator amplifier Figure 2-13 \\
\hline V1809 & & Not Used & \\
\hline V1810 & & \[
\begin{aligned}
& \text { ELECTRON TUBE: diode; MIL type \#OA2WA, per spec MIL-E-1C; } \\
& 21964701166
\end{aligned}
\] & Reference voltage Figure 2-13 \\
\hline V1811 & & Same as V1810 & Reference voltage Figure 2-13 \\
\hline V1812 & & Same as V1810 & Reference voltage Figure 2-13 \\
\hline V1813 & & Same as V1810 & Reference voltage Figure 2-13 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline V1814 & & Same as V1810 & Reference voltage Figure 2-13 \\
\hline XDS1801 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; 125 v , 6 watts; MIL type LH63BR3 per MIL-L-3661, dwg MS-90286; 21964 \#A2133080-1; Same as XDS1002 & Holds DS1801 \\
\hline XDS1802 & 6 & LAMPHOLDER: 125 v ; accommodates double contact bayonet base lamp; Military Standard lampholders dwg MS90290; 72619 9S4634-L-46; MIL spec no. MIL-L-3661; MIL type no. LH-71-XXO; 21964 \#A9152053 or A2142519; Same as XDS502 & \begin{tabular}{l}
Holds DS1802 \\
Figure 2-13
\end{tabular} \\
\hline XDS1803 & & LIGHT, INDICATOR: supplied \(w /\) lens, accommodates neon T-3-1/4 NE- 51 lamp, \(125 \mathrm{v}, 75\) watt; includes built in \(51,000 \mathrm{ohm} 1 / 3\) watt composition resistor; MIL type LH64PA5 per MIL spec MLL-L-3661 and MS90287; 21964 \#A2133081-2; Same as XDS901 & Holds DS1803 \\
\hline XF1801 & & FUSEHOLDER: extractor post type; accommodates 2 fuses \(1-1 / 4^{\prime \prime} \mathrm{lg}\) by \(1 / 4^{\prime \prime}\) dia; blown fuse indicating type; sealed; MIL type FHL10G per BuShips dwg \#9000-S6202-74228 and MIL-F-19207 (Ships); 21964 *A2060402; Same as XF501 & Holds F1801 \& F1804 Figure 6-66 \\
\hline XF1802 & & Same as XF1801 & Holds F1802 \& F1805 Figure 6-66 \\
\hline XF1803 & & Same as XF1801 & Holds F1803 \& F1806 Figure 6-66 \\
\hline XV1801 & 6 & SOCKET, ELECTRON TUBE: 4 contacts, beryllium copper, silver plated; jumbo size; round body; 74970 \#123-210-200; per 21964 \#B2141951-1 & Socket for V1801 \\
\hline XV1802 & & Same as XV1801 & Socket for V1802 \\
\hline XV1803 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, phosphor bronze and beryllium copper, silver plated; jumbo size; 74970 \#122-101-200; 21964 \#B2141950; Same as XV1603 & Socket for V1803 Figure 6-10 \\
\hline XV1804 & & Same as XV1803 & Socket for V1804 Figure 6-10 \\
\hline XV1805 & & Same as XV1803 & Socket for V1805 Figure 6-10 \\
\hline XV1806 & & Same as XV1803 & Socket for V1806 Figure 6-10 \\
\hline XV1807 & & Same as XV1803 & Socket for V1807 Figure 6-10 \\
\hline XV1808

XV1809 & & \begin{tabular}{l}
SOCKET, ELECTRON TUBE: 9 contacts, brass, nickel plated; miniature; JAN type \#TS103C01, per spec JAN-S-28A-1; 21964 \#740005 \\
Not Used
\end{tabular} & Socket for V1808 \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1765/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline XV1810 & 6 & SOCKET, ELECTRON TUBE: 7 contacts, brass, nickel plated; miniature; JAN type *TS102C01, per spec JAN-S-28A-1; 21964 *740003 & Socket for V1810 \\
\hline XV1811 & & Same as XV1810 & Socket for V1811 \\
\hline XV1812 & & Same as XV1810 & Socket for V1812 \\
\hline XV1813 & & Same as XV1810 & Socket for V1813 \\
\hline XV1814 & & Same as XV1810 & Socket for V1814 \\
\hline & & POWER SUPPLY PP-1763/URN & \\
\hline 1901-1999 & & POWER SUPPLY, PP-1763/URN: rectification data, electronic type, 8020 tube, full-wave bridge; output data, DC, \(-12250 \mathrm{v}, 90 \mathrm{ma}\), unregulated; input data, AC, \(120 \mathrm{v}, 60\) cycles 1 phase, 9440 v , 60 cycles, 3 phase; overall dim. \(26-25 / 32^{\prime \prime} \mathrm{lg}, 23-1 / 16^{\prime \prime}\) wide, 12-21/32" high; filter incl; rack mounted with pull-out slides, front access only; housed in an open aluminum framework, provides high voltage for the system; 21964 \#J2060336; u/o AN/GRN-9D & Part of Power Supply Assembly OA-1537/GRN-9A Figure 6-67 \\
\hline C1901 & & CAPACITOR, FIXED, PAPER DIELECTRIC: 1.0 uf, \(\pm 25-5 \%\); 14, 000 v DC working; similar to 56289 \#25P61; per MIL-C-25A; 21964 \#A2060579; u/o AN/GRN-9D & \begin{tabular}{l}
HV filter \\
Figure 6-68
\end{tabular} \\
\hline C1902 & & Same as C1901; u/o AN/GRN-9D & \begin{tabular}{l}
HV filter \\
Figure 6-68
\end{tabular} \\
\hline C1903 thru C1905 & & Not Used & \\
\hline C1906 & & CAPACITOR, FLXED, PAPER DIELECTRIC: 0.47 uf, \(\pm 10 \%\) tolerance, 200 v DCW; MIL type CP09A1KC474K, per MIL-C-25A; 21964 \#643510 & Filtering capacitor Figure 6-ï1 \\
\hline DS1901 & & LAMP, INCANDESCENT: 115-125 v, 10 watts, 40 lumens, double contact bayonet base; 24446 \#10C7/1DC; 21964 \#710071; Same as DS501 & \begin{tabular}{l}
HV "ON" \\
Figure 3-8
\end{tabular} \\
\hline DS1902 & & Same as DS1901 & Ready for HV Figure 3-8 \\
\hline DS1903 & & LAMP, GLOW: neon gas, 0.04 watt; 120 v ; T-3-1/4 bulb; miniature bayonet base; MIL type NE-51 per MIL-L-15098B; 21964 \#A2141970; Same as DS901 & High voltage overload Figure 3-8 \\
\hline E1901 & & CLIP, ELECTRICAL: beryllium copper; cadmium plated; 42498 \#SD-D198 part 4; 21964 \#A2141723; Same as E1801 & Plate clip for V1901 \\
\hline E1902 & & Same as E1901 & Plate clip for V1902 \\
\hline E1903 & & Same as E1901 & Plate clip for V1903 \\
\hline
\end{tabular}

TABLŁ 7-3. RADIG SET A \({ }^{\top} /\) GRN-9D, MAINTENANCE PAKTS LIST

POWER SUPPLY PP-1763/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline E1904 & & Same as E1901 & Plate clip for V1904 \\
\hline E1905 & & Same as E1901 & Plate clip for V1905 \\
\hline E1906 & & Same as E1901 & Plate clip for V1906 \\
\hline E1907 & 2 & TERMINAL, STUD: two \(1 / 4\) " \(\mathbf{- 2 0}\) studs on mtg plate; nuts \& washers not included; brass, nickel pl; 2" \(\lg , 13 / 16^{\prime \prime}\) wide; mounts by two 0.193 " dia holes on \(0.353^{\prime \prime}\) mounting center, plate voltage connections; 21964 \# A2142232 and A2142233-1 & Tie point \\
\hline E1908 & & Same as E1907 & Tie point \\
\hline E1909 & & Same as E1907 & Tie point \\
\hline E1910 & & Not Used & \\
\hline E1911 & 6 & INSULATOR, STANDOFF: ceramic; grade L-4A per JAN-I-10, brown glaze finish; cylindrical pillar; JAN type NS4AB0316 per JAN-I-8 and spec MIL-STD-242A (Ships); 21964 \# A2133083-3 (4 each used) & Standoff insulator \\
\hline E1912 & & INSULATOR, STANDOFF: "Mycalex 410", grade L-4B white glazed; square pillar; 21964 \#A2143189; Same as E1330 (10 each used) & Standoff insulator \\
\hline E1913 & 6 & INSULATOR, STANDOFF: ceramic, grade L-4A, white glazed; square pillar; JAN type \# NS4AW1408 per JAN-I-8; 21964 \#A2133220-1 (3 each used) & Standoff insulator \\
\hline E1914 & 6 & CONTACT, ELECTRICAL: u/w interlock switch; furnishes conducting surface for switch; one brass contact, silver plated, rd, approx 7/16" dia; 1-7/8" lg, 1-1/2" wide, \(11 / 16^{\prime \prime}\) thk, approx o/a dim.; \(10 \mathrm{amp}, 110\) or 220 v AC or DC; two 0.154 " dia mounting holes on \(1-1 / 4^{\prime \prime}\) mounting center, recessed \(5 / 8^{\prime \prime}\) deep to clear \#6 hex nut; 21964 \# B2141184-2, this is one half of Navy type Switch \#CG-24067A or 24446 \#M7460330-GA (See S1004); Same as E1317 & u/w interlock switch \\
\hline E1915 & & TERMINAL STUD: breakdown voltage \(14,000 \mathrm{v}\) DC; 2 solder connections; brass, hot tin tipped; moulded asbestos filled melamine body; \(3 / 8^{\prime \prime} \mathrm{lg}, 1 / 4\) " dia body; mtd by no. 4-40 thd brass insert; 81312 \#756; 21964 \# A2142287-1; u/o AN/GRN-9A & Standoff insulator \\
\hline F1901 & & FUSE, CARTRIDGE: \(3 \mathrm{amp}, 125 \mathrm{v}\); time delay, \(135 \%\) for \(0-1\) hour and \(300 \%\) for 6 sec ; enclosed type; MIL type F02D3R00B, per spec MIL-F-15160A and MIL STD MS90078-27-1; 21964 \#882237; Same as F501 & \begin{tabular}{l}
Primary T1901 \\
protection \\
Figure 3-8
\end{tabular} \\
\hline F1902 & & Same as F1901 & Spare \\
\hline K1901 & & RELAY, ARMATURE: contact arrangement 2A1B, single break, \(5 \mathrm{amp}, 120 \mathrm{v} \mathrm{AC}\); single winding, 120 v AC, 60 cycles; 6 terminals on contacts, 2 terminals on coil; continuous duty; hermetically sealed; 71482 \#SG36015 type "GAC", per spec MIL-R-5757C; 21964 \# A2 140532 ; Same as K1802 & HV overload auxiliary \\
\hline
\end{tabular}

