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Colin Hinson
In the village of Blunham, Bedfordshire.

# OSCILLOSCOPE TYPE RM529 

## GENERAL, AND TECHNICAL INFORMATION

BY COMMAND OF THE DEFENCE COUNCIL
T.Dunnett
(Ministry of Defence)
FOR USE IN THE
ROYAL AIR FORCE

## NOTE TO READERS

The subject matter of this publication may be affected by Defence Council Instructions, Servicing schedules (Volume 4 and 5), or 'General Orders and Modifications' leaflets in this A.P., or even in some others. If possible, Amendment Lists are issued to correct this publication accordingly, but it is not always practicable to do so. When an Instruction, Servicing schedule, or leaflet contradicts any portion of this publication, the Instruction, Servicing schedule, or leaflet is to be taken as the overriding authority.

The inclusion of references to items of equipment does not constitute authority for demanding the items.

Each leaf, except the original issue of preliminaries, bears the date of issue and the number of the Amendment List with which it was issued. New or amended technical matter will be indicated by black triangles positioned in the text thus:- $4 \cdots \cdots \cdot . . . . .-$ to show the extent of amended text, and thus:- to show where text has been deleted. When a Part, Section, or Chapter is issued in a completely revised form, the triangles will not appear.

The reference number of this publication was altered from A.P. 101S-0202-1, Cover 5 to A.P.116T-1202-1 by A.L. action in Feb. 69.

## DANGER-HIGH VOLTAGE

## LEARN THESE SAFETY RULES

1. ELECTRICAL SYSTEM. Voltages in excess of 100 volts, a.c. or d.c. can be extremely dangerous in certain circumstances. Personnel should therefore ensure that the electrical system is electrically safe before any servicing is attempted. Where it is essential for tests or adjustments to be made with the electrical power switched on, the greatest care must be exercised.
2. SHOCK. Learn how to deal with cases of electric shock.


## APPARATUS IS SAFE-ONLY IF YOUR APPROACH IS CORRECT

TYPE RM529<br>MOD 188A

This insert has been written to supplement the Instruction Manual furnished with this modified instrument. The information given in this insert will supersede that given in the manual.

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TYPE RM529

MOD 188A

This manual insert describes the special features of the Type RM529, MOD 188A which has been modified for use with the CCIR, 625/50 system. The following changes have been made to this instrument:

## Vertical Deflection System - Frequency Response

HIGH PASS - The center frequency has been changed from 3.58 MHz to 4.43 MHz . At 3.93 MHz and at $5.13 \mathrm{MHz}, 60 \mathrm{mV}$ produces not more than $85 \%$ nor less than $65 \%$ full screen deflection. At $4.43 \mathrm{MHz}, 60 \mathrm{mV}$ produces full screen deflection. The gain of the amplifier is X 2 in the HIGH PASS position.

BAND PASS - The response is down not more than 1 dB (89.3 IEEE units) at 0.9 and 1.3 MHz referred to 1.096 MHz center frequency, and not less than -18 dB ( 12 IEEE units) at 200 kHz . Sensitivity is 60 mV full scale at 1.096 MHz . The gain of the amplifier is X 2 in the BAND PASS position.

LOW PASS - (unchanged) -12 dB or $75 \%$ down or more at 500 kHz .
IEEE - Rolloff extends to 4.43 MHz .
FLAT - (unchanged) Within $\pm 1 \%, 60 \mathrm{~Hz}$ to 5 MHz ; within $\pm 3 \%$ to 8 MHz (DC Restorer off).

## Calibrator

The F.S. (Full Scale) position of the CALIBRATOR remains the same. The .714 F.S. position has been changed to .700 F.S.

## Horizontal

The sweep rates for the 2 LINE and 2 FIELD positions of the Horizontal DISPLAY switch have been changed to correspond with the $625 / 50$ CCIR System.

The nomenclature on the Horizontal DISPLAY switch has been changed as follows:
$.25 \mathrm{H} / \mathrm{CM}$ changed to $.1 \mathrm{H} / \mathrm{CM}$ $.125 \mathrm{H} / \mathrm{CM}$ changed to $10 \mu \mathrm{~S} / \mathrm{CM}$ In the Line Selector positions:
$.25 \mathrm{H} / \mathrm{CM}$ changed to $.2 \mathrm{H} / \mathrm{CM}$
$.125 \mathrm{H} / \mathrm{CM}$ changed to $.1 \mathrm{H} / \mathrm{CM}$
The sweep-time relationships are shown by the table on the following page, which replaces Table 2-1 in the manual.

TYPE RM529, MOD 188A

| HORIZONTAL) <br> MAG | DISPLAY Switch Setting |  |  |
| :---: | :--- | :--- | :--- |
|  | $.1 \mathrm{H} / \mathrm{CM}$ | $.2 \mathrm{H} / \mathrm{CM}$ | $10 \mu \mathrm{~S} / \mathrm{CM}$ |
| X 1 | $.1 \mathrm{H} / \mathrm{cm}$ | $.2 \mathrm{H} / \mathrm{cm}$ | $10 \mu \mathrm{~s} / \mathrm{cm}$ |
|  | $6.4 \mu \mathrm{~s} / \mathrm{cm}$ | $12.8 \mu \mathrm{~s} / \mathrm{cm}$ | $10 \mu \mathrm{~s} / \mathrm{cm}$ |
|  | $.02 \mathrm{H} / \mathrm{cm}$ | $.04 \mathrm{H} / \mathrm{cm}$ | $2 \mu \mathrm{~s} / \mathrm{cm}$ |
|  | $1.28 \mu \mathrm{~s} / \mathrm{cm}$ | $2.56 \mu \mathrm{~s} / \mathrm{cm}$ | $2 \mu \mathrm{~s} / \mathrm{cm}$ |
| X 25 | $.004 \mathrm{H} / \mathrm{cm}$ | $.008 \mathrm{H} / \mathrm{cm}$ | $.4 \mu \mathrm{~s} / \mathrm{cm}$ |
|  | $.256 \mu \mathrm{~s} / \mathrm{cm}$ | $.512 \mu \mathrm{~s} / \mathrm{cm}$ | $.4 \mu \mathrm{~s} / \mathrm{cm}$ |

## Graticule

Display Area -7 cm high by 10 cm wide. Two types of graticules are furnished with this modified instrument. They are: (a) Composite CCIR video, 0-100 IEEE units with 30 -unit blanking level (331-0184-00), installed; and (b) Composite CCIR video, $\sin ^{2}$ and K factor: ruled $0-100$ IEEE units with 30 -unit blanking level, 2 and $4 \% \mathrm{~K}$ factor for $0.1 \mu \mathrm{~s}$ T pulse and $0.2 \mu \mathrm{~s} 2 \mathrm{~T}$ pulse (331-0185-00), added to the accessory kit.

## Power Supplies - Transformer Wiring

The Type RM529, MOD 188A is wired for 230 -volt operation, unless otherwise specified.

## Trace Rotation

The locations of the GAIN control, R814, normally on the front panel, and the CRT BEAM ROTATOR (TRACE ROTATION) control, R655, have been interchanged. The TRACE ROTATION control is now on the front panel.

## CALIBRATION

The following changes and additions should be made to the Calibration section of the manual.

1. The . 714 F.S. position of the CALIBRATOR has been changed to .700 F.S. - Check for 7 major divisions of signal. R885 and R886 have been changed to set this level ( $\pm 1 \%$ ).
2. Check Vertical Amplifier High-Frequency Response
(a) Set the RESPONSE switch to FLAT and follow the procedure as described in Table 5-4 in the manual.
(b) Change to IEEE and follow the table (IRE), extending the check to 4.43 MHz . At 4.43 MHz the deflection should be 2-5 IEEE units.
(c) Change to LOW PASS and follow the procedure in the table.
(d) Change to BAND PASS. The sensitivity is 60 mV full scale at 1.096 MHz ( X 2 gain in this position). The response should be down not more than 1 dB ( 89.3 IEEE units) at 0.9 and 1.3 MHz , and down 18 dB ( 12 IEEE units) or more at 200 kHz .

Connect a 2 Hz to 2 MHz constant amplitude signal generator to A VIDEO INPUT; switch RESPONSE to FLAT; VOLTS FULL SCALE to 0.2; and VARIABLE to the CALIB position. Set the signal generator frequency to 1.096 MHz and adjust amplitude for 50 IEEE units. Then change to BAND PASS and adjust L136, C 140 B , and C 140 H (in the 1.09 MHz filter for the center frequency and X2 gain - see Response Switch diagram in this insert) for 100 IEEE units. Check the upper and lower limits for not less than 89.3 IEEE units at 0.9 and 1.3 MHz . (A slight readjustment may be necessary to set the two limits.) Change frequency to 200 kHz and check response for 12 IEEE units or less.
(e) Change to HIGH PASS. The sensitivity is 60 mV full scale at 4.43 MHz ( X 2 gain in this position). At 3.93 MHz and at $5.13 \mathrm{MHz}, 60 \mathrm{mV}$ produces not more than $85 \%$ nor less than $65 \%$ full scale deflection.

Connect a modulated stairstep signal of 10 steps with 4.43 MHz burst superimposed to A VIDEO INPUT; switch RESPONSE to FLAT; VOLTS FULLSCALE to 0.2; and VARIABLE to the CALIB position. Externally, adjust the amplitude of the signal for 50 IEEE units. Change to HIGH PASS position. In this position, the filter in the RESPONSE switch strips the stairstep providing bandpass filtering centered at 4.43 MHz with X 2 gain. Adjust C 140 C and C140G for 100 IEEE units with best waveform response. There is interaction between C140C and C140G.

Check the upper and lower limits, using a constant amplitude signal generator set to $4.43 \mathrm{MHz} ; 3.93 \mathrm{MHz}$; and 5.13 MHz . 60 mV produces not more than $85 \%$ nor less than $65 \%$ of full scale deflection by adjusting C140C and C140G for gain.
3. Horizontal Amplifier (Omit this step if $625 / 50$ is available). The sweep rates have been changed to correspond with the $625 / 50$ CCIR system. Apply composite $525 / 60$ video signal to Vertical and set Horizontal DISPLAY switch to 2 FIELD. Adjust Horiz. Gain (R568) for 8.33 cm display of video, $\pm 5 \%$. Then change DISPLAY switch to $10 \mu \mathrm{~S} / \mathrm{CM}$ and apply $10 \mu \mathrm{sec}$ from 180A to Vertical and Ext. Trigger. Adjust C481 for $10 \mu \mathrm{sec} / \mathrm{cm}$. Change Horizontal DISPLAY switch to . $1 \mathrm{H} / \mathrm{CM}$ and readjust Horiz. Gain for $63.5 \mu \mathrm{sec}$, or one horizontal line in 10 cm of video. (Measure from trailing edge to trailing edge only.) Recheck $10 \mu \mathrm{~S} / \mathrm{CM}$ range.
4. Horizontal Amplifier (Using Conrac Generator for 625/50 clock). Apply composite sync from Conrac to Vertical and set Horizontal DISPLAY switch to 2 FIELD. Adjust Horiz. Gain (R568) for 10.2 cm of sweep, $\pm 5 \%$. Turn Horizontal DISPLAY switch to $10 \mu \mathrm{~S} / \mathrm{CM}$ and adjust C481 for 6.4 cm between trailing edges of successive horizontal sync pulses. Turn Horizontal DISPLAY switch to . $1 \mathrm{H} / \mathrm{CM}$ and check for 1 horizontal line in 10 cm (trailing edge to trailing edge). MAG switch in Xl for above checks.
5. The sweep length will increase in the Line Mode operation, to approximately 11 cm (Spec. is $10.5 \mathrm{~cm} \min$.).
6. Adjust X 25 MAG (C523). $4 \mu \mathrm{sec} / \mathrm{cm}$.

Set for 5 MHz from 180A, Ext Sync, and adjust C523 for 2 cycles/cm or 20 pulses in $10 \mathrm{~cm}, \pm 7 \%$.
7. Check X5 MAG $2 \mu \mathrm{sec} / \mathrm{cm}$.

Set for $1 \mu \mathrm{sec}$ from 180A, Ext Sync, should be 20 pulses in 10 cm .
8. Change Horizontal DISPLAY to $.1 \mathrm{H} / \mathrm{CM}$ (This is only a check. If out of tollerance, readjust C523 in $10 \mu \mathrm{~S} / \mathrm{CM}$ position). With MAG switch in X1, display 1 and $5 \mu \mathrm{sec}$ markers. Check for 13 markers counting the first marker of $5 \mu \mathrm{sec}$ markers plus 4 ea $1 \mu \mathrm{sec}$ marker in $10 \mathrm{~cm}(64 \mu \mathrm{sec} \pm 2 \%)$. With MAG switch in X5, display $1 \mu \mathrm{sec}$ markers. Check for 13.8 markers in 10 cm counting the first marker, $\pm 3 \%$. With MAG switch in X25, display 5 MHz markers. Check for 13.8 markers in 10 cm counting the first marker, $\pm 7 \%$.
9. Adjust Field Sync (R360).

The FIELD switch states ONE or TWO. This is referring to the start of the sweep, not the center of the sweep that is viewed on the screen. The procedure for setting this up is the same as standard, except that the $625 / 50$ system uses only five equalizing pulses. Therefore, R360 should be adjusted for only 5 pulses instead of 6 (reset Conrac for 5 pulses).

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9. (cont.) Set the FIELD switch to ONE. Determine that only $1 / 2$ line of video precedes the Vertical Unblanking Pulse appearing incenter screen (use X25 MAG). Compare line and $1 / 2$ line, looking at adjacent horizontal sync pulses.

## NOTES

When setting the VIT Line Sel Range potentiometer (R458), set the LINE SELECTOR switch to line 19, although the actual line, according to the CCIR System of counting, is line 12.

When checking the brightening pulse set the LINE SELECTOR switch to VARIABLE and rotate the VARIABLE throughout its range. The brightening pulse must cover at least one field.

The locations of the GAIN control, R814, and the CRT BEAM ROTATOR have been interchanged. The Vertical GAIN is now adjusted through the hole in the dust cover (at the left of the CRT), and the TRACE ROTATION is now on the front panel.

## PARTS LIST

The following parts have been added to this modified instrument. When ordering replacement parts, specify instrument type, serial number, and MOD number. Include the circuit number, part number, and description of the desired item.

## CAPACITORS

| C132 | Add | $281-0594-00$ | 150 pF | 100 V |  | cer |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| C134 | Delete |  |  |  |  |  |
| C135 | Delete |  |  |  |  |  |
| C136 | Change | $283-0602-00$ | 53 pF | 300 V |  | mica |
| C137 | Delete |  |  |  |  |  |
| C140A | Add | $283-0602-00$ | 53 pF | 300 V |  | mica |
| C140B | Add | $281-0092-00$ | $9-35 \mathrm{pF}$ |  | var |  |
| C140C | Add | $281-0091-00$ | $2-8 \mathrm{pF}$ |  | var |  |
| C140D | Add | $281-0577-00$ | 14 pF | 500 V |  | cer |
| C140E | Add | $281-0577-00$ | 14 pF | 500 V |  | cer |
| C140F | Add | $281-0504-00$ | 10 pF | 500 V |  | cer |
| C140G | Add | $281-0093-00$ | $5.5-18 \mathrm{pF}$ |  | var |  |
| C140H | Add | $281-0091-00$ | $2-8 \mathrm{pF}$ |  | var |  |
| C205 | Add | $283-0002-00$ | $.01 \mu \mathrm{~F}$ | 500 V |  | cer |
| C232 | Add | $281-0594-00$ | 150 pF | 100 V |  | cer |
| C236 | Change | $283-0602-00$ | 53 pF | 300 V |  | mica |
| C237 | Delete |  |  |  |  |  |
| C482 | Change | $283-0604-00$ | 304 pF | 300 V | $2 \%$ | mica |
| C452 | Change | $281-0543-00$ | 270 pF |  | $10 \%$ | cer |

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## INDUCTORS

| L132 | Add | $037-2036-00$ | $72 \mu \mathrm{H}$ |  |
| :--- | :--- | :--- | :--- | :--- |
| L133 | Add | $108-0360-00$ | $46 \mu \mathrm{H}$ |  |
| L134 | Add | $037-2037-00$ | $36 \mu \mathrm{H}$ |  |
| L136 | Add | $037-2038-00$ | $364 \mu \mathrm{H}$ | var |
| L137 | Change | $037-2036-00$ | $72 \mu \mathrm{H}$ |  |
| L232 | Add | $037-2036-00$ | $72 ; \mu \mathrm{H}$ |  |
| L233 | Add | $108-0360-00$ | $46 \mu \mathrm{H}$ |  |
| L237 | Add | $037-2036-00$ | $72 \mu \mathrm{H}$ |  |

## RESISTORS

| R122 | Change | $321-0265-00$ | 5.62 k | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R124 | Add | $321-0184-00$ | $806 \Omega$ | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R135 | Delete |  |  |  |  |  |
| R362 | Change | $323-0498-00$ | 1.5 M | $1 / 2 \mathrm{w}$ | $1 \%$ | film |
| R453 | Change | $303-0273-00$ | 27 k | 1 w | $5 \%$ | comp |
| R467 | Add | $316-0562-00$ | 5.6 k | $1 / 4 \mathrm{w}$ | $10 \%$ | comp |
| R468 | Change | $323-0394-00$ | 124 k | $1 / 2 \mathrm{w}$ | $1 \%$ | film |
| R481 | Change | $321-0417-00$ | 215 k | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R482 | Change | $321-0417-00$ | 215 k | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R483 | Change | $321-0427-00$ | 274 k | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R484 | Delete |  |  |  |  |  |
| R492 | Change | $321-0335-00$ | 30.1 k | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R834 | Change | $323-0465-00$ | 681 k | $1 / 2 \mathrm{w}$ | $1 \%$ | film |
| R885 | Change | $321-0143-00$ | $301 \Omega$ | $1 / 8 \mathrm{w}$ | $1 \%$ | film |
| R886 | Change | $321-0178-00$ | $698 \Omega$ | $1 / 8 \mathrm{w}$ | $1 \%$ | film |

## SWITCHES

| SW135 | Change | 031-0045-00 | Vertical RESPONSE |
| :--- | :--- | :--- | :--- |
| SW430 | Change | $031-0005-00$ | Horizontal DISPLAY |

## TRANSFORMERS

T135 Delete
MECHANICAL

| DUST COVER, Top | Change | 1 | $386-1097-01$ |
| :--- | :--- | :--- | :--- |
| ETCHED CIRCUIT BOARD, Film \#937X | Add | 1 | $037-6007-00$ |
| GRATICULE, $7 \times 10 \mathrm{~cm}$ (Installed) | Change | 1 | $331-0184-00^{*}$ |
| GRATICULE, $7 \times 10 \mathrm{~cm}$ (In Accessories) Change | 1 | $331-0185-00^{*}$ |  |
| PANEL, Front, Film \#3703 | Change | 1 | $034-0169-00$ |
| ROD, Aluminum, Hex, $1 / 4 \times 7 / 16$ | Add | 3 | $385-0080-00$ |

* See page 2 of this insert for GRATICULE descriptions.

TYPL RM529, MOD 188A


PARTIAL SWP. GEN.

## INSTRUCTION MANUAL

Serial Number

$\qquad$

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## WARRANTY

All Tektronix instruments are warranted against defective materials and workmanship for one year. Tektronix transformers, manufactured in our own plant, are warranted for the life of the instrument.

Any questions with respect to the warranty mentioned above should be taken up with your Tekronix Field Higineer.

Tektron ix-repair and replacement-part service is geared directly to the field, therefore all requess for rep $:$ and inem $^{2}$ placement parts should be in your ared. thistprocedure will assure you the fastest possible service, Please. incluae the instrument Type and Serial or Model Number with all requests for parts or service.

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## SECTION I

## CHARACTERISTICS

## General Information

The Tektronix Type RM529 Waveform Monitor is a selfcontained cathode-ray oscilloscope specifically designed for video-waveform monitoring at television transmitters and studio facilities. With this monitor, any portion of the tele-vision-signal waveform can be displayed on a 5 -inch rectangular cathode-ray tube.

A frequency-response switch is included which enables the selection of several frequency-response characteristics including that characteristic recommended by the IEEE Standards Committee for standardized pulse-level measurements.

An internal $30-\mathrm{kHz}$ amplitude calibrator provides 0.714 -volt or 1.0 -volt pulses for calibrating the vertical amplifier. The sweep system provides calibrated sweeps which eliminates the need for time markers.

The following characteristics apply over an ambient temperature range of $0^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$. Warm-up time for the given accuracies is 20 minutes at $25^{\circ} \mathrm{C}, \pm 5^{\circ} \mathrm{C}$.

The performance requirements throughout this manual are stated in either percentage or IEEE units. The compatible dB point is also inserted using the formula: $d B=20 \log \frac{E 1}{E 2}$.

## NOTE

On instruments with the Serial Numbers below 400, the following control names and labels are used: 1. The HIGH PASS position of the RESPONSE switch is labeled CHROMA.
2. The IEEE position of the RESPONSE switch is labeled IRE.
3. The VOLTS FULL SCALE switch is labeled MAG.
4. The $1.0,0.5$ and 0.2 positions of the VOLTS FULL SCALE switch are labeled X1, X2 and X5 respectively.
5. The FULL SCALE position of the CALIBRATION switch is labeled F. S.
6. The FIELD switch is labeled FIELD SHIFT.
7. The ONE and TWO positions of the FIELD switch are labeled EVEN and ODD respectively.
8. The LINE SELECTOR variable control is labeled DELAY.
9. The LINE SELECTOR . $125 \mathrm{H} / \mathrm{CM}$ and LINE SELECTOR . $25 \mathrm{H} / \mathrm{CM}$ positions of the DISPLAY switch are labeled DELAYED LINE . $125 \mathrm{H} / \mathrm{CM}$ and DELAYED LINE . 25 H/CM respectively.

## VERTICAL DEFLECTION SYSTEM

| Characteristic | Performance Requirement | Supplemental Information |
| :---: | :---: | :---: |
| Frequency Response FLAT (1 V gain sensitivity) | Flat to within $+0 \%,-1 \%(0.1 \mathrm{~dB})$ from 50 Hz to 6 MHz . Flat to within $+0 \%,-3 \%$ $(0.3 \mathrm{~dB})$ from 6 MHz to 8 MHz . |  |
| FLAT 10.2 and 0.5 gain sensitivities) | Flat to within $+0 \%,-1 \%(0.1 \mathrm{~dB})$ from 50 Hz to 6 MHz . |  |
| LOW PASS | Down not less than $80 \%$ ( 14 dB ) at 500 kHz or above. |  |
| HIGH PASS | 3.58 MHz center frequency $15 \%$ to $35 \%$ down in amplitude + and -400 kHz . |  |
| IEEE | See Fig. 1-2. |  |
| Transient Response |  |  |
| High Frequency | T/2 pulse must be between 94 and 100 IEEE units high for 100 IEEE units of bar signal amplitude applied and have less than or equal to 3 IEEE units of overshoot. | Any ringing as observed on the test oscilloscope (Type 547 with 1 Al plug-in used for check) must be added to the overshoot tolerance. |
| Middle Frequency | Top of bar signal must be flat within $\pm 1 / 2$ IEEE unit. | Flainess measured at +100 IEEE unit graticule line. |
| Gain Sensitivity | 1 V -Adjustable to 1 V . 0.2 V -Adiustable to 0.2 V . 0.5 V -less than $\pm 3 \%$ error. |  |
| Variable Gain Sensitivity | Must attenuate the gain by a ratio of at least 2.5:1. | Ratio of maximum amplitude to minimum amplitude. |

HORIZONTAL DEFLECTION SYSTEM

| Characteristics | Performance Requirement | Supplemental Information |
| :---: | :---: | :---: |
| Calibrated Sweep Rates |  |  |
| $\times 1$ | Adjustable to $0.125 \mathrm{H} / \mathrm{CM}$. |  |
| $\times 5$ | Should be within $\pm 3 \%$ of $0.025 \mathrm{H} / \mathrm{CM}$. |  |
| $\times 25$ | Should be within $\pm 3 \%$ of $0.005 \mathrm{H} / \mathrm{CM}$. |  |
| Staircase (RGB-BW) Relay | When relay $K 501$ is energized, sweep will be at either line or field rate (depends on DISPLAY switch setting), and 2.5 cm or less in length. |  |
| Line Selector (Variable) |  |  |
| Minimum Delay | Line selection will start on or before the 15th line of either field. |  |
| Discrete Line Selector (SN 2997-up) | Sweep will start on the line indicated by the LINE SELECTOR (switch) position on both fields. |  |
| Field Selector |  |  |
| ONE | Sweep is triggered by field one. |  |
| TWO | Sweep is triggered by field two. |  |

## TRIGGERING

| External Trigger | Stable triggering must be obtained on an <br> input composite video signal $\leq 250 \mathrm{mV}$ to <br> $\geq 1 \mathrm{~V}$ in amplitude. |
| :--- | :--- |
| Internal Trigger | Stable triggering must be obtained on an <br> input composite video signal $\leq 200 \mathrm{mV}$ to <br> $\geq 1 \mathrm{~V}$ in amplitude. |

## AMPLITUDE CALIBRATOR

| Signal Accuracy |  |  |
| :--- | :--- | :--- |
| .714 FS | Adjustable to 0.714 V. |  |
| FULL SCALE | Within $\pm 1 \%$ of 1 V. | Approximately 30 kHz. |
| Frequency |  |  |

## POWER SUPPLY

| Power Source | $115 \mathrm{VAC}, \pm 10 \%, 50$ to 60 Hz. | Can be connected for 230-VAC operation. |
| :--- | :--- | :--- |
| Power Source Fuse | Type 3AG, 1.25 A slow-blowing. | Type $3 \mathrm{AG}, 0.6 \mathrm{~A}$ slow blowing for 230-VAC <br> operation. |



## CATHODE-RAY TUBE

| Characteristics | Information |
| :--- | :--- |
| Tube Type | T5290-31 rectangular, glass enve- <br> lope. |
| Phosphor | P31 standard. Others available on <br> special order. |
| Accelerating <br> Potential | Approximately 5300 V. |
| Graticule <br> Type | External. See Standard Accessories <br> list for graticules. |
| Scan Area | The equivalent of 7 or more centi- <br> meters of vertical area and the <br> equivalent of 10 or more centime- <br> ters of horizontal area. |
| Graticule |  |
| Illumination | Variable edge lighting. |


| Unblanking | DC used on all sweep rates with <br> AC coupled brightening pulses for <br> line Selector modes of operation. |
| :---: | :--- |
| CRT Beam | Electrical. Will vary the beam <br> across horizontal by $1^{\circ}$ in either <br> direction (total range is equal to <br> or greater than $6^{\circ}$ ). |

MECHANICAL CHARACTERISTICS

| Characteristics | Information |
| :--- | :--- |
| Construction | Aluminum-alloy chassis and panel. |
| Finish | Anodized panel. |
| Overall Dimensions $51 / 4$ inches high, 19 inches wide, <br> (measured at <br> maximum points)knobs). |  |

## Standard Accessories

Information on accessories for use with this instrument is included at the rear of the mechanical parts list.

## SECTION 2

## OPERATING INSTRUCTIONS

## General

This section of the manual provides general operating information. Included is a brief description of the Type RM529 controls and a suggested first-time operating procedure.

## Power Requirements

The regulated power supplied in the Type RM529 will operate with line voltages from 103.5 to 126.5 VAC $(115$ VAC, $\pm 10 \%$ ) or from 207 to 253 VAC ( $230 \mathrm{VAC}, \pm 10 \%$ ). The linevoltage operating range for which your instrument is wired at the factory is indicated on a metal tag fastened to the rear panel near the power receptacle.

The power transformer is wound with two 115-volt primaries, connected in parallel for 115 -volt operation or in series for 230-volt operation. Fig. 2-1 shows the connections for both voltages. When the transformer connections are changed, the metal tag should be turned around so the back side becomes the front. The unmarked side can then be marked with a pencil for the new operating voltage.

For maximum dependability and long life, the line voltage applied to the Type RM529 should be near the voltage indicated on the tag. If the line voltage exceeds the operating limits, or has a poor waveform (distorted sine waves), unstable power-supply operation may result. Check for proper line voltage and waveform before checking for other causes of unstable operation.

## Cooling

The Type RM529 is cooled by convection air flow through the instrument. If possible, allow two inches clearance at the
sides and rear of the instrument for proper air circulation. Temperature of the circulating air should not exceed $50^{\circ} \mathrm{C}$ $\left(122^{\circ} \mathrm{F}\right)$ for safe operation.

## Radiation

To prevent high-voltage power-supply radiation of $30-\mathrm{kHz}$ fundamental and harmonic frequencies from affecting the Type RM529 display and adjacent instruments in the rack, it is important to keep the top and bottom dust covers in place.

## FUNCTIONS OF FRONT-PANEL CONTROLS AND CONNECTORS

## VERTICAL Controls

INPUT
Four-position switch to select one of four input signals: internal calibrator, input $A$, input $B$ or $A-B$ differential.

## POSITION

Positions the trace vertically on the CRT.

## RESPONSE

Four-position switch to select the amplifier frequencyresponse characteristics as listed in Section 1 of this manual.

## VOLTS FULL SCALE

Three-position switch to select the calibrated vertical gain settings of $1.0,0.5$ and 0.2 .


Fig. 2-1. Power transformer connections for 115-and 230-volt operation.
zontal sync pulses, or the time from the start of one horizontal line to the start of the next line). When the (HORIZ) MAG switch is set to $\times 1$, one complete horizontal line is displayed in a sweep length of 8 cm (see Fig. 2-2). In addition, refer to Table 2-1 which lists the sweep-time relationship between $\mathrm{H} / \mathrm{cm}$ and $\mu \mathrm{s} / \mathrm{cm}$.

For pulse measurements at $.125 \mathrm{H} / \mathrm{CM}$, one cm equals 0.125 H . For example, in the NTSC (National Television Standards Commission) signal specifications, 0.125 H is the minimum time interval between the leading edge of the horizontal sync pulse and the end of the color burst.

If the (HORIZ) MAG switch is set to $\times 5$ when the DISPLAY switch is at $.125 \mathrm{H} / \mathrm{CM}$, the time-base sweep rate is 0.025 $\mathrm{H} / \mathrm{cm}$. This sweep rate is used, for example, to make horizontal sync-pulse waveform measurements such as those shown in Fig. 2-2B.

If the (HORIZ) MAG switch is set to $\times 25$ when the DISPLAY switch is at the $.125 \mathrm{H} / C M$ position, the sweep rate is $0.005 \mathrm{H} / \mathrm{CM}$. This sweep rate is useful for measuring the risetime and falltime of the horizontal sync pulses, to count the cycles of color burst (see Fig. 2-2C) and to examine portions of a complete line.