TABLE 7-3. RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST
POWER SUPPLY PP-1763/URN
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{l}
REF \\
DESIG
\end{tabular} & NOTES & NAME AND DESCRIPTION & \begin{tabular}{l}
LOCATING \\
FUNCTION
\end{tabular} \\
\hline K1902 & & Not Used & \\
\hline K1903 & & RELAY, ARMATURE: contact arrangement 1C, single break, 2 amp , 115 v AC ; 1 inductive winding, \(\mathrm{DC}, 16,000\) ohms resistance, 12.8 v operating voltage, 0.8 ma continuous operating current; 3 terminals on contacts, 2 terminals on coil; continuous duty; hermetically sealed; per spec MIL-R-5757C; 78277 \#5RJ90764-SIL; 21964 \#A2143385; Same as K1803 & HV overload \\
\hline M1901 & & METER, TIME TOTALIZING, ELECTRIC: calibrated in hr; max reading \(9999.9 \mathrm{hr}, 0.1 \mathrm{hr}\) smallest increment, recycles, black numerals on white background, nonreset type; synchronous type, AC, \(120 \mathrm{v}, 60\) cycles; single phase; self starting; ambient temperature range of \(-54^{\circ} \mathrm{C}\) to \(+85^{\circ} \mathrm{C}\); 2 connections; per spec MIL-M-10304A; 21964 \#A2060476 & Plate total time Figure 3-8 \\
\hline M1902 & & Same as M1901 & Filament total time Figure 3-8 \\
\hline MP1901 & & BOLT, REDUCED SHANK: steel rod, type no. 303 per MIL-S-853, class 7, type C; passivate finish; head data not applicable to MBCA Ref Dwg Group 29, knurled thumb head socket recess, \(1 / 2^{\prime \prime}\) high, \(7 / 8^{\prime \prime}\) dia, o/a dim., recess dim. , \(0.3130^{\prime \prime}\) dim. across flats, \(3 / 8^{\prime \prime}\) deep; reduced shank data \(5 / 8^{\prime \prime}\) dia, \(25 / 32^{\prime \prime} \lg ; 3 / 8^{\prime \prime}-16 \mathrm{NC}-2\) thd, 3/8' min lgth; 2-5/32' nominal lgth; 21964 \#A9140059 (4 each used); Same as H903 & Used to secure unit in cabinet \\
\hline MP1902 & 1 & GASKET: synthetic rubber, MIL-R-900C, class 1; style no. 10 , MBCA Ref Dwg Group 75; 2-15/64' dia aperture in center, three \(1 / 8^{\prime \prime}\) dia holes spaced 120 deg apart on 2-7/16" dia; 2-11/16" OD, 1/16" thk; 21964 \#B2060910; Same as MP205 & Sealing for meters \\
\hline MP1903 & 1 & GASKET: synthetic rubber; MIL-R-900A, class 2; cross-sectional style no. 7, Ref Dwg Group 74; 1/8" wide, \(5 / 32^{\prime \prime}\) high w/1/16" radius, approx \(4 \mathrm{ft} 1 / 8^{\prime \prime} \mathrm{lg} ; 21964\) \#A9140800; Same as MP201 & Seals front panel to cabinet \\
\hline MP1904 & & BOOT, DUST AND MOISTURE SEAL: silicone rubber bonded to a brass, nickel plated hex nut \(15 / 32-32\) thd; \(3 / 4^{\prime \prime}\) across flats, 7/8" lg; 97539 \#1030; 21964 \#A2132649-1; Same as MP202 & Dust cover for toggle switch on front panel \\
\hline R1901 & & RESISTOR, FIXED, FILM (HIGH STABILITY): 500,000 ohms, \(\pm 5 \%\); 55 watt; \(225^{\circ} \mathrm{C}\) hot spot temperature; 14674 type RW- 37 per MIL-R-11804A; 21964 \#A2141186-4 & \begin{tabular}{l}
Bleeder \\
Figure 6-68
\end{tabular} \\
\hline R1902 & & Same as R1901 & \begin{tabular}{l}
Bleeder \\
Figure 6-11
\end{tabular} \\
\hline R1903 & & Same as R1901 & \begin{tabular}{l}
Bleeder \\
Figure 6-11
\end{tabular} \\
\hline R1904 & & Same as R1901 & \begin{tabular}{l}
Bleeder \\
Figure 6-11
\end{tabular} \\
\hline R1905 & & Not Used & \\
\hline R1906 & & RESISTOR, FIXED, FILM (HIGH STABILITY): 150 ohms, \(\pm 5 \%\); 55 watt; \(225^{\circ} \mathrm{C}\) hot spot temperature; 14674 type RW-37 per MIL-R-11804A; 21964 \#A2141186-1 & K1903 shunt \\
\hline
\end{tabular}

\section*{TABLE 7-3, RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST}

POWER SUPPLY PP-1763/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { REF } \\
& \text { DESIG }
\end{aligned}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline \[
\begin{aligned}
& \text { R1907 } \\
& \text { R1908 } \\
& \text { thru } \\
& \text { R1911 }
\end{aligned}
\] & & \begin{tabular}{l}
RESISTOR, FIXED, FILM (HIGH STABILITY): 1000 ohms, \(\pm 5 \%\); \\
55 watt; \(225^{\circ} \mathrm{C}\) hot spot temperature; 14674 type RW-37; 21964 \# A2141186-2; Same as R1314 \\
Not Used
\end{tabular} & HV discharge \\
\hline R1912 & & RESISTOR, VARIABLE: composition element; 1 section, \(25,000 \mathrm{ohms}\), \(\pm 10 \%\); 2 watt; MIL type RV4LAVSA253A per MIL-R-94 and MIL-STD242(Ships); 21964 \# A2133049-1; Same as R1470 & Overload relay trip adj Figure 6-68 \\
\hline R1913 & & RESISTOR, FIXED, WIREWOUND: \(280 \mathrm{ohms}, 3\) watt; \(350^{\circ} \mathrm{C}\) maximum continuous operating temperature; MIL type RW59V281 per MIL-R26C; 21964 \# A2132711-01; Same as R520 & Voltage dropping resistor \\
\hline \[
\begin{aligned}
& \text { R1914 } \\
& \text { thru } \\
& \text { R1916 }
\end{aligned}
\] & & Not Used & \\
\hline R1917 & & Same as R1913 & Limiting resistor for DS1902 \\
\hline R1918 & & RESISTOR, DISC: thyrite compound; non-linear; 3 watts maximum continuous power rating at 55 deg C ; DC test conditions, 25 v \(\pm 21 \%\) at 1 amp ; exponent \(\mathrm{a}=0.63 \pm 8 \%\); change in resistance at constant voltage is from \(-0.4 \%\) to \(-0.73 \%\) per deg C , over the temperature range 0 deg C to \(100 \mathrm{deg} \mathrm{C} ; 24446\) \# 3993060 G 1 ; 21964 \#A2130066; u/o AN/GRN-9D & Meter protection M1301 \\
\hline S1901 & & SWITCH, SHORTING: high voltage discharge, DC; SPST, normally closed, double break; 21964 \#C2140529 and \#A2140528-1 & HV condenser shorting switch \\
\hline S1902 & & SWITCH, TOGGLE: single-pole, single throw; \(0.75 \mathrm{amp}, 125 \mathrm{v}\) DC, \(15 \mathrm{amp}, 125 \mathrm{v}\) AC, resistive load rating; JAN type ST42A per spec JAN-S-23; 21964 \#828212; Same as S502 & \begin{tabular}{l}
HV "ON-OFF" \\
Figure 3-8
\end{tabular} \\
\hline T1901 & & TRANSFORMER, POWER, STEPDOWN: encapsulated, epoxy resin; primary \(120 \mathrm{v}, 60\) cycles, single phase; 4 output winding, secondary no. \(1,5.1 \mathrm{v} 18 \mathrm{amp}\), secondary no. 2,3 and \(4,5.1 \mathrm{v} 6 \mathrm{amp}\); insulation to withstand 600 v rms test on primary and \(18,000 \mathrm{v}\) rms test on secondaries; 49956 \# 292-3674G1; MIL type TF2TX01ZZ per MIL-T-27A; 21964 \#A1069473 & HV rectifier filament Figure 6-67 \\
\hline TB1901 & & TERMINAL BOARD: 10 terminals; double screw type; barrier type; 20 studs; voltage rating 300 v AC; MIL type 8 TB 10 per MIL-T16784 and Navy dwg \#9000-S6505G-73214; 21964 \#A2133063-4; Same as TB701 & Terminal board \\
\hline TB1902 & & Same as TB1901 & Terminal board \\
\hline
\end{tabular}

TABLE 7-3, RADIO SET AN/GRN-9D, MAINTENANCE PARTS LIST

POWER SUPPLY PP-1763/URN
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{gathered}
\text { REF } \\
\text { DESIG }
\end{gathered}
\] & NOTES & NAME AND DESCRIPTION & LOCATING FUNCTION \\
\hline V1901 & & ELECTRON TUBE: diode; glass envelope; RMA envelope T-18; 5 terminations, 4 pin type and 1 cap type, located on bottom and top respectively; high vacuum, half-wave rectifier; MIL type 8020, per spec MIL-E-1C; 21964 \#700203 & \begin{tabular}{l}
Rectifier \\
Figure 6-68
\end{tabular} \\
\hline V1902 & & Same as V1901 & \begin{tabular}{l}
Rectifier \\
Figure 6-68
\end{tabular} \\
\hline V1903 & & Same as V1901 & \begin{tabular}{l}
Rectifier \\
Figure 6-68
\end{tabular} \\
\hline V1904 & & Same as V1901 & \begin{tabular}{l}
Rectifier \\
Figure 6-11
\end{tabular} \\
\hline V1905 & & Same as V1901 & \begin{tabular}{l}
Rectifier \\
Figure 6-11
\end{tabular} \\
\hline V1906 & & Same as V1901 & \begin{tabular}{l}
Rectifier \\
Figure 6-11
\end{tabular} \\
\hline XDS1901 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; \(125 \mathrm{v}, 6\) watts, MIL type LH63BR3 per MIL-L-3661, dwg MS-90286; 21964 \# A2133080-1; Same as XDS1 002 & Holder for DS1901 Figure 6-68 \\
\hline XDS1902 & & LIGHT, INDICATOR: friction mtg lens holder; accommodates style S-6 lamp; \(125 \mathrm{v}, 6\) watts; MIL type LH63BB3 per MIL-L-3661, dwg MS-90286; 21964 \#A2133080-4; Same as XDS1102 & Holder for DS1902 Figure 6-68 \\
\hline XDS1903 & & LIGHT, INDICATOR: supplied w/lens, \(5 / 8^{\prime \prime}\) dia, amber, plain design, stovepipe shape, fluted, screw type holder, accommodates neon T-3-1/4 NE-51 lamp; 125 v , 75 watt; MIL type LH64PAS per MIL spec MIL-L-3661 and MS-90287; 21964 \# A2133081-2; Same as XDS901 & \begin{tabular}{l}
Holder for DS1903 \\
Figure 6-68
\end{tabular} \\
\hline XF1901 & & FUSEHOLDER: extractor post type, accommodates 2 fuses; MIL type FHL10G per BuShips Dwg \#9000-S-6202-74228 and MIL-F-19207 (Ships); 21964 \# A2060402; Same as XF501 & \begin{tabular}{l}
Holds F1901 \& F1902 \\
Figure 6-68
\end{tabular} \\
\hline XV1901 & 6 & SOCKET, ELECTRON TUBE: 4 contacts, beryllium copper, silver plated, jumbo size; 74970 \#123-210-200 per 21964 \# B2141951 modified and 21964 \#B2143570-1 & Socket for V1901 \\
\hline XV1902 & & Same as XV1901 & Socket for V1902 \\
\hline XV1903 & & Same as XV1901 & Socket for V1903 \\
\hline XV1904 & & Same as XV1901 & Socket for V1904 \\
\hline XV1905 & & Same as XV1901 & Socket for V1905 \\
\hline XV1906 & & Same as XV1901 & Socket for V1906 \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|}
\hline NAME & \[
\begin{gathered}
\text { MFG } \\
\text { CODE }
\end{gathered}
\] & ADDRESS \\
\hline Aerovox Corp. & 00656 & New Bedford, Mass. \\
\hline Air-Maze Corp. & 00736 & 5200 Havard Ave., Cleveland, Ohio \\
\hline Aircraft Radio Corp. & 00781 & Boonton, N.J. \\
\hline Sangamo Electric Co. & 00853 & Marion, Ill, \\
\hline Alden Products Co. & 01009 & 117 North Main St., Brockton 64, Mass. \\
\hline Pulse Engineering Co. & 01961 & 2431 Spring St., Redwood City, Calif. \\
\hline Prode Lin & 02114 & 307 Bergen Ave., Kearny, N.J. \\
\hline Wheelock Signal, Inc. & 02116 & 273 Branchport Ave., Long Branch, N.J. \\
\hline American Phenolic, Corp. & 02660 & 1830 South 54th Ave., Chicago 50, Ill. \\
\hline Dynamic Gear Co. & 03151 & Amityville, L.I., N.Y. \\
\hline Arrow-Hart and Hegeman Elec. Co. & 04009 & 100 Hawthorne St., Hartford 6, Conn. \\
\hline Birtcher Corp. & 07387 & North Los Angeles, Calif. \\
\hline Continental Rubber Co. & 14370 & Erie, Pa. \\
\hline Corning Glass Works & 14674 & 1943 Crystal St., Corning, N.Y. \\
\hline Cramer, R.W., Inc. & 14907 & Miller St., Centerbrook, Conn. \\
\hline Cutler Hammer, Inc. & 15605 & Milwaukee, Wis. \\
\hline I.T.T. Federal Div. & 21964 & 100 Kingsland Road, Clifton, N.J. \\
\hline General Electric Co. & 24446 & 1 River Road, Schenectady 5, N.Y. \\
\hline General Radio Co. & 24655 & Cambridge, Mass. \\
\hline Marlin-Rockwell Corp. & 38443 & 402 Chandler St., Jamestown, N.Y. \\
\hline Miniature Precision Bearing Co. & 40920 & 101 Carpenter St., Keene, N.H. \\
\hline National Co. & 42498 & 61 Sherman St., Malden 48, Mass. \\
\hline Raytheon Mig. Co. & 49956 & Waltham, Mass. \\
\hline Reeves Instrument Corp. & 50222 & 215 East 91st St., New York, N.Y. \\
\hline Sperry Gyroscope Co., Div. of the Sperry Corp. & 56232 & Great Neck, L.I., N.Y. \\
\hline Sponge Rubber Products Co. & 56277 & Shelton, Conn. \\
\hline Sprague Electric Co. & 56289 & 201 Beaver St., North Adams, Mass. \\
\hline Steward-Warner Corp. & 57733 & Chicago, Ill. \\
\hline Williams, J.H. and Co. & 65814 & Buffalo, N.Y. \\
\hline Admiral Corp. & 70117 & 3800 West Cortland St., Chicago, III. \\
\hline Allen Mig. Co. & 70276 & 100 Sheldon St., Hartford, Conn. \\
\hline Allied Control Co. & 70309 & 2 East End Ave., New York 21, N.Y. \\
\hline C.P. Clare Co. & 71482 & 3101 Pratt Blvd., Chicago 45, Ill. \\
\hline Centralab, Div. of Globe Union Inc. & 71590 & 900 East Keefe Ave., Milwaukee 1, Wisc. \\
\hline
\end{tabular}