The $.25 \mathrm{H} / \mathrm{CM}$ position of the DISPLAY switch is another calibrated sweep rate which is useful for making horizontal line- and sync-pulse waveform measurements. In the $\times 1$ position of the (HORIZ) MAG switch approximately $21 / 2$ horizontal lines are displayed. Table 2-1 lists the sweep-time relationship between $\mathrm{H} / \mathrm{cm}$ and $\mu \mathrm{s} / \mathrm{cm}$ for each MAG switch position.

When the DISPLAY switch is set to either of the LINE SELEC. TOR positions and the LINE SELECTOR control is used, it is possible to range into the top of the picture to examine any one or two lines, depending on whether the DISPLAY switch is set to the $.125 \mathrm{H} / \mathrm{CM}$ LINE SELECTOR or $.25 \mathrm{H} / \mathrm{CM}$ LINE SELECTOR position. Also, the LINE SELECTOR control can be set so the portion of the vertical blanking pulse which may contain vertical-interval test signals can be examined in detail. The . $25 \mathrm{H} / \mathrm{CM}$ LINE SELECTOR position, in particular, is useful for observing $\sin ^{2}$ (sine-squared) pulses.

The range of the LINE SELECTOR control is such that any portion of field 1 or field 2 can be examined. Either field 1 or field 2 is selected by means of the FIELD switch. A special bright-up circuit in the Type RM529 increases the CRT wiriting rate in either of the two LINE SELECTOR positions.

## MAG

Three-position switch to select sweep magnification ratios of the $\times 1, \times 5$ and $\times 25$ for all positions of the DISPLAY switch.

## LINE SELECTOR

Ten-turn variable control (and a seven position switch, SN 2997-up) for starting the sweep at the beginning of any selected line in the field so that a particular line can be examined in detail. Used in conjunction with all positions of the (HORIZ) MAG and FIELD switches when the DISPLAY switch is set to LINE SELECTOR . $125 \mathrm{H} / \mathrm{CM}$ or $.25 \mathrm{H} / \mathrm{CM}$

## FIELD

Two-position level switch to select either field 1 or field 2. Used in conjunction with the LINE SELECTOR and 2 FIELD positions of the DISPLAY switch.

## SYNC

Two-position lever switch to select either internal or external sync sources.

## REAR-PANEL CABLE CONNECTIONS

## VIDEO INPUTS A, VIDEO INPUTS B

Two pairs of signal-input coaxial connectors are provided. These are VIDEO INPUTS A and VIDEO INPUTS B. These video inputs are designed for high-impedance loop-through, compensated for 75 -ohm systems. Bridging capacitance is approximately 20 pF .

If the second connector of each pair is not used, it can either remain unused, or it can be used for terminating the line with a 75 -ohm termination.

## EXT NEG SYNC INPUT

A pair of coaxial connectors marked EXT NEG SYNC INPUT is provided on the rear panel to couple external sync signals to the Type RM529. This input is a high-impedance loop-through connector and is compensated for 75 -ohm systems. Bridging capacitance is about 20 pF . To select external sync, set the SYNC switch to the EXT position.

## EXT CAL INPUT

The pair of connectors marked EXT CAL INPUT, located on the rear panel, is provided to couple external calibration signals to the instrument. The connectors are connected in parallel to couple the signal in and out of the instrument. To select the external calibration signal, set the INPUT switch to CAL and the CALIBRATOR switch to EXT.

## VIDEO OUTPUT

A single VIDEO OUTPUT connector is provided for driving a picture or line monitor. It is important that the VIDEO OUTPUT connector be terminated into 75 ohms to ensure correct frequency response of the vertical amplifier. When properly terminated, the signal available at this connector is approximately the same amplitude as the signal applied to the Type RM529.

Added to the VIDEO OUTPUT signal is a line intensifying pulse. This pulse is approximately 0.1 volt in amplitude or about $10 \%$ of the VIDEO OUTPUT signal when the input video signal is 1 volt.
The line intensifying pulse is generated only when the DISPLAY switch is set to LINE SELECTOR . $125 \mathrm{H} / \mathrm{CM}$ or LINE SELECTOR . $25 \mathrm{H} / \mathrm{CM}$. The LINE SELECTOR control is used to select the line(s) to be examined in detail on the Type RM529 CRT and the picture monitor. The line intensifying pulse brightens the selected line(s) on the picture monitor for easy identification.

## $J 501$ Connector

A 9-pin female connector ( J 501 ) is provided to connect an external staircase signal to the Type RM529. Fig. 2-3 shows how to connect the signal and remotely actuate relay K385.


To energize relay K385 in instruments below SN 787 it is necessary to only ground pin D of the 9-pin plug connector, i.e., no connection is made to either pins $F$ or $E$ of the 9 -pin connector. To energize part $C$ of the figure it will be necessary to install an external switch between pins $D$ and $K$ of the 9 -pin plug connector.

Fig. 2-3. Front view of 9-pin plug connector. (Tektronix Part No. 134-0049-00) showing jumper wire connections to: (A) Cause relay K385 to be energized whenever the plug is in place. (B) Energize the relay when an external voltage and ground connection are used. (C) Energize the relay when a GE system is connected. (D) Energize the relay when a RCA system is connected.

When K385 is actuated and the DISPLAY switch is set to any position, the sweep length is reduced to about $21 / 2 \mathrm{~cm}(3 \mathrm{~cm}$, SN $100-786$ ). Thus, when a $20-\mathrm{Hz}$ staircase signal of correct amplitude (about 12 volts overall amplitude) is applied through pin C of J501, the display is positioned in accordance with the staircase output from a color processor.

## FIRST-TIME OPERATION

## NOTE

It is necessary to check and adjust the VERT GAIN control (internal adjustment) each time the type of graticule is changed.

To place the instrument in operation for the first time, the following procedure is suggested:

1. Connect the instrument to a source of power specified by the metal tag located near the power connector.
2. Set the front-panel controls as follows:

| POWER and <br> ILLUM | $2 / 3$ clockwise |
| :--- | :--- |
| FOCUS |  |
| INTENSITY | Centered |
|  | VERTICAL |
|  | $2 / 3$ rotation controls |
| INPUT | CAL |
| POSITION | Centered |
| RESPONSE | FLAT |
| VOLTS FULL SCALE | 1.0 |


| VARIABLE (VOLTS | CALIB |
| :--- | :--- |
| FULL SCALE |  |
| DC RESTORER | ON |
| CALIBRATOR | FULL SCALE |

## HORIZONTAL Controls

| POSITION | Centered (five full turns <br> from either end) |
| :--- | :--- |
| DISPLAY | 2 LINE |
| MAG | $\times 1$ |
| LINE SELECTOR | As is |
| FIELD | One or Two |
| SYNC | INT |

3. After the instrument has warmed up for a few minutes, adjust the INTENSITY control for adequate brightness of the square-wave calibrator waveform.
4. Adjust the (VERTICAL) POSITION control to center the display.
5. Adjust the FOCUS control to obtain a sharply defined display.
6. To observe other waveforms, connect a video signal to either the VIDEO INPUTS A or B connector and set the INPUT switch to the appropriate position.

To observe an external calibration waveform, connect the calibration signal from the external source to the EXT CAL connector. Place the INPUT switch to CAL and set the CALIBRATOR switch to EXT.

## CRT Beam Rotator

If the trace does not coincide with the graticule lines, the CRT BEAM ROTATOR (R655) needs to be adjusted. To adjust the control, proceed as follows:

1. Perform steps 1 through 5 in the First-Time Operation procedure.
2. Set the CALIBRATOR switch to .714 F. S., and the DISPLAY switch to 2 FIELD.
3. Adjust the CRT BEAM ROTATOR control so the bottom
trace of the calibrator pulses coincides with the 0 IEEE graticule line. Location of the control can be found by referring to Fig. 6-7 in the Calibration section of this manual.

## GAIN Adjustment

A front-panel GAIN screwdriver adjustment is provided to correct for long-term change in the high-voltage supply. A change in the supply voltage will affect both the vertical and horizontal calibration.


Fig. 2-4. Modification for sync-fip restoration.

To check calibration, check the vertical-amplifier calibration first as follows:

1. Perform steps 1 through 5 in the First-Time Operation procedure.
2. Check that vertical deflection is 140 IEEE units. If the deflection is not 140 IEEE units, adjust the GAIN control to obtain proper deflection.
3. If desired, the horizontal calibration can be checked by performing steps 15 through 18 in the Calibration section of this manual. If the HORIZ GAIN R568 or C481 are adjusted, then steps 17 and 18 should also be performed to fully calibrate the horizontal sweep rates.

## MODIFICATIONS

## Introduction

Four modifications are available to make the Type RM529 satisfy certain studio conditions. The first three can be made in the field, but the last one is more complex and, therefore, is normally done at the factory.

## 1. Changing to Sync-Tip Restoration

To change the Type RM529 circuitry so sync-tip restoration can be used instead of back-porch clamping.
a. Unsolder the yellow-on-white wire (refer to Fig. 2-4) and


Fig. 2-5. Modification to DC couple VIDEO INPUTS A.

R289 from the INPUT switch contact. Leave the wire and resistor leads connected together.
b. Solder a jumper wire between the two contacts on wafer IF of the INPUT switch as shown in Fig. 2-4.

## 2. Changing to DC Input Coupling

Sometimes it is necessary to observe the demodulated output from a television transmitter using a DC-coupled oscilloscope. For this purpose the Type RM529 can be DC coupled, using VIDEO INPUTS A, as follows:
a. Refer to the Vertical Amplifier diagram at the back of this manual and the partial diagram shown in Fig. 2-5.
b. Remove C104 and C204 and solder jumper wires in their place.
c. Disconnect the ground lead that connects from the J201/ J202 connector outer conductor to the INPUT switch contact.
d. Remove R201 from its location on the INPUT switch. Connect R201 between J201/J202 connector outer conductor and ground.
e. Connect one of the removed capacitors between J201/ J202 connector outer conductor and the INPUT switch contact (where one end of R201 was formerly connected).
f. Locate the jumper wire going from J201 connector center conductor to the INPUT switch contact. Disconnect this jumper at J201 and cut off about 2 inches to shorten it. Connect the second capacitor in series between the shortened end of the jumper lead and the center conductor of J201.

## NOTE

After completing this modification, the DC RESTORER is automatically off when the INPUT switch is set to $A$.

## 3. Changing the Sweep Repetition Rate

Since the field rate in some countries differs from the 30 Hz rate used in the United States, the Type RM529 must be modified to operate at the different rate.

To modify the instrument to operate at a longer time per field (slower sweep-repetition rate) than 30 Hz , increase the value of C483. For less time per field (faster sweep-repetition rate), decrease the value of C483 by substituting a smaller value. Refer to the base circuit of Q483 on the Sweep Generator diagram at the back of the manual to locate C483 on the diagram.

## 4. Changing to $4.4-\mathrm{MHz}$ Chroma Response

In countries using a $4.4-\mathrm{MHz}$ color-burst frequency, the Type RM529 must be modified and adjusted to pass this center frequency when the RESPONSE switch is set to HIGH PASS. This modification is much more complex and is, therefore, normally performed in the factory at the request of the purchaser at the time the instrument is ordered.

When the factory modification is made, prepared insert sheets showing the changes are inserted in the manuals accompanying the modified instrument. For this reason, no further information is provided in this section of the manual.

## SECTION 3

## CIRCUIT DESCRIPTION

## General Information

The Type RM529 Waveform Monitor circuits contain both vacuum tubes and transistors. Portions of both the vertical and horizontal systems contain amplifiers with special feedback for gain stability independent of tubes or transistors. Several multivibrators in the trigger and horizontal systems provide precise display triggering. Refer to the block and circuit diagrams at the back of this manual during the fallowing circuit descriptions.

All connectors are rear-panel mounted. Four of the input circuits are 75 -ohm coaxial loop-through; two VIDEO INPUTS, EXT NEG SYNC INPUT and EXT CAL INPUT. The Staircase Input (J501) is a special nine-pin socket (see Staircase Input discussion in Section 2 for mating connector). The VIDEO OUTPUT coaxial jack has a 75 -ohm unbalanced output impedance.

## BLOCK DIAGRAM

The (VERTICAL) INPUT switch selects either of two video signals, or the A signal minus the B signal, or the CALIBRATOR signal, (the calibrator signal can be from an external source) and applies it to the input of the preamplifier. The preamplifier and magnifier supplies the signal to both the response filters and the sync amplifier. The response filter passes the signal on to the output amplifier and to the CRT deflection plates. The output amplifier also supplies the signal to the keyed DC restorer circuit. The sync amplifier supplies an AC-coupled signal to the VIDEO OUTPUT jack (with an open circuit gain of 2, and 75 -ohm loaded gain of 1 referred to the video input), and an AC-coupled signal to the sync separator.

The sync separator regenerates the horizontal sync pulses so their shape and amplifude is always the same. Plus and minus regenerated horizontal sync pulses are available for operating the keyed DC restorer circuit. Minus H pulses are used when displaying video, and plus $H$ pulses are used when displaying the calibrator.

The keyed DC restorer circuit holds the display steady at the video back-porch level or the negative level of the internal calibrator. The circuit operates by controlling the $D C$ level of the preamplifier and magnifier minus input. The video input signals are AC coupled, but the preamplifier and magnifier, response filters, and output amplifier are DC coupled. The DC-restorer circuit virtually eliminates display shift with change in signal amplitude, but response time is slow enough for hum or tilt to be observed.

The sync separator - H signal is used by the trigger selector matrix, when the display is of a line nature (undelayed). The $+H$ signal does not go directly to the trigger selector matrix, but to the vertical sync separator, and then to both the field 1 recognition circuit and the field trigger generator (Q375. Q385). The field trigger generator triggers the sweep gatuig multivibrator via the trigger selector matrix for field displays (undelayed), and triggers the sweep galing multivibrator through the delay generator and trigger selector matrix for delayed field displays.

The sweep gating multivibrator and sweep generator triggering source and sweep rate is set by the front-panel DISPLAY switch. Triggers are received by the sweep gating multivibrator, which allows the sweep generator to run and drives the unblanking amplifier to turn on the CRT beam at the time of the sweep. The unblanking amplifier also sends a brightening pulse to the CRT and the VIDEO OUTPUT jack during delayed line modes. The sweep generator drives both the horizontal amplifier and the staircase amplifier. The staircase amplifier is inserted between the sweep generator and the horizontal amplifier when external control (through J501) switches the sweep generator function to read the red, blue, green (and black-white SN787-up) portions of a color studio camera.
The high voltage supply contains the CRT high-voltage power supply. A portion of the power-supply circuit forms the calibrator signal at the $\simeq 30 \mathrm{kHz}$ rate of the high-voltage oscillator. An external calibrator signal can be substituted for the internal signal.

## VERTICAL AMPLIFIER

The video input circuits of the vertical amplifier are shown in simplified form in Fig. 3-1. The 10 -ohm resistor in Fig. 3-1 A is optional, but necessary in the event there is any AC potential difference between the input coaxial cable and the Type RM529 chassis. It presents any cable-to-chassis signal differentially to the vertical amplifier so the signal will not become part of the display. (Any signal on the outside of the braid of a coaxial cable is also on the center conductor, but with the same polarity. The equal signals are applied to the + and - input terminals, and cancelled by the differential rejection characteristics of the vertical amplifier.) The A-B input of Fig. 3-1B does not use the 10 -ohm resistors because the cables are likely to have the same unwanted information. Since the unwanted information appears on both center conductors, it is presented to the vertical amplifier in differential form and cancelled.

## Operating With the DC Restorer Circuit Off

Operation of the vertical amplifier will be described first with the $D C$ restorer circuit turned off.

The input signals are AC coupled to both the + and - input grids of V113 and through C104 and C204, see 1 megohm refurn to ground. The rest of the vertical amplifier is $D C$ coupled.

Preamplifier. The preamplifier consists of two input cathode followers (V113A and V113B), and two-transistor amplifiers Q114 and Q214. The preamplifier is shown in simplified form in Fig. 3-2A. The cathodes of V113 return to the same constant-current circuit to which the emitters of Q114Q214 return. The VOLIS FULL SCALE control between emitters of Q114 Q214 couples the signal between emitters, causing boih sides of the amplitier to have an output signal when only one inpui receives a signal.

The tubes serve basically as impedance transformers, changing the 1 -megohm input resistance to about 400 ohms to drive


Fig. 3-1. Simplifled vertical amplifier input circuits.
each transistur base. The cathode-return resistors have a value about 20 times the cathode-follower output impedance; theretore, do not attenuate the signal significantly. Each cathode follower passes about $93 \%$ of the input signal to the following transistor base.

The emitter resistors would normally cause considerable dege nerative effect, and would thus keep the stage gain very low. However, the VOLTS FULL SCALE resistance between the two emitters also couples the signal from one side to we other. Fig. 3-2B shows a simplified concept of the VOLTS FULL SCALE control signal path. If, in this theoretical circuit, the IOLTS FULL SCALE resistor were made zero ohms, the input signal to one transistor base would divide equally between the two halves of the stage. Fig. 3-2B shows the internal emitter resistance in series. Thus, VOLTS FULL SCALE equal to zero ohms degeneration on one side of the amplifier is the emitter resistance of the other side. This causes both sides of the amplifier to have gain. The emitter return


Fig. 3-2. Simplified circuif (5N 1600-up). Some circuit values are different in earlier SN instruments.
resistors are many times greater than the emitter internal resistance, and, therefore, do not attenuate the signal when the VOLTS FULL SCALE resistance is low. The actual minimum VOLTS FULL SCALE resistance is about 590 to 600 ohms between emitters setting the push-pull output signal equal to about 2 times the single-ended input signal.
A typical single input signal will cause the following action (assume the VOLTS FULL SCALE resistance to be 600 ohms): Q114 base is driven in the positive direction 1 volt and its emitter follows it nearly 1 volt. The $600-\mathrm{ohm}$ resistor allows the emitter current to increase and the emitter voltage to follow the base voltage nearly one volt. The increased forward bias of Q114 is about 0.02 volt. The signal current is essentially 1.66 mA greater than the static current. The only source for the signal current is the emitter of Q214; therefore, both transistors receive the same amount of signal current (but of opposite polarity) for a single input signal. The result is that both collector resistors have a 1.66 mA signal current. The collector of Q114 goes negative, and the collector of Q214 goes positive producing a push-pull output signal about 2.2
volts peak to peak. Since the collector load resistors have equal and opposite current changes, the voltage at their center does not change. A common-mode signal reaching the preamplifier would change the voltage at the junction of the collector load resistors, and degrade the common-mode rejection of the amplifier except for presence of the constant current stage.
The high-frequency gain of the preamplifier is adjusted to equal the low-frequency gain by making the RC time constant of the emitter circuit equal to the RC time constant of the collector circuit. The cathode followers' output impedance allows the Miller capacitance of the transistors to affect the highfrequency response. To minimize the Miller effect, the transistor stage is neutralized by $\mathrm{Cl13}$ and C 213 . The variable capacitors ( Cl 18 B and $\mathrm{Cl18C}$ ) across the VOLTS FULL SCALE resistors R118B and R118C permit the preamplifier frequency response to be properly adjusted. There is no need for a variable capacitor across R118A, due to wiring stray capacitance.

In the event of minor differences in bias of the input cathode followers, (and the resultant output voltage difference) the DC BAL control ( R 115 ) is set to create a compensating change in current in the cathode return circuit. The DC BAL control final setting is correct if the trace does not shift when changing the VOLTS FULL SCALE switch position (with the DC RESTORER OFF).

The high impedance of the preamplifier transistor collectors allows the output voltage to be varied a slight amount without significant change in current. The VAR DC BAL control slightly alters the voltage balance of the preamplifier output to allow the output amplifier VARIABLE control (between emitters of Q144-Q244) to be adjusted without shifting the trace position.

Constant Current Stage. The constant current stage cancels any push-pull output from the preamplifier in the event both input leads receive equal amplitude-equal polarity signals. The circuit causes the voltage of the constant current leads of Fig. 3-2 to shift and follow any common-mode input voltages. (The high collector resistance of Q114 and Q214 prevents any change in the preamplifier output voltage.) Fig. 3-3 shows simplified connections between the constant current stage and the preamplifier. Assume both input leads to be positive. The result is that both collector-load resistors receive an increase in current. The increased current pulls down on R121. R122 divides the change to the base of Q124. Q124 base goes negative and causes its collector to go positive on amount equal to the original common-mode signal. This cancels its effect and returns the current in the collec-tor-load resistors to the original value. The input cathode followers' negative supply is the same as Q114-Q214 negative supply, to assure signal linearity in the event of common-mode signal cancellation by Q124.

The principal reason for keeping the common-mode currents out of the preamplifier is that even though the currents may be equal, the collector load resistors may not be precisely equal, and equal currents would generate unequal output voltages. The circuit does stop the preamplifier output from moving positive or negative with common-mode signals.

Response Filters. The frequency response of the overall monitor is altered for special purposes by the RESPONSE switch and its filters.

The FLAT position of the RESPONSE switch gives the widest


Fig. 3-3. Simplified constant current stage connections on preamplifier.
bandwidth, with a direct connection from the preamplifier to the output amplifier.

The IEEE position of the RESPONSE switch inserts components that cause the overall monitor bandwidth to be low-pass to agree with 1958 Standard 23S-1.

The LOW PASS position of the RESPONSE switch inserts components that alter the overall response so that it is about $12-\mathrm{dB}$ down at 500 kHz .

The HIGH PASS position of the RESPONSE switch inserts a critically-coupled transformer between the preamplifier and the output amplifier, making the overall monitor bandpass about 800 kHz centered at 3.58 MHz . The DC level at the input of the output amplifier is maintained by connecting the center of the primary and secondary windings together at a cold RF point.

Output Amplifier. The output amplifier includes two sets of push-pull amplifiers, each with variable emitter coupling to vary the gain. The first amplifier is Q144-Q154 and Q244Q254. The second amplifier is driven by the first, and is a combination of transistors and tubes giving a large voltage output swing.

The driver portion of the amplifier has negative feedback from the collector of Q154 to the emitter of Q144 (and from Q254 to Q244). The negative feedback makes the input impedance at the base of Q1 44 very high and the output impedance at the collector of Q154 quite low. The high input impedance prevents loading of the response filters. The low, output impedance is needed to drive the base of Q164 (and Q264). R154 is the negative feedback path and is also the collector load resistor for Q154 (see Fig. 3-4).

The VARIABLE gain control (concentric with the VOLTS FULL SCALE switch) varies the emitter-to-ground degeneration between Q144 and Q244 to vary the overall vertical amplifier gain by a $2.5: 1$ ratio. The VARIABLE control mechanically switches R241 into the circuit in the CALIB position, and out of the circuit (SW240 closed) when not in the CALIB position. If the VARIABLE control is counterclockwise at lower than cali-


Fig. 3-4. Simpliffed one-half oulput driver stage.
brated gain, clockwise rotation can increase the monitor gain so it is greater than normal. Then, as the clockwise end of rotation is reached and the control is rotated to snap into the CALIB position, the overall gain drops about $70 \%$ as R241 is switched into the circuit. At the same time a second part of SW240 closes and turns on the front-panel CALIB neon lamp.

The output driver signal is coupled to the base of Q164 (Q264) of the output cascode amplifier. The combination of a transistor (supplying cathode drive) and a tube not only gives stable gain but also gives the wide voltage output swing. This amount of swing can only be obtained by a cascode amplifier consisting of a tube and transistor. The output cascode stage also has emitter-to-emitter degeneration used to adjust the overall vertical amplifier gain to match the CRT deflection factor. The emitter circuit also contains the HF COMP capacitors that permit the output stage high-frequency gain to be adjusted a bit higher than the low-frequency gain. This adjustment helps make the bandpass correct for the FLAT position of the RESPONSE switch.

While reading the following description of the cascode stage operation, keep in mind that (1) a transistor's emitter follows its base, just as a tube's cathode follows its grid-if the return circuit is a higher impedance than the internal emitter or cathode impedance, and (2) a transistor's collector has quite a high impedance, as high as the plate impedance of some triode tubes.

A signal that drives the base of Q164 in the positive direction causes several simultaneous circuit changes. The emitter voltage of Q164 follows the base voltage, with emitter voltage change about 2 percent less than base voltage change, offset by normal silicon transistor bias. The positive swing of Q164 base drives the grid voltage of V164 positive the same amount, and the cathode of V164 follows, lagging its grid about 20 percent. The 20 percent positive bias occurring in V164 as a result of cathode-follower action increases plate current, and the consequent plate current increase causes the output plate voltage to drop in the negative direction an amount determined by R162 and Ohm's Law.

Push-pull signals that drive the bases of Q164-Q264 drive the two halves of the output stages equally. (The degenerative action of the resistors between emitters is one half what it would be if only one base received a signall. The signal voltages at Q164-Q264 bases cause plate-current changes of V164 and V264 to be about 3.3 mA per centimeter of spot deflection each, producing a push-pull voltage output to the CRT deflection plates of about 20 volts per centimeter. The peaking coils in each plate circuit compensate for deflection-plate capacitance, and aid in obtaining flat frequency response of the vertical amplifier.

Positioning the CRT display (with DC RESTORER OFF) is by current injection into the emitter circuits of Q144-Q244 through R143 and R243. The POSITION control (R245) sends current toward the cascode output stage bases, but this current does not affect the display position so long as the DC restorer is off. Voltage changes at the bases of Q164 and Q264 do not significantly affect the positioning circuit because of two germanium diodes D271-D272, which limit the voltage difference between R149-R249 junctions with R148-R248. The two diodes appear on the DC restorer diagram.

## Operation With DC RESTORER ON

The $D C$ restorer circuit provides an automatic $D C$ positioning voltage to the -input grid of V113B. The source of DC positioning voltage is the signal in the base circuit of the output cascode stage. The signal is usually composite video (sometimes it is the calibrator). The DC restorer circuit positions the CRT display firmly around the level of the composite video horizontal sync pulse back porch. Because of these facts, the restorer must look at the video only at the correct time. The DC restorer circuit is keyed by the horizontal trigger system to sample the video back porch for about $0.4 \mu \mathrm{~s}$, and remember the DC level until the next horizontal sync pulse occurs.

When the DC restorer circuit is on, a current injection path through R148 and R248 into the input of the DC restorer Comparator permits the POSITION control to operate. The positioning current changes the DC level of the composite video at the point where it is looked at by the restorer.

Video Output Amplifier. The video output amplifier receives its signal from the emitter of Q114. The input impedance of Q174 is greater than $50 \mathrm{k} \Omega$ due to the large amount of emitter degeneration, which loads Q114 lightly. Q174 produces an inverted current drive to the feedback amplifier Q184. Q193 of essentially 1 mA per 1 volt. The emitter impedance of Q174 is R172-R173 in parallel, or $1.06 \mathrm{k} \Omega$. Since the collector current of Q174 changes linearly with base-voltage drive, the signal-source resistance of Q184 base is $1.05 \mathrm{k} \Omega$. Then, the voltage gain of Q184-Q193 (set by the feedback resistance divided by the input resistance) is $2.2 \mathrm{k} \Omega / 1.06 \mathrm{k} \Omega$ or about 2.06. Assuming $3 \%$ signal loss in the preamplifier, the gain from input to Q193 collector is 2. R198 in series with a 75ohm load makes the overall gain 1. The feedback (R192) makes the video output amplifier have a very low output impedance. Thus, the amplifier is matched to the output coaxial line by inserting a series 75 -ohm resistor (R198). The reactance of C 198 is so low at the frequencies passed by the circuit that it does not increase the output resistance over that of R198. R199 assures that C198 is properly charged.

The video output amplifier also serves as an internal trigger amplifier. The output lead to the sync clamping amplifier (diagrammed with the sync separator) rests at -5 volts.


Fig. 3-5. Simplified keyed DC Restorer circuit.

The sweep generator applies a positive pulse to the video output jack when operating in a line selector mode. The intensifying pulse amplitude is about 0.2 volt at the video output jack ( 0.1 volt when loaded with 75 ohms). The value of the pulse is set by current from a +100 -volt pulse in the sweep generator unblanking circuit applied through R476 diagrammed near the unblanking amplifier with the sweep generator to the 75 -ohm output resistor R198. The very low output impedance of the video output amplifier prevents the intensifying pulse from disturbing the internal triggering signal.

## Keyed DC Restorer

The keyed DC Restorer circuit includes the DC restorer Comparator, the blocking oscillator, and the restorer cathode follower. Voltages and waveforms on the DC restorer diagram were taken with the $D C$ restorer circuit on. The simplified diagrams of Fig. 3-5, 3-7 and 3-8, and waveforms of Fig. 3-6 will help during the following discussion of the DC restorer circuit operation.

The DC restorer comparator is a dual-input single output amplifier that amplifies a small part of the composite video which is normally near the CRT screen center. The signal peaks are limited by parallel back-to-back germanium diodes D271D272 (see Fig. 3-5). One of the two diodes conducts whenever the voltage across them exceeds 0.2 to 0.3 volt. When the diodes are not conducting, the comparator bases are fed pushpull signals from the two bases of the output amplifier cascode stages. When a diode is conducting, the two bases of the comparator amplifier are essentially shorted together, and there is no gain. When the signal at the base of Q274 goes negative (and the signal at the base of Q284 goes positive) D271 conducts. The opposite polarity signal causes D272 to conduct. The peak-to-peak signal input to the comparator is, therefore, limited to about 0.45 volt. The comparator output signal is typically 4.2 volts peak-to-peak at the emitter of
the emitter follower (Q273). The comparator functions in the same manner as the differential preamplifier previously described, except there is just one output lead. Fig. 3-6 shows the signal as it enters the memory gate. The other waveforms of Fig. 3-6 are discussed with the blocking oscillator below.

Blocking Oscillator. The blocking oscillator is normally biased to cutoff by current through R282 and D282. A negative pulse applied to the base of Q280 will cause it to conduct and go through one cycle of oscillation. The negative pulse arrives at the base of Q280 through a diode switching network from the sync regenerator (diagrammed with the sync separator).
Assume the vertical INPUT switch is at A, as shown in Fig. 3-7. The diode switching circuit then reverse biases D285 about 45 volts and reverse biases D286 about 1 volt. Regenerated horizontal sync pulses arriving at C285 and C286 have a peak-


Fig. 3-6. Time-coincident waveforms of keyed DC Restorer.