\section*{TABLE 7-4, RADIO SET AN/URN-9D, LIST OF MANUFACTURERS (cont)}
\begin{tabular}{|c|c|c|}
\hline NAME & \[
\begin{gathered}
\mathrm{MFG} \\
\mathrm{CODE}
\end{gathered}
\] & ADDRESS \\
\hline Cinch Mfg. Corp. & 71785 & 1026 South Homan Ave., Chicago 24, Ill. \\
\hline Dialight Corp. & 72619 & 60 Steward Ave., Brooklyn 37, N.Y. \\
\hline Erie Resistor Corp. & 72982 & 640 West 112th St., Erie, Pa. \\
\hline Industrial Products Co, & 74868 & Danbury, Conn. \\
\hline E.F. Johnson Co. & 74970 & Waseca, Minn. \\
\hline Millen, James Mfg. Co., Inc. & 76487 & 150 Exchange St., Malden, Mass. \\
\hline Oak Mfg. Co. & 76854 & 1260 Clybourn Ave., Chicago 10, Ill. \\
\hline Sigma Instruments, Inc. & 78277 & 180 Pearl St., South Braintree 85, Mass. \\
\hline White, SS Dental Mfg. Co. & 79555 & Philadelphia, Pa. \\
\hline Winchester Electronics Inc. & 81312 & Norwalk, Conn. \\
\hline Filtron Co., Inc. & 81831 & 131-05 Fowler Ave., Flushing, L.I., N.Y. \\
\hline Barry Corp, The & 81860 & 700 Pleasant St., Watertown 72, Mass. \\
\hline Electro Switch Corp. & 82121 & South Weymouth, Mass. \\
\hline Jeffers Electronics, Division of Speer Carbon Co. & 82142 & Dubois, Pa. \\
\hline Kewanee Private Utilities Co. & 82181 & Kewanee, Ill. \\
\hline Rotron Mfg. Co. Inc. & 82877 & 7-9 Schoonmaker Place, Woodstock, N.Y. \\
\hline Flexible Tubing Corp. & 83144 & Guilford, Conn. \\
\hline Hunt Corporation & 84678 & Carlisle, Pa. \\
\hline General Products Corp. & 88223 & Union Springs, N.Y. \\
\hline Holtzer Cabot, Division of National Pneumatic Co., Inc. & 89482 & Woodside, Long Island, N.Y. \\
\hline Micro Switch Div. of Minneapolis-Honeywell Reg. Co. & 91929 & Freeport, ill. \\
\hline Torrington Co., Specialties Div. & 92172 & 37 Field St., Torrington, Conn. \\
\hline Vier Mfg. Co. & 92214 & Los Angeles 4, Calif. \\
\hline Frequency Standards Corp. & 93341 & Ashbury Park, N.J. \\
\hline Dietz, H.G. Co. & 93652 & 45 Dobbia St., Brooklyn, N.Y. \\
\hline Atlas Electronics Corp. & 95114 & Park Square Bldg., Boston, Mass. \\
\hline Philamon Labs., Inc. & 95267 & 90 Hopper St., Westbury, L.I., N.Y. \\
\hline Revcor & 95933 & Chicago, Ill. \\
\hline Ippolito, James, Co., Inc. & 96458 & New York, N.Y. \\
\hline Juniper Elbow Co., Inc. & 97537 & Middle Village, N.Y. \\
\hline Automatic Precision Mfg. Co. & 97539 & Yonkers, N.Y. \\
\hline Marman, Div. of Aeroquip Corp. & 98625 & Los Angeles, Calif. \\
\hline Flexible Tubing Corp. & 98683 & Amesburg, Mass. \\
\hline International Electronic Research Corp. & 98978 & Burbank, Calif. \\
\hline
\end{tabular}

\section*{SECTION 8}

Chapter 1
MODIFICATIONS, ELECTRICAL DESCRIPTION

\section*{CONTROL DUPLEXER (Mod strike-off number 3)}
1. A switch, S1109, has been fitted to all drawers by Modification A4295. This is wired across tags 9 and 10 of TB1103. Diagrams affected are Figures 6-16a, 6-27a, 6-29a and 6-60. These points are the external H.V. Interlock pair to the TMC equipment, and S1109 permits them to be bridged where TMC equipment is not in use at the beacon site. In Figure 1 the Switch can be seen above and to the left of the centre of the front panel.


Fig. 1 Control-Duplexer C-2226A/GRN-9

LOW VOLTAGE POWER SUPPLY (Mod strike off number 3.)
2. A Switch, S1602 is wired in series with the blue wire connecting between Thermal Delay Switch K1607 and TB1602 tag 10, by modification No. A4299. Diagrams affected are Figures 6-45a and 6-62. The opening of S1602 avoids K1607 becoming permanently closed in non-TMC beacon installations. In Figure 2 the Switch can be seen mounted below the socket in the centre of the front panel.


Fig.2. Low-Voltage
Power Supply PP-1766/URN

AMPLIFIER MODULATOR (Mod strike-off number 3)
3. A radio frequency socket and lead is fitted to the front panel by modification No. A3825. Diagrams affected are Figures 6-20 and 6 - 57. The modification permits R.F. to be directed from the drawer at socket E1324 and taken to an external Filter Cavity unit. This makes the drawer compatible for use with URN 3A beacon installations. The new socket is to the right of the right-hand meter (Fig.3) and to the left of the pilot lamp. The connecting lead is stored in an internal clip when not in use.


Fig. 3. Amplifier Modulator AM-1701/URN
HIGH VOLTAGE POWER SUPPLY (Mod strike-off number 3)
4. A socket, J1901, and associated internal circuitry has been added by modification No. A3375 for the purpose of
a) limiting the working peak voltage across A1912 to 250 volts.
b) providing an oscilloscope monitoring point for viewing the Klystron current pulse.
Diagrams affected are Figures 6-26 and 6-47, part of which are shown below after modification (Figs. 4 and 5). J1901 is mounted below the two left-hand fuses (Figure 6).
When installed, the peak voltage shown on an oscilloscope connected to J1901 should fairly equate to the peak current in amperes drawn by the Klystron. Typical values are 2.8 Amps (High Band) to 3.1 Amps (Low Band), at best output.


Fig.4.Part of figure 6-26
CONTROL-DUPLEXER (Mod strike-off number 4)

\section*{Technical Description}
5. A new Filter cavity unit has been fitted by modification Nos. A4837 and A4838. The modification scarcely affects the electrical circuit diagrams, and does not alter the performance per se. Mechanical changes to the Control-Duplexer drawer involve the fitting of modified brackets, and the internal appearance is altered, (see Figures 1 and 7), in that the new filter cavity is a single cylindrical drum, rather than two, as were originally fitted.
6. In the new cavity, injection and take-off probes are mounted exactly as right-angles, i.e., the take off probe is one quarter of the way around the periphery relative to the injection probe. The plane of the injected waves is such that no output would be obtained from the take-off if the interior of the cavity were smooth. Half-way between the probes is a "coupling probe". This is in \(45^{\circ}\) relationship with both injection and output, and is capable, therefore, of creating an interference wave, permitting coupling to occur which is proportional to depth.
7. Since a perfectly cylindrical drum is resonant at the same frequency across any diameter, the one cavity behaves like an accurately tuned twin circuit. To correct for manufacturing imperfections, a preset adjustment is provided exactly opposite each probe to ensure that both input and output resonances track accurately at a similar frequency, when the main turning knob is turned. The preset tracking adjustment holds good over a number of channels, and the response curve is similar to the bandpass response previously obtained with the original twin-cavity unit. Setting up, therefore, is simplified, since the two resonances cannot be misset far from each other. Otherwise the procedure to be followed is that given in 2.51 (2) step 26.

CAUTION ......
On no account must the coupling probe cover be removed or coupling adjustment attempted except by 3 rd line personnel with 3rd line measuring equipment.

The coupling probe cover is also the gas seal for this adjustment, removing this cover will allow de-pressurizing to occur.


Fig 5 Part of figure 6-47


Fig.6. High Voltage Power Supp1y PP-1763/URN


Fig.7. Control Duplexer, overhead view

\section*{MAINTENANCE AND RE-PRESSURIZING}
8. The transmission filter cavity is pressurized with dry Freon 12 gas. The pressure reading on the cavity gauge is a function of both ambient temperature and barometric pressure, and may vary from 1 to 8 psi over extreme operating conditions. Under normal environmental conditions with the equipment in standby, the nominal pressure gauge reading is 3 psi . Over a certain period of operation, the cavity may lose gas, and normal servicing should be limited to adding Freon 12 when the pressure drops below one pound per square inch. This leaflet described two procedures (1) for use when scavenging is not required, (i.e., the cavity has not been opened, and a small residual pressure still exists) and (2) when scavenging is required (i.e., where the cavity has been opened, or where pressure is zero.) In the latter case two procedures are described for situations where (A), a vacuum pump is available and (B) not available.

Procedure where a small residual pressure exists
9. (1) Remove the valve cap located on the front of the cavity.
(2) Connect a tank of commercial grade dry Freon to the valve.
(3) Open the valve on the tank of Freon and admit gas until the filter cavity pressure gauge reads 3 psi.
(4) Close the valve on the tank.
(5) Disconnect the tank from the valve on the cavity.
(6) Replace the valve cap on the cavity.
(7) Tune the transmission line filter cavity.

\section*{Procedure A where no discernible pressure exists}
10. (1) Remove the valve cap located on the front of the cavity.
(2) Connect a pneumatic Tee connector with a tap in each of the input legs and fitted with a deflator, in the valve leg.
(3) Connect a vacuum pump to one leg and a tank of dry commercial grade Freon to the other. Close both taps.
(4) Open the tap to the vacuum pump and evacuate the cavity to a vacuum of at least 29 inches of mercury. Hold this vacuum for at least 20 minutes. Close the tap to the vacuum pump.
(5) Open the tap to the tank of Freon gas and admit gas until the pressure gauge reads 3 to 5 psi. Disconnect the Tee piece.
(6) Using a halogen gas leak locator (for example CT 105) check around all 0-ring seals, joints, and the valve stem. Vary all tuning controls while checking for leaks. Any leak greater than \(1 / 10\) oz per year ( \(8.0 \mathrm{mg} /\) day approx) shall cause the assembly to be rejected.
(7) If no leaks are detected, replace the valve cap and recheck for a pressure of 3-5 psi.

\section*{CAUTION ...}

Gas leak locators such as CT105 are very sensitive to the presence of small amounts of contaminating gas or smoke in the air and should be operated only under clean-air conditions i.e., after the test bay itself has been purged of Freon gas which may have been released during the pressurization process. Avoid the use of aerosols, paints and varnishes, methylated spirits, and do not smoke in the test area.
Smoke can cause actual permanent damage to the sensitive element in the gas leak locator, and will certainly cause a high "zero" setting. resulting in loss of sensitivity.

\section*{Procedure B where no discernible pressure exists}
11. (1) Carry out procedure paragraph 2 (1), (2) and (3) but raise pressure to 10 psi .
(2) Repeat steps (4) and (5) of paragraph 2.
(3) Depress the valve needle on the filter cavity and allow gas to escape until the gauge reads zero.
(4) Repeat steps (1), (2), and (3) of this paragraph at least 10 times.
(5) Repeat pressurization steps (2) and (5) inclusive, of paragraph 2.
(6) Search for gas leaks as in paragraph 3 (6) observing the CAUTION.
(7) If no leaks are detected, replace the valve cap and recheck pressure.

Pressure cannot be maintained
12. If pressure is not being maintained, the unit should be returned for third-1ine maintenance in accordance with current instructions from the relevant authority.

FREQUENCY MULTIPLIER OSCILLATOR (Mod strike-off 3)
13. A resistor of 2.7 K has been introduced in series with the drive and of R1470. (Shaped Pulse Amplitude Control) by modification No. A4620. The resistor, R1475, provides pulse current limiting in the event of R1470 and R1471 both being inadvertently adjusted to minimum resistance at the same time. Diagrams affected are Figures \(4-35,6-18,6-36\). The resistor is mounted just to the right of R1470, to which it is connected at one end, and to a new mounting tag fitted for the purpose of supporting the opposite end of R1475.

CODER-INDICATOR (Mod strike-off number 4)
14. The mechanical keyer unit is being superseded by an Electronic keyer unit by modification No.A6364. Many diagrams and a great deal of text is affected by this change, but only insofar as the following points apply generally:-


Fig. 8. Keyer unit - panel controls
(1) The word "mechanical" becomes redundant.
(2) References to "mechanical keyer motor" and "motor switch" should be ignored.
(3) References to "motor lubrication" should be ignored.
(4) TB50, mounted on the side of the electronic keyer replaces and has a similar function to TB601 which is removed. The four original wires to it are used with TB50, plus a further eight.
(5) A new switch, S608, is fitted to the front panel. This is a test switch to call up an additional code message signifying that a fault condition exists, or the TACAN beacon is undergoing maintenance. This is a warning to pilots and navigators that the beacon is unreliable.
(6) The "ERROR" code of the previous paragraph can also be accessed remotely after extra wiring and equipment is laid in. (See Figure 12 for wiring changes, and chapter 2 for a technical description of the electronic keyer.)
15. The length of one dot on the electronic keyer is \(1 / 256\) th of the message repetition tine. In general the message will in future be repeated every 30 seconds instead of every \(37 \frac{1}{2}\) seconds. Whereever \(37 \frac{1}{2}\) seconds is mentioned in the text, therefore, read 30 seconds. The length of one dot is reduced from 125 milliseconds to 117 milliseconds. The keying speed is adjustable from approximately 100 to 130 milliseconds dot length by means of a preset control not accessible without taking the unit out of its box.
16. The additional facilities afforded by the electronic keyer include a gate waveform known as VOR GATE. This is for use in ground beacon stations where VOR and TACAN are co-sited or coaxially sited (VORTAC). The waveform supppresses the VOR identification whenever the TACAN sends its identification code, so that they do not both transmit ident together.

\section*{TRANSMITTER-RECEIVER CABINET CY-3163 (Mod strike-off number 4)}
17. Additional frame wiring is fitted to enable all the facilities afforded by an electronic identification tone keyer unit to be used. (Modification No. A6368). The modification is mandatory with VORTAC installations. Figure 12 shows the combined effect of modification A6368 and A6364 described in paragraphs 14, 15 and 16.
18. The four external connections continue on via beacon station permanent wiring to a VORTAC INTERFACE unit. Other changes are required in the TMC equipment, so that the TMC Monitors, MM-209 can signal back to the electronic keyer directly and call up the ERROR code whenever the TACAN is unmonitored. These special installations are dealt with in AP 116C-0709-1 and 10, and in the TMC series of handbooks, AP 116C-0702-1A6A etcetera.


NOTE: V.O.R. changeover relay contacts are operated by the \(64 / 192\) bit suppression wave (1:3 ratio)

Fig.9. Setting up the code

\section*{SETTING UP IDENTIFICATION CODE}
19. Instructions for setting up identification code on the Electronic Keyer are given on its facia plate and in figure 9. In principle, the operation is not different from that described for the superseded mechanical keyer in paragraph \(2-5 \mathrm{~J}\) (3) step 5 onwards in the main publication. It is advisable to precede the code by at least three spaces (step 5); ten are shown in figure 9 with twelve subsequently before the start of the ERROR code because the code shown is a short one.

Step 6. Set up first character of code by pressing the " 1 " button once for each dot, followed by a space, inserted by pressing the " 0 " button once; or pressing the " 1 " button three times, followed by a space, for a dash.

Step 7. After a whole character has been inserted, the space separating it from the next character should be three presses on the " 0 " button.

Step 8. After the last character has been inserted, continue pressing the " 0 " button until the red lamp on the keyer unit lights. Then place S 608 on the front panel of the coder-indicator unit to ON .

Step 9. The ERROR code may now be inserted in the same way as in steps 6 and 7. At the end of the 16 bit ERROR code the red light will go out. (Alternatively the existing error code may be left intact.)

Step 10. Check keying by placing the READ/WRITE switch on the keyer unit to READ, S608 to ON.

Step 11. Place S 608 to OFF and return coder indicator drawer to its normal position. With S608 at OFF, only the ident code without the error code is transmitted. (However, see also Technical Description of Keyer Unit, Chapter 2.)


Fig.10. Coder-indicator KY-382/GRN-9D (Right side)


Fig. 11 Coder Indicator, Front View


Fig. 12 Coder Indicator, Keyer Connections

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CODER INDICATOR (Mod strike-off number 2)
20. Modification \(A 3831\) permits the coder indicator to be used in URN-3A beacon installations. The modification provides a method of mechanically locking switch \(S 601\) in the \(O N\) position and changes to wiring between connectors J605, J608 and TB604, see Fig. 13. Diagrams affected are Figures 6-23 and 6-41.


Fig. 13 Coder Indicator Wiring Change

HV POWER SUPPLY (Mod strike-off number 5)
21. Modification \(A 6726\) substitutes four resistors in series-parallel connection for the single resistor R1919 introduced by modification A3375, see paragraph 4. Figures 4 and 5 show the four resistors R1919a - R1919d.

FREQ. MULT. OSC. - OSC. SUB. ASSY. HB/LB (Mod strike-off number 3)
22. Modification A7031 substitutes valve types Y561 and Y616 for valve type 2C39A. V1504 and V1510 become type Y561; V1505 V1511 and V1512 become type Y616. The modification affects Table 1-4 and figure 6-19.

AMPLIFIER MODULATOR (Mod strike-off number 4)
23. Modification \(B 0790\) introduces a resistor (R1390) in parallel with the klystron filament to provide additional loading for the filament transformer and so reduce the filament voltage.
24. The resistor is selected from Rl390 Resistor Set for the Amplifier Modulator, see Table \(7-3\). Resistor selection is required at initial installation of the equipment and when a new klystron is fitted. Figures \(2-7,4-37,5-20,6-20\) and \(6-39\) show the details. The procedure for selecting the appropriate resistor is given in paragraph 2-5c.

\section*{SECTION 8}

\author{
Chapter 2 \\ ELECTRONIC KEYER UNIT (INTRODUCED BY MOD A6364)
}

\section*{INTRODUCTION}

\section*{Description}
1. The unit is an all electronic replacement for the mechanical coder units fitted in GRN-9D and URN-3A ground TACAN beacon transmitters.
2. It consists of a 64 bit integrated circuit read/write memory and means for programming it with the required message, and reading out that message without destroying it, repetitively.
3. The unit operates on \(120 / 240\) volts \(50 / 60 / \mathrm{Hz}\) mains and the memory is rendered non-volatile by the incorporation of a nickel/cadmium battery pack to maintain the memory during periods when power is disconnected. The estimated discharge time of the battery is 3 months approximately, and it is maintained on trickle-charge during normal operation.
4. The unit is built into a die-cast case, \(185 \times 120 \times 56 \mathrm{~mm}\), and is mounted vertically. Vertical mounting ensures that the mercury wetted contacts of the keying relays do not become excessively wetted by free mercury within the sealed capsules.


Fig. 1. Electronic Keyer Unit
5. ICll is a 64 bit read/write memory addressed by means of a 256 bit counter, ICl2. Associated gates and the coding bistable, used to operate the keying relay via TR34, are contained in IC13 and IC14. IClO is the clock.