Fig. 3-7. Operation of Diode switch feeding Blocking Oscillator.
to-peak amplitude of about 8 volts. Thus, the -H pulse will not cause D285 to conduct, but the +H pulse will cause D286 to conduct at the end of the pulse as it goes negative. C286 charges almost the full 8 volts of the +H pulse rise, and then causes the cathode of D286 to fall about 7 volts. The base of Q280 does not fall as much as 8 volts because of the low base-to-emitter impedance at the time of turn on.

The blocking oscillator turns on at the time the composite video horizontal sync pulse ends and starts toward the backporch level. The back-porch level occurs about $0.25 \mu$ s later, so the blocking oscillator does not sample the video at the time of turn-on. As Q280 conducts, the L/R time constant of the collector circuit inductance and resistance keeps Q280 conducting for about $0.6 \mu$ s before the base drive decays. As Q280 regenerative base turn-on drive is stopped, the collector current drops rapidly. Dropping collector current is transformercoupled back to the base of Q280 as a fast turn-off signal. The collector voltage waveform is shown in Fig. 3-6. Changing collector current is also transformer-coupled to the tapped secondary that drives the memory gate.

Memory Gate. The memory gate consists of the centertapped secondary of T280 with its DC level set by the emitter follower, two parallel RC circuits and two silicon diodes. As Q280 is turned on, the secondary voltage of T280 reverse biases D292 and D293 and no current flows. As Q280 stops conducting, the secondary of T280 drives D292 and D293 into conduction and at the same time charges both C292 and C293 to about 7 volts. (The energy for charging the two capacitors comes from the core of T280.) D292 and D293 are computer diodes with equal forward drop at the time they conduct, making the voltage at their junction with C294 equal to the voltage at the center of T280 secondary. Thus, during the backswing time of T280, the voltage at the center of T280 secondary appears at C294. The backswing lasts for about
$0.4 \mu \mathrm{~s}$, which is plenty of time to fully charge C294 to the voltage of the emitter follower. During each backswing, C292 and C293 are recharged to replace the small amount of voltage discharged by the resistors R292 and R293. The time constant of the two RC circuits is 1 ms each, many times longer than the $63.5 \mu \mathrm{~s}$ between sampling times.

Memory Circuit. The memory circuit includes the memory capacitor C294 and the grid of V293A. Since D292-D293 are silicon diodes with very high reverse leakage, the memory capacitor charge is essentially constant between samples.

The four waveforms of Fig. 3-6 (taken with a four-channel oscilloscope) show the time-coincidence of the DC restorer circuit. Note that some of the color burst is seen by the memory gate and memory capacitor. The reactance of the memory capacitor is about 440 ohms at 3.58 MHz ; and the sampling diodes are turned on hard by T280 secondary so there is no color-burst rectification. Thus, the DC restorer circuit acts upon the average voltage of the color burst, keeping the display at the same stable position with or without the color burst.

Restorer Cathode Follower. The restorer cathode follower acts as an impedance transformer that couples the sampled and stored voltage into the vertical amplifier minus input grid. The two resistors, R298 and R299, offset the DC level of V293A cathode to the correct value for the minus input, setting the minus grid to essentially ground voltage when the system is correctiy balanced.

Restorer Operation on Calibrator Signal. This mode of restorer operation uses the -H regenerated horizontal sync pulse to fire the blocking oscillator. The -H signal starts negative at the same time calibrator signal goes negative. The blocking oscillator fires as the -H signal goes negative, causing the DC restorer circuit to sample the signal voltage about $0.88 \mu \mathrm{~s}$ after the beginning of the calibrator negative


Fig. 3-8. Sampling and memory portions of DC Restorer circuit.
half-cycle. Thus, the display is stabilized at the bottom of the calibrator signal and held in the same position as the back porch.

## Sync Separator

The sync separator processes composite video so the sweep generator is triggered properly for the various modes of the DISPLAY switch.

The input to the sync clamping amplifier can be from one of two sources; the internal trigger signal from the video output amplifier or an external sync input, usually composite video. The selection of source is made by the SYNC switch. Source switching is by diodes, and the actual SYNC switch is isolated from the video leads by R305. When the SYNC switch is set to INT, D301 is back biased and D304 is forward biased. The signal passes through forward-biased D304 into the grid of V293B. When the SYNC switch is set to EXT, D304 is back biased and D301 is forward biased, so the signal passes through D301. The internal-external sync selection can be made from the front panel for all vertical input modes except when viewing the calibrator signal. When the vertical INPUT switch is at CAL, the sync input is automatically switched over to internal.

## Sync Clamping

The sync clamping amplifier has two feedback loops. One is a normal type consisting of R315, with the gain of Q314 set by R315 and the transconductance of V293B.

A feedback amplifier of the type in the sync clamping amplifier, shown in Fig. 3-9, has low input impedance called virtual
ground, and a low output impedance. The virtual ground is easy to visualize when we find equal and opposite currents in the input resistor $\left(R_{i}\right)$ and the feedback resistor $\left(R_{f}\right)$. Assume $R_{f}$ of Fig. 3-9 to be $22 \mathrm{k} \Omega$ and $R_{i}$ to also be $22 \mathrm{k} \Omega$. A one-volt IN signal will cause 0.045 mA to flow in $\mathrm{R}_{\mathrm{i}}$. The transistor collector will change voltage level (also 1 volt) until an opposite 0.045 mA flows in $\mathrm{R}_{\mathrm{f}}$ at which time the input signal is balanced, so none is left for the base. When $R_{i}=R_{f}$ the voltage gain is unity.

V293B cathode output impedance is approximately equal to $1 / \mathrm{Gm}$ or typically $1 / 0.001 \mathrm{~S}^{1}=1000 \Omega$. (Normal range of


Fig. 3-9. Simplifed Feedback amplifier.
output resistance between tubes will be from about 600 to $1200 \Omega$ ). The cathode-follower output resistance can be considered directly in series with the input grid for calculating signal current to the base of Q314. Thus, the typical voltage gain of Q314 is $\frac{22 \mathrm{k} \Omega}{1 \mathrm{k} \Omega}=22$.

A second feedback loop around the Sync Clamping Amplifier is composed of R317, R318 and C317. This loop acts as a DC restorer for signals into the rest of the triggering circuitry. Negative-going composite video at the grid of V293B causes the collector of Q314 to go positive. As each negative-going sync tip occurs, C304 charges slightly positive, then as the collector voltage of Q314 falls, C317 gains a negative charge that is the average of the input signal amplitude. C304 thus receives a charge as each sync tip occurs, then discharges through R317 to C317 at all other times. The discharge current for C304 is approximately proportional to video level. The effect of the action just described is that C304 acts as a DC restorer for the Sync Clamping Amplifier for a wide range of signal levels. Restorer action thus holds the Sync Clamping Amplifier output (at the sync pulse tips) at a stable level of about -0.5 volt.

Any large noise pulses riding on the negative-going composite video will cause the collector of Q314 to go positive enough to back bias D318; while at the same time, the large negative going pulse at the grid of V293B will cause D317 to be forward biased. Forward biased D317 will now cause the charge rate of C304 to be limited by R319.

Video stripping occurs in the Sync Clamping Amplifier as the input signal goes positive, because available Q314 collector current through R314 is all taken by the feedback resistor R315. As V293B cathode applies positive-signal turnoff current to the base of Q314, Q314 collector goes negative until the current in R315 equals the current in from V293B cathode. At that point, the collector voltage stops going negative and the remaining positive signal input to V293B grid is not amplified. Thus, the DC-restored sync tips out of the Sync Clamping Amplifier have a maximum peak amplitude of about 13 volts with the video information removed from large signals.

## Sync Regenerator

The Sync Regenerator is a Schmitt multivibrator whose operation is bistable due to the DC coupled input signal from Q314 collector. Q335 conducts when the base of Q325 is near ground, and Q325 conducts when the input is more negative than about -4 volts. Output signals are each about 8 or 9 volts peak to peak. The TRIG MULTI BIAS control is adjusted for proper triggering on low-level video sync signals in case the Sync Regenerator input signal is less than normal.

Assume Q325 is conducting. As the input signal goes positive, current in Q325 is reduced, allowing its emitter to go positive and its collector to go negative. Q325 emitter is coupled to Q335 emitter and Q325 collector is coupled to Q335 base. Initially the back bias at the base-emitter junction of Q335 prevented it from conducting. As Q335 bias reaches the point of conduction, regenerative action flips the conduction from Q325 to Q335 rapidly. As long as a sync tip holds the base of Q325 up near ground, Q335 will conduct. As Q325 base starts negative, Q325 begins to con-
duct and a second regenerative action switches Q335 off and Q325 on. The regenerative path is between the emitters of Q325-Q335 and from the collector of Q325 to the base of Q335.

Both the +H and -H signals are available for the keyed DC Restorer circuit previously described, and for the rest of the triggering circuitry.

## FIELD SELECTOR

The Field Selector circuit includes the Vertical Sync Separator, the Field 1 Recognition circuit and the Field Trigger Generator.

Vertical Sync Separator. The Vertical Sync Separator is primarily a differentiator and an amplifier biased off about 3 volts. The differentiator, C341-R341, shifts the signal output DC level depending on the pulse duty cycle. If the incoming square-wave signal negative peaks are of longer duration than the positive peaks, the output will be more positive than negative. Likewise, if the incoming signal positive peaks are of longer duration that the negative peaks (vertical sync), the output will be more negative than positive. During the time C341 receives only regenerated horizontal sync pulses, the signal at the base of 344 shifts between about 2 volts negative and 6.5 volts positive and Q344 does not conduct. As the vertical sync group occurs, the signal at the base of Q344 shifts to between about 6 volts negative and 2.5 volts positive, turning Q344 on hard each time the signal goes below about -3.5 volts.

Both the Field 1 Recognition circuit and the Field Trigger Generator require a single pulse, the first of the vertical sync pulses. The parallel combination of R346-D346 and the capacitance of C347 allow only the first vertical pulse to pass through. As the collector of Q344 rises positive 20 volts, D346 passes the whole pulse to C347 (and C351). C347 charges to more than half the peak voltage of the first pulse. The very high reverse resistance of D346 and the resistance of R346 let C347 keep its charge. The second vertical sync pulse is, thus, not able to be coupled on since the cathode of D346 is already several volts more positive than it was before the arrival of the first pulse. (Some of the second pulse gets through the coupling capacitors, but does not affect the following circuits.) R346 discharges C347 (and C351) before the next vertical pulse arrives.

Field 1 Recognition. The field 1 recognition circuit is a one-shot multivibrator (mono-stable) with two input paths. The single vertical sync pulse that arrives through C351 to the base of Q355 turns Q355 on and Q365 off. The switching action is regenerative due to emitter coupling, and coupling from Q355 collector to Q365 base. C360 was initially charged to about 13 volts. As Q355 collector falls, the base of Q365 is taken about 11 volts negative. The FIELD 1 SYNC control (R360), in series with R361, starts the base of Q365 back toward ground, discharging C360. As the voltage at the base of Q365 nears a value that would cause Q365 to turn on, a positive pulse coupled to the base through C361 will turn it on and reset the multi. The time constant of C360 and R360R361 is set such that the multi is reverted at the end of the last vertical equalizer pulse. (The waveform near the collector of Q365 on the diagram at the back of this manual shows capacitively-coupled pulses that pass through C361 and the
base-to-collector capacitance of Q365. This is normal and does not indicate Q365 to be defective). As Q365 collector goes negative at the end of the last equalizing pulse, C364 and R368 form a negative pulse that ramps up for a period of 50 to $55 \mu \mathrm{~s}$. C370 couples differentiated -..H pulses and adds them to the ramp at the junction of R369 and D370. If a horizontal pulse occurs during the time the ramp is running up, the output through D370 is more negative than at any other time. A two-field interlace horizontal sync pulse occurs in the middle of every other ramp.

All the other negative pulses at the junction of R369-D370 charge C371 (through R372) to an essentially stable DC voltage (R371 does not appreciably discharge C371 between puises). As a field 2 occurs, the more negative pulse that coincides with the field 1 recognition ramp is coupled through D371 to the base of Q375, flipping the field trigger generator so that Q375 conducts.

Field Trigger Generator. The field trigger generator is a bistable multivibrator that changes state each time a positive pulse arrives through C347 from the vertical sync separator. The triggering pulse is coupled to the bases of Q375Q385 through diodes D374-D384 and the RC networks of C375-C385. The positive-polarity pulse turns off the conducting transistor regardless of which is conducting. The pulses arrive at a 60 -hertz output rate, causing the field trigger generator to have a 30 -hertz output rate at each collector.

If Q375 is off when the negative-going field 1 signal from the field 1 recognition circuit arrives at the base of Q375, Q375 will be turned on. A positive signal from the sync separator to each collector at the start of each field, and a negative pulse to Q375 base at each field 1 assures that the field trigger generator output is always related to field 1 and field 2 of the composite video. The collector of Q375 always goes positive (toward ground) at the beginning of each field 1. The collector of Q385 always goes positive at the beginning of each field 2.

Field shift switching is the selection of the correct field trigger generator output pulse by a dual input single output diode switch. Positive-going trigger pulses are needed by the sweep generator and by the delay generator. Thus, to trigger on a field 1, the field shift switch causes Q375 collector signal to be coupled on, and for a field 2, Q385 collector signal to be coupled on.

Assume a field 2 trigger is selected. The CRT display will start the sweep on a field 2 and show the field 1 at center screen. The FIELD switch (set at TWO) applies a negative bias to D377 anode, assuring that it cannot conduct the signal from Q375 collector to the following circuits. D387 will pass the positive portion of the differentiated Q385 collector signal. Differentiation of Q385 collector signal is by C384 and the parallel resistance of R388 and R379-R389. As Q385 collector rises, C384 couples the first of the full step through to D387 and the rest of the circuit. C384 soon charges, dropping the voltage at the cathode of D387 back to ground level. As Q385 collector falls, D387 disconnects the signal from the rest of the circuit and R388 recharges C384 for the next positive pulse. The contacts of K385 are described with the staircase amplifier later in this section.

## Line Selector (SN 1910-up)

The line selector circuit includes the delay generator and the line pickoff circuit. The selected line-trigger pulses occur once each field, at an adjustable time interval after each vertical sync pulse.

Delay Generator. The delay generator is normally biased so Q405 is conducting and Q415 is cut off. Q415 collector rests at +24 volts because of the voltage divider R414, R415, R418 and Q420. (The LINE SELECTOR variable control current from -25 volts through R428 to the junction of R419-C419 will not take the junction significantly below ground, because a 24 -volt drop exists across R415 and another of up to 25 volts across R428). Q405 collector rests at -1 volt, holding Q415 base of about -2.6 volts by the drop across R405-R406. Q414 is saturated (collector voltage pulled down very near emitter voltage) due to base current through R417. Thus, the emitter and collector current of Q405 is set by R419 and the -24 volts at Q414 collector. The delay generator will remain in this condition until a positive trigger pulse arrives at the base of Q415.

As a positive pulse turns on Q415, the current through Q414R419 shifts to Q415, and Q405 turns off. As Q415 collector starts negative, C417 couples the voltage change into the base of Q414 in a direction to reduce its collector current. As the base of Q414 is taken far enough negative to almost turn off its collector current, the drop in Q415 collector voltage is nearly eliminated until the current through R417 discharges C417. As C417 discharges a bit, the base voltage of Q414 turns on a bit more current. The current of Q414 is also the current in Q415, which again pulls down on C417. The result of the feed-back just described is that C417 is discharged in a very linear manner by current through R417. The voltage at the junction of C417-R417 remains essentially constant while the collector of Q415 pulls the other side of C417 negative at a rate set by the current through R4I7.

When the collector voltage of Q415 reaches ground level and stops going negative, current through R417 raises the base voltage of Q414 and increases its current. Increased current in Q414 pulls both Q415 emitter and base elements negative, allowing the collector to go negative also. The common emitter-to-emitter lead of Q405-Q415 drops negative until Q405 again tuins on. The collector voltage of Q405 drops and quickly turns Q415 off, letting its collector voltage rise in the positive direction as R414 charges C 417 to its original state. (C414 cancels Q415 initial negative collector surge caused by shifting Q414 current from about 5 mA in Q405 to about 0.27 mA in Q415. Without C414, the collector voltage of Q415 would drop sharply negative at the time Q415 was triggered into conduction.) C417 charging current is limited only by R414 since the negative end of the capacitor is tied to - 25 volts through Q414 base-emitter junction.

## Line Selector (SN 100-1909)

The line selector circuit includes the delay generator and the line pickoff circuit (blocking oscillator). The selected linetrigger pulses occur once each field, an adjustable amount of time after each vertical sync pulse.

Delay Generator. The delay generator is normally biased so Q405 is conducting and Q415 is cut off. Q415 collector rests
at +24 volts because of the voltage divider R414, R415-D415. The LINE SELECTOR variable control current from - 25 volts through R428 to the junction of R415-D415 will not take the junction significantly below ground because a 24 volt drop exists across R415 and another of up to 25 volts across R428.) Q405 collector rests at -1 volt, holding Q415 base at about -2.6 volts by R405-R406. Q414 is saturated (collector voltage pulled down very near emitted voltage) due to base current through R417. Thus the emitter and collector current of Q405 is set by R419 and the -24 volts at Q414 collector. The delay generator will remain in this condition until a positive trigger pulse arrives at the base of Q415.

As a positive pulse furns on Q415, the current through Q414R419 shifts to Q415 and Q405 turns off. As Q415 collector starts negative, C417 couples the voltage change into the base of Q414 in a direction to reduce its collector current. As the base of Q414 is taken far enough negative to almost turn off its collector current, the drop in Q415 collector voltage is nearly eliminated until the current through R417 discharges C417. As C417 discharges a bit, the base voltage of Q414 turns on a bit more current. The current of Q414 is also the current in Q415 which again pulls down on C417. The result of the feed-back just described is that C417 is discharged very linearly by current through R417. The voltage at the junction of C417-R417 pulls the other side of C417 negative at a rate set by the current of R417.

When the collector voltage of Q415 reaches ground level and stops going negative, current through R417 raises the base voltage of Q414 and increases its current. Increased current in Q414 pulls both Q415 emitter and base elements negative, allowing the collector to go negative also. The common emit-ter-to-emitter lead of Q405-Q415 drops negative until Q405 again turns on. The collector voltage of Q405 drops and quickly turns Q415 off, letting its collector voltage rise in the positive direction as R414 charges C417 to its original state. (C414 cancels Q415 initial negative collector surge caused by shifting Q414 current from about 5 mA in Q405 to about 0.27 mA in Q415. Without C414, the collector voltage of Q415 would drop sharply negative at the time Q415 was triggered into conduction.) C417 charging current is limited only by R414 since the capacitors negative end is tied to -25 volts through Q414 base-emitter junction.

The blocking oscillator section of the delay generator and its signals are shown in Fig. 3-10. The knee of waveform C where D415 stops conducting is adjustable by the LINE SELEC. TOR variable control. The knee is the point at which R415R428 voltage division of the sawtooth output waveform causes the voltage at the blocking oscillator input to start negative. Negative differentiated horizontal sync pulses (waveform B, with their positive peaks removed by D427) are added to the sawtooth so that the blocking oscillator will fire at the time of a horizontal sync pulse. As the base of Q420 is pulsed far enough negative to cause it to conduct, transformer regenerative feedback turns it on hard. The collector is held stable for a short period of time by C424, causing the emitter to go sharply negative until it is more negative than the base. This turns off the drive and T420 aids in quickly turning off the pulse. R420 helps dissipate base winding inductive energy and D420 helps dissipate emitter winding energy so a second ringing type pulse is not generated. The negative emitter pulse is coupled to the trigger selector switch through R436-C436.


Fig. 3-10. Blocking oscillator section of the Delay Generator (SN 10019091 and waveforms.

## Sweep Generator (SN 2997-up)

The sweep generator is a triggered sweep system for all positions of the DISPLAY switch except the 2 FIELD position, at which it is a recurring synchronized sweep. Positive fieldtrigger pulses prevent the sweep from operating in 2 FIELD and both LINE SELECTOR positions (LINE SELECTOR set to a line, lines 16 through 21). Negative line-trigger or selected line pulses start the sweep in all other modes of operation. The sweep rate at 2 LINE permits viewing the interlacing of the color burst. The sweep rate at $0.125 \mathrm{H} / \mathrm{cm}$ permits a look at


Fig. 3-11. Simplified Sweep Generator.
every other horizontal line displaying a non-interlaced color burst. Refer to the simplified sweep generator diagram of Fig. 3-11 and the complete diagram at the back of this manual during the following circuit description.

## Trigger Selector Matrix

Selection of recurrent negative line trigger pulses at the beginning of each horizontal line, or of selected line pulses, is made in a diode switching network of the DISPLAY switch.

When the DISPLAY switch is at a LINE SELECTOR position and the LINE SELECTOR switch is set to a line (lines 16 through 21) position, both D430 and D436 are reverse biased so that no negative triggers get to the sweep gating multi. At the same time, D452 is forward biased through R450 so positive field triggers are available to the sweep gating multi.

When the DISPLAY switch is at its LINE SELECTOR positions and the LINE SELECTOR switch is set to VARIABLE, the cathode of D430 is raised about 9.5 volts positive and the diode is reverse biased so it cannot conduct negative line triggers to the sweep gating multi. D436 does conduct negative selected line pulses to the sweep gating multi.

When the DISPLAY switch is at 2 FIELD, both D430 and D436 are reverse biased, so that no negative triggers get to the sweep gating multi. At the same time, D452 is forward biased through R450 so positive field triggers are available to the sweep gating multi.

## Sweep Gating Multi

The sweep generator is operated in two basically different modes of operation as suggested earlier. The sweep gating
multi operation is altered from a triggered system for 2 LINE, $.25 \mathrm{H} / \mathrm{CM}, .125 \mathrm{H} / \mathrm{CM}$ and both LINE SELECTOR positions of the DISPLAY switch with the LINE SELECTOR switch set to VARIABLE to a stopped-sweep system for both LINE SELEC. TOR positions of the DISPLAY switch when LINE SELECTOR switch is set to a line (lines 16 through 21), and to a free-running stopped-sweep systems for 2 FIELD displays.

2 LINE DISPLAY. (Vertical INPUT switch at A, DISPLAY switch at 2 LINE.) The sweep generator is held in one state by the sweep gating multi until the arrival of a negative trigger pulse. Before receipt of a trigger pulse, the following conditions exist:
a. Q455 is conducting, Q465 is in a state of non-conduction.
b. Both disconnect diodes are conducting. D482 is applying positive turn-on current from R468 to the miller runup input base, while D481 is limiting the turn-on current, as the collector of Q481 pulls down and takes some of the current flow from R468.
c. Q481 collector voltage is at about +1 volt, so that essentially no current is delivered through R520 (see horizontal amplifier diagram) to the horizontal amplifier.
d. The unblanking amplifier output is near ground, turning off the CRT beam.
e. The CRT horizontal deflection plates hold the blanked beam at the left side of the CRT (depending upon the setting of the POSITION controll.

Q455 is held in conduction by current through the series resistors R464-R465 and D466, limited by R470 current into the base-emitter junction of Q474. The base turn-on current to

Q455 is enough to saturate it; however, D455 bypasses some of the intended base current when the collector voltage drops slightly below D466 anode voltage. This prevents the transistor from saturating. (If Q455 were to saturate, the base-emitter junction would hold so many carriers that the transistor could not be turned off quickly.) The fact that Q455 collector voltage is near ground assures that no current reaches the base of Q465, and Q465 remains cut off.

As the negative-going line trigger pulse arrives at the base of Q455 through C452, Q455 is turned off. The voltage rise at the collector of Q455 is coupled to the base of Q465, turning it on. As the current begins to flow in Q465, its collector voltage drop aids in turning Q455 off and the switching action takes place very rapidly. (Consider the emitter of Q465 as grounded; the components in its emitter circuit are used in 2 FIELD and LINE SELECTOR operation when LINE SELECTOR switch is set to a line, line 16 through 21 and are of no importance in 2 LINE operation.)

## Miller Runup

As Q465 collector voltage falls below about +1.3 volts, D464 conducts and takes the anodes of the disconnect diodes toward ground. Both D481 and D482 stop conducting. The timing resistor current that had been flowing through D482 is immediately transferred to the base of Q483. The current that had been flowing in D481 through Q481 is cancelled by a slight drop in voltage at the base of Q481. As Q483 base starts negative, the base of Q481 also starts negative and reduces its collector current, causing its collector voltage to start positive. The timing capacitor couples the positive voltage of Q481 collector back to Q483 base, essentially stopping its negative travel. The result is that the timing capacitor receives a charge at a rate set by the timing resistor, creating a very linear positive-going sawtooth voltage at the collector of Q481. The miller runup circuit can be defined as a feedback amplifier, with the feedback element a timing capacitor, and the input resistor a timing resistor; the input signal is the -25 volt supply (see Fig. 3-9 and associated text for description of a feedback amplifier).

The sweep voltage rises positive until R492 raises the base voltage of Q455 far enough to revert the sweep gating multi. As Q455 conducts, the collector voltage of Q465 raises in the positive direction. D464 stops conducting and R468 raises the base voltage of Q483 positive through D482. This causes collector current in Q481 to increase rapidly. This collector current discharges the timing capacitor at a linear rate set by R468. As Q481 collector voltage approaches the voltage at the base of Q483, D481 takes some of the R468 current and stops the rundown. (D486 offsets the base voltage of Q481 in a direction to limit the quiescent current in D481, permitting the next sweep runup to start linearly.) The rate of rundown is slow enough that the sweep is triggered every other horizontal sync pulse, presenting a non-interlaced color burst. The sweep generator then waits for another negative line-trigger pulse to turn off Q455 and start the cycle over again.

2 FIELD DISPLAY. Operation of the sweep gating multivibrator is changed from a state where a trigger is required to start the sweep, to a condition where the sweep starts automatically, and is stopped by a trigger pulse. If the sweep is not running when the DISPLAY switch is set to 2 FIELD, Q465
of the sweep gating multi is not conducting. The DISPLAY switch connects R461A to the -25 -volt supply and the emitter voltage starts negative. D461 is reverse biased, and the rate of fall is set by the time constant of R461A-C463. Approximately 1 millisecond after Q465 emitter voltage starts negative, the sweep gating multi switches so that Q465 is on and Q455 off. The sweep voltage runs up as described for 2 LINE operation.

The DISPLAY switch also changes the output of the trigger selector matrix, forward biasing D452 through R450 so that positive pulses will come through D452, and will turn on Q455 to stop the sweep. The positive pulse that turns Q455 on occurs at every other vertical sync pulse. The sweep is stopped, runs down very rapidly (due to additional rundown current from R453 in parallel with R468), waits 1 millisecond and automatically starts again, just before the video portion of the next field.

In the event vertical input composite video stops, the sweep will continue to cycle, but instead of positive pulses stopping the sweep, Q455 is turned on by sweep voltage feedback through R491-R492 in the same manner as described for 2 line operation. Thus, the Type RM529 Monitor will show a sweep without vertical information when the DISPLAY switch is set to 2 FIELD, but requires a trigger signal from the sweep to operate in all other positions of the DISPLAY switch.

With the INPUT switch set to CAL, R469 is placed in parallel with R468 so the rundown rate will be rapid enough to prepare the sweep to run again at the next calibrated signal transition. This assures a cleanly triggered calibrator display without the possible jitter caused by a longer rundown.

The runup rate of the miller runup circuit is slowed by adding C483 across the timing capacitor used in 2 LINE operation. C483 does not affect the sweep voltage peak value, but changes only the rate at which the spot moves across the CRT. Television systems with different time per field than the 30 hertz U.S. A. rate require a change in the value of C483 to change the sweep rate. For longer time per field, increase C483 value; for less time per field, decrease C483 value. Modification of C483 is normally made at the factory at time of purchase.

The miller runup circuit drives the horizontal amplifier and staircase amplifier.

LINE SELECTOR DISPLAY. Operation of the sweep gating multivibrator is changed from a state where a trigger is required to start the sweep, to a condition where the sweep gating multivibrator starts automatically, runs until a-H pulse latches it and causes it to switch and start the sweep voltage running up. After the sweep voltage has run up, the sweep gating multivibrator is reset by a field selected frame rate trigger pulse. If the sweep is not running when the DISPLAY switch is set to the LINE SELECTOR position (LINE SELECTOR switch set to line 21), Q465 of the sweep gating multi is not conducting. The DISPLAY switch connects R46IA to the -25 volt supply through R461B, R461C, R461D, R461E, R461F and R461G (if FIELD switch is set to 2) and the emitter voltage starts negative. D461 is reverse biased, and the rate of fall is set by the time constant of C463-R461A, R461B, R461C, R461D, R461E, R461F and R461G. At a time which is determined by the setting of the LINE SELECTOR switch and the FIELD switch, after Q465 emitter voltage starts negative, it will be negative
enough to be latched by one of the -H pulses applied through C462 to the emitter of Q465. The latching by the -H pulse causes the sweep gating multi to switch so that Q465 is on and Q455 off. The sweep voltage runs up as described for 2 LINE operation. After the sweep voltage has run up, the sweep gating multi is reset by a field selected frame rate trigger pulse.

Since the VIT LINE SEL RANGE control, R458, varies the base voltage of Q465 only a small amount, it is used to set the exact time that Q465 will turn on.

The DISPLAY switch also changes the output of the trigger selector matrix, forward biasing D452 through R450 so that positive pulses will come through D452, and will turn on Q455 to stop the sweep. The positive pulse that turns Q455 on occurs at every other vertical sync pulse. The swcep is stopped, runs down, waits for the time set by the LINE SELECTOR switch and the FIELD switch, then automatically starts again, just before the desired horizontal line.

## Unblanking Amplifier

The unblanking amplifier (Q474) responds to the sweep gating multi (Q465) collector signal. When there is no sweep, the CRT beam is pulled away from the deflection plates and phosphor screen, preventing any spot from being seen. Q474 collector is near ground at the time of no sweep, turning off the CRT beam. As the sweep gating multi switches states to start a sweep, Q474 is biased to cutoff and its collector rises to +101 volts, limited by conduction of D474 and D475.

The unblanking amplifier provides two more output signals during line selector sweep operation. One is the video output intensification discussed with the vertical amplifier description. The other increases the CRT beam current to intensify the CRT trace for the short duration of the line selector sweeps.

The collector signal of Q474 does not pull down on the trace intensification line; rather, that line is pulled down by R476 and the - 5 volts of the video output amplifier circuit between sweeps when the DISPLAY switch is set to either Line Selector position. The collector voltage of Q474 is near ground most of the time in line selector modes, because of the shortduration sweeps recurring at the 30 -hertz rate lonce every 33.3 ms ). The trace intensification line (at R477-R478 junction) drops to +5 volts in about 2.6 ms as the combination of R476-R477 discharges C478 and changes the charge on C477.