\section*{Reading}
6. The feedback path enabling IC10 to oscillate continuously at approximately 8.5 Hz , is from Q output pin 2 (Test Point 10) via the integrator Rll ( 100 k ) C12 ( \(0.22 \mu \mathrm{f}\) ), one pair of contacts of the CODE switch S3l back to the S connection of IC10, pin 6 . The time constant is Cll ( \(0.22 \mu \mathrm{f})\), R10 (390K), RV10 (10K) and R13 (22K). The RV10 is the code speed control.
7. Each pulse from IClO clocks the address counter ICl2 on its clock input, pin 9. Six of the outputs of ICl2 address the memory unit, which is therefore taken through all of its 64 bits in \(7 \frac{1}{2}\) seconds approximately.
8. Pulses also leave ICl0 pin 13 (STROBE,TPll) to pin 5 of ICll (see Fig 2E). These interrogate the memory. If a "l" is stored at the selected address, a " 1 " pulse of \(50 \mu \mathrm{~s}\) duration emerges from pin 10 (Fig 2F) and trips the code bistable, two NOR sections of IC14. A "1" transition leaves IC14 pin 10 (Fig 2G) and passes via R45 ( 22 K ) to drive TR34 into conduction, closing RLB and lighting the lamp D38 (yellow) to indicate that a "mark" is being sent.
9. The next pulse from IC10 (a) changes the address by one digit (Fig 2 B and C), and also resets the code bistable (ICl4 pin 6). The pulse which emerges from ICll pin 10 to unset the code bistable should a " 1 " be stored at this address also, occurs on the trailing edge of the STROBE pulse, (compare waveforms Fig 2 E and F ). Should a " 0 " be stored at the address, no pulse leaves IC11, the coding bistable remains set, and TR34 remains cut-off, extinguishing the yellow lamp D38.
10. During periods when a space (" 0 ") is being sent, the potential on TR34 is high. This potential, connected via R4l ( 22 K ) to TR33, enables it, and since TR 35 can be assumed to be conductive at this time, D 40 (Green) lamp will light to indicate that a space is being sent. Thus D38 and D40 operate on an exclusive \(O R\) basis - i.e., they cannot be alight together.
11. The description in (5) to (10) assumes that the ERROR switch, S30, is in the TEST position or S 608 selecting the Unreliability Code. In the TEST position, pin 13 of IC13 is earthed. This pin is one input of a three input NAND, whose output, pin 10 , is connected to pin 6 of IC11. Pin 6 of ICll is an enable pin and with a "l" present, the memory is fully accessible.
12. With the ERROR switch at REMOTE, S608 at normal (and assuming that the remote circuit has not also earthed the connection due to a fault in the TACAN beacon equipment), pin 13 of IC13 is permanently enabled from the +14 V supply rail via R22 (100K). The other two inputs cycle according to waveform \(F\) (figure 3), whence it will be seen that 16 bits of the memory become suppressed, (but not erased). These bits contain an error code to be sent after the call-sign in the event of the TACAN station being temporarily unmonitored over the full range of TACAN parameters.
10. During periods when a space (" 0 ") is being sent, the potential on TR34 is high. This potential, connected via R41 (22K) to TR33, enables it, and since TR35 can be assumed to be conductive at this time, D40 (Green) lamp will light to indicate that a space is being sent. Thus D38 and D40 operate on an exclusive OR basis - i.e., they cannot alight together.
11. The description in (5) to (10) assumes that the ERROR switch, S30, is in the TEST position or S 608 is selecting "Unreliability Code". In the TEST position, pin 13 of ICl3 is grounded. This pin is one input of a three input NAND, whose output, pin 10, is connected to pin 6 of IC11. Pin 6 of IC11 is an enable pin and with a " 1 " present, the memory is fully accessible.
12. With the ERROR switch at REMOTE, S608 at normal (and assuming that the remote circuit has not also earthed the connection) pin 13 of IC13 is permanently enabled from the +14 V supply rail via R22 (100K). The other two inputs cycle according to waveform \(F\) (figure 3), whence it will be seen that 16 bits of the memory become suppressed, (but not erased). These bits contain an error code to be sent after the call-sign in the event of the TACAN station being temporarily unmonitored over the full range of TACAN parameters.
13. In a similar manner, with S30 at TEST (or when signalled whilst at REMOTE), pin 1 of IC13, (one input of a three input NAND), is permanently enabled by IC13 pin 10. Hence the other two pins, 8 and 2, cycle, yielding waveform J (Fig 3) at the output pin 9. This is inverted and causes TR31 to conduct for the 16 bits ERROR period, lighting the ERROR 1amp D35 (Fig 3K).
14. With S30 at REMOTE, and normal operation, IC13 delivers an inverted edition of waveforms 3 and 4 (waveform F, fig 3) to IC13 pin 1 at the same time as pins 8 and 2 of IC13 are receiving the normal waveforms 3 and 4. The net result is that IC13 remains inhibited, and the " 1 " output, inverted to become " 0 ", cuts of TR31, inhibiting the ERROR 1 amp (Fig 3 H ).
15. Waveform L (Fig 3) is derived from the 128 and 256 outputs of IC12 combined, and goes to three places:
(a) to pin 8 of IC11, where it inhibits the code for 192 bits out of every 256 bits, yielding a code repetition of once every 30 seconds approximately, and (b) to TR 35 via R42 (22K), and (c) TR32 via R39 (22K).
16. TR35 is an overriding enable/inhibit preventing the " 0 " (green) lamp remaining alight during the 192 bit period when no code is being sent. TR32 operates RLA, and this also is inhibited except when code is being sent. RLA is the V.O.R. GATE RELAY, and, hence, waveform \(L\) is known as V.O.R. GATE waveform.

\section*{Reset}
17. Reset is accomplished by the RESET button (S32) which puts +14 V on the reset pins of IC1O, returning the address to count 1 . The operation is independent of all other operations, and does not erase the memory.

\section*{Enter}
18. Placing the code switch to ENTER:-
a) Breaks the feedback path of IC1O so that it no longer oscillates.
b) connects IC10 "S" input to the " 1 " and " 0 " buttons.
c) connects the second \(Q\) output of IC1O (pin 12) to the READ/WRITE connection of IC11, pin 9.
19. After pressing RESET, if S33 is now depressed once, C38, previously charged to +14 volts via R32 (470K) is made to discharge via D36 and R33 (22K). The short voltage pulse passed C33 (330pf) and travels via two contacts of S31 to IC10 pin 6. The output of IC10 at pin 2 (Test Point 1) clocks IC12 by one digi.t. The output at pin 12 of IC10 passes via the second pair of contacts of S 31 to reach pin 9 of IC-1, allowing new data to be entered at the end of the \(50 \mu\) s period. An enable leaves pin 13 of IClO and reaches pin 5 of IC11, while the same waveform resets the coding bistable, (pin 6 of IC14).
20. The initiating pulse from C38 also passes via the delaying circuit R34 (4.7K) C31 (2200pf) to pin 13 of ICl1, (waveform A, fig 2) reaching it slightly after the previous operations. This allows a " 1 " to be injected into memory, and this is also read out from pin 10 of ICll (waveform F, Fig 2) to set the coding bistable to the " 1 " state, causing the yellow " 1 " lamp to light.
21. Pressing the " 0 " button similarly causes C38 to discharge but now the pulse passes only via C33 to perform the operations described in (19). The path to R34 is inhibited by the diode D36, which is reverse biased by the pulse. Hence no potential is injected into the memory data input, and IC11 stores a " 0 " at that address.

Note ...
The sequencing operations performed by the unit are the same for entering the code as for reading it out, i.e., with S30 at REMOTE, bits No. 48 to 64 are inaccessible, and code can be written in only during the first 48 bits of every 256 bits.

\section*{Setting up the code}
22. Instructions for setting up the code are given in paragraph 19 of Chapter 1 of this section.

Speed adjustment

WARNING ...

\section*{DANGEROUS VOLTAGES EXIST IN THE TRANSPONDER CODER-INDICATOR DRAWER. AVOID PERSONAL CONTACT WITH LIVE PARTS.}
23. The coding speed adjustment R110 can be reached by withdrawing the Coder-Indicator drawer to its fullest extent and letting down the chassis at the left-hand side. The adjustment to R110 in the electronic keyer can then be made using a grubscrewdriver through the hole in the back of the keyer case.
24. After adjusting the length of one dot to 110 ms approx, the chassis should be resecured and the drawer pushed back and secured.


Fig.2. Timing diagram for entry of " 1 " at \(t=0\) (after reset)


Fig. 3. Clock timing diagram


SEction AA'


Fig 4 Control Disolav Board


Fig 5 Logic Board


Fig 6 Key Unit Assembly


Chap. 2

\section*{INDEX}
\begin{tabular}{|c|c|c|c|}
\hline SUBJECT & PARA． GRAPH （Figure） ＊Table & SUBJECT
B（cont） & \begin{tabular}{l}
PARA－ \\
GRAPH \\
（Figure） \\
＊Table
\end{tabular} \\
\hline Adjustment： & & \multicolumn{2}{|l|}{Built－in test equipment：} \\
\hline Amplifier－Modulator AM－1701／URN．． & 2－51，（2－20） & Adjustment & 2－4d \\
\hline Coder－Indicator KY－382／ARN－9 ．．． & 2－5j，6－2e & \multicolumn{2}{|l|}{Block diagrams ．．．．．．（4－8），（4－9），（4－10），（4－11）} \\
\hline Control－Duplexer C－2226A／GRN－9 ． & －5f，（2－14）， & \multicolumn{2}{|l|}{Front panels．．．．．．．（3－14），（3－15），（3－16），（3－17）} \\
\hline & （2－16），6－2g & & 4－3a（7） \\
\hline Frequency Multiplier－Oscillator & & Function switch positions & ＊2－4 \\
\hline CV－1171／GRN－9D．．．．．．．．．．．．．．．．． & －5h，（2－17）， & Installation ．．．．．．．．． & 2－4d \\
\hline & －1文），（2－21） & \multicolumn{2}{|l|}{Interconnections ．．．．．．．．．．．．．．．（2－11），（3－13）} \\
\hline Initial checks & 2－5a & Test principles of operation ．．．．．．． & 4－3c \\
\hline Power Supply PP－1765／URN ．．．．．．．． & \[
\begin{array}{r}
2-5 \mathrm{e}(2), \\
-13), 6-2 \mathrm{c}(2)
\end{array}
\] & \multicolumn{2}{|l|}{C} \\
\hline Power Supply PP－1766／URN．．．．．．．．． & \[
\begin{gathered}
2-5 \mathrm{e}(1), \\
-12), 6-2 \mathrm{c}(1)
\end{gathered}
\] & Cabinet CY－3163／GRN－9D & \\
\hline Preliminary & 2－5b & Blower & （3－6） \\
\hline Radio Receiver R－824／URN & 2－5i，6－2d， & Controls & ＊3－1 \\
\hline & 6－3b（3） & Fuses & ＊3－4 \\
\hline Test equipment，built－in & 2－5d & Routine checks & ＊3－3 \\
\hline Transmitter & 2－51，6－2f & Schematic diagram & （6－27） \\
\hline Amplifier－Modulator AM－1701／URN & （6－57） & Wiring diagram & （6－48） \\
\hline Adjustment & 2－51 & Cabinet CY－3164／GRN－9D & （6－49） \\
\hline Capabilities and limitations & 3－1b（4） & Blower ． & （ \(5-10)\) \\
\hline Circuit analysis．． & 4－3b（3）（b） & Controls & ＊3－2 \\
\hline Double－slug tuner & （2－20） & Fuses & ＊3－4 \\
\hline Front panel． & （3－4） & Routine checks & ＊3－3 \\
\hline Functional description ．．．．．．． \(1-2 \mathrm{c}\)（1） & ），4－3a \({ }^{\text {（3）（b）}}\) & Schematic diagram & （6－28） \\
\hline Fuses． & ＊3－4 & Wiring diagram & （6－49） \\
\hline Simplified schematic & （4－32） & Cables ： & \\
\hline Subassembly description & 1－5d & Fabrication．．．．．．．．．．．．．2－4a，（2－3） & 2－4），（2－5） \\
\hline Troubleshooting & 5－4d（3） & Installation & 2－4b \\
\hline Tubes．．． & ＊1－4，＊3－5 & Layout & \(2-4 \bar{b}\) \\
\hline Tuning and adjustment & 6－2f & Location & （2－6） \\
\hline \multicolumn{2}{|l|}{\multirow[t]{2}{*}{Wiring diagrams ．．．．．．．．．．．．．．．\({ }^{(6-39), ~(6-40) ~}\)}} & Wiring list & ＊2－2 \\
\hline & & Capabilities and limitations： & \\
\hline \multirow{3}{*}{B} & & Amplifier－Modulator AM－1701／URN．． & 3－1b（4） \\
\hline & & Coder－Indicator KY－382／GRN－9D & 3－1立（3） \\
\hline & & Control circuits & 3－1立（5） \\
\hline Beacon identification & 1－2a & \multicolumn{2}{|l|}{Frequency Multiplier－Oscillator} \\
\hline Bearing information & 1－2 \({ }_{\text {c }}\) & CV－1171／GRN－9D．．．．．．．．．．．．．． & 3－1b（4） \\
\hline Block diagrams： & & Radio Receiver R－824／URN ．．．．．．．． & 3－1立（2） \\
\hline Oscilloscope OS－54／URN－3， simplified & （4－11） & Transmitter Changes： & 3－1酐（4） \\
\hline Power Meter－Pulse Counter & & \multirow[t]{2}{*}{Call code Crystals} & 3－2c（2）（b； \\
\hline TS－891／URN－3，simplified． & （4－10） & & 2）（a），2－5 \\
\hline Pulse Analyzer－Signal Generator & & Frequencies & 3－3c \\
\hline TS－890A／URN－3，simplified & （4－9） & \multicolumn{2}{|l|}{Circuit analysis：} \\
\hline Pulse Sweep Generator & & Amplifier－Modulator AM－1701／URN．． & \(4-3 \mathrm{~b}(3)(\mathrm{b})\) \\
\hline SG－121A／URN－3，simplified & （4－8） & \multirow[t]{2}{*}{Coder－Indicator KY－382／GRN－9D ．．．．} & 4－3b（2） \\
\hline Radio Beacon，overall functional & （4－1） & \multicolumn{2}{|l|}{\multirow[b]{2}{*}{Frequency Multiplier－Oscillator \({ }^{\text {a }}\)－}} \\
\hline Radio Set AN／GRN－9D，simplified & （4－7） & & \\
\hline Switch－Test Adapter SA－420／URN－3， simplified． & （4－12） & \multicolumn{2}{|l|}{Power distribution and control} \\
\hline Blower ： & & circuits & 4－3b（6） \\
\hline Cabinet CY－3163／GRN－9D． & （3－6） & Power supplies & 4－3b（ 5 ） \\
\hline Cabinet CY－3164／GRN－9D & （3－10） & Radio Receiver R－824／URN & 4－3b（1） \\
\hline Fuses． & ＊3－4 & Transmitter & 4－3b） 3 ） \\
\hline
\end{tabular}

\begin{tabular}{|c|c|}
\hline SUBJECT
I & PARAGRAPH (Figure) *Table \\
\hline Identification code & 1-2a \\
\hline \multicolumn{2}{|l|}{Installation:} \\
\hline Cables . & 2-4b \\
\hline Klystron & (2-10) \\
\hline Layout. & 2-3 \\
\hline Requirements & 2-4 \\
\hline Tubes..... & *2-3 \\
\hline Typical procedure & 2-1b, (2-2) \\
\hline Unpacking and handling & 2-1 \\
\hline Introduction . & 1-1 \\
\hline \multicolumn{2}{|l|}{K} \\
\hline \multicolumn{2}{|l|}{Klystron:} \\
\hline Aging . & 2-5k \\
\hline Access door & (2-7) \\
\hline Grid and heater connections & (2-8) \\
\hline Characteristics & (2-9) \\
\hline Installation details & (2-10), 2-4c \\
\hline Waveshapes & (2-19) \\
\hline Test setup. & (5-22) \\
\hline \multicolumn{2}{|l|}{L} \\
\hline Location of parts & 5-6 \\
\hline \multicolumn{2}{|l|}{M} \\
\hline \multicolumn{2}{|l|}{Maintenance:} \\
\hline Emergency & 3-6c \\
\hline Operating checks & 3-6a \\
\hline Operator & 3-6 \\
\hline Parts list & 7-4,*7-3 \\
\hline Routine checks. & 3-6b, *3-3 \\
\hline Manufacturers. & 7-5, *7-4 \\
\hline \multicolumn{2}{|l|}{0} \\
\hline \multicolumn{2}{|l|}{Operating procedures:} \\
\hline Changing call code . & 3-2c(2)(b) \\
\hline Changing crystals .. & c(2)(a), 2-5g \\
\hline Changing frequencies & 3-3c \\
\hline Checks and adjustments. & 3-6a \\
\hline Emergency maintenance & 3-6 \({ }^{\text {c }}\) \\
\hline Emergency operation & 3-4 \\
\hline Maintenance . . . & 3-6 \\
\hline Routine checks... & 3-6b \\
\hline Securing equipment. & 3-3- \\
\hline Starting . . . . . . . . . & 3-3ā \\
\hline Tuning and adjusting. & 3-3b \\
\hline \multicolumn{2}{|l|}{Operation :} \\
\hline Controls & 3-2b \\
\hline Functional. & 3-1 \\
\hline Indications & 3-2d \\
\hline Procedures. & 3-2 \\
\hline Remote & 3-2c(2)(c) \\
\hline Sequence. & 3-2] \\
\hline Summary of procedures. & 3-3 \\
\hline
\end{tabular}
Parts locations 5-6,6-4c
Power: Primary power distribution diagram ..... (6-15)
Requirements and distribution ..... 2-2
Power distribution and control:
Circuit analysis ..... 4-3b(6)
Functional description ..... 4-3"(6)
Routine maintenance ..... *3-3
Servicing block diagram ..... (5-25)
Troubleshooting chart ..... *5-10
Power Supply Assembly
OA-1537A/GRN-9A ..... (1-3)
Controls ..... 3-2b(2)
Functional description ..... -5d(3)
Power Supply PP-1763/GRN (HV) ..... (6-67)
Controls ..... *3-2
Front panel ..... (3-8)
Fuses ..... *3-4
Overload relay adjustment ..... 6-3b(2)
Routine checks ..... *3-3
Schematic diagram ..... (6-26)
Simplified schematic ..... (4-41)
Troubleshooting chart ..... *5-9
Tubes ..... *1-4, *3-5
Voltage and resistance diagram ..... (5-24)
Wiring diagram ..... (6-47)
Power Supply PP-1765/URN (MV) ..... (6-65)
Adjustments ..... \(-3 b(1)\)
Controls
(3-9)
(3-9)
Front panel
Front panel ..... *3-4
Fuses
6-3b(1)
Overload relay adjustment ..... *3-3
Schematic diagram ..... (6-25)
Simplified schematic ..... (4-40)
Troubleshooting chart* \(5-\mathrm{d}\)
* 3.5
Tubes ..... *1-4, *3. 5
Voltage and resistance diagram ..... (6-46)
Power Supply PP-1766/URN (LV) ..... (6-32)
Adjustment ..... 6-2c(1)
Controls ..... -3-2
Front panel ..... (3-7)
Fuses ..... *3-4
Routine checks ..... *3-3
Troubleshooting chart ..... *S-"
Tubes ..... *1-4,*3-5
Voltage and resistance diagram ..... (5-24)
Wiring diagram ..... (6-45)
Principles of operation, general ..... 4-1
Q
Quick reference data ..... \(1-4\)
R
Radio Beacon ..... (1-1)
Block diagram ..... (4-1)
Capabilities and limitations ..... \(3-1 b(1)\)
Information, bearing, distance identification ..... 1-2