As the sweep starts, Q474 collector rises quickly, sending an integrated pulse to the CRT grid circuit. R478 permits the step to rise abruptly to +22 volts, then continue to tise at an $R C$ rate. The rising signal to the CRT grid is required to keep the cathode current constant during the intensification period, assuring a uniform CRT intensity throughout each sweep.

R476 also conducts current into the 75 ohms of the VIDEO OUTPUT connector, adding about 01 volt to the video output to intensify a line of the studio montor, identifying which line the Type RM529 Monitor is viewing

## Sweep Generator (SN 100-2996)

The sweep generator is a triggered sweep system for all positions of the DISPLAY switch except the 2 FIELD position, at which it is a recurring synchronized sweep. Positive field.
trigger pulses slop the sweep in 2 FIELD operation. Negative line-trigger or selected line pulses start the sweep in all other modes of operation. The sweep rate at 2 LINE permits viewing the interlacing of the color burst. The sweep rate at 0.125 $\mathrm{H} / \mathrm{cm}$ permits a look at every other horizontal line displaying a noninterlaced color burst. Refer to the simplified sweep generator diagram of Fig. 3.11 and the complete diagram at the back of this manual during the following circuit description.

## Trigger Selector Matrix

Selection of recurrent negative line trigger pulses at the beginning of each horizontal line, or of selected line pulses, is made in a diode switching network of the DISPLAY switch.

When the DISPLAY switch is at either of its LINE SELECTOR positions, the cathode of D430 is raised about 9.5 volts positive and the drode is reverse biased so it cannot conduct negative line friggers to the sweep gating multi. D436 does conduct negative selected line pulses to the sweep gating multi.

When the DISPLAY switch is at 2 LINE, $.25 \mathrm{H} / \mathrm{CM}$, or .125 H/CM, D436 cathode is reverse biased about +29 volts to prevent selected line pulses from getting to the sweep gating multi. D430 does conduct negative line-trigger pulses to the sweep gating multi.

When the DISPLAY switch is at 2 FIELD, both D430 and D436 are reverse biased so that no negative triggers get to the sweep gating multi. At the same time, D452 is forward biased through R450 so positive field triggers are available to the sweep gating multi.

## Sweep Gating Multi

The sweep generator is operated in two basically different modes of operation as suggested earlier. The sweep gating multi operation is altered from a triggered system for line displays to a free-running stopped-sweep system for 2 field displays.

2 LINE DISPLAY. (Vertical INPUT switch at A, DISPLAY switch at 2 LINE.) The sweep generator is held in one state by the sweep gating multi until the arrival of a negative trigger pulse. Before receipt of a trigger pulse, the following conditions exist:
a. Q455 is conducting, Q465 is in a state of nonconduction.
b. Both disconnect diodes are conducting. D482 is applying positive turn-on current from R468 to the miller runup input base, while D481 is limiting the turn-on current, as the collector of Q481 pulls down and takes some of the current flow from R468.
c. Q481 collector voltage is at about +1 volt, so that essentially no current is delivered through R520 (see horizontal amplifier diagram) to the horizontal amplifier.
d. The unblanking amplifier output is near ground, turning off the CRT beam.
e. The CRT horizontal deflection plates hold the blanked beam at the left side of the CRT (depending upon the setting of the POSITION control).

Q455 is held in conduction by current through the series resistors R464-R465 and D466, limited by R470 current into the
base-emitter junction of Q474. The base turn-on current to Q455 is enough to saturate it; however, D455 bypasses some of the intended base current when the collector voltage drops slightly below D466 anode voltage, which prevents the transistor from saturating. If Q455 were to saturate, the base-emitter junction would hold so many carriers that the transistor could not be turned off quickly.) The fact that Q455 collector voltage is near ground assures that no current reaches the base of Q465, and Q465 remains cut off.

As the negative-going line trigger pulse arrives at the base of Q455 through C452, Q455 is turned off. The voltage rise at the collector of Q455 is coupled to the base of Q465, turning it on. As current begins to flow in Q465, its collector voltage aids in turning Q455 off and the switching action takes place very rapidly. (Consider the emitter of Q465 as grounded; the three components in its emitter circuit are used in 2 FIELD operation and are of no importance in 2 LINE operation.)

## Miller Runup

As Q465 collector voltage falls below about +1.3 volts, D464 conducts, and takes the anodes of the disconnect diodes toward ground. Both D481 and D482 stop conducting. The timing resistor current that had been flowing through D482 is immediately transferred to the base of Q483. The current that had been flowing in D481 through Q481 is cancelled by a slight drop in voltage at the base of Q481. As Q483 base starts negative, the base of Q481 also starts negative and reduces its collector current, causing its collector voltage to start positive. The timing capacitor couples the positive voltage of Q481 collector back to Q483 base, essentially stopping its negative travel. The result is that the timing capacitor receives a charge at a rate set by the timing resistor, creating a very linear positive-going sawtooth voltage at the collector of Q481. The miller runup circuit can be defined as a feedback amplifier, with the feedback element a timing capacitor, and the input resistor a timing resistor; the input signal is the -25 -volt supply (see Fig. 3-9 and associated text for description of a feedback amplifier.)

The sweep voltage rises positive until R492 raises the base voltage of Q455 far enough to revert the sweep gating multi. As Q455 conducts, the collector voltage of Q464 rises in the positive direction. D464 stops conducting and R468 raises the base voltage of Q483 positive through D482. This causes collector current in Q481 to increase rapidly. This collector current discharges the timing capacitor at a linear rate set by R468. As Q481 collector voltage approaches the voltage at the base of Q483, D481 takes some of the R468 current and stops the rundown. (D486 offsets the base voltage of Q481 in a direction to limit the quiescent current in D481, permitting the next sweep runup to start linearly.) The rate of rundown is slow enough that the sweep is triggered every other horizontal sync pulse, presenting a non-interlaced color burst. The sweep generator then waits for another negative linetrigger pulse to turn off Q455 and start the cycle over again.

2 FIELD DISPLAY. Operation of the sweep gating multivibrator is changed from a state where a trigger is required to start the sweep, to a condition where the sweep starts automatically, and is stopped by a trigger pulse. If the sweep is not running when the DISPLAY switch is set to 2 FIELD, Q465 of the sweep gating multi is not conducting. The DISPLAY switch connects R461 to the -25 -volt supply and the emitter
voltage starts negative. D461 is reverse biased, and the rate of fall is set by the time constant of R461-C461. Approximately 1 millisecond after Q465 emitter voltage starts negative, the sweep gating multi switches so that Q465 is on and Q455 off. The sweep voltage runs up as described for 2 LINE operation.

The DISPLAY switch also changes the output of the trigger selector matrix, forward biasing D452 through R450 so that positive pulses will come through D452, and will turn on Q455 to stop the sweep. The positive pulse that turns Q455 on occurs every other vertical sync pulse. The sweep is stopped, runs down very rapidly due to additional rundown current from R453 in parallel with R468, waits 1 millisecond and automatically starts again, just before the video portion of the next field.

In the event vertical input composite video stops, the sweep will continue to cycle, but instead of positive pulses stopping the sweep, Q455 is turned on by sweep voltage feedback through R491-R492 in the same manner as described for 2 line operation. Thus, the Type RM529 Monitor will show a sweep without vertical information when the DISPLAY switch is set to 2 FIELD, but requires a trigger signal for the sweep to operate in all other positions of the DISPLAY switch.

With the INPUT switch set to CAL, R469 is placed in parallel with R468 so the rundown rate will be rapid enough to prepare the sweep to run again at the next calibrator signal transition. This assures a cleanly triggered calibrator display without the possible jitter caused by a longer rundown.

The runup rate of the miller runup circuit is slowed by adding C483 across the timing capacitor used in 2 LINE operation. C483 does not affect the sweep voltage peak value, but changes only the rate at which the spot moves across the CRT Television systems with different time per field than the 30 hertz U.S.A. rate require a change in the value of C483 to change the sweep rate. For longer time per field, increase C483 value; for less time per field, decrease C483 value. Modification of C483 is normally made at the factory at time of purchase.

The miller runup circuit drives both the horizontal amplifier and the staircase amplifier.

## Unblanking Amplifier

The unblanking amplifier (Q474) responds to the sweep gating multi (Q465) collector signal. When there is no sweep, the CRT beam is pulled away from the deflection plates and phosphor screen, preventing any spot from being seen. Q474 collector is near ground at the time of no sweep, turning off the CRT beam. As the sweep gating multi switches states to start a sweep, Q474 is biased to cutoff. Its collector rises to +101 volts, limited by conduction of D474 and D475.

The unblanking amplifier provides two more output signals during line selector sweep operation. One is the video output intensification discussed with the vertical amplifier description. The other increases the CRT beam current to intensify the CRT trace for the short duration of the line selector sweeps.

The collector signal of Q474 does not pull down on the trace intensification line; rather, that line is pulled down by R476 and the -5 volts of the video output amplifier circuit between sweeps when the DISPLAY switch is set to either Line Selector position. The collector voltage of Q474 is near ground most of the time in line selector modes, because of the short-


Fig. 3-12. Simplified Horizontal Amplifier.
duration sweeps recurring at a 30 -hertz rate (once every 33.3 ms ). The trace intensification line (at R477-R478 junction) drops to -5 volts in about 2.6 ms as the combination of R476-R477 discharges C478 and changes the charge on C477.

As the sweep starts, Q474 collector rises quickly, sending an integrated pulse to the CRT grid circuit. R478 permits the step to rise abruptly to +22 volts, then continue to rise at an RC rate. The rising signal to the CRT grid is required because the high-voltage power supply does not follow the increased current immediately, and the increasing grid signal turns on the CRT at about the same rate as the supply current decreases, assuring a steady CRT intensity throughout each sweep.
R476 also conducts current into the 75 ohms of the VIDEO OUTPUT connector, adding about 0.1 volt to the video oulput to intensify a line of the studio monitor, identifying which line the Type RM529 Monitor is viewing.

## Horizontal Amplifier

The horizontal amplifier circuit includes the horizontal amplifier and the staircase amplifier. Refer to the simplified horizontal amplifier diagram of Fig. 3-12 and the complete diagram at the back of this manual during the following circuit description.

Horizontal Amplifier. The horizontal amplifier is a combination of feedback and paraphase amplifier. The base of Q533 is the virtual ground summing input terminal to the whole amplifier. Voltage gain of the overall amplifier is the ratio of the MAG resistance to the input resistance of R520. The DC level of the output (positioning) is through R525 to the base of Q533. The input to a feedback amplifier can have several input resistors and signals. The gain of each is the
ratio of feedback resistor to input resistor. Feedback is from V544A cathode to the base of Q533. V544A cathode is also the signal source for the inverting half of the amplifier, through the HORIZ GAIN control R558-R568 to the base of Q574. Feedback in the inverting half of the amplifier is the cathode resistance of V554B to the base of Q574. The SWP/MAG REGIS control sets the DC balance of cathode voltages of V544A/V554B so the display center does not shift as the MAG switch is changed.

The sweep sawtooth enters through R520. Q533 is an emitter follower and current-gain transistor, driving the inverting amplifier Q544. Q544 signal output receives current gain in the cathode of V544A, assuring linear feedback from a low impedance. The plate of V554A provides a +150 -volt swing that would be impossible to achieve with transistors. It acts in a normal vacuum tube fashion, with the input grid signal appearing inverted at the plate output.

The HORIZ GAIN resistance is degenerative to V554A, and is the signal coupling path to Q574. The signal from V554A cathode to Q574 base runs negative, increasing the current in Q574 collector. The collector voltage of Q574 becomes less negative and drives the grid of V554B to increase V554B current, raising the cathode to the level it had before the signal started negative. Note that the base of Q574 acts as a virtual ground for signals. V544B grid swings about 6.6 volts, turning on plate current so the plate swings about -150 volts.

## Staircase Amplifier (SN 787-up)

V514 is a feedback amplifier with two input resistors to sum the sawtooth and studio color camera staircase voltages. When 25 volts is applied between pins D and E of J501, K385 causes R516 to become the third input to the horizontal amplifier. V514 inverts the sawtooth voltage so that the summed
sawtooth signal to Q533 base is one-fourth its normal amplitude. The external input negative staircase signal is also inverted by V514.
With the staircase most positive, the sweep runs for the period of 1 field, and is reverted by a vertical sync trigger. At the time the sweep is reverted, the staircase drops negative to its second level. The sweep starts again, but begins onefourth of the way across the CRT due to the staircase positioning signal. Again the sweep runs for 1 field, is reverted and the staircase drops to its third level. Once again the sweep starts, but one-half of the way across the CRT. Again the sweep runs for 1 field, is reverted and the staircase drops to its fourth level. Once again the sweep starts, but three-fourths of the way across the CRT. Thus, the three-color and blackwhite camera signals can all be viewed in one CRT display.

The staircase level shift takes about $800 \mu \mathrm{~s}$. With the sweep gating multi operating in 2 FIELD, the sweep restarts in about 1 millisecond, so the change in staircase is not seen because the CRT beam is blanked off at the same time.

Closing the staircase relay also changes the timing resistor of the sweep generator so the sweep rate is twice as fast as that for 2 FIELD operation. The relay also changes the operation of the field selector to put out a positive pulse at each vertical sync pulse time instead of at every other one. Thus, the sweep recurs at a 60 -hertz rate, taking four sweeps to get across the CRT.

## Staircase Amplifier (SN 100-786)

V514 is a feedback amplifier with two input resistors to sum the sawtooth and studio color camera staircase voltages. When the control lead, pin D of J501, is externally grounded, K385 causes R516 to become the third input to the horizontal amplifier. V514 inverts the sawtooth voltage so that the summed sawtooth signal to Q533 base is one-third of its normal amplitude. The external input negative staircase signal is inverted by V514.

With the staircase most positive, the sweep runs for the period of one field, and is reverted by a vertical sync trigger. At the time the sweep is reverted, the staircase drops negative to its second level. The sweep starts again, but begins one-third of the way across the CRT due to the staircase positioning signal. Again the sweep runs for one field, is reverted and the staircase drops to its third level. Once again the sweep starts, but two-thirds of the way across the CRT. Thus, the three color camera signals can all be viewed on one CRT display.

The staircase level shift takes about $800 \mu \mathrm{~s}$. With the sweep gating multi operating in 2 FIELD, the sweep restarts in about 1 ms , so the change in staircase is not seen because the CRT beam is blanked off at the same time.

Closing the staircase relay also changes the timing resistor so the sweep rate is twice as fast as that for 2 FIELD operation. The relay also changes the operation of the field trigger generator to put out a positive pulse at each vertical sync pulse time instead of at every other one. Thus the sweep recurs at a 60 -hertz rate, taking three sweeps to get across the CRT.

## Power Supply

The low-voltage power supply provides regulated -25 volts, +100 volts, and unregulated +360 volts to the circuits
of the Type RM529. The -25 volt supply is the reference voltage for the +100 -volt supply and the calibrator circuit.

The Type RM529 is powered by a dual primary power transformer for operation on either 115 or 230 volt $50-60$ hertz line. Refer to the Operating Instructions section of this manual for converting from one supply voltage to the other.

## -25-Volt Supply

Voltage for the -25 -volt power supply comes from the fullwave rectifier system of D610-D611 and C610. Voltage across C610 is nominally 35 volts.
The -25 -volt regulator consists of a comparator that compares a portion of -25 volts (divided by R624-R626 and the - 25 VOLTS/CAL AMPL control R620) against the voltage of a precision zener diode D614. D614 zener voltage is about 9.1 volts. The comparator output at Q616 collector is inverted and amplified by Q634, which drives the series transistor Q637 in a direction to compensate for changes in the output voltage.

Assume the -25 -volt supply level decreases and the voltage goes slightly positive. Q626 turns on harder, reducing the current in Q616 so its collector goes positive. Q634 turns on harder and pulls Q637 base in the negative direction, causing it to conduct harder, raising the output voltage back to its proper negative level. Since the collector of Q637 is grounded, the whole supply is moved by the emitter of Q637 to make the correction. R617-C617 at the base of Q634 reduce the feedback loop high-frequency gain for more stable operation with high-frequency load transients. C620 and C626 aid in reducing the high-frequency output impedance of the supply.

The -25 -volt supply is the voltage source for the heaters of V113 and V293. R621 across V293 heater compensates the heater voltage for current taken by the constant current stage of the vertical preamplifier.
The value of the -25 -volt supply directly sets the peak-topeak amplitude of the calibrator signal; therefore the control used to adjust the supply is labeled - 25 VOLTS/CAL AMPL. See the Calibration procedure for adjustment.

## +100-Volt Supply

Voltage for the +100 -volt supply is provided by the fullwave bridge rectifiers D640A-B-C-D and C640. The voltage across C640 is nominally 130 volts.

The +100 -volt regulator compares a portion of the +100 volts (referenced to the -25 -volt supply through the divider R641-R642) to ground at the emitter of Q644. Q643 is an emitter follower acting as an impedance transfer device to raise the base impedance of Q644 base to prevent loading the divider. Q644 amplifies and inverts any change at the base of Q643 and applies the change directly to the base of Q647. Q644 collector current is the total base current of Q647. Q647 emitter voltage follows the inverted correction signals, chang ing the level of the whole supply when needed.

Assume that the load increases, taking the +100 volts slightly negative. Q643 drives Q644 base negative, increasing its collector current. Increased Q644 collector current means increased base current in Q647, raising the emitter positive the correct amount to restore the output voltage.

Fuse F648 protects Q647 from accidental short circuit of the +100 -volt supply bus. R648 discharges C640 if the fuse is blown, but only after the AC power is turned off.

C649 and C644 aid in reducing the supply high-frequency impedance. R644 limits the peak current through C644 to the base of Q643 in case the supply is accidentally shorted.

R646-C646 decouple the +100 -volt bus for peak current of the CRT unblanking circuit.

## +360-Volt Supply

Voltage for the +360 -volt unregulated supply is provided by the full-wave bridge rectifiers D650A-B-C-D and C650A (C650 below SN 787). The voltage across C650A (C650 below SN 787) is nominally 255 volts, which is added to the +100 volt supply. The supply is used by the CRT high-voltage supply and the vertical output stage, whose current passes through the beam rotator coil.

Beam Rotator Coil. The rectangular CRT is not easily rotated physically. Also, the trace changes its alignment with the graticule slightly, depending upon the monitor's relation to the earth's magnetic field. Thus, a coil is included around the CRT proper, allowing the operator to adjust the trace alignment with the graticule.

## CRT Circuit and Calibrator

The Type T5290 (V859) cathode-ray tube is a rectangular, flat-faced, mono-accelerator, deflection-blanked type, designed especially for the Type RM529 Waveform Monitor. Acceleration voltage is 5500 volts with -5300 V at the cathode, and nominally +200 volts at the deflection plates. The phosphor is aluminized, permitting bright displays and preventing any chance of phosphor damage at any position of the IN . TENSITY control.

The beam is blanked between sweeps by special deflection plates (located in the focus gun area of the tube) that pull all electrons away from the screen. Special intensifying circuits described with the sweep generator automatically brighten selected line displays for easy viewing of fast sweeps at lowrepetition rates.

## High-Voltage Power Supply and Calibrator

High-Voltage Power Supply. The high-voltage supply is actually a cathode-modulated amplifier with positive feedback sustaining oscillation. The cathode modulation is voltage
feedback from the high-voltage output that controls the level of oscillation. The calibrator transistor Q874 is directly in the feedback path that sustains oscillation.

As the monitor is turned on, V800B is turned off due to its cold heater. The voltage divider of R875-R876 turns on Q874 so its collector voltage is about -10 volts. Q874 collector is directly connected to the grid of V800B. V800B will conduct with its grid at -10 volts. As V800B warms up and pulls plate current, Q874 collector receives a transformer-coupled turn-off signal and its collector voltage furns on V800B even more. The secondary of T801 is a tank circuit, resonant at about 30 kHz . Thus, Q874 first receives a turn-off pulse, and then as T801 secondary swings through a cycle, Q874 is turned on full, turning V800B completely off. The cycle of oscillation repeats, heating the cathodes of V822 and V832. As they conduct, high voltage is developed that soon reduces current in V800A and Q804 to limit the current of V800B. Any further changes in output high voltage will change the conduction level of V800B to correct and restore the supply voltage.

V822 and V832 are the diodes of a half-wave voltage doubler with C837 and C848, the main filter capacitors. C837 also couples fast output voltage changes to the control tube V800A.

The multiple-resistor bleeder of R834 through R847 also provides voltage division for the INTENSITY and FOCUS controls. C849 assures that there is no voltage ripple between the cathode and grid of the CRT, which would otherwise in-tensity-modulate the trace.

Neon bulbs placed across the ASTIG control assure that the voltage of the astigmatism element remains constant to the average voltage of the vertical defective plates, which also use the unregulated +360 -volt supply.

Calibrator. The calibrator voltage is a secondary benefit of the high-voltage oscillator. Q874 collector voltage swings between about ground and the -25 -volt supply, providing a siable square wave. D881 sets the ground level, and the - 25 volt supply sets the negative ievel. R881, R885 and R886 divide the 25 -volt swing for use in the vertical amplifier when the VOLTS FULL SCALE control is at 1.0 . As the gain of the vertical amplifier is increased with the VOLTS FULL SCALE switch, R882 and/or R883 reduce the calibrator output amplitude to keep the display on the CRT screen.

External calibrator signals see a 1 -megohm load when the switch is set to EXT.

## SECTION 4

## MAINTENANCE

## Visual Inspection

If trouble occurs in the Type RM529, make sure the associated equipment is operating and the controls are properly set. If it is determined that the trouble is definitely in the Type RM529, a visual check may reveal the cause. Defects such as loose or broken connections, frayed or broken cables, damaged connectors, burned components, and broken switches can generally be detected by a visual inspection. Except for heat-damaged components, the remedy for such defects is obvious. Overheating of components is usually a symptom of other, less apparent, troubles in the circuit. For this reason, it is essential to determine the actual cause of overheating before the damaged parts are replaced; otherwise, the damage may be repeated.

## Parts Removal and Replacement

Whenever a part is replaced, check and adjust the instrument calibration as necessary. Most parts in the Type RM529 can be replaced without detailed instructions. Some, however, are best removed and replaced by using definite procedures contained in the following paragraphs. (Parts ordering information is located on the back of the Abbreviations And Symbols page which immediately precedes Section 7 of this manual.)

## CAUTION

Turn AC power off before removing tubes or transistors from their sockets.

Transistor Replacement. Transistors should not be replaced unless they are actually defective. Transistor defects usually take the form of the transistor opening, shorting, or developing excessive leakage. To check a transistor for these and other defects, use a transistor curve display instrument


Fig. 4-1. In-circuit voltage checks NPN or PNP transistors.
such as a Tektronix Type 575. However, if a good transistor checker is not readily available, a defective transistor can be found by signal-tracing, by making in-circuit voltage checks, by measuring the transistor forward-fo-back resistance using proper ohmmeter resistances, or by using the substitution method. The locations of all transistors are silk-screened on the chassis next to each socket.

To check transistors using a voltmeter, measure the emitter-to-base and emitter-to-collector voltages and determine whether the voltages are consistent with the normal resistances and currents in the circuit (see Fig. 4-1).

To check a transistor using an ohmmeter, know your ohmmeter ranges, the currents they deliver, and the internal battery voltage(s). If your ohmmeter does not have sufficient resistance in series with its internal voltage source, excessive current will flow through the transistor under test. Excessive current and/or high internal source voltage may permanently damage the transistor.

## NOTE

As a general rule, use the $R \times 1 \mathrm{k}$ range where the current is usually limited to less than 2 mA and the internal voltage is usually $11 / 2$ volts. You can quickly check the current and voltage by inserting a multimeter between the ohmmeter leads and measuring the current and voltage for the range you intend to use.

When you know which ohmmeter ranges will not harm the transistor, use those ranges to measure the resistance with the ohmmeter connected both ways as given in Table 4-1.

TABLE 4-1
Transistor Resistance Checks

| Ohmmeter <br> Connections | Resistance Readings That Can Be Ex- <br> pected Using the $R \times 1 \mathrm{k}$ Range |
| :---: | :--- |
| Emitter-Collector | High readings both ways (about $60 \mathrm{k} \Omega$ to <br> around $500 \mathrm{k} \Omega$ ). |
| Emitter-Base | High rading one way (about $200 \mathrm{k} \Omega$ or <br> more). Low reading the other way (about <br> $400 \Omega$ to $2.5 \mathrm{k} \Omega$ ). |
| Base-Collector | High reading one way (about $500 \mathrm{k} \Omega$ or <br> more). Low reading the other way (about <br> $400 \Omega$ to $2.5 \mathrm{k} \Omega)$. |

Test prods from the ohmmeter are first connected one way to the transistor leads and then reversed lconnected the other way). Thus, the effects of the polarity reversal of the voltage applied from the ohmmeter to the transistor can be observed.

If there is doubt about whether the transistor is good or not, substitute a new transistor; but, first be certain the circuit voltages applied to the transistor are correct before making the substitution. If a transistor is substituted without first checking out the circuit, the new transistor may immediately be damaged by some defect in the circuit.

Replacement of either Q637 or Q647 requires removal of only the transistor mounting bolts.

Remove the mounting bolts and pull the transistor and its leads a short distance away from the rear panel. Note the wire color code for correct resoldering to the leads of the new transistor. Unsolder the defective transistor. Wipe a small amount of non-melting silicone grease such as Dow Corning 4 Compound on the under side of the new transistor.

## WARNING

Silicone grease will irritate and may damage eye tissues. Wash your hands thoroughly after this procedure before touching the face.

Solder the leads to the new transistor using long-nose pliers on the transistor lead as a heat sink. Push the transistor into place making sure the leads are separated, and re-install the mounting bolts. Wipe excess silicone grease away from the transistor edge with a disposable tissue.

Tube Replacement. Tester checks on lubes used in the Type RM529 are not recommended. Tube testers sometimes indicate a tube to be defective when that tube is operating satisfactorily in a circuit, or they may fail to indicate tube defects which affect the performance of the circuits. The standard of usability of a tube is whether or not it works properly in the circuit. If it does not, it should be replaced. Unnecessary replacement is not only expensive, but may also cause needless recalibration of the instrument.

Lamp Replacemer:. The graticule illumination lamps are bayonet Type 47, 6- $\delta$ volt bulbs. Remove the four bezel nuts, lift away the graticule, and replace the lamps in the normal manner.

The four neon bulbs just to the left of the CRT (two are not visible through the front panel) are soldered in place. Removal and replacement requires a small iron and long-nose pliers.

## Recalibration

To assure accurate measurements, check the calibration of this instrument after each 500 hours of operation or every six months if used intermittently. Complete calibration instructions are given in Section 6.
The calibration procedure can also be helpful in localizing certain troubles in the instrument. In some cases, recalibration may reveal and correct minor troubles that do not show up during regular operation.

## Cleaning

The Type RM529 should be cleaned as often as operating conditions require. Accumulation of dirt in the instrument can cause overheating and component breakdown. Dirt on components acts as an insulating blanket and prevents efficient heat dissipation. It also provides a possible electrical conduction path.

Loose dust accumulated on the outside of the Type RM529 can be removed with a cloth or small paint brush. The paint brush is particularly useful for dislodging dust on and around the front-panel controls. Dirt which remains can be removed
with a soft cloth dampened in a mild solution of water and detergent. Abrasive cleaners should not be used.

The high-voltage circuits, including parts enclosed by the high-voltage shield, should receive special attention. Excessive dust and dirt in these areas may cause high-voltage arcing and result in improper instrument operation.

## CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in this instrument. Some chemicals to avoid are benzene, toluene, xylene, acetone, or similar solvents.

To clean the graticule and the face of the CRT, first remove the four graticule nuts. Then remove the bezel and the graticule. Clean the graticule and the face of the CRT with a sott, lint-free cloth dampened with mild detergent and water. Repeat with a cloth dampened with water only.

## Standard Parts

All electrical and mechanical part replacements for the Type RM529 can be obtained through your local Tektronix Field Office or representative. However, since many of the components are standard parts, they can generally be obtained locally in less time than from the factory. Before purchasing replacement parts, consult the Parts Lists for value, tolerance rating and Tektronix Part Number.

## Special Parts

In addition to the standard components some special parts are used in the production of the Type RM529. These parts are manufactured or selected by Tektronix, Inc. to meet specific performance requirements, or are manufactured for Textronix, Inc. in accordance with our specifications. Most of the mechanical parts used in this instrument have been manufactured by Tektronix, Inc. Order all special parts directly from your Textronix Field Office or representative. Parts ordering information is located on the Abbreviations and Symbols page which immediately precedes Section 7.

## Resistor Coding

The Type RM529 uses a number of very stable metal-film resistors identified by their gray background color and color coding.

If the resistor has three significant figures with a multiplier the resistor will be EIA color coded. If it has four significant figures with a multiplier, the value will be printed on the resistor. For example, a $333-\mathrm{k} \Omega$ resistor will be color coded, but a $333.5-\mathrm{k} \Omega$ resistor will have its value printed on the resistor body.

The color-coding sequence is shown in Fig. 4-2.

## Ceramic Terminal Strip Replacement

A complete ceramic terminal strip assembly is shown in Fig. 4-3. Replacement strips (including studs) and spacers are supplied under separate part numbers. The old spacers may be re-used unless they are damaged.


Fig. 4-2. Standard EIA cotor code for metal-film resistors.

After the damaged strip has been removed, place the undamaged spacers in the chassis holes. Then, carefully press the studs into the spacers until they are completely seated. If necessary, use a soft mallet and tap lightly, directly over the stud area of the strip.


Fig. 4-3. Ceramic terminal strip assembly.

## Soldering

Ceramic Terminal Strips. Solder used on the ceramic terminal strips should contain about $3 \%$ silver. Ordinary 60/40 solder can be used occasionally without damage to the ceramic terminal strips. Use a 40 - to 75 -watt soldering iron with a $1 / 8$ inch wide chisel-shaped tip. If ordinary solder is used repeatedly, or if excessive heat is applied, the solder-toceramic bond can be broken.

A small supply of solder containing about $3 \%$ silver is included on a spool mounted inside this instrument on the rear panel. Additional solder should be available locally, or it can be purchased from Tektronix in one-pound rolls; order by Tektronix Part No. 251-0514-00.

Observe the following precautions when soldering ceramic terminal strips:

1. Use a hot iron for a short time. Apply only enough heat to make the solder flow freely.
2. Maintain a clean, properly tinned tip.
3. Avoid putting pressure on the ceramic terminal strip.
4. Do not attempt to fill the terminal-strip notch with solder; use only enough solder to cover the wires adequately.

Metal Terminals. When soldering to metal terminals (e.g., switch terminals, potentiometers, etc.), ordinary $60 / 40$ solder can be used. The soldering iron should have a 40 -to 75 -watt rating with a $1 / 8$ inch wide chisel-shaped tip.

Observe the following precautions when soldering to metal terminals:

1. Apply only enough heat to make the solder flow freely.
2. If a wire extends beyond the solder joint, clip the excess wire close to the joint.
3. Apply only enough solder to form a solid connection. Excess solder may impair the function of the part.

## Rotary Switches

Individual wafers or mechanical parts of rotary switches are normally not replaced. If a switch is defective, replace the entire assembly. The availability of replacement switches, either wired or unwired, is detailed in the Parts List.

## Cathode-Ray Tube

Use the following procedure for removal and replacement of the CRT.

## WARNING

Use care when handling a CRT. Avoid striking it on any object that might cause it to crack and implode. Flying glass from an imploding CRT can cause serious injury. Wear safety glasses or a plastic face mask.

1. Disconnect the instrument power.
2. Place the instrument on a level workbench.
3. Remove the graticule.
4. Carefully remove the five neck leads. Use long-nose pliers and slowly pull each clip off its neck pin.
5. Loosen the 6-32 bolt in the white plastic CRT rear neck clamp.
6. Place one hand over the CRT face. With the other hand push gently on the CRT socket until the tube moves slightly forward. Remove the socket and push on the center of the CRT base. Carefully guide the tube out the front, without touching the magnetic shield with the neck pins.

To install a new CRT:

1. Position the tube with the single neck pin at the top, two neck pins at both the side and bottom.
2. Carefully insert the tube into the magnetic shield, being careful not to touch the shield with the neck pins.
3. Extend the finger of one hand into the rear end of the shield to help guide the base into place. Push the CRT the last $1 / 4$ inch with the plastic graticule so the front of the tube is flush with the front panel.
4. Tighten the $6-32$ bolt in the plastic clamp untit the CRT neck is held firmly. DO NOT OVERTIGHTEN.
5. Use long-nose pliers and carefully install the neck clips to the neck pins; observe the color code as marked on the shield near each opening.
6. If the CRT face is not parallel with the front panel, use a $7 / 64$-inch hexagonal wrench to loosen the two hexagonal headed bolts at the mounting clamp. Raise, lower, or otherwise position the CRT socket so the face is correctly positioned. Tighten the hexagonal headed bolts and check that the neck pins are not grounded.
7. Re-install the graticule and recalibrate the instrument in accordance with the Calibration procedure.

## Troubleshooting

In the event of trouble, help with the particular problem may be obtained by reading the Circuit Description. Voltage checks and normal troubleshooting procedures will aid in finding and correcting the trouble.

Power-Supply Problems. The Type RM529 can still present a display and appear to operate if certain problems develop in the power supplies. The following table of symptoms and their related causes may help solve power-supply failures.

TABLE 4-2

| Problem <br> 1. Short sweep, excess high <br> voltage and ripple horizon- <br> tally. | Q647 or Q644 of +100-volt <br> supply is shorted. |
| :--- | :--- |
| 2. Same as No. 1; in addi- <br> tion, calibrator waveform <br> shows considerable hum. | Q637 or Q634 of -25-volt <br> supply is shorted. |
| 3. No trace. No heater flow <br> in two 12AT7 tubes. Power | Q637 or Q634 of -25-volt <br> supply is open or F637 is <br> blown. Or, if $12 A T 7 ~ h e a t e r s ~$ |
| Glowing, V833-V832 filaments |  |

## SECTION 5

## PERFORMANCE CHECK

## Introduction

This section of the manual provides a means of rapidly checking the performance of the Type RM529. It is intended to check the calibration of the instrument without the need for performing the complete Calibration procedure. The Performance Check does not provide for the adjustment of any internal controls Failure to meet the requirements given in this procedure indicates the need for internal checks or adjustments, and the user should refer to the Calibration procedure in this manual.

## EQUIPMENT REQUIRED

## General

The following equipment, or its equivalent is required for a complete performance check of the Type RM529. Specifications given are the minimum necessary to accurately check the performance of this instrument. All test equipment is assumed to be correctly calibrated and operating within the original specificatıons. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

## Special Test Equipment

For the quickest and most accurate calibration, special calibration fixtures are used where necessary. All calibration fixtures listed under Equipment Required can be obtained from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Constant amplitude sine-wave generator. Frequency, 50 kHz and 350 kHz to above 10 MHz ; output amplitude, 200 mV to 1 volt adjustable; amplitude accuracy, within $\pm 3 \%$ at 50 kHz and 350 kHz to above 10 MHz . Tektronix Type 191 recommended.
2. Test oscilloscope. Bandwidth, DC to 1 MHz ; minimum deflection factor, 0.005 volts/division. Tektronix Type 545B Oscilloscope with Type B Plug-In Unit, and Tektronix P6006 and P6028 Probes recommended.
3. Standard amplitude calibrator. Amplitude accuracy, within $025 \%$; signal amplitude, 0.2 volt to 2 volts; output frequency, 1 kHz . Tektronix calibration fixture 067-0502-00 recommended.
4. Time-mark generator. Marker outputs of $1 \mu \mathrm{~s}, 5 \mu \mathrm{~s}, 10 \mu \mathrm{~s}$, 01 ms and 0.1 j s ; accuracy, within $0.001 \%$. Tektronix Type 184 recommended.
5. Composite video signal source. Calibrated signal amplitude of 1 volt, variable from 200 mV to 1 volt. For example, Conrac model AU 12C receiver.

6 Square-wave generator. Fiequency of 120 hertz; output amplitude variable from 4 to 12 volts. Tektronix Type 105, $r$ e 106, or equivalent.
7. Termination. Impedance, 75 ohms; accuracy, within $\pm 3 \%$; connector, UHF. Tektronix Part No. 011-0023-00.
8. Three cables. Impedance, 75 ohms; Type RG11/ $U_{\text {; length }}$ 42 inches; connectors, BNC. Tektronix Part No. 012-0074-00.
9. Two adapters. Connectors, BNC female to UHF male. Tektronix Part No. 103-0015-00.
10. One capacitor. $2 \mu \mathrm{~F}$ at 150 WVDC . Tektronix Part No. 290-0121-00.

## PERFORMANCE CHECK PROCEDURE

## General

In the following procedure, test equipment connections or control settings should not be changed except as noted. If only a partial check is desired, refer to the preceding step(s) for setup information.

The following procedure uses the equipment listed under Equipment Required. If substitute equipment is used, control settings or setup must be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Remove the oscilloscope from any enclosure, to provide access to rear panel connectors.
2. Check that a 160 -IEEE unit $7-\mathrm{cm}$ composite graticule (331-0161-00) is installed and that the VIDEO OUTPUT connector is terminated into 75 ohms.
3. Connect the Type RM529 power cord to a suitable power source.
4. Set the Type RM529 POWER switch to on. Allow at least 20 minutes warm up, for checking the instrument to the given accuracies.

| POWER | On |
| :--- | :--- |
| SCALE ILLUM | Fully clockwise |
| FOCUS | Midrange |
| INTENSITY | Fully counterclockwise |
| GAIN | As is |
|  | $\quad$ VERTICAL |
|  | Controls |
| RESPONSE | FLAT |
| DC RESTORER | OFF |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE | CALIB |
| (VOLTS FULL SCALE |  |
| CAL | EXT |
| POSITION | Midrange |

## HORIZONTAL Controls

| POSITION | Midrange |
| :--- | :--- |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 FIELD |
| FIELD | ONE |
| VARIABLE (LINE SELECTOR) | Midrange |
| LINE SELECTOR switch | VARIABLE |

## 1. Check Graticule Illumination

a. Requirement-Graticule illumination must be maximum when the SCALE ILLUM control is fully clockwise. There should be no illumination when the SCALE ILLUM control is fully counterclockwise. The graticule illumination must smoothly change intensity with smooth rotation of the SCALE ILLUM control.
b. With the SCALE ILLUM control fully clockwise, check for maximum graticule illumination.
c. Slowly and smoothly rotate the SCALE ILLUM control counterclockwise, noting that the graticule illumination decreases smoothly as the control is rotated.
d. Check-There is no graticule illumination.
e. Adjust the SCALE ILLUM control for desired graticule illumination.

## 2. Check CRT Beam Rotator and Horizontal Geometry

a. Requirement-CRT Beam Rotator is adjustable for no horizontal tilt.

Horizontal Geometry: Trace bowing or trace deviation from a straight horizontal line must not exceed 2 mm .
b. Rotate the INTENSITY control clockwise until a trace can be seen.
c. Ground the upper VIDEO INPUTS A connector.

## NOTE

The trace should be parallel to the horizontal graticule lines, but due to the different effects of the earth's magnetic field at various locations, it is impossible to state that the trace should be aligned within plus or minus a specific tolerance. If the frace is not parallel to the horizontal graticule lines, it will be necessary to adjust the internal CRT BEAM ROTATOR control until the trace is parallel to the horizontal graticule lines.
d. Position the start of the trace to the left edge of the graticule and vertically position the trace to the +30 IEEE units graticule line.
e. Check-Amount of trace bowing or deviation from a straight line.
f. Remove ground from upper VIDEO INPUTS A connector.

## 3. Check FOCUS and INTENSITY Controls

a. Requirement-Focus: The FOCUS control must adjust for a well-defined display without being at either end of its adjustment range.

Intensity: With the INTENSITY control fully counterclockwise there must be no display. Clockwise rotation of the control must increase the intensity smoothly with smooth rotation of the control.
b. Reset the following controls:

| INPUT | CAL |
| :--- | :--- |
| CAL | $.714 \mathrm{~F} . \mathrm{S}$. |
| DISPLAY | 2 LINE |

c. Adjust the FOCUS control for a well-defined display.
d. Check-FOCUS control should not be at either end of its adjustment range.
e. Rotate the INTENSITY control fully counterclockwise.
f. Check-No display.
g. Slowly and smoothly rotate the INTENSITY control clockwise.
h. Check-For a smooth and constant increase in display brightness.
i. Adjust the INTENSITY control for normal display brightness.

## 4. Check Vertical Geometry

a. Requirement-Vertical trace bowing and/or tilt must not exceed 2 mm .
b. Reset the following controls:

| INPUT | A |
| :--- | :--- |
| SYNC | EXT |
| DISPLAY | $.25 \mathrm{H} / \mathrm{cm}$ |

c. Connect $5-\mu \mathrm{s}$ time markers to the upper VIDEO INPUTS A connector using a 75 -ohm coaxial cable.
d. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
e. Connect . 1 ms time-marker trigger pulses to the upper EXT NEG SYNC INPUT connector using a 75 -ohm coaxial cable.
f. Adjust the (VERTICAL) POSITION control and the VOLTS FULL SCALE switch and its VARIABLE control so the time markers over-scan the CRT viewing area.
g. Check--For not more than 2 mm of bowing and/or tilt.
h. Disconnect the time markers from the upper VIDEO $\mathbb{N}$. PUTS A connector, and the time-marker trigger pulses from the upper EXT NEG SYNC INPUT connector.

## 5. Check IVERTICAL) POSITION Control

a. Requirement-Range: POSITION control must be able
to position the trace off the top and bottom of the graticule area.

Direction: Clockwise rotation of the control must move the trace up, and counterclockwise rotation must move the trace down.
b. Reset the following controls:

| (VERTICAL) POSITION | Fully clockwise |
| :--- | :--- |
| SYNC | INT |
| DISPLAY | 2 FIELD |

c. Check-For upward trace movement beyond the graticule viewing area.
d. Rotate the POSITION control fully counterclockwise.
e. Check-For downward trace movement beyond the graticule limits.

## 6. Check Vertical Gain and Calibrator

a. Requirement-Vertical gain:
1.0 position; 1 volt of square wave from a standard amplitude calibrator must produce 140 IEEE units of deflection, $\pm 1 \%$.
0.2 position; 0.2 volt of square wave from a standard amplitude calibrator must produce 140 IEEE units of deflection, $\pm 2 \%$.
0.5 position; 0.5 volt of square wave from a standard amplitude calibrator must produce 140 IEEE units of deflection, $\pm 3 \%$.

VARIABLE (VOLTS FULL SCALE) ratio must be 2.5:1 or greater.

Calibrator:
FULL SCALE; calibrator deflection must match (1 volt) standard amplitude calibrator deflection ( 140 IEEE units), $\pm 1 \%$.
.714 F.S.; calibrator deflection must be 100 IEEE units, $\pm 1 \%$, when FULL SCALE setting of calibrator produces 140 IEEE units of deflection.
b. Connect 1 volt of standard amplitude calibrator square wave through a 75 -ohm coaxial cable to the upper VIDEO INPUTS A connector.
c. Set the VOLTS FULL SCALE switch to 1.0 .
d. Check-For 140 IEEE units of deflection, $\pm 1 \%$.
e. Set the standard amplitude calibrator for a 0.5 -volt square wave.
f. Set the VOLTS FULL SCALE switch to 0.5.
g. Check-For 140 IEEE units of deflection, $3 \%$.
h. Set the standard amplitude calibrator for a 0.2 -volt square wave.
i. Set the VOLTS FULL SCALE switch to 0.2.

1. Check--For 140 IEEE units of deflection, $+-2 \%$.
$k$ Set the VOLTS FULL SCALE switch to 1.0 .
I. Adjust the VARIABLE (VOLTS FULL SCALE) control to produce maximum signal deflection. Note the amount of deflection.
m. Adjust the VARIABLE (VOLTS FULL SCALE) control to produce minimum signal deflection. Note the amount of deflection.
n. Check $-\frac{\text { Maximum signal deflection }}{\text { Minimum signal deflection }}=$ a ratio of 2.5:1 or greater.
o. Reset the following controls:

VARIABLE
(VOLTS FULL SCALE)

## CAL

. Set the standard amplitude calibrator for a 1 volt squarewave signal and note the signal amplitude.
q. Change the INPUT switch to CAL.
r. Check-The calibrator signal amplitude matches the standard amplitude calibrator signal amplitude within $1 \%$. Note any error.
s. Change the CAL switch to $714 \mathrm{~F} . \mathrm{S}$.
t. Check-The calibrator signal amplitude is 100 IEEE units $\pm 1 \%$, taking into account any error noted in part $r$ of this step.

## 7. Check External Calibrator Input

a. Requirement-1 volt of standard amplitude calibrator square-wave signal must produce 140 IEEE units of deflection, $\pm 1 \%$.
b. Remove the standard amplitude calibrator signal from the upper VIDEO INPUTS A connector and connect it to the right EXT CAL INPUT connector.
c. Set the CAL switch to EXT.
d. Check-For 140 IEEE units of deflection, $\pm 1 \%$.
e. Reconnect the standard amplitude calibrator signal to the upper VIDEO INPUTS A connector.
f. Set the INPUT switch to A.

## 8. Check Compression and Expansion

a. Requirement-Compression and expansion must not exceed one IEEE unit.
b. Change the standard amplitude calibrator to obtain a 0.2 -volt square wave.
c. Using the VARIABLE (VOLTS FULL SCALE) and the (VERTICAL) POSITION controls, obtain a signal 40 IEEE units high, centered vertically in the graticule area.
d. Position the top of the display to the top graticule line.
e. Check-For less than one IEEE unit of compression or expansion.
f. Position the bottom of the display to the bottom graticule line.
g. Check-For less than one IEEE unit of compression or expansion.
h. Return the VARIABLE (VOLTS FULL SCALE) control to CALIB.
i. Disconnect the standard amplitude calibrator.

## 9. Check DC RESTORER Switch

a. Requirement-Reference level must shift no more than $\pm 4$ IEEE units for a gain change within the graticule area.
b. Set the DC RESTORER switch to ON.
c. Connect a composite video signal to the upper VIDEO INPUTS A connector.
d. Adjust the amplitude of the incoming composite video signal to obtain a display 30 IEEE units high.
e. Position the 0 IEEE signal level (back porch) to the 0 IEEE graticule line.
f. Rotate the VOLTS FULL SCALE switch through its 0.2 and 0.5 positions.
g. Check-Amount of vertical shift of the 0 IEEE signal level (back porch). It must not exceed $\pm 4$ IEEE units.
h. Set the VOLTS FULL SCALE switch to 1.0 .

## 10. Check Horizontal Gain

a. Requirement-See Table 5-1.

TABLE 5-1

| DISPLAY <br> Switch | Trace <br> Length | Tolerance |
| :---: | :---: | :---: |
| 2 FIELD | $10.2 \operatorname{div}$ | $\pm 5 \%$ |
| 2 LINE | $10.2 \operatorname{div}$ | $\pm 5 \%$ |
| $.125 \mathrm{H} / \mathrm{CM}$ | $10.2 \operatorname{div}$ | $\pm 2 \%$ |
| $.25 \mathrm{H} / \mathrm{CM}$ | $10.2 \operatorname{div}$ | $\pm 2 \%$ |

b. Set the DISPLAY switch to each of the positions listed in Table 5-1.
c. Check-For a trace length within the tolerance listed in Table 5-1.
d. Set the DISPLAY switch to $.125 \mathrm{H} / \mathrm{CM}$.
e. Disconnect the composite video signal.

## 11. Check Horizontal Sweep Rates

a. Requirement-See Table 5-2.

TABLE 5-2

| DISPLAY Switch | Mag <br> Switch | Time <br> Markers Applied | Markers per 10 Major Divisions | Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| . $125 \mathrm{H} / \mathrm{CM}$ | $\times 1$ | $\begin{gathered} 5 \mu \mathrm{~s} \text { and } \\ 10 \mu \mathrm{~s} \end{gathered}$ | 8 | $\pm 2 \%$ |
| . $125 \mathrm{H} / \mathrm{CM}$ | $\times 5$ | ${ }^{-1} \mu \mathrm{~s}$ | 16 | $\pm 3 \%$ |
| . $125 \mathrm{H} / \mathrm{CM}$ | $\times 25$ | $0.1 \mu \mathrm{~s}$ | 32 | $\pm 5 \%$ |

b. Connect the output of a time-mark generator through a 75 -ohm coaxial cable to the upper VIDEO INPUTS A connector.
c. Connect 0.1 ms time-marker trigger pulses from the timemark generator through a 75 -ohm coaxial cable to the upper EXT NEG SYNC INPUT connector.
d. Set the SYNC switch to EXT.
e. Adjust the VOLTS FULL SCALE switch and the VARIABLE (VOLTS FULL SCALE) control to obtain a display 50 IEEE units high.
f. Set the time-mark generator and Type RM529 controls as listed in Table 5-2.
g. Check-For the proper number of markers for 10 divisions within the tolerance listed in Table 5-2.

## 12. Check (HORIZONTAL) Position Control

a. Requirement-The trace must move to the right with clockwise rotation of the POSITION control. The trace must move to the left with counterclockwise rotation of the POSITION control.
b. Rotate the POSITION control to its fully clockwise posifion.
c. Check-That the trace moves to the right.
d. Rotate the POSITION control to its fully counterclockwise position.
e. Check-That the trace moves to the left.
f. Set the (HORIZ) POSITION control to midrange.
g. Disconnect the time-mark generator time markers and time-marker trigger pulses from the Type RM529.
h. Reset the following controls:

| SYNC | INT |
| :--- | :--- |
| DISPLAY | 2 FIELD |

## 13. Check FIELD Switch

a. Requirement-With the FIELD switch set to ONE, the last horizontal sync pulse will be one-half line ( $31.75 \mu \mathrm{~s}$ ) away from the first equalizing pulse. With the FIELD switch set to TWO, the last horizonial sync pulse will be a full line ( $63.5 \mu \mathrm{~s}$ ) away from the first equalizing pulse.
b. Connect a 1 volt composite video signal to the upper VIDEO INPUTS A connector.
c. Reset the following controls:

| DISPLAY | 2 FIELD |
| :--- | :--- |
| MAG | $\times 25$ |
| FIELD | ONE |

d. If vertical sync pulse group is not completely displayed, position it to the horizontal center of the viewing area with the (HORIZ) POSITION control.
e. Check-The position (in time) of the last horizontal sync pulse before the first equalizing pulse. It should be 31.75 .
f. Set the FIELD switch to TWO.
g. Check-The position (in time) of the last horizontal sync pulse before the first equalizing pulse. It should be 63.5 .

## 14. Check Triggering

a. Requirement-Must trigger internally on a 200 mV peak-to-peak signal connected to the VIDEO INPUT connectors. Must trigger externally on a 250 mV peak-to-peak signal connected to the EXT NEG SYNC INPUT connectors.
b. Remove the composite video signal from the upper VIDEO INPUTS A connector and connect it to the upper EXT NEG SYNC INPUT connector.
c. Connect a 75 -ohm coaxiai cable from the lower EXT NEG SYNC INPUT connerior to the upper VIDEO INPUTS A connector.
d. Reset the following controls:

| VOLTS FULL SCALE | 0.2 |
| :--- | :--- |
| DISPLAY | 2 FIELD |

e. Adjust the amplitude of the composite video signal to obtain a display amplitude of 140 IEEE units on the CRT.
f. Check-For a stable display on internal triggering.
g. Set the VOLTS FULL SCALE switch to .5 .
h. Adjust the amplitude of the composite video signal to obtain a display amplitude of 70 IEEE units on the CRT
i. Set the SYNC switch to EXT.
i. Check-For a stable display on external triggering.
$k$. Reset the following controls:

| VOLTS FULL SCALE | 1.0 |
| :--- | :--- |
| SYNC | INT |
| MAG | $\times 25$ |

I. Position the vertical sync block to the center of the graticule area.

## 15. Check Line Selector Operation (SN 2997-up)

a. Requirement-Brightening pulse amplitude must be 100 mV or more.

## NOTE

The start of the brightening pulse corresponds to the start of the sweep, as observed on the Type RM529 CRT, while the width of the brightening pulse corresponds to the length of the sweep, as observed on the Type RM529 CRT.

With the LINE SELECTOR switch set to VARIABLE and the LINE SELECTOR variable set fully counterclockwise, the brightening pulse must start in the vertical blanking time on or before the fifteenth line; with the LINE SELECTOR variable set fully clockwise, the brightening pulse must start after the first $25 \%$ of the second field; the display on the Type RM529 must remain stable throughout the rotation of the LINE SELEC. TOR variable control.

With the LINE SELECTOR switch set to 16, the brightening pulse must start at the start of line 16; with the LINE SELECTOR switch set to 17, the brightening pulse must start at the start of line 17; with the LINE SELECTOR switch set to 18, the brightening pulse must start at the start of line 18; with the LINE SEIECTOR switch set to 19 , the brightening pulse must start at the start of line 19; with the LINE SELECTOR switch set to 20 , the brightening pulse must start at the start of line 20; with the LINE SELECTOR switch set to 21 the brightening pulse must start at the start of line 21.
b. Connect a 75 -ohm coaxial cable from the VIDEO OUTPUT connector of the Type RM529 to the vertical input connector of the test oscilloscope.
c. Set the test oscilloscope controls as follows:

| Input Selector | AC |
| :--- | :--- |
| Volts/Div | 0.02 |
| Time/Div | 2 ms |
| Triggering Mode | Adjusted for stable display |
| Trigger Slope | + External |

## NOTE

The external triggering signal must be at the video field rate.
d. Set the Type RM529 DISPLAY switch to LINE SELECTOR $.125 \mathrm{H} / \mathrm{CM}$ and the LINE SELECTOR switch to VARIABLE.
e. Rotate the LINE SELECTOR variable control fully counterclockwise.
f. Check-The position (in time) and the amplitude of the brightening pulse on the test oscilloscope. The brightening pulse must be at least 100 mV high and its start should be on or before the 15 th line.
g. Rotate the LINE SELECTOR variable control fully clockwise.
h. Check-The position (in time) and the amplitude of the brightening pulse on the test oscilloscope. The brightening pulse must be at least 100 mV high and its start must occur after the first $25 \%$ of the second field.
i. Set the LINE SELECTOR switch to each numbered line position.
i. Check-That the brightening pulse is at least 100 mV high and that it starts at the start of the line to which the LINE SELECTOR switch is set.
k. Set the FIELD switch to ONE and repeat parts d through i.

## NOTE

LINE 10 starts at the first horizontal pulse following the last equalizing pulse in both fields (field one and twol. Lines 16 through 21 can be found by counting forward from this point of reference.

## 16. Check Line Selector Operation (SN 100-2997)

a. Requirement-Brightening pulse amplitude must be 100 mV or more. With the LINE SELECTOR control fully counterclockwise, the brightening pulse must start in the vertical blanking time before the sixteenth line. With the LINE SELECTOR control fully clockwise, the brightening pulse must start after the first $25 \%$ of the second field. The display on the Type RM529 must remain stable throughout the rotation of the LINE SELECTOR control.
b. Connect a 75 -ohm coaxial cable from the VIDEO OUTPUT connector of the Type RM529 to the vertical input connector of the test oscilloscope.
c. Set the test oscilloscope controls as follows:

| Input Selector | AC |
| :--- | :--- |
| Volts/Div | 0.02 |
| Time/Div | 2 ms |
| Triggering Mode | Adjusted for stable display |
| Trigger Slope | + External |

NOTE
The external triggering signal must be at the video field rate.
d. Set the Type RM529 DISPLAY switch to LINE SELECTOR .125 H/CM.
e. Rotate the LINE SELECTOR control fully counterclockwise.
f. Check-The position (in time) and the amplitude of the brightening pulse on the test oscilloscope. The brightening pulse must be at least 100 mV high and its start should be before the sixteenth line.
g. Rotate the LINE SELECTOR control fully clockwise.
h. Check-The position (in time) and the amplitude of the brightening pulse on the test oscilloscope. The brightening pulse must be at least 100 mV high and its start must occur after the first $25 \%$ of the second field.
i. Remove all connections to the Type RM529.

## NOTE

The last equalizing pulse in the vertical blanking time is the ninth line.

## 17. ${ }^{\text { }}$ Check Frequency Response

a. Requirement-See Table 5-3.
b. Connect the output of a constant amplitude sine-wave generator through a 75 -ohm coaxial cable to the upper VIDEO INPUTS A connector.
c. To the lower VIDEO INPUTS A connector, connect a 75ohm termination.
d. Set the Type RM529 controls and apply the indicated signal frequencies as listed in Table 5-3.
e. Check-For the required amount of deflection as listed in Table 5-3.
${ }^{1}$ An optional method of checking high-frequency response of the vertical amplifier will be found in step 18.

TABLE 5-3

| Response Switch Set to: | VARIABLE (VOLTS FULL SCALE) Set to: | VOLTS FULL SCALE Set to: | Check or Procedure |
| :---: | :---: | :---: | :---: |
| FLAT | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
| FLAT | CALIB | 1.0 | Check for flat frequency response from 50 kHz to 6 MHz ; within $+0 \%,-1 \%$ ( -0.1 dB ) or 1 IEEE unit. |
| FLAT | CALIB | 1.0 | Check for flat frequency response from 6 MHz to 8 MHz ; within $+0 \%,-3 \%(-0.3 \mathrm{~dB})$ or 3 IEEE units. |
| FLAT | CALIB | 0.2 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
| FLAT | CALIB | 0.2 | Check for flat frequency response from 50 kHz to 6 MHz ; $+0 \%,-1 \%(-0.1 \mathrm{~dB})$ or 1 IEEE unir. |
| FLAT | CALIB | 0.5 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 500 kHz . |
| FLAT | CALIB | 0.5 | Check for flat frequency response from 500 kHz to 6 $\mathrm{MHz}_{i}+0 \%,-1 \%(-0.1 \mathrm{~dB})$ or 1 IEEE unit. |
| FLAT | Counterclockwise | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
| FLAT | Counterclockwise | 1.0 | Check for flat frequency response from 50 kHz to 6 $\mathrm{MHz} ;+0 \%,-2 \%(-0.2 \mathrm{~dB})$ or 2 IEEE units. |

TABLE 5-3 (Continued)

| Response Switch Set to: | VARIABLE IVOLTS FULL SCALE) Set to: | VOLTS FULL SCALE Set to: | Check or Procedure |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { LOW } \\ & \text { PASS } \end{aligned}$ | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference ampli tude at 50 kHz . |
| $\begin{aligned} & \text { LOW } \\ & \text { PASS } \end{aligned}$ | CALIB | 1.0 | Check for 20 IEEE units (down 14 dB ) or less of deflection at 500 kHz . |
| FLAT | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference ampli tude at 3.58 MHz of deflection. |
| $\begin{aligned} & \text { HIGH } \\ & \text { PASS } \end{aligned}$ | CALİB | 1.0 | Check for 100 IEEE units $+0 \%,-1 \%(-0.1 \mathrm{~dB})\{1$ IEEE unit) of deflection at 3.58 MHz . |
| $\begin{aligned} & \text { HIGH } \\ & \text { PASS } \end{aligned}$ | CALIB | 1.0 | Check for 65 to 85 IEEE units of deflection at 3.18 MHz . |
| $\begin{aligned} & \text { HIGH } \\ & \text { PASS } \end{aligned}$ | CALIB | 1.0 | Check for 65 to 85 IEEE units of deflection at 3.98 MHz . |
| ieee | C̄Alīb | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
| IEEE | CALIB | 1.0 | Check for 94 to 97.5 IEEE units of deflection at 350 kHz . |
| IEEE | CALIB | 1.0 | Check for 70 to 80 IEEE units of deflection at 1 MHz . |
| IEEE | CALIB | 1.0 | Check for 31.2 to $\overline{42.5}$ IEEE units of deflection at 2 MHz . |
| IEEE | CALIB | 1.0 | Check for 7 to 14 IEEE units of deflection at 3.6 MHz . |

f. Remove all connections to the Type RM529.

## 18. Check J501 Staircase Input (SN 787-up)

a. Requirement-Four displays per ten centimeters. Each display should have some separation from neighboring displays.
b. Wire the 9 -pin plug connector (Tektronix Part No. 134-0049-00) as shown in Fig. 5-1. Make sure that the $2 \mu \mathrm{~F}$ capacitor is in series between the Type RM529 J501 connector pin $C$ and the output of the square-wave generator.
c. Connect the plug to J 501 on the Type RM529.
d. Connect a 12 -volt, 120 -hertz signal from a square-wave generator to pin C of the plug via the $2 \mu \mathrm{~F}$ capacitor.
e. Connect a test oscilloscope to the monitoring point to measure the output amplitude of the square-wave generator.
f. Apply one volt of composite video to the upper VIDEO INPUTS A connector.
g. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
h. Check-For a display as shown in Fig. 5-2A. Note righthand display position.
i. Reduce the signal from the square-wave generator to 8 volts.
i. Check-For a display as shown in Fig. 5-2B. Note right. hand display position.
k. Reduce the signal from the square-wave generator to 4 volts.
I. Check-For a display as shown in Fig. 5-2C. Note righthand display position.
m . Check-That each display has some separation from its neighbors.