PARA-

\section*{GRAPH (Figure) *Table \\ P \\ SUBJECT} ,




\begin{tabular}{|c|c|}
\hline SUBJECT
S (cont) & PARAGRAPH (Figure) *Table \\
\hline \multicolumn{2}{|l|}{Simplified schematic diagrams (cont)} \\
\hline Radio Receiver, i-f amplifier & (4-15) \\
\hline Radio Receiver, one-shot multivibrator and receiver output... & (4-20) \\
\hline Radio Receiver, power supply ...... & (4-39) \\
\hline Radio Receiver, preamplifier. & (4-14) \\
\hline Radio Receiver, squitter control voltage regulator & (4-22) \\
\hline Radio Receiver, video amplifier . . . . & (4-18) \\
\hline Radio Set AN/GRN-9D, transmitter output circuit. & (4-33) \\
\hline Special tools . & 6-2a \\
\hline Starting 3-2¢¢(1)(a), 3-2c & 1)(b), 3-3ā \\
\hline \multicolumn{2}{|l|}{Subassembly description :} \\
\hline Amplifier-Modulator & 1-5d \\
\hline Coder-Indicator . & 1-5d \\
\hline Frequency Multiplier-Oscillator & 1-5 \({ }^{\text {d }}\) \\
\hline Radio Receiver & 1-5 \({ }^{\text {d }}\) \\
\hline \multicolumn{2}{|l|}{T} \\
\hline Terminal lugs, attaching & (2-3) \\
\hline \multicolumn{2}{|l|}{Test equipment:} \\
\hline Built-in, adjustment. & 2-5d \\
\hline Built-in, front panels.............. . . (3 & \[
\begin{aligned}
& \text { 4), (3-15), } \\
& \text { 16), (3-17) }
\end{aligned}
\] \\
\hline Built-in, installation & 2-4d \\
\hline Built-in, interconnection, schematic. & (2-11) \\
\hline Required & 5-2,*5-1 \\
\hline Tuning and adjustment test equipment and special tools & 6-2a \\
\hline Test principles & 4-3' \\
\hline Test procedures & 3-5 \\
\hline Tools, special. & 5-2b \\
\hline Transmission line filter cavities, tuning curves & (2-15) \\
\hline \multicolumn{2}{|l|}{Transmitter:} \\
\hline Adjustment . & 2-51, 6-2f \\
\hline Capabilities and limitations & 3-1b(4) \\
\hline Circuit analysis. & 4-35 \({ }^{\text {b }}\) ( 3 ) \\
\hline Functional description & 4-3ā(3) \\
\hline Pulse sequence & (4-34) \\
\hline Routine checks & *3-3 \\
\hline Servicing block diagram & (5-15) \\
\hline Troubleshooting. . . . . . . . . . . . . . . . 5 & c(3), *5-5 \\
\hline Waveforms . . . . . . . . (5-16), (3-18), (3 & 19), (3-20) \\
\hline \multicolumn{2}{|l|}{Troubleshooting:} \\
\hline Amplifier-Modulator. & 5-4d(3) \\
\hline Coder-Indicator & 5-4效(2) \\
\hline Functional section troubleshooting charts & \(5-4 \mathrm{~d}\) \\
\hline Overall & 5-3 \\
\hline \multicolumn{2}{|l|}{Power distribution and control circuits . . . . . . . . . . . . . . . . . . . . . . . . . . 5-4d(5)} \\
\hline Power supplies. & 5-4效(4) \\
\hline Preliminary check & 5-3a \\
\hline Radio Receiver & 5-4d(1) \\
\hline System troubleshooting chart & 5-3d \\
\hline Transmitter & 5-4d (3) \\
\hline
\end{tabular}
\begin{tabular}{|c|c|}
\hline SUBJECT
T (cont) & PARAGRAPH (Figure) *Table \\
\hline \multicolumn{2}{|l|}{Troubleshooting charts:} \\
\hline Coder-Indicator KY-382/GRN-9D & *5-5 \\
\hline Power distribution and control circuits. & *5-10 \\
\hline Power Supply PP-1763/URN & *5-9 \\
\hline Power Supply PP-1765/URN. & *5-8 \\
\hline Power Supply PP-1766/URN. & *5-7 \\
\hline Radio Receiver R-824/URN & *5-4 \\
\hline Transmitter & *5-6 \\
\hline \multicolumn{2}{|l|}{Tubes, electron:} \\
\hline Complement . & 1-5d, *1-4 \\
\hline Installation & 2-4 \(\overline{\mathrm{c}}\), *2-3 \\
\hline Location & *3-5 \\
\hline \multicolumn{2}{|l|}{Tuning and adjustment:} \\
\hline Amplifier-Modulator & 6-2f \\
\hline Operating & 3-35 \\
\hline Radio Receiver & 6-2 \(\overline{\mathrm{d}}\) \\
\hline \multicolumn{2}{|l|}{U} \\
\hline \multicolumn{2}{|l|}{Units, major:} \\
\hline Colloquial names & *7-2 \\
\hline List & *7-1 \\
\hline Unpacking and handling & (2-1), 2-1 \\
\hline \multicolumn{2}{|l|}{V} \\
\hline \multicolumn{2}{|l|}{Voltage and resistance diagrams:} \\
\hline Amplifier-Modulator AM-1701/URN & (5-20) \\
\hline Coder-Indicator KY-382/GRN-9D . . & (5-12), (5-13) \\
\hline Frequency Multiplier-Oscillator CV-1171/GRN-9D . . . . . . . . . . . . & \[
\text { . }(5-18),(5-19)
\] \\
\hline Power Supply PP-1763/URN. . & (5-24) \\
\hline Power Supply PP-1765/URN & (5-23) \\
\hline Power Supply PP-1766/URN. & (5-22) \\
\hline Radio Receiver R-824/URN .. & \[
\begin{array}{r}
.(5-5),(5-6), \\
(5-7),(5-8)
\end{array}
\] \\
\hline Voltage chart : & \\
\hline Preamplifier alignment . . . . . & *6-1 \\
\hline Radio Receiver, i-f amplifier & *6-2 \\
\hline \multicolumn{2}{|l|}{W} \\
\hline \multicolumn{2}{|l|}{Waveforms:} \\
\hline Coder-Indicator KY-382/GRN-9D & \[
\begin{array}{r}
(5-11), \\
(4-30),(4-24)
\end{array}
\] \\
\hline Composite north and auxiliary reference burst. & (3-19) \\
\hline Klystron . . . & (2-19) \\
\hline Overall system delay & (6-8) \\
\hline Radio Receiver R-824/URN & . (5-4), (4-17) \\
\hline Transmitter . . . . . . . . . . . . & (3-18), (5-16) \\
\hline Transmitter pulse sequence & (4-34) \\
\hline Zero distance delay & (3-20) \\
\hline Wiring diagrams. & 6-4b \\
\hline Amplifier-Modulator & (6-39) \\
\hline Amplifier-Modulator, bias supply. & (6-40) \\
\hline Cabinet CY-3163/GRN-9D & (6-48) \\
\hline Cabinet CY-3164/GRN-9D.. & (6-49) \\
\hline
\end{tabular}

Issued June 73
\begin{tabular}{cc} 
SUBJECT & \begin{tabular}{c} 
PARA- \\
GRAPH \\
(Figure)
\end{tabular} \\
*Table
\end{tabular}
\begin{tabular}{|c|c|}
\hline SUBJECT
W (cont) & \begin{tabular}{l}
PARA GRAP \\
(Figure *Tabl
\end{tabular} \\
\hline \multicolumn{2}{|l|}{Wiring diagrams (cont)} \\
\hline Frequency Multiplier-Oscillator, video chassis & (6-31 \\
\hline Power Supply PP-1763/URN (HV) & (6-4) \\
\hline Power Supply PP-1765/URN (MV) & (6-4) \\
\hline Power Supply PP-1766/URN (LV) & (6-4! \\
\hline Radio Receiver, frame & (6-3) \\
\hline Radio Receiver, i-f amplifier subassembly & (6-3: \\
\hline Radio Receiver, power supply & (6-3) \\
\hline Radio Receiver, preamplifier and mixer subassembly & (6-3 \\
\hline Radio Receiver, video chassis & (6-3) \\
\hline
\end{tabular}```