## 19. Check J501 Staircase Input (SN 100-786)

a. Requirement-Three displays per ten centimeters. Each display should have some separation from neighboring displays.
b. Wire the 9 -pin plug connector (Tektronix Part No. 134-0049-00) as shown in Fig. 5-1. Make sure that the $2 \mu \mathrm{~F}$ capacitor is in series between the Type RM529 J501 connector pin $C$ and the output of the square-wave generator.
c. Connect the plug to J501 on the Type RM529.
d. Connect a 12 volt, 120 hertz signal from a square-wave generator to pin C of the plug via the $2 \mu \mathrm{~F}$ capacitor.
e. Connect a test oscilloscope to the monitoring point to measure the output amplitude of the square-wave generator.


Fig. 5-1. Front view of 9-pin plug connector (Tektronix Part No. 134-0049-00) showing lumper wire connections to cause relay K385 to be energized whenever the plug is in place.


Fig. 5-2. Checking to insure that four displays per 10 centimeters can be obtained.
f. Apply one volt of composite video to the upper VIDEO INPUTS A connector.
g. Connect a 75-ohm termination to the lower VIDEO INPUTS A connector.
h. Check-For a display as shown in Fig. 5-3A. Note righthand display position.
i. Reduce the signal from the square-wave generator to 6 volts.


Fig. 5-3. Checking to insure that three displays per 10 centimeters can be obtained.
i. Check-For a display as shown in Fig. 5-3B. Note righthand display position.
k. Check-That each display has some separation from its neighbors.

## 20. (Optional Method) Check Frequency Response

a. Set the Type RM529 front-panel controls as follows:

POWER
SCALE ILLUM
FOCUS
INTENSITY

GAIN

## VERTICAL Controls

| VARIABLE (VOLTS FULL <br> SCALE) | CALIB |
| :--- | :--- |
| CAL | .714 F.S. |
| POSITION | Midrange |

HORIZONTAL Controls
POSITION
Midrange
SYNC
MAG
DISPLAY
FIELD

INT
$\times 1$
$.125 \mathrm{H} / \mathrm{CM}$
ONE

## VARIABLE (LINE SELECTOR) Midrange <br> LINE SELECTOR switch VARIABLE

b. Connect to upper VIDEO INPUTS A connector 1 volt of multi-burst signal.
c. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
d. Check each position of the RESPONSE switch for the display shown in Fig. 5-4.
This completes the performance check procedure for the Type RM529. Disconnect all test equipment. If the instrument has met all performance requirements given in this procedure, it is correctly calibrated and within the specified tolerances.


Fig. 5-4. Waveforms showing the display which will result when 1 -volt of multi-burst signal is connected to the Type RM529 and the RESPONSE switch is set to (A) FLAT, (B) IEEE, (C) LOW PASS, (D) HIGH PASS.

## SECTION 6

## CALIBRATION

## Introduction

The Type RM529 Waveform Monitor is a stable instrument which will provide many hours of trouble-free operation. However, to insure measurement accuracy, it is suggested that you recalibrate the instrument after each 500 hours of operation, or every six months if used intermittently. It will also be necessary to recalibrate certain sections of the instrument when tubes, transistors or other components that affect the calibration accuracy of the instrument are replaced.

This calibration procedure can be used either for complete calibration of the Type RM529 to return it to original performance, or as an operational check of instrument performance. Completion of every step in this procedure returns the Type RM529 to original factory performance standards. If it is desired to merely touch up the calibration, perform only those steps entiiled Adjust...

## NOTE

The Adjust . . . steps provide a check of instrument performance before the adjustment is made. To prevent recalibration of other circuits when performing a partial calibration, readjust only if the listed tolerance is not met.

## General Information

Any needed maintenance should be performed before proceeding with calibration. Troubles which become apparent during calibration should be corrected using the techniques given in the Maintenance section of this Instruction Manual.
The procedure is arranged in a sequence which allows this instrument to be calibrated with the least interaction of adjustments and reconnection of equipment. If desired, the steps may be performed out of sequence or a step may be done individually. However, some adjustments affect the calibration of other circuits within the instrument. In this case, it will be necessary to check the operation of other parts of the instrument. When a step interacts with others, the steps which need to be checked will be noted.

The location of test points and adjustments is shown in each step. Waveforms which are helpful in determining the correct adjusiment or operation are also shown.

## EQUIPMENT REQUIRED

(see Fig. 6-1)

## General

The following equipment, or its equivalent, is required for complete calibration of the Type RM529. Specifications given are the minumum necessary for accurate calibration of this instrument All test equipment is assumed to be correctly calibrated and operating within the original specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

## Special Test Equipment

For the quickest and most accurate calibration, special calibration fixtures are used where necessary. All calibration fixtures listed under Equipment Required can be obtained Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. DC voltmeter. Minimum sensitivity, 20,000 ohms/volt; accuracy, checked to within $1 \%$ at 25 and 100 volts, and checked to within $3 \%$ at 5300 volts. For example, Triplett Model 630 N A .
2. Constant amplitude sine-wave generator. Frequency 50 kHz and 350 kHz to above $10 \mathrm{MHz}_{\text {; }}$ output amplitude, 200 mV to 1 volt adjustable; amplitude accuracy, $\pm 3 \%$ at 50 kHz and 350 kHz to above 10 MHz . Tektronix Type 191 or equivalent.
3. Test oscilloscope. Bandwidth, DC to 1 MHz ; minimum deflection factor, 0.005 volts/division. Tektronix Type 545B Oscilloscope with Type B Plug-In Unit, and Tektronix P6006 and P6028 Probes, or equivalent.
4. Precision DC voltmeter. Accuracy, within $\pm 0.25$; meter resolution, $50 \mu \mathrm{~V}$ range, 0.02 to 30 volts. For example, Fluke Model 825A meter.
5. Time-Mark generator. Marker outputs of $1 \mu \mathrm{~s}, 5 \mu \mathrm{~s}, 10 \mu \mathrm{~s}$, 0.1 ms and $0.1 \mu \mathrm{~s}$ accuracy, $0.001 \%$. Tektronix Type 184 or equivalent.
6. 'Variable autotransformer. Must be capable of supplying at least 80 watts to the Type RM529 over a voltage range of 96 to 137 volts ( 192 to 274 volts for 230 -volt normal line). If autotransformer does not have an AC voltmeter to indicate output voltage, monitor output with an AC voltmeter (RMS) with range of at least 137 (or 274 ) volts. For example, General Radio WIOMT3W Metered Variac Autotransformer.
7. Composite video signal source. Calibrated signal amplilude of 1 volt, variable from 200 mV to 1 volts. For example, Conrac model AV 12E receiver.
8. Square-wave generator. Frequency of 120 hertz; output amplitude variable from 4 to 12 volts. Tektronix Type 106, or equivalent.
9. Three Terminations. Impedance 75 ohms; accuracy, $\pm 3 \%$; connector, UHF. Tektronix Part No. 011-0023-00.
10. Two cables. Impedance 75 ohms; type RG11/U; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0074-00.
11. Two adapters. Connectors, BNC female to UHF male. Tektronix Part No. 103-0015-00.
12. Adapter. Connectors, BNC female to female. Tektronix Part No. 103-0028-00.
13. Adapter. Connectors, BNC $T$ with two female and one male. Tektronix Part No. 103-0030-00.
Used only to check power-supply ripple in step 2. May be deleted if this check is not made.


Fig. 6-1. Recommended calibration equipment.
14. One capacitor. $2 \mu \mathrm{~F}$ at 150 WVDC. Tektronix Part No. 290-0121-00.
15. One resistor, $27 \mathrm{k} \Omega, 1 / 4$ watt. Tektronix Part No. 315. 0273-00.
16. Adjustment tools (see Fig. 6-1).
a. Screwdriver, shank about 3 inches long by $y_{32}$-inch wide tip. Tektronix Part No. 003-0192-00.
b. Insulated low-capacitance screwdriver, Jaco No. 125, $11 / 2$-inch long shank by $1 / 8$-inch wide metal tip. Tektronix Part No. 003-0000-00.
c. Hexagonal wrench 5 inches long, for 0.100 -inch inside diameter powdered-iron hex slug. Tektronix Part No. $003-$ 0301-00.

## CALIBRATION RECORD AND INDEX

This abridged calibration procedure is provided to aid in checking the operation of the Type RM529. It may be used as a calibration guide by the experienced calibrator, or it may be used as a calibration record. Since the step numbers and titles used here correspond to those used in the complete Calibration procedure, the following short-form list may serve as an index. Characteristics are those listed in the Calibration section of this Instruction Manual.

## Type RM529, Serial No.

## Calibration Date

1. Adjust - VOLTS/CAL AMPL (R620). Page 6-5. -25 volts.
2. Check Low-Voltage Power-Supply Regulation and Ripple.

Page 6-7.
See Table 6.1 and Fig. 6-3A.
[ 3. Adjust HIGH VOLTAGE (R835)
Page 6-8.
-5300 volts.
$\square$ 4. Check High Voltage Regulation.
Page 6.8.
Within $\pm 5 \%$ of -5300 volts.
$\square$ Adjust ASTIG (R864).
Page 6.9.
Well-defined display.
6. Adjust CRT BEAM ROTATOR (R655). Page 6-9. Trace parallel to horizontal graticule lines.
[-] 7. Adjust DC BAL (R115).
Page 6-9.
No vertical trace movement as VOLTS FULL SCALE switch is rotated.

L] 8. Adjust VAR DC BAL (R130).
Page 6-10.
No vertical trace movement as VARIABLE (VOLTS FULL SCALE) control is rotated.
1.] 9 Adjust VERT GAIN (R169).

Page 6-11. 1 volt peak to peak of calibrator signal must produce 140 IEEE units of deflection. VOLTS FULL SCALE switch at 1.0.10. Adjust Vertical 0.2 VOLTS GAIN (R119). Page 6-12. Calibrator signal must produce 140 IEEE units of deflection. VOLTS FULL SCALE switch at 0.2 .11. Check Vertical 0.5 VOLTS FULL SCALE Gain Accuracy

Page 6.12.
Calibrator signal must produce 140 IEEE units of deflection $\pm 4 \%$. VOLTS FULL SCALE switch at 0.5 .12. Adjust TRIG MULTI BIAS (R325). Page 6-13.

Set for stable display.13. Check External Sync. Page 6-14.

Stable display with 20 IEEE units of display. VOLTS FULL SCALE switch at 0.2.

## 14. Check DC RESTORER Switch.

Page 6-14.
Less than $\pm 4$ IEEE units of shift as VOLTS FULL SCALE switch is rotated through its settings.15. Adjust HORIZ GAIN (R568).

Page 6.15.
10.2 cm sweep length.16. Adjust Miller Timing Capacitor (C481). Page 6-16. $80 \mu \mathrm{~s}$ of sweep in 10 cm .17. Adjust $\times 25$ Horizontal Sweep Magnifier Capacitor (C523, SN 1606-up) (C521, SN 101-1605). Page 6-16. Thirty-two $0.1 \mu \mathrm{~s}$ time markers per 10 cm .18. Check $\times 5$ Magnified Sweep Timing. Page 6-17. Sixteen $1 \mu$ s time markers per $10 \mathrm{~cm}, \pm 3 \%$.19. Adjust FIELD 1 SYNC (R360).

Page 6-18. Ramp starts after sixth equalizing pulse.20. Check FIELD Switch.

Page 6-19. ONE field- $31.75 \mu$ s between last horizontal sync pulse and first equalizing pulse.

TWO field- $63.5 \mu$ s between last horizontal sync pulse and first equalizing pulse.21. Adjust SWP/MAG REGIS (R575).

Page 6-20.
Display in center of graticule does not shift horizontally as MAG switch is changed from $\times 25$ to $\times 1$.22. Check Line Selector Brightening Pulse Amplitude.

Page 6-22
At least 100 mV high.23. Adjust VIT LINE SEL RANGE (R458); SN 2997-up.

Page 6-23.
Set for a DC voltmeter reading which is halfway between the two reading obtained when the brightening pulse just started to jump between the 21 st and 22nd lines and the 20th and 21 st lines.24. Check Line Selector Operation, SN 997-up. Page 6-23. With LINE SELECTOR switch set to VARIABLE and

VARIABLE fully counterclockwise, brightening pulse must start on or before the 15 th line. With VARIABLE (LINE SELECTOR) fully clockwise, brightening pulse must start after the first $25 \%$ of the second field.

When LINE SELECTOR switch is set to a numbered position, the brightening pulse must start at the start of that numbered line.25. Check Vertical Amplifier High-Frequency Response. Page 6-24. Refer to Table 6-2.26. Adjust Vertical-Amplifier 1.0 Flat-Frequency Response (C269, L162 and L262).

Page 6-24.
Flat-frequency response from 500 kHz to 5 MHz , $\pm-1 \%$ and flat response from 500 kHz to 8 MHz , $\pm 3 \%$.27. Adjust Vertical Amplifier 0.2 Flat-Frequency Response (C118B).

Page 6-26.
Flat frequency response from 500 kHz to 5 MHz , $\pm 1 \%$.28. Adjust Vertical Amplifier 0.5 Flat-Frequency Response (C118C).

Page 6-26. Flat-frequency response from 500 kHz to 5 MHz , $\pm 1 \%$.29. Adjust Common Mode Rejection (SN 930-up).

Page 6-26.
Minimum display amplitude of common 2 MHz signal.30. Adjust Vertical Amplifier Chroma Frequency Response (T135).

Page 6-27.
Set bottom transformer slug for 100 IEEE units of deflection at 3.58 MHz .

Set top transformer slug for 70 to 85 IEEE units of deflection at 3.18 MHz .

Check for 70 to 85 IEEE units of deflection at 3.98 MHz .
$\square$ 31. Check 1501 Staircase Input.
Four displays in 10 cm (SN 787-up).
Three displays in 10 cm (SN 100-786).32. Adjust Bar Response of Pulse and Bar VIT Signal. Page 6-29.
Bar portion of pulse and bar VIT signal should have no tilt.33. (Optional Method) Check Vertical Amplifier HighFrequency Response. Page 6-30.

## General

In the following calibration procedure, a test equipment setup is shown for each major setup change. Complete control settings are listed below the picture. If only a partial calibration is performed, start with the nearest setup preceding the desired portion.

## NOTE

When performing a complete recalibration, best performance will be provided if each adjustment is made to the exact setting, even if the Check is within the allowable tolerance.

The following procedure uses the equipment listed under Equipment Required. If substitute equipment is used, control settings or setup must be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Remove the oscilloscope from any enclosure and remove the top and bottom covers to provide access to all internal adjustments and test points, including rear-panel connectors.
2. Check that a 160 -IEEE unit $7-\mathrm{cm}$ composite graticule ( $331-0161-00$ ) is installed and that the VIDEO OUTPUT connector is terminated into 75 ohms.
3. Connect the autotransformer (if used) to a suitable power source.
4. Connect the Type RM529 power cord to the autotransformer output (or directly to the power source).
5. Set the autotransformer to 115 (or 230) volts.
6. Set the Type RM529 POWER switch to on. Allow at least 20 minutes warm up for checking the instrument to the given accuracies.

## NOTES



Fig. 6-2. Test equipment setup for steps 1 and 2.

Set Type RM529 controls as follows.

| POWER | On |
| :--- | :--- |
| SCALE ILLUM | $2 / 3$ clockwise |
| FOCUS | Midrange |
| INTENSITY | Fully counterclockwise |
| GAIN | Midrange |
|  |  |
|  | VERTICAL |


| RESPONSE | Flat |
| :--- | :--- |
| DC RESTORER | OFF |
| INPUT | CAL |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL | CALIB |
| SCALE) |  |
| CAL | FULL SCALE |
| POSITION | Midrange |
|  |  |
|  | HORIZONTAL Controls |
| POSITION | Midrange |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 FIELD |
| FIELD | TWO |
| VARIABLE (LINE | Midrange |
| SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

## PROCEDURE

## 1. Adjust -25 VOLTS/CAL AMPL (R620)

## NOTE

Do not reset the -25 VOLTS/CAL AMPL (R620) unless the power-supply voltages are actually out of tolerance or you are planning to perform a complete calibration of the instrument.
a. Test equipment setup is shown in Fig. 6-2.
b. Connect a precision DC voltmeter between the -25 V supply and ground. See Fig. 6-3A.
c. Check for a meter reading of -25 volts.
d. Adjust the -25 VOLTS/CAL AMPL control (R620; see Fig. 6-3B) for a meter reading of -25 volts.
e. Disconnect the voltmeter.
f. Turn off the Type RM529 power.
g. Remove Q804 and Q874.
h. Turn on the Type RM529 power.
i. Connect the precision $D C$ voltmeter between the junction of R885-R881 and ground; see Fig. 6-3C.
i. Note the exact meter reading.
k. Turn off the Type RM529 power.
I. Reinstall Q874 and connect a $1 / 4$ watt, $27 \mathrm{k} \Omega$ resistor between the base of Q874 and ground.
m. Turn the Type RM529 power on.
n. Note the exact meter reading; it will be approximately -0.976 volts.


Fig. 6-3. (A) Location of low-voltage power supply test points. (B) Location of -25 VOLTS/CAL AMPL adjustment. (C) Location of R885-R881 junctions.
o. Check that 1.0 volt minus the meter reading noted in part $i$ of this step equals the meter reading noted in part $n$ of this step.
p. Adjust the -25 VOLTS/CAL AMPL control (R620; see Fig. $6-3 B$ ) until the meter reading equals 1.0 volt minus the meter reading noted in part $j$ of this step.

## NOTE

Without the use of a high input impedance precision $D C$ voltmeter such as item number four in the Equip-
ment Required list, adjustment accuracy within $1 \%$ cannot be obtained.
q. Turn off the Type RM529 power.
r. Remove the $27 \mathrm{k} \Omega$ resistor from Q874 and re-install Q804.
s. Disconnect the voltmeter.
t. Turn the Type RM529 power on.
u. Interaction-May affect operation of all circuits.

1A. Adjust $\mathbf{- 2 5}$ VOLTS/CAL AMPL (R620)
(Alternate method of adjusting the -25 VOLTS/CAL AMPL (R620) using a good DC voltmeter.)

## NOTE

This method of adjustment may lack some of the accuracy of the method outlined in Step 1. Therefore, it is recommended that a precision voltmeter be used to make this adjustment. Factors affecting the accuracy of this method include the calibration of the DC voltmeter and the calculation of the correction factor for meter loading.
a. Test equipment setup is as shown in Fig. 6-2.
b. Connect a DC voltmeter between the -25 volt supply and ground. See Fig. 6-3A.
c. Check for a meter reading of -25 volts.
d. Adjust the -25 VOLTS/CAL AMPL control (R620; see Fig. 6-3B) for a meter reading of -25 volts.
e. Disconnect the voltmeter.
f. Turn off the Type RM529 power.
g. Remove Q804 and connect a $27 \mathrm{k} \Omega, 1 / 4 \mathrm{~W}, 5 \%$ resistor from the base of Q874 to ground.
h. Turn the Type RM529 power on.
i. Connect the DC voltmeter between the junction of R885R881 and ground; see Fig. 6-3C.
i. Note the exact meter reading; it will be approximately -.976 volts.
k. Adjust the -25 VOLTS/CAL AMPL control (R620) for a meter reading of -.97 volts minus the correction factor for meter loading.

Example: a $20,000 \mathrm{ohm} /$ volt voltmeter on the 1.5 volt full scale range has an input resistance of 30,000 ohms and will
cause a $3 \%$ error in this circuit. ( $\frac{\text { Circuit resistance }}{\text { Meter resistance }}=\%$ Load ing Error.)

Therefore, the - 25 VOLT/CAL AMPL control should be adjusted for a reading of -.94 volts ( .97 minus $.03=.94$ ).

## 2. Check Low-Voltage Power-Supply Regulation and Ripple

a. Test equipment setup is shown in Fig. 6-2.
b. Set the CAL switch to .714 F. S. to display 100 IEEE units of vertical deflection.
c. Vary the autotransformer so the line voltage is set $10 \%$ above design center (for $115 \mathrm{~V},+10 \%$ is 126.5 V ) and hold for 1 minute at this voltage extreme. Check voltage regulation and ripple according to the information given in Table 6-1 and Fig. 6-3A.
d. Vary the autotransformer so the line voltage is set $10 \%$ below design center (for $115 \mathrm{~V},-10 \%$ is 103.5 V ) and hold
for 1 minute at this voltage extreme. Check voltage regulation and ripple as given in Table 6-1 and Fig. 6-3A.

TABLE 6-1
Typical Ripple Amplitudes

| Supply | Voltage <br> Deviation | Ripple <br> Amplitude |
| :---: | :---: | :---: |
| $-25 \mathrm{~V}^{-}$ | $\pm 3 \%$ or 0.75 | $\leq 10 \mathrm{mV}$ |
| +100 V | $\pm 5 \%$ or 5 V | $\leq 100 \mathrm{mV}$ |

${ }^{2}$ Deviation from the voltage reading obtained at design center; for example, if -25 V supply indicates a reading of -25.7 V on the DC volimeter at design center, deviation should be within the range from - 24.95 V to -26.45 V .
e. Set the autotransformer for design center line voltage.
f. Disconnect the $D C$ voltmeter and $1 \times$ probe.

## NOTES



Fig. 6-4. Test equipment required for steps 3 and 4.

| POWER | On |
| :--- | :--- |
| SCALE ILLUM | $2 / 3$ clockwise |
| FOCUS | Midrange <br> Adjust for normal display <br> brightness |
| INTENSITY | Midrange |
| GAIN | VERTICALControls |
| RESPONSE | FLAT |
| DC RESTORER | OFF |
| INPUT | CAL |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL | CALIB |
| SCALE) |  |
| CAL | .714 F.S. |
| POSITION | Midrange |

HORIZONTAL Controls

| POSITION | Midrange |
| :--- | :--- |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 FIELD |
| FIELD | TWO |
| VARIABLE (LINE | Midrange |
| $\quad$ SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

## 3. Adjust HIGH VOLTAGE (R835)

## ©

a. Test equipment setup is shown in Fig. 6-4.
b. Connect the DC voltmeter between the CRT cathode (see Fig. 6-5) and ground.
c. Rotate the GAIN control from one extreme to the other.
d. Check that the meter reading varies.
e. Set the GAIN control to its midrange position.
f. Check for a meter reading of -5300 V .
g. Adjust the HIGH VOLTAGE control (R835; see Fig. 6-5) to obtain a meter reading of -5300 V .
h. Interaction-May affect operation of all circuits.

## 4. Check High Voltage Regulation

a. Test equipment setup is shown in Fig. 6-4.
b. Vary the autotransformer so the line voltage is set $10 \%$ above design center and hold for 1 minute at this extreme. Check that the high voltage remains essentially constant (within $\pm 5 \%$ or 265 volts of the -5300 -volt reading).


Fig. 6-5. Location of (A) high-voltage test point, (B) HIGH VOLTAGE adjustment.


Fig. 6-6. Location of ASTIG adjustment.
c. Vary the autotransformer so the line voltage is set $10 \%$ below design center and hold for 1 minute at this extreme.


Fig. 6-7. Location of CRT BEAM ROTATOR adjustment.

Check that the high voltage remains essentially constant (within $\pm 5 \%$ or 265 volts of the -5300 -volt reading).
d. Set the autotransformer for design-center line voltage.
e. Disconnect the DC voltmeter.

## 5. Adjust ASTIG (R864)

a. Set the DISPLAY switch to 2 LINE.
b. Check for well-defined display with normal brightness.
c. Adjust the FOCUS and ASTIG controls (R864; see Fig. 6-6) to obtain a well-defined display using normal brightness.

## 6. Adjust CRT BEAM ROTATOR (R655)

a. Set the DISPLAY switch to 2 FIELD.
b. Check that flat bottoms of the calibrator square waves coincide with the graticule line.
c. Adjust the CRT BEAM ROTATOR control (R655; see Fig. 6-7) so the flat bottom of the calibrator square waves coincides with the graticule line.

## 7. Adjust DC BAL (R115)

a. Set the INPUT switch to A (no signal applied to VIDEO INPUTS A connector).
b. Check for no vertical trace movement as (VERTICAL) VOLTS FULL SCALE switch is changed from 1.0 to 0.2 and 0.5 positions.
c. Adjust the DC BAL. control (R115; see Fig. 6-8) for no vertical movement of the trace as (VERTICAL) VOLTS FULL SCALE switch is set to 0.2 , to 0.5 , and then returned to 1.0 . Repeat this procedure, if necessary, to check that the adustment is made properly.


Fig. 6-8. Location of DC BAL adjustment.

## 8. Adjust VAR DC BAL (R130)

a. Check that the (VERTICAL) VOLTS FULL SCALE switch is set to 1.0 .
b. Check for no vertical trace movement as the (VERTICAL) VARIABLE (VOLTS FULL SCALE) control is rotated from extreme to extreme.


Fig. 6-9. Location of VAR DC BAL adjustment.
c. Adjust the VAR DC BAL control (R130; see Fig. 6-9) for no vertical movement of the trace as the (VERTICAL) VARIABLE (VOLTS FULL SCALE) control is rotated from extreme to extreme.
d. Set the (VERTICAL) VARIABLE (VOLTS FULL SCALE) control to the CALIB position.
e. Interaction-Recheck step 7.

## NOTES



Fig. 6-10. Test equipment required for steps 9 through 11.

## Control settings:

POWER
SCALE ILLUM
FOCUS
INTENSITY
GAIN

## 9. Adjust VERT GAIN (R169)

a. Test equipment setup is shown in Fig. 6-10.
b. Set the (VERTICAL) VOLTS FULL SCALE switch to 1.0.
c. Adjust the VERT GAIN control (R169; see Fig. 6-11) to obtain exactly 140 IEEE units of vertical deflection.


Fig. 6-11. Location of VERT GAIN adjustment.

## 10. Adjust Vertical 0.2 VOLTS FULL SCALE GAIN (R119)

a. Test equipment setup is given in step 9.
b. Set the (VERTICAL) VOLTS FULL SCALE switch to 0.2 .
c. Check for exactly 140 IEEE units of vertical deflection.
d. Adjust the 0.2 VOLTS GAIN control (R119; see Fig. 6-12) for exactly 140 IEEE units of vertical deflection.

## 11. Check Vertcial 0.5 VOLTS FULL SCALE Gain Accuracy

a. Test equipment setup is given in steps 9 and 10 .
b. Set the (VERTICAL) VOLTS FULL SCALE switch to 0.5 .
c. Check that the vertical deflection of the display is 140 IEEE units within a tolerance of $\pm 4$ IEEE units.

O


Fig. 6-12. Location of 0.2 VOLTS GAIN adjustment.

## NOTES



Fig. 6-13. Test equipment required for steps 12, 13 and 14.

| Control settings: |  |
| :--- | :--- |
| POWER | On |
| SCALE ILLUM | 2/3 clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal |
| display brightness |  |
| GAIN | Midrange |


| DISPLAY | 2 FIELD |
| :--- | :--- |
| FIELD | TWO |
| VARIABLE (LINE | Midrange |
| $\quad$ SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

## 12. Adjust TRIG MULTI BIAS (R325)

a. Test equipment setup is shown in Fig. 6-13.
b. Connect a composite video signal to the lower EXT NEG SYNC INPUT connector.
c. Connect a coaxial cable from the upper EXT NEG SYNC INPUT connector to the upper VIDEO INPUTS A connector.
d. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
e. Adjust the source signal level to produce 140 IEEE units of sync amplitude.
f. Check for a stable display.
g. Adjust by first rotating the TRIG MULTI BIAS control (R325; see Fig. 6-14) full counterclockwise. Then, rotate the control slowly clockwise until the display is synchronized; that is, a stationary display is obtained.


Fig. 6-14. Location of TRIG MULTI BIAS adjustment.

## NOTE

If the Type RM529 is used to monitor video signals containing noise, rotate the TRIG MULTI BIAS control about $20^{\circ}$ further clockwise from the point where a stable display was first obtained. If the control is turned too far clockwise, a jittery display will be obtained. The control should always be set within the stable display range.
h. As a check that the TRIG MULTI BIAS control is properly adjusted, set the (VERTICAL) VOLTS FULL SCALE switch to 1.0 , adjust the source signal level for a larger sync amplitude (up to 140 IEEE units) and check that the display remains synchronized.

## 13. Check External Sync

a. Test equipment setup is given in step 12.
b. Set the SYNC switch to EXT.
c. Set the (VERTICAL) VOLTS FULL SCALE switch to 0.5 .
d. Adjust the video source signal level so the vertical deflection is 70 IEEE units of sync amplitude.
e. Check that a stable display is obtained.

## 14. Check DC RESTORER Switch

a. Test equipment setup is given in step 12.
b. Set the front-panel controls to these settings:

| VOLTS FULL SCALE | 1.0 |
| :--- | :--- |
| DC RESTORER | ON |
| INPUT | CAL |
| CALIBRATOR | $.714 \mathrm{~F} . \mathrm{S}$. |
| SYNC | INT |

c. Using the (VERTICAL) POSITION control, position the bottom of the calibrator waveform so it coincides with the 0 IEEE graticule line.
d. Set the INPUT switch to A.
e. Check that the back porch level of the video signal coincides with the 0 IEEE graticule line.
f. Set the INPUT switch to CAL.
g. Set the (VERTICAL) VOLTS FULL SCALE switch from 1.0 to 0.2 , then to 0.5 . Check for $\pm 4$ IEEE units or less vertical movement of the calibrator waveform from 0 IEEE.
h. Set the (VERTICAL) VOLTS FULL SCALE switch to 1.0 and DC RESTORER switch to OFF.
i. Disconnect the video signal from the lower EXT NEG SYNC INPUT connector.
j. Disconnect the jumper coaxial cable.

## NOTES



Fig. 6-15. Test equipment required for steps 15 through 18.

| Control settings: |  |
| :---: | :---: |
| POWER | On |
| SCALE ILLUM | 2/3 clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal display brightness |
| GAIN | Midrange |
| VERTICAL Controls |  |
| RESPONSE | FLAT |
| DC RESTORER | OFF |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL SCALE) | CALIB |
| CAL | . 714 F. S. |
| POSITION | Midrange |
| HORIZONTAL Controls |  |
| POSITION | Midrange |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 FIELD |
| FIELD | TWO |
| VARIABLE (LINE SELECTOR) | Midrange |
| LINE SELECTOR switch | VARIABLE |

## 15. Adjust HORIZ GAIN (R568)

a. Test equipment setup is shown in Fig. 6-15.
b. Connect $5-\mu \mathrm{s}$ and $10-\mu \mathrm{s}$ time markers from the timemark generator to the upper VIDEO INPUTS A connector.
c. Check that the 75 -ohm termination is still connected to the lower VIDEO INPUTS A connector.
d. Apply $100-\mu$ s trigger pulses from the time-mark generator to the upper EXT NEG SYNC INPUT connector.
e. Set the SYNC switch to EXT and the DISPLAY switch to $.125 \mathrm{H} / \mathrm{CM}$.

## NOTE

Use the (VERTICAL) VOLTS FULL SCALE and VARIABLE (VOLTS FULL SCALE) controls to adjust the vertical amplitude of the display in steps 15 through 18.
f. Check for a sweep length of 10.2 cm .
g. Adjust the HORIZ GAIN control (R568; see Fig. 6-16) for a sweep length of 10.2 cm .
h. Interaction-Check step 16.


Fig. 6-16. Location of HORIZ GAIN adjustment.

## 16. Adjust Miller Timing Capacitor (C481)

a. Test equipment setup is given in step 15.
b. Check for $80 \mu s$ of sweep in 10 cm .
c. Adjust the Miller timing capacitor (C481; see Fig. 6-17) for $80 \mu$ s per 10 cm (see Fig. 6-18).
d. Interaction-Check step 15.


Fig. 6-17. Location of C481 adjustment.

## 17. Adjust X25 Horizontal Sweep Magnifier (1) Capacitor (C523, SN 1606-up); (C521, SN 101-1605)

a. Test equipment setup is given in step 15 .


Fig. 6-18. Adjusting C481 for correct $\times 1$ sweep timing.
b. Set the time-mark generator for $1 \mu$ s time markers.
c. Set the (HORIZONTAL) MAG switch to $\times 25$.
d. Check for 32 time markers per 10 cm .
e. Adjust the horizontal sweep magnifier capacitor (C523 or C521; see Fig. 6-19), primarily for sweep timing and secondarily for linearity. For correct timing, 32 time markers per 10 cm should be displayed (see Fig. 6-20). For checking linearity, display should show 8 time markers for any $2.5-\mathrm{cm}$ portion of the display.


Fig. 6-19. Location of (A) C521 SN 101-1605 (B) C523 SN 1606 and up adjustment.

## NOTE

To minimize horizontal jitter, set the time-mark generator trigger rate for 1 ms trigger output. After completing this step, set trigger rate to 0.1 ms .


Fig. 6-20. Adjusting C521 for optimum $\times 25$ sweep linearity.

## 18. Check X5 Magnified Sweep Timing

a. Test equipment setup is given in step 15.
b. Set the time-mark generator output for $1-\mu s$ time-marker output and check that the trigger rate is 0.1 ms .
c. Set the (HORIZONTAL) MAG switch to $\times 5$.
d. Check for $16 \mu \mathrm{~s}$ of sweep time per 10 cm (see Fig. 6-21). Sweep-fiming tolerance should be within $\pm 3 \mathrm{~mm}$.
e. Disconnect the time markers and external trigger.


Fig. 6-21. Checking the $\times 5$ sweep timing.

NOTES


Fig. 6-22. Test equipment required for steps 19 through 21.

## Control settings:

```
POWER
SCALE ILLUM
FOCUS
INTENSITY
GAIN
```


## On

2/3 clockwise
Midrange
Adjust for normal display brightness
Midrange

## VERTICAL Controls

| RESPONSE | FLAT |
| :--- | :--- |
| DC RESTORER | ON |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL |  |
| $\quad$ SCALE) | CALIB |
| CAL | .714 F.S. |
| POSITION | Midrange |

HORIZONTAL Controls

POSITION
SYNC
MAG
DISPLAY
FIELD

Midrange
INT
$\times 25$
2 FIELD
TWO

## VARIABLE (LINE

 SELECTOR)LINE SELECTOR switch
Midrange
VARIABLE
a. Test equipment setup is shown in Fig. 6-22.
b. Connect a 1 -volt composite video signal to the upper VIDEO INPUTS A connector.
c. Check that a 75 -ohm termination is connected to the lower VIDEO INPUTS A connector.
d. Set the test oscilloscope controls as follows:

| Sweep Rate | $50 \mu \mathrm{~s} / \mathrm{cm}$ |
| :--- | :--- |
| Triggering | $+\mathrm{Ext}, \mathrm{AC}$ |
| Signal Input Coupling | AC |
| Vertical Deflection Factor | $5 \mathrm{Volts} / \mathrm{cm}$ |
| (with 10× attenuator probe) |  |

e. Connect the $10 \times$ probe from the vertical input connector to the junction of D370 and C370 (see Fig. 6-23).
f. Connect the $1 \times$ probe from the external trigger input connector to the collector of Q344.
g. Check that the ramp starts just after the sixth equalizing pulse.


Fig. 6-23. Location of D370/C370 junction.
h. Adjust by first rotating the FIELD 1 SYNC control (R360; see Fig. 6-24) fully counterclockwise. Then, rotate the control slowly in a clockwise direction until the ramp starts just after the sixth equalizing pulse (see Fig. 6-25A). The sixth equalizing pulse is the last pulse in the equalizing-pulse group following the vertical sync pulses. Fig. $6-25 \mathrm{~B}$ and $6-25 \mathrm{C}$ show two possible displays that can be obtained when the control is incorrectly adjusted.
i. Disconnect the $10 \times$ and $1 \times$ probes.


Fig. 6-24. Location of FIELD 1 SYNC adjustment.

## 20. Check FIELD Switch

a. Test equipment setup is given in step 19.

(a) Correct display.

(b) Incorrect display; control R360 set too far counterclockwise.

(c) Incorrect display; control R360 set too far clockwise.

Fig. 6-25. Adjusting the FIELD 1 SYNC control (R360) for proper triggering. Displays obtained on the test oscilloscope CRT.
b. Set the FIELD switch to TWO.

NOTE
If vertical sync pulse is not completely displayed, position it to the horizontal center of the viewing area with the (HORIZONTAL) POSITION control.

## Calibration-Type RM529

c. Check for a horizontal distance of $1 \mathrm{H}(63.5 \mu \mathrm{~s})$ between the last horizontal sync pulse and the first equalizing pulse (see Fig. 6-26A). This indicates that field one is displayed at the center of the CRT.
d. Set the SYNC switch to EXT and back to INT several times to check that a field display is obtained each time the SYNC switch is returned to the INT position. This is a double check on step 19. A stable display of field one means that R360 is adjusted properly.
e. Set the FIELD switch to ONE.

(b) FIELD switch set to ONE.

Fig. 6-26. Checking for proper field display when operating the FIELD and SYNC switches.
f. Check for $0.5 \mathrm{H}(31.75 \mu \mathrm{~s})$ horizontal distance between the last horizontal sync pulse and the first equalizing pulse (see Fig. 6-26B). This indicates that field two is displayed at the center of the CRT.
g. Repeat part $d$, except check that a field two display is obtained each time the SYNC switch is returned to INT.

## 21. Adjust SWP/MAG REGIS (R575) Pulse Amplitude

a. Test equipment setup is given in step 19.
b. Using the (HORIZONTAL) POSITION control, position the display so the center of the vertical-sync pulse group coincides with graticule center (see Fig. 6-27A).


Fig. 6-27. Adjusting the SWP/MAG REGIS control (R575) for proper display registration. The Horizontal MAG switch was set to (A) $\times 25$ (B) $\times 1$.
c. Set the (HORIZONTAL) MAG switch to $\times 1$.
d. Check that the vertical-pulse group coincides with graticule center (see Fig. 6-27B).
e. Adjust the SWP/MAG REGIS control (R575; see Fig. $\therefore 28)$ so the vertical pulse group coincides with graticule enter (see Fig. 6-27B).
f. To check whether the adjustment has been set properly, set the (HORIZONTAL) MAG switch to $\times 25$ and then to $\times 1$. If the display as observed at graticule center shifts horizontally, readjust the SWP/MAG REGIS control (R575) for no horizontal shift of the display when switching from $\times 25$ to $\times 1$.
g. Disconnect the composite video signal.


Fig. 6-28. Location of SWP/MAG REGIS adjustment.

## NOTES

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Fig. 6-29. Test equipment required for steps 22 through 24.
Control settings:

POWER
SCALE ILLUM
FOCUS
INTENSITY
GAIN

On
2/3 clockwise
Midrange
Adjust for normal display brightness
Midrange

## VERTICAL Controls

| RESPONSE | FLAT |
| :--- | :--- |
| DC RESTORER | OFF |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL |  |
| SCALE) | CALIB |
| CAL | $.714 \mathrm{~F} . \mathrm{S}$. |
| POSITION | Midrange |

## HORIZONTAL Controls

POSITION
SYNC
MAG
DISPLAY
FIELD
VARIABLE (LINE SELECTOR)
LINE SELECTOR switch

Midrange
INT
$\times 1$
LINE SELECTOR $.125 \mathrm{H} / \mathrm{CM}$
TWO
Midrange
21

## 22. Check Line Selector Brightening Pulse Amplitude

a. Test equipment setup is shown in Fig. 6-29.
b. Apply one volt of composite video to the upper VIDEO INPUTS A connector.
c. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
d. Connect a 75 -ohm coaxial cable from the VIDEO OUTPUT connector of the Type RM529 to the vertical input connector of the test oscilloscope.
e. Connect a $1 \times$ probe from the appropriate Trigger Input connector of the test oscilloscope to the junction of D377 and D387 (see Fig. 6-30).
f. Set the test oscilloscope controls as follows:

| Input Selector | AC |
| :--- | :--- |
| Volts/Div | 0.02 |
| Time/Div | 2 ms |
| Triggering Mode | Adjusted for stable |
| display |  |
| Trigger Slope | + External |

The external triggering signal must be at the video field rate.
g. Check that the brightening pulse amplitude is at least 100 mV high.


Fig. 6-30. Location of D377/D387 junction.

## 23. Adjust VIT LINE SEL RANGE (R458); SN 2997-up

a. Test equipment setup is given in step 22.
b. Connect a DC voltmeter between the center arm of R458 and ground.

## NOTE

Before proceeding with this step, the position of the LINE SELECTOR should be checked to insure that the knob has not been misaligned.


Fig. 6-31. Location of VIT LINE SEL RANGE control (R458).
c. Adjust the VIT LINE SEL RANGE control (R458; see Fig. 6-31) so the brightening pulse just starts to jump between the 21 st and 22 nd lines as observed on the test oscilloscope.

## NOTE

LINE 10 starts at the first horizontal pulse following the last equalizing pulse in both fields (field one and two). Lines 16 through 21 can be found by counting forward from this point of reference.
d. Note the DC voltmeter reading.
e. Adjust the VIT LINE SEL RANGE control (R458) so the brightening pulse just starts to jump between the 21 st and 20th lines as observed on the test oscilloscope.
f. Note the DC voltmeter reading.
g. Adjust the VIT LINE SEL RANGE control (R458) for a DC voltmeter reading halfway between the two readings noted in parts $d$ and $f$ of this step.
h. Disconnect the DC voltmeter.

## 24. Check Line Selector Operation; SN 2997-up

a. Test equipment setup is given in step 22.
b. Set the LINE SELECTOR switch to VARIABLE and rotate the VARIABLE (LINE SELECTOR) control fully counterclockwise.
c. Check the position (in time) of the brightening pulse on the test oscilloscope. The brightening pulse must start on or before the 15th line.
d. Rotate the VARIABLE (LINE SELECTOR) control fully clockwise.
e. Check the position (in time) of the brightening pulse on the test oscilloscope. The brightening pulse must start after the first $25 \%$ of the second field.
f. Set the LINE SELECTOR switch to each numbered line position.
g. Check that the brightening pulse starts at the start of the line to which the LINE SELECTOR switch is set.
h. Set the FIELD switch to ONE and repeat parts $b$ through g.

## NOTE

LINE 10 starts at the first horizontal pulse following the last equalizing pulse in both fields (field one and two). Lines 16 through 21 can then be found by counting forward from this point of reference.
i. Disconnect the composite video signal and the test oscilloscope from the Type RM529.


Fig. 6-32. Test equipment required for steps 25 through 30.

| Control settings: |  |
| :---: | :---: |
| POWER | On |
| SCALE ILLUM | 2/3 clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal display brightness |
| GAIN | Midrange |
| VERTICAL Controls |  |
| RESPONSE | FLAT |
| DC RESTORER | OFF |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL SCALE) | CALIB |
| CAL | . $71.4 \mathrm{~F} . \mathrm{S}$. |
| POSITION | Midrange |

HORIZONTAL Controls

| POSITION | Midrange |
| :--- | :--- |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 FIELD |
| FIELD | ONE |
| VARIABLE (LINE | Midrange |
| SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

## 25. Check Vertical Amplifier High-Frequency Response ${ }^{3}$

a. Test equipment setup as shown in Fig. 6-32.
b. Apply a $50-\mathrm{kHz}$ sine-wave signal from the constant amplitude sine-wave generator to the VIDEO INPUT A connector.
c. Adjust the constant amplitude sine-wave generator for 100 IEEE units of vertical deflection; this is the reference amplitude.
d. Follow the remaining sequence of instructions given in Table 6-2 to check the vertical-amplifier frequency response and rolloff for all the front-panel control positions listed.

## 26. Adjust Vertical-Amplifier 1.0 Flat-Frequency Response (C269, L162 and L262)

a. Test equipment setup is given in step 25.
b. Check the vertical-amplifier response from 500 kHz to 8 MHz . It should be flat within $\pm 1 \%$ to $5 \mathrm{MHz}, \pm 3 \%$ to 8 MHz .
c. Adjust the vertical amplifier components (see Fig. 6-33) as listed in Table 6-3 to obtain flat frequency response from 500 kHz to 8 MHz within $\pm 1 \%$ to 5 MHz and flat to within $\pm 3 \%$ to 8 MHz .

[^0]TABLE 6-2

## Checking Vertical Amplifier Frequency Response

| RESPONSE <br> Switch <br> Set To: | Signal ${ }^{4}$ <br> To: <br> INPUT <br> Switch <br> Set To: | VARIABLE IVOLTS FULL SCALE) Set To: | (VERTICAL) <br> VOLTS <br> FULL <br> SCALE <br> Switch <br> Set To: | Check or Procedure |
| :---: | :---: | :---: | :---: | :---: |
| FLAT | A | CALIB | 1.0 | Check the flat frequency response from 500 kHz to $8 \mathrm{MHz}^{5}$; within $\pm 1 \%( \pm 0.1 \mathrm{~dB})$ or 1 IEEE unit to $5 \mathrm{MHz}, \pm 3 \%$ $( \pm 0.3 \mathrm{~dB})$ or 3 units to 8 MHz . |
|  |  |  | 0.2 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
|  |  |  | 0.5 |  |
|  |  | Fully CCW | 1.0 | Check for flat frequency response from 500 kHz to $5 \mathrm{MHz}^{6}$; within $\pm 1 \%( \pm 0.1 \mathrm{~dB})$ or 1 IEEE unit. |
|  | B | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units or reference amplitude at 50 kHz . |
|  |  |  |  | Check for flat frequency response from 500 kHz to $8 \mathrm{MHz}_{\text {; }}$ within $\pm 1 \%( \pm 0.1 \mathrm{~dB})$ to $5 \mathrm{MHz}, \pm 3 \%( \pm 0.3 \mathrm{~dB})$ to 8 MHz . |
| LOW PASS | A | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplifude at 50 kHz . |
|  |  |  |  | Check for vertical deflection of 25 units or less at 500 kHz . |
| FLAT | A | CALIB | 1.0 | ${ }^{7}$ Set the constant amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz . |
| HIGH PASS | A | CALIB | 1.0 | Check for exactly 100 IEEE units of vertical deflection at 3.58 MHz (center frequency); 65 to 85 units at 3.18 MHz and 3.98 $\mathrm{MHz} .{ }^{8}$ |
| IEEE | A | CALIB | 1.0 | Set the constant amplitude sine-wave generator for 100 IEEE units of vertical deflection at 50 kHz . |
|  |  |  |  | Check high-frequency rolloff at the following points: |
|  |  |  |  | At $350 \mathrm{kHz}-94$ to 97.5 units. At $1 \mathrm{MHz}-70$ to 80 units. At $2 \mathrm{MHz}-31.2$ to 42.5 units. At $3.6 \mathrm{MHz}-7$ to 14 units. |

## NOTE

Adjust $\mathrm{Cl}^{\circ}{ }^{\circ}$ ' (see Fig. 6-34) so the frequency response is down approximately $1 \%$ from the response at the 5 MHz point.

TABLE 6-3
Vertical Amplifier Flat-Frequency
Response Adjustments Shown in Fig. 6-33

| Adiustment | Affects Frequency <br> Response in These <br> Frequency Ranges |
| :---: | :--- |
| C269 | 5108 MHz <br> $2 t 06 \mathrm{MHz}$, particularly <br> at 2.5 MHz |
| Physical spacing of <br> R162 and R262 | 3106 MHz, particularly <br> at 4 MHz |
| L162 and L262 Slugs | 5 to 10 MHz |

4 Apply the signal to the upper VIDEO INPUT connector as indicated in the column and terminate the appropriate lower VIDEO INPUT connector with a 75 -ohm termination.

If frequency response cannot be oblained within the tolerance specified, perform step 26 before completing the checks given in the remaining portion of Table 6-2.

If frequency response within the tolerance cannot be obtained for the 0.2 and 0.5 vertical VOLTS FULL SCALE switch position, perform step 27 for the 0.2 position and step 28 for 0.5 .

This is a preliminary sefup procedure for performing the high-pass frequency-response check that follows.

If this frequency-response characteristic cannot be met, perform step 30.

Adjust C133 as part of this step only if instrument serial number is below 5N 930.


Fig. 6-33. Location of C269, R162, R262, L162 and 1262.
d. Recheck the response between 500 kHz and 8 MHz at several points to determine if any of the adjustments in this , step need to be readjusted to obtain the desired response.


Fig. 6-34. Location of C133 (A) Vertical Response Switch SN 101. 929, (B) Vertical Volts Full Scale Switch SN 930 and up.

## 27. Adjust Vertical-Amplifier 0.2 Flat-Frequency Response (C118B)

a. Test equipment setup is given in step 25 .
b. Set the (VERTICAL) VOLTS FULL SCALE switch to 0.2 .
c. Set the constant-amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz .
d. Check for a flat-frequency response within $\pm 1 \%$ from 500 kHz to 5 MHz .
e. Adjust C 118 B (see Fig. 6-35) to obtain flat-frequency response from 500 kHz to 5 MHz within $\pm 1 \%$.
28. Adjust Vertical-Amplifier 0.5 Flat-Frequency Response (C118C)
a. Test equipment setup is given in step 25 .
b. Set the (VERTICAL) VOLTS FULL SCALE switch to 0.5 .
c. Set the constant-amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz .
d. Check for a flat-frequency response within $\pm 1 \%$ from 500 kHz to 5 MHz .
e. Adjust C118C (see Fig. 6-35) to obtain flat-frequency response from 500 kHz to 5 MHz within $\pm 1 \%$.

## 29. Adjust Common Mode Rejection (SN 930-up)

a. Test equipment setup is given in step 25 .
b. Disconnect the constant-amplitude sine-wave generator from the A VIDEO INPUT connector.


Fig. 6-35. Loration of C 118 B and C 118 C adjustments.
c. To the constant-amplitude sine-wave generator 50 ohm GR to BNC termination connect a female to female BNC adapter and a BNC T connector to the female to female BNC adapter. Connect a 75 -ohm coaxial cable from one end of the T connector to the upper A VIDEO INPUT connector. Connect another 75 ohm coaxial cable from the other end of the T connector to the upper B VIDEO INPUT connector.
d. Connect a 75 ohm termination to the lower B VIDEO INPUT connector.
e. Set the VOLTS FULL SCALE switch to 1.0 .
f. Apply 40 IEEE units of 2 MHz signal from the constantamplitude sine-wave generator to the Type RM529.
g. Set the INPUT switch to A-B.
h. Adjust Cl 33 for minimum display amplitude. If desired, the VOLTS FULL SCALE switch may be set to provide a larger signal.
i. Recheck steps 25 through 28 and this step several times to eliminate any interaction.
i. Remove the female to female BNC adapter, the BNC T connector and the two 75 ohm cables. Remove the 75 ohm termination from the lower B VIDEO INPUT connector and reconnect the constant-amplitude sine-wave generator to the upper A VIDEO INPUT connector.

## 30. Adjust Vertical-Amplifier Chroma Frequency Response (T135)

a. Test equipment setup is given in step 25 .
b. Set the RESPONSE switch to FLAT and the VOLTS FULL SCALE switch to 1.0.
c. Set the constant-amplitude sine-wave generator for 100 IEEE units of reference amplitude at 50 kHz .
d. Set the constant-amplitude sine-wave generator for an output frequency of 3.58 MHz .
e. Set the RESPONSE switch to HIGH PASS.
f. Check for 100 IEEE units of vertical deflection.
g. Adjust the bottom powdered-iron slug in T135 (see Fig. 6-36) to obtain 100 IEEE units of vertical deflection.
h. Set the constant-amplitude sine-wave generator for an output frequency of 3.18 MHz .
i. Check for 65 to 85 IEEE units of vertical deflection.
i. Adjust the top slug in T 135 to obtain 65 to 85 IEEE units of vertical deflection.
k. Set the constant-amplitude sine-wave generator for an output frequency of 3.98 MHz .
I. Check that the vertical deflection of the display is 65 to 85 IEEE units in amplitude. If necessary, repeat steps $d$ through k to obtain proper frequency response characteristics.
m . After completing the adjustment of T135 and the checks in Table 6-2, disconnect the constant-amplitude sine-wave generator from the Type RM529.


Fig. 6-36. Location of transformer T135.

## NOTES



Fig. 6-37. Test equipment required for steps 31 and 32 .

## Control settings:

| POWER | On |
| :---: | :---: |
| SCALE ILLUM | $2 / 3$ clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal display brightness |
| GAIN | Midrange |
| VERTICAL | Controls |
| RESPONSE | FLAT |
| DC RESTORER | ON |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL SCALE) | CALIB |
| CAL | . 714 F. S. |
| POSITION | Midrange |

HORIZONTAL Controls

| POSITION | Midrange |
| :--- | :--- |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | 2 LINE |
| FIELD | ONE |
| VARIABLE (LINE | Midrange |
| $\quad$ SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

## 31A. Check J501 Staircase Input (SN 787-up)

a. Test equipment setup is shown in Fig. 6-37.
b. Wire the 9-pin plug connector (Tektronix Part No. 134-$0049-00$ ) as shown in Fig. 6-38. Make sure that the $2-\mu \mathrm{F}$ capacitor is in series between the Type RM529 J501 connector pin C


Fig. 6-38. Front view of 9-pin plug connector (Tektronix Part No. 134-0049-00) showing jumper wire connections to cause relay K385 to be energized whenever the plug is in place.
and the output of the square-wave generator.
c. Connect the plug to J501 on the Type RM529.
d. Connect a 12 -volt, 120 -hertz signal from a square-wave generator to pin $C$ of the plug via the $2-\mu \mathrm{F}$ capacitor.
e. Connect a test oscilloscope to the monitoring point to measure the output amplitude of the square-wave generator.
f. Apply one volt of composite video to the upper VIDEO INPUTS A connector.
g. Connect a 75 -ohm termination to the lower VIDEO $\mathbb{N}$ PUTS A connector.
h. Check for a display as shown in Fig. 6-39A. Note righthand display position.
i. Reduce the signal from the square-wave generator to 8 volts.
i. Check for a display as shown in Fig. 6-39B. Note righthand display position.
k. Reduce the signal from the square-wave generator to 4 volts.
I. Check for a display as shown in Fig. 6-39C. Note righthand display position.
m . Check that each display had some separation from its neighbors.

## 31B. Check J501 Staircase Input (SN 100-786)

a. Test equipment setup is shown in Fig. 6-37.
b. Wire the 9 -pin plug connector (Tektronix Part No. 134-$0049-00$ ) as shown in Fig. 6-38. Make sure that the $2-\mu \mathrm{F}$ capacitor is in series between the Type RM529 J501 connector pin C and the output of the square-wave generator.
c. Connect the plug to J 501 on the Type RM529.
d. Connect a 12 -volt, 120 -hertz signal from a square-wave generator to pin $C$ of the plug via the $2-\mu \mathrm{F}$ capacitor.
e. Connect a test oscilloscope to the monitoring point to measure the output amplitude of the square-wave generator.
f. Apply one volt of composite video to the upper VIDEO INPUTS A connector.
g. Connect a 75 -ohm termination to the lower VIDEO $\mathbb{N}$ PUTS A connector.
h. Check-For a display as shown in Fig. 6-40A. Note right-hand display position.
i. Reduce the signal from the square-wave generator to 6 volts.
i. Check-For a display as shown in Fig. 6-40B. Note right-hand display position.


Fig. 6-39. Checking to insure that four displays per 10 centimeters can be obtained.
k. Check-That each display has some separation from its neighbors.

## 32. Adjust Bar Response of Pulse and Bar VIT (1) Signal (SN 4400-up only)

a. Connect a 1 -volt composite video signal to the upper A VIDEO INPUTS connector.
b. Check that a 75 -ohm termination is connected to the lower A VIDEO INPUTS connector.


Fig. 6-40. Checking to insure that three displays per 10 centimeters can be oblained.
c. Set the Type RM529 front-panel controls as follows:

| POWER | On |
| :---: | :---: |
| SCALE ILLUM | $2 / 3$ clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal display brightness |
| GAIN | As is |
| VERTICAL | Controls |
| RESPONSE | FLAT |
| DC RESTORER | ON |
| INPUT | A |
| VOLTS FULL SCALE VARIABLE (VOLTS FULL SCALE) | Adjusted for 100 IEEE units of pulse and bar VIT pulse |
| CAL | . 714 F . S. |
| POSITION | Midrange |

## HORIZONTAL Controls

POSITION
SYNC
MAG
DISPLAY

VARIABLE (LINE SELECTOR
FIELD
LINE SELECTOR switch

Midrange
INT
$\times 1$
LINE SELECTOR . 125 H/CM

Midrange

Set as required to obtain pulse and bar VIT signal
d. Adjust Cl 67 (see Fig. 6-41) for optimum flat top, i.e., no tilt of bar top, of the bar portion of the pulse and bar VIT signal.


Fig. 6-41. Location of C167.

## 33. (Optional Method) Check Vertical Amplifier High-Frequency Response

Control settings:

| POWER | On |
| :--- | :--- |
| SCALE ILLUM | $2 / 3$ clockwise |
| FOCUS | Midrange |
| INTENSITY | Adjust for normal <br> display brightness |
| GAIN | Midrange |



Fig. 6-42. Waveforms showing the display which will result when 1 -volt of multi-burst signal is connected to the Type RM529 and the RESPONSE switch is set to (A) FLAT, (B) IEEE, (C) LOW PASS and (D) HIGH PASS.

| VERTICAL C | Controls |
| :---: | :---: |
| RESPONSE | FLAT |
| DC RESTORER | ON |
| INPUT | A |
| VOLTS FULL SCALE | 1.0 |
| VARIABLE (VOLTS FULL SCALE) | CALIB |
| CAL | . 714 F. S. |
| POSITION | Midrange |
| HORIZONTAL | Controls |
| POSITION | Midrange |
| SYNC | INT |
| MAG | $\times 1$ |
| DISPLAY | . $125 \mathrm{H} / \mathrm{CM}$ |


| FIELD | ONE |
| :--- | :--- |
| VARIABLE (LINE | Midrange |
| $\quad$ SELECTOR) |  |
| LINE SELECTOR switch | VARIABLE |

a. Connect to upper VIDEO INPUTS A connector 1 volt of multi-burst signal.
b. Connect a 75 -ohm termination to the lower VIDEO INPUTS A connector.
c. Check each position of the RESPONSE switch for the display shown in Fig. 6-42.

This completes the calibration of the Type RM529. Disconnect all test equipment. If the instrument has been completely calibrated to the tolerances given in this procedure, it will perform to the limits given in the Characteristics section of this Instruction Manual.

| A or amp | amperes |  | Inductance |
| :---: | :---: | :---: | :---: |
| $A C$ or ac | alternating current | $\lambda$ | lambda-wavelength |
| AF | audio frequency | $\gg$ | large compared with |
| $\boldsymbol{\alpha}$ | alpha-common-base current amplification factor | $<$ | less than |
| AM | amplitude modulation | LF | low frequency |
| $\approx$ | approximately equal to | lg | length or long |
| $\beta$ | beta-common-emitter current amplification factor | LV | low voltage |
| BHB | binding head bross | M | mega or $10^{6}$ |
| BHS | binding head steel | m | milli or $10^{-3}$ |
| BNC | baby series ' N ' connector | MS or meg | megohm |
| $\times$ | by or limes | ${ }_{\mu}^{\mu}$ | micro or $10^{-6}$ megacycle |
| C | carbon | met. | metal |
| cap. | capacitor | MHz | megahertz |
| cer | ceramic | mm | millimeter |
| cm | centimeter | ms | millisecond |
| comp | composition | - ${ }^{\text {d }}$ | minus |
| conn | connector | mtg hdw | mounting hardware |
| $\sim$ | cycle | $n \quad \#$ | nano or $10^{-9}$ |
| c/s or cps | cycles per second | no. or \# | number |
| CRT | cathode-ray tube | ns | nanosecond |
| csk | countersunk | OD | outside diameter |
| $\Delta$ | increment | OHB | oval head brass |
| dB | decibel | OHS | oval head steel |
| dBm | decibel referred to one milliwatt | $\Omega$ | omega-ohms |
| DC or de | direct current | $\omega$ | omega-angular frequency |
| DE | double end | $p$ | pico or $10^{-12}$ |
|  | degrees | 1 | per |
| ${ }^{\circ} \mathrm{C}$ | degrees Celsius (degrees centigrade) | \% | percent |
| ${ }^{\circ} \mathrm{F}$ | degrees Fahrenheit | PHB | pan head brass |
| ${ }^{\circ} \mathrm{K}$ | degrees Kelvin | $\boldsymbol{\phi}$ | phi-phase angle |
| dia | diameter | $\pi$ | pi-3.1416 |
| $\div$ | divide by | PHS | pan head steel |
| div | division | + | plus |
| EHF | extremely high frequency | $\pm$ | plus or minus |
| elect. | electrolytic | PIV | peak inverse voltage |
| EMC | electrolytic, metal cased | pistc | plastic |
| EMI | electromagnetic interference (see RFI) | PMC | paper, metal cased |
| EMT | electrolytic, metal tubular | poly | polystyrene |
| $\stackrel{\varepsilon}{\Sigma}$ | epsilon-2.71828 or \% of error | prec | precision |
| $\geq$ | equal to or greater than | PT | paper, tubular |
| $\leq$ | equal to or less than | PTM | paper or plastic, tubular, molded |
| $\stackrel{-}{\text { ext }}$ | external | pwr | power |
| F or 1 | farad | Q | figure of merit |
| F \& 1 | focus and intensity | RC | resistance capacitance |
| FH8 | flot head brass | RF | radio frequency |
| FHS | flat head steel | RFI | radio frequency interference (see EMI) |
| Fil HB | fillister heod brass | RHB | round head brass |
| Fil HS | fillister head steel | R RHS R | rho-resistivity round head steel |
| FM | frequency modulation | RHS | round head steel revolutions per minute |
| ft | feet or fool | r/min or rpm <br> RMS | root mean square |
| G | acceleration due to gravity | s or sec. | second |
| Ge | germanium |  | single end |
| GHz | gigahertz | Si | silicon |
| GMV | guaranteed minimum value | ${ }_{\ll}^{\text {SN }}$ or S/N | serial number |
| GR | General Radio |  | small compared with tera or $10^{12}$ |
| ${ }_{H}$ | greater than | TC | tera or terature compensated |
| $h$ | height or high | TD | turnel diode |
| hex. | hexagonal | THB | truss head bross |
| HF | high frequency | 0 | theto-angular phase displacement |
| HHB | hex head brass | thk | thick |
| HHS | hex head steel | THS | truss head steel |
| HSB | hex socket brass | tub. | tubular |
| HSS | hex socket steel | UHF | ultra high frequency |
| HV | high voltage | $\checkmark$ | volt |
| Hz | heriz (cycles per second) | VAC | volts, alternating current |
| 10 | inside diameter | var | variable |
| IF | intermediate frequency | VDC | volts, direct current |
| in. | unch or inches | VHF | very high frequency |
| incd | incandescent | WSWR | voltage standing wave ratio watt |
| ${ }_{\text {int }}$ | infinity | w | wide or width |
| int | internal | w/ | with |
| k | kilohms or kilo (103) | w/o | without |
| k $\Omega$ | kilohm | WW | wire-wound |
| kc | kilocycle | xmfr | transformer |
| kHz | kilohertz |  |  |

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

## SPECIAL NOTES AND SYMBOLS

$\times 000$ Part first added at this serial number
$00 \times$ Part removed after this serial number
*000-0000-00 Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, Inc., or reworked or checked components.

Use 000-0000-00 Part number indicated is direct replacement.
(1) Screwdriver adjustment.

Control, adjustment or connector.

## SECTION 7

## ELECTRICAL PARTS LIST

Values are fixed unless marked Variable.

| Ckt. No. | Tektronix <br> Part No. |  | Description |  |
| :--- | :---: | :--- | :--- | :--- |
|  |  |  | Bulbs |  |
|  |  |  | CAL |  |
| B242 | $150-030$ | Neon, NE-2V | Graticule Light |  |
| B604 | $150-001$ | Incandescent, \# 47 | Graticule Light |  |
| B605 | $150-001$ | Incandescen, \# 47 |  |  |
| B864 | $150-030$ | Neon, NE-2V |  |  |
| B865 | $150-030$ | Neon, NE-2V | POWER ION |  |

## Capacitors

Tolerance $\pm 20 \%$ unless otherwise indicated.

| Cl01 | 281-509 | 15 pf | Cer |  | 500 v | 10\% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C104 | Use 285-623 | 0.47 f | PTM |  | 100 v |  |  |
| C106 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C113 | Use 281-0604-00 | 2.2 pf | Cer |  | 500 v | $\pm 0.25 \mathrm{pf}$ |  |
| C118B | 281-061 | 5.5-18 pf | Cer | Var |  |  |  |
| C118C | 281.063 | 9.35 pf | Cer | Var |  |  |  |
| C118D | Use 281-0509.00 | 15 pf | Cer |  | 500 v | 10\% |  |
| C122 | 283-004 | $0.02 \mu \mathrm{f}$ | Cer |  | 150 v |  |  |
| C124 | 283-003 | $0.01 \mu \mathrm{f}$ | Cer |  | 150 v |  |  |
| Cl 30 | 283-0006-00 | $0.02 \mu \mathrm{f}$ | Cer |  | 500 v |  | X328-up |
| C133 | 281-060 | 2-8 pf | Cer | Var |  |  |  |
| C134 | Use 281-0629-00 | 33 pf | (nominal value) | Selected |  |  |  |
| C135 | 281.620 | 21 pf | Cer |  | 500 v | 1\% |  |
| C136 | 283-600 | 43 pf | Mica |  | 500 v | 5\% |  |
| C137 | 281-503 | 8 pf | Cer |  | 500 v | $\pm 0.5 \mathrm{pf}$ |  |
| C138 | 281-594 | 150 pf | Cer |  | 500 v | 5\% |  |
| C139 | 283-594 | $0.001 \mu \mathrm{f}$ | Mica |  | 100 v | 1\% |  |
| C144 | 281-558 | 18 pf | Cer |  | 500 v |  |  |
| C160 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C163 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| Cl 65 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| Cl 67 | 281-0063-00 | 9.35 pf | Cer | Var |  |  | X4400-up |
| C198 | 290-217 | $250 \mu \mathrm{f}$ | EMT |  | 12 V |  |  |
| C201 | 281-509 | 15 pf | Cer |  | 500 v | 10\% |  |
| C204 | Use 285-623 | $0.47 \mu \mathrm{f}$ | PTM |  | 100 v |  |  |
| C206 | 283.001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C213 | Use 281-0604-00 | 2.2 pf | Cer |  | 500 v | $\pm 0.25 \mathrm{pf}$ |  |
| C236 | 283-600 | 43 pf | Mica |  | 500 v | 5\% |  |
| C237 | 281-503 | 8 pf | Cer |  | 500 v | $\pm 0.5 \mathrm{pf}$ |  |
| C244 | 281-558 | 18 pf | Cer |  | 500 v |  |  |
| C263 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C265 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C267 | 281-512 | 27 pf | Cer |  | 500 v | 10\% |  |
| C269 | 281.012 | 7.45 pf | Cer | Var |  |  |  |
| C281 | 283-026 | 0.2 uf | Cer |  | 25 v |  |  |

Capacitors (cont)

Tekłronix
Ckt. No.
Part No.

C285
C285

## C286

C286
C292
C293
C294
C297
C301
C301
C302
C303
C304
C304
C317
C317
C327
C327
C335
C335
C341
C342
C351
C360
C360
C360
C361
C364
C370
C371
C372
C375
C375
C377
C379
C384
C385
C385
C387
C409
C410
C414
C417
C418
C419 C420 C420
C422
C423
C424
C425
C427

| 281-518 | 47 pf |
| :---: | :---: |
| 281-0549-00 | 68 pf |
| $281-518$ | 47 pf |
| 281-0549-00 | 68 pf |
| 283-001 | $0.005 \mu \mathrm{f}$ |
| 283-001 | $0.005 \mu \mathrm{f}$ |
| 281-523 | 100 pf |
| 283-067 | $0.001 \mu \mathrm{f}$ |
| 285-604 | $0.01 \mu \mathrm{f}$ |
| 285-0622-00 | $0.1 \mu \mathrm{f}$ |
| 281-0543-00 | 270 pf |
| 283-0041-00 | $0.0033 \mu \mathrm{f}$ |
| 283-104 | $0.002 \mu \mathrm{f}$ |
| 283-0596-00 | 528 pf |
| 281-525 | 470 pf |
| 213-0059-00 | $1 \mu \mathrm{f}$ |
| 281-521 | 56 pf |
| 281-0516-00 | 39 pf |
| 281-623 | 650 pf |
| 281-0546-00 | 330 pf |
| 283-000 | $0.001 \mu \mathrm{f}$ |
| 283-001 | $0.005 \mu \mathrm{f}$ |
| 281-523 | 100 pf |
| 281-513 | 27 pf |
| 285-598 | 0.01 ¢f |
| 283-0593-00 | $0.01 \mu \mathrm{f}$ |
| 283-0593-01 | $0.01 \mu \mathrm{f}$ |
| 281-0534-00 | 3.3 pf |
| 283-596 | 528 pf |
| 281-546 | 330 pf |
| 283-081 | $0.1 \mu \mathrm{f}$ |
| 281-0550-00 | 120 pf |
| 283-000 | $0.001 \mu \mathrm{f}$ |
| 283.000 | $0.001 \mu \mathrm{f}$ |
| 281-0550-00 | 120 pf |
| 283-000 | $0.001 \mu \mathrm{f}$ |
| 283-000 | $0.001 \mu \mathrm{f}$ |
| 283-000 | $0.001 \mu \mathrm{f}$ |
| $283-000$ | $0.001 \mu f$ |
| 281-0550-00 | 120 pf |
| 283.000 | $0.001 \mu \mathrm{f}$ |
| 281-0519-00 | 47 pf |
| 283.000 | $0.001 \mu f$ |
| 283-001 | $0.005 \mu \mathrm{f}$ |
| 285-633 | $0.22 \mu \mathrm{f}$ |
| 281.0511.00 | 22 pf |
| 281-0621-00 | 12 pf |
| 281.536 | $0.001 \mu \mathrm{f}$ |
| 281-0546-00 | 330 pf |
| 283-0010-00 | $0.05 \mu \mathrm{f}$ |
| 281-0580-00 | 470 pf |
| 283.001 | $0.005 \mu \mathrm{f}$ |
| 283.0002-00 | $0.01 \mu \mathrm{f}$ |
| 281-621 | 12 pf |


| Cer | 500 v |  | 100-929 |
| :---: | :---: | :---: | :---: |
| Cer | 500 v | 10\% | 930-up |
| Cer | 500 v |  | 100-929 |
| Cer | 500 v | 10\% | 930-up |
| Cer | 500 v |  |  |
| Cer | 500 v |  |  |
| Cer | 350 v |  |  |
| Cer | 200 v | 10\% |  |
| PTM | 400 v |  | 100-5519 |
| PTM | 100 v |  | 5520-up |
| Cer | 500 v | 10\% | X4480-up |
| Cer | 500 v | 5\% | X4480-up |
| Cer | 500 v |  | 100-4479 |
| Mica | 300 v | 1\% | 4480-up |
| Cer | 500 v |  | 100-4479 |
| Cer | 25 v | +80\%-20\% | 4480-up |
| Cer | 500 v | 10\% | 100-4479 |
| Cer | 500 v | 10\% | 4480-up |
| Cer | 500 v |  | 100-4479 |
| Cer | 500 v | 10\% | 4480-ur, |
| Cer | 500 v |  |  |
| Cer | 500 v |  |  |
| Cer | 350 v |  |  |
| Cer | 500 v |  |  |
| PTM | 100 v | 5\% | 100-4025 |
| Mica | 100 v | 1\% | 4026-4909 |
| Mica | 100 v | 5\% | 4910-up |
| Cer | 500 v | $\pm 0.25 \mathrm{pf}$ |  |
| Mico | 300 v | 1\% |  |
| Cer | 500 v | 10\% |  |
| Cer | 25 v |  |  |
| Cer | 500 v | 10\% | X4026-up |
| Cer | 500 v |  |  |
| Cer | 500 v |  | 100-4025 |
| Cer | 500 v | 10\% | 4026-up |
| Cer | 500 v |  |  |
| Cer | 500 v |  |  |
| Cer | 500 v |  |  |
| Cer | 500 v |  | 100-4025 |
| Cer | 500 v |  | 4026-up |
| Cer | 500 v |  |  |
| Cer | 500 v | 10\% | X4480-up |
| Cer | 500 v |  |  |
| Cer | 500 v |  |  |
| PTM | 100 v | 10\% |  |
| Cer | 500 v | 10\% | X1910-up |
| Cer | 500 v | 1\% | X1910-up |
| Cer | 500 v | 10\% | 100-1909 |
| Cer | 500 v | 10\% | 1910-up |
| Cer | 50 v |  | X1910-up |
| Cer | 500 v | 10\% | X1910-up |
| Cer | 500 v |  | 100-1909x |
| Cer | 500 v |  | X1910-up |
| Cer | 500 v | 1\% | 100.1909X |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. | Description |  |  |  | S/N Range |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C430 | 281-524 | 150 pf | Cer |  | 500 v |  |  |
| C436 | 281-525 | 470 pf | Cer |  | 500 v |  |  |
| C452 | 281-550 | 120 pf | Cer |  | 500 v | 10\% |  |
| C455 | 281-523 | 100 pt | Cer |  | 350 v |  |  |
| C461 | 283-081 | $0.1 \mu \mathrm{f}$ | Cer |  | 25 v |  | 100-2996X |
| C462 | 283-0600-00 | 43 pf | Mica |  | 500 v | 5\% | X2997-4479 |
| C462 | 281-0528-00 | 82 pf | Cer |  | 500 v | 10\% | 4480-up |
| C463 | 285-0595-00 | $0.1 \mu \mathrm{f}$ | PTM |  | 100 v |  | X2997-up |
| C464 | 281-0551-00 | 390 pf | Cer |  | 500 v | 10\% | X1719-up |
| C465 | 281-519 | 47 pf | Cer |  | 500 v | 10\% |  |
| C470 | 281-551 | 390 pf | Cer |  | 500 r | 10\% | 100-2996 |
| C470 | 281-0523-00 | 100 pf | Cer |  | 350 V |  | 2997-up |
| C477 | 283-096 | 500 pf | Cer |  | 20000 v |  | 100-5519 |
| C477 | 281-0556-00 | 500 pf | Cer |  | 10000 v |  | 5520-up |
| C478 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C481 | 281-012 | 7-45 pf | Cer | Var |  |  |  |
| C482 | 283-519 | 360 pf | Mica |  | 500 v | 5\% |  |
| C483 | 285.595 | $0.1 \mu \mathrm{f}$ | PTM |  | 100 v | 1\% |  |
| C484 | Use 283-0028-00 | $0.0022 \mu \mathrm{f}$ | Cer |  | 50 v |  |  |
| C501 | 281-0616-00 | 6.8 pf | Cer |  | 200 v |  | X787-up |
| C509 | 281.609 | 1 pf | Cer |  | 200 v | 10\% | 100.786 |
| C509 | 281-0613-00 | 10 pf | Cer |  | 200 v | 10\% | 787-up |
| C517 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C519 | 281-0558-00 | 18 pf | Cer |  | 500 v |  | X1606-1718 |
| C519 | 281-0504-00 | 10 pf | Cer |  | 500 v | 10\% | 1719-up |
| C521 | 281-010 | 4.5-25 pf | Cer | Var |  |  | 100-1605 |
| C521 | 281-0546-00 | 330 pf | Cer |  | 500 v | 10\% | 1606-1718x |
| C522 | 281-0518-00 | 47 pf | Cer |  | 500 v |  | X1606-up |
| C523 | 281-0012-00 | 7-45 pf | Cer | Var |  |  | X1606-up |
| C553 | 283-0000-00 | $0.0001 \mu \mathrm{f}$ | Cer |  | 500 v |  | X1606-1718 |
| C553 | 283-0003-00 | $0.01 \mu \mathrm{f}$ | Cer |  | 150 v |  | 1719-up |
| C558 | 285-0627-00 | $0.0033 \mu f$ | PTM |  | 100 v | 5\% | X1606-1718X |
| C575 | 283.081 | $0.1 \mu \mathrm{f}$ | Cer |  | 25 v |  | 100.1605 |
| C575 | 283-0026-00 | $0.2 \mu \mathrm{f}$ | Cer |  | 25 v |  | 1606-1718 |
| C575 | 283-0059-00 | $1 \mu \mathrm{f}$ | Cer |  | 25 v | +80\%-20\% | \% 1719-up |
| C579 | 283-079 | $0.01 \mu \mathrm{f}$ | Cer |  | 250 v |  | X150-up |
| C610 | 290-0122-00 | $1000 \mu \mathrm{f}$ | EMC |  | 50 v |  |  |
| C617 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C620 | 290-145 | $10 \mu \mathrm{f}$ | EMT |  | 50 v |  |  |
| C626 | 283-003 | $0.01 \mu \mathrm{f}$ | Cer |  | 150 v |  |  |
| C640 | 290-0180-00 | $300 \mu \mathrm{f}$ | EMC |  | 250 v |  |  |
| C644 | 283.079 | $0.01 \mu \dagger$ | Cer |  | 250 v |  |  |
| C646 | 283-057 | $0.1 \mu \mathrm{f}$ | Cer |  | 200 v |  |  |
| C649 | 290-149 | $5 \mu \mathrm{f}$ | EMT |  | 150 v |  |  |
| C650 | 290-0179-00 | $125 \mu \mathrm{f}$ | EMC |  | 250 v |  | 100-786 |
| C650A, B | 290-0059-00 | 160-10 $\mu \mathrm{f}$ | EMC |  | 350 v |  | 787-up |
| C800 | 290-213 | $10 \mu \mathrm{f}$ | EMT |  | 450 v |  |  |
| C801 | 283-0111-00 | $0.1 \mu \mathrm{f}$ | Cer |  | 50 v |  | X1600-up |
| C804 | 283-004 | $0.02 \mu \mathrm{f}$ | Cer |  | 150 v |  | 100-205X |
| C822 | 283-036 | $0.0025 \mu \mathrm{f}$ | Cer |  | 6000 V |  |  |
| C832 | 281.556 | 500 pf | Cer |  | 10000 v |  |  |

Capacitors (cont)

| Ckt. No. | Tekłronix Part No. | Description |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C834 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C837 | 281-556 | 500 pf | Cer | 10000 v |  |  |
| C848 | 283-096 | 500 pf | Cer | 20000 v |  | 100-5519 |
| C848 | 281-0556-00 | 500 pf | Cer | 10000 v |  | 5520-up |
| C849 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C850 | 281-0543-00 | 270 pf | Cer | 500 v | 10\% | X1660-up |
| C875 | 281-0513-00 | 27 pf | Cer | 500 v |  | X860-up |
| C876 | 283-032 | 470 pf | Cer | 500 v | 5\% |  |
| Diodes |  |  |  |  |  |  |
| D109 | *152-0185-00 | Silicon | Replaceable by 1 N3605 |  |  | X1606-up |
| D209 | *152-0185-00 | Silicon | Replaceable by 1N3605 |  |  | X1606-up |
| D271 | *152.075 | Germanium | Tek Spec |  |  |  |
| D272 | *152-075 | Germanium | Tek Spec |  |  |  |
| D282 | *152-061 | Silicon | Tek Spec |  |  |  |
| D285 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D286 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D292 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D293 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D301 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D304 | *152-185 | Silicon | Replaceable by 1N3605Replaceable by 1N3605 |  |  |  |
| D314 | *152-185 | Silicon |  |  |  |  |
| D315 | *152-0185-00 | Silicon | Replaceable by 1N3605Replaceable by 1N3605 |  |  | X5520-up |
| D317 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D318 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D323 | *152-0185-00 | Silicon | Replaceable by 1 N 3605 |  |  | X4480-up |
| D333 | *152-0185-00 | Silicon | Replaceable by 1N3605 |  |  | X4480-up |
| D346 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D351 | *152-185 | Silicon | Replaceable by 1N3605 |  |  | X4026-up |
| D362 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D363 | *152-185 | Silicon | Replaceable by 1N3605 |  |  | X4026-up |
| D368 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D370 | *152-185 | Silicon | Replaceable by 1 N 3605 |  |  |  |
| D371 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D374 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D377 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D384 | *152-185 | Silicon | Replaceable by 1 N 3605 |  |  |  |
| D387 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D410 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D411 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D415 | *152-185 | Silicon | Replaceable by 1N3605 |  |  | 100-1909X |
| D416 | *152-0185-00 | Silicon | Replaceable by 1N3605 |  |  | X1910-up |
| D417 | *152-0185-00 | Silicon | Replaceable by 1 N 3605 |  |  | X1910-up |
| D418 | Use *152-0075-00 | Germanium | Tek Spec |  |  | X1910-up |
| D420 | *152-185 | Silicon | Replaceable by 1N3605 |  |  | 100-1909X |
| D427 | *152-185 | Silicon | Replaceable by 1N3605 |  |  | 100-1909X |
| D430 | *152-185 | Silicon | Replaceable by 1N3605Replaceable by IN3605 |  |  |  |
| D436 | *152-185 | Silicon |  |  |  |  |
| D452 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |
| D455 | *152-185 | Silicon | Replaceable by 1N3605 |  |  |  |

Diodes (cont)

| Ckt. No. | Tektronix Part No. |  | Description | S/N Range |
| :---: | :---: | :---: | :---: | :---: |
| D456 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X2997-up |
| D461 | *152-075 | Germanium | Tek Spec | 100-2996 |
| D461 | *152-0185-00 | Silicon | Replaceable by 1N3605 | 2997 -up |
| D462 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X2997-up |
| D463 | *152-0075-00 | Germanium | Tek Spec | X2997-up |
| D464 | *152.075 | Germanium | Tek Spec |  |
| D466 | *152.185 | Silicon | Replaceable by 1N3605 |  |
| D470 | 152-0142-00 | Zener | 1N972A 0.4 w, 30 v , 10\% | X2997-up |
| D471 | *152-0061-00 | Silicon | Tek Spec | X2997-up |
| D472 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X2997-up |
| D473 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X2997-up |
| D474 | *152-061 | Silicon | Tek Spec |  |
| D475 | *152-061 | Silicon | Tek Spec |  |
| D481 | *152-185 | Silicon | Replaceable by 1N3605 |  |
| D482 | *152-185 | Silicon | Replaceable by 1N3605 |  |
| D486 | *152-185 | Silicon | Replaceable by 1 N 3605 |  |
| D553 | 152-0142-00 | Zener | 1N972A 0.4 w, $30 \mathrm{v}, 10 \%$ | X1719-up |
| D556 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X1606-up |
| D571 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X1606-up |
| D610 | 152-066 | 1N3194 |  |  |
| D611 | 152-066 | 1N3194 |  |  |
| D614 | 152-123 | Zener | 1N935A 0.4 w, 9.1 v, 5\% |  |
| D640A,B,C,D | 152-066 | 1N3194 |  |  |
| D643 | *152-0185-00 | Silicon | Replaceable by 1N3605 | X5179-up |
| D649 | 152-0066-00 | Silicon | 1N3194 | X5179-up |
| D650A,B,C,D | 152-066 | 1N3194 |  |  |
| D881 | *152-185 | Silicon | Replaceable by 1N3605 |  |

## Fuses

| F601 | $159-041$ |
| :--- | :--- |
| F601 | $159-043$ |
| F637 | $159-031$ |
| F648 | $159-030$ |

## K385

148-024
4 PDT $24 v$

## Inductors

| $150 n h$ |  |  |
| :--- | :--- | :--- |
| $60 \mu \mathrm{~h}$ |  |  |
| $400 \mu \mathrm{~h}$ |  |  |
| $0.1 \mu \mathrm{~h}$ |  |  |
| $58-90 \mu \mathrm{~h}$ | Var | Core 276-511 (2) |
| 150 nh |  |  |
| $60 \mu \mathrm{~h}$ |  |  |
| $400 \mu \mathrm{~h}$ |  |  |
| $0.1 \mu \mathrm{~h}$ |  |  |
| $58-90 \mu \mathrm{~h}$ |  |  |
| CRT Beam Rotator | Var | Core 276-511 (2) |

## Transisfors

|  | Tektronix |  |
| :--- | :---: | :--- |
| Ckt. | No. | Part No. | Description $\quad$ S/N Range

Transistors (cont)

| Ckt. No. | Tektronix Part No. | Description | S/N Range |
| :---: | :---: | :---: | :---: |
| Q644 | *151-134 | Replaceable by 2N2905 |  |
| Q647 | *151-148 | RCA 40250 Selected |  |
| Q804 | *151-136 | Replaceable by 2 N 3053 |  |
| Q874 | 151-040 | 2N1302 | 100-859 |
| Q874 | Use *151-0103-00 | Replaceable by 2 N 2219 | 860-up |

Resistors
Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R101 | 315-100 | $10 \Omega$ | $1 / 4$ w |  |  | 5\% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R104 | Use 319-031 | 1 meg | 1/4w |  | Prec | 1\% |  |
| R106 | 316-474 | 470 k | 1/4w |  |  |  |  |
| R110 | 316-101 | $100 \Omega$ | 1/4w |  |  |  |  |
| R113 | 316-272 | 2.7 k | $1 / 4 w$ |  |  |  | 100-1599 |
| R113 | 315-0682-00 | 6.8 k | 1/4w |  |  | 5\% | 1600-up |
| R114 | 321-227 | 2.26 k | $1 / 8 w$ |  | Prec | 1\% |  |
| R115 | 311-310 | 5 k |  | Var |  | DC BAL | 100-1599 |
| R115 | 311-0546-00 | 10 k |  | Var |  | DC BAL | 1600-up |
| R118A | 321-247 | 3.65 k | 1/8w |  | Prec | 1\% |  |
| R118B | 321-219 | 1.87 k | 1/8w |  | Prec | 1\% |  |
| R118C | 321-167 | $536 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R119 | 311-169 | $100 \Omega$ |  | Var |  | X5 MAG GAI |  |
| R120 | 321-175 | $649 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R121 | 308-212 | 10 k | 3 w |  | WW | 5\% | 100-1599 |
| R121 | 308-0334-00 | 7 k | 3 w |  | WW | 3\% | 1600-up |
| R122 | 321-271 | 6.49 k | 1/8w |  | Prec | 1\% |  |
| R123 | 321-253 | 4.22 k | 1/8w |  | Prec | 1\% | 100-1599 |
| R123 | 321-0250-00 | 3.92 k | 1/8w |  | Prec | 1\% | 1600-up |
| R130 | 311-224 | 50 k |  | Var |  | VAR DC BAL |  |
| R131 | 316-273 | 27 k | 1/4w |  |  |  | 100-327 |
| R131 | 315-0823-00 | 82 k | 1/4w |  |  | 5\% | 328-up |
| R135 | 321-279 | 7.87 k | 1/8w |  | Prec | 1\% |  |
| R141 | 321-131 | $226 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R143 | 305-153 | 15 k | 2 w |  |  | 5\% |  |
| R144 | 321-297 | 12.1 k | 1/8w |  | Prec | 1\% |  |
| R148 | 301-333 | 33 k | 1/2w |  |  | 5\% |  |
| R149 | 316-392 | 3.9 k | 1/4w |  |  |  |  |
| R154 | 321-213 | 1.62 k | 1/8w |  | Prec | 1\% |  |
| R160 | 308-107 | 1 k | 5 w |  | WW | 5\% | 100-619 |
| R160 | 308-0017-00 | 2 k | 10 w |  | WW | 5\% | 620-up |
| R162 | *310-621 | 3 k | 8 w |  | Prec | 1\% |  |
| R163 | 316-104 | 100 k | 1/4w |  |  |  |  |
| R164 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R166 | 308-077 | 1 k | 3 w |  | WW |  |  |
| R167 | 321-0335-00 | 30.1 k | 1/8w |  | Prec | 1\% | X4400-up |
| R168 | 315-910 | $91 \Omega$ | 1/4w |  |  | 5\% | 100-929 |
| R168 | 315-0750-00 | $75 \Omega$ | 1/4w |  |  | 5\% | 930-up |
| R169 | 311-003 | $100 \Omega$ |  | Var |  | VERT GAIN |  |
| R172 | 315-112 | 1.1 k | 1/4w |  |  | 5\% |  |
| R173 | 304-273 | 27 k | 2 w |  |  |  |  |
| R183 | 316-271 | $270 \Omega$ | 1/4w |  |  |  |  |

Resistors (cont)

Tektronix
Ckt. No.
Part No.
Description

| R184 | 316.103 | 10 k | $1 / 4 w$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R192 | 316-222 | 2.2 k | $1 / 4 w$ |  |  |  | 100-4259 |
| R192 | 315-0242-00 | 2.4 k | 1/4w |  |  | 5\% | 4260-up |
| R193 | 316-122 | 1.2 k | $1 / 4 w$ |  |  |  | 100-4259 |
| R193 | 304-0122-00 | 1.2 k | 1 w |  |  |  | 4260-up |
| $\mathrm{R198}$ | 301.750 | $75 \Omega$ | $1 / 2 w$ |  |  | 5\% |  |
| R199 | 316-103 | 10 k | 1/4w |  |  |  |  |
| R201 | 315-100 | $10 \Omega$ | 1/4w |  |  | 5\% |  |
| R204 | Use 319-031 | 1 meg | 1/4w |  | Prec | 1\% |  |
| R206 | 316-474 | 470 k | 1/4w |  |  |  |  |
| R210 | 316-101 | $100 \Omega$ | 1/4w |  |  |  |  |
| R213 | 316-272 | 2.7 k | 1/4w |  |  |  | 100-1599 |
| R213 | 315-0682-00 | 6.8 k | 1/4w |  |  | 5\% | 1600-up |
| R214 | 321-227 | 2.26 k | 1/8w |  | Prec | 1\% |  |
| R220 | 321-175 | 649 ת | 1/8w |  | Prec | 1\% |  |
| R231 | 316-273 | 27 k | 1/4w |  |  |  | 100-327 |
| R231 | 315-0823-00 | 82 k | 1/4w |  |  | 5\% | 328-up |
| R240 ${ }^{6}$ | 311-506 | $500 \Omega$ |  | Var |  | VARI |  |
| R241 | 321-121 | $178 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R242 | 316-224 | 220 k | 1/4w |  |  |  |  |
| R243 | 305-153 | 15 k | 2 w |  |  | 5\% |  |
| R244 | 321-297 | 12.1 k | 1/0w |  | Prec | 1\% |  |
| R245 | 311-016 | 10 k |  | Var |  | POSI |  |
| R248 | 301-333 | 33 k | 1/2w |  |  | 5\% |  |
| R249 | 316-392 | 3.9 k | 1/4w |  |  |  |  |
| R254 | 321-213 | 1.62 k | 1/8w |  | Prec | 1\% |  |
| R262 | *310-621 | 3 k | 8 w |  | Prec | 1\% |  |
| R263 | 316-104 | 100 k | 1/4w |  |  |  |  |
| R264 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R266 | 308-077 | 1k | 3 w |  | WW |  |  |
| R267 | 316-271 | $270 \Omega$ | 1/4w |  |  |  |  |
| R268 | 315-910 | $91 \Omega$ | $1 / 4 w$ |  |  | 5\% | 100-929 |
| R268 | 315-0750-00 | 75, | 1/4w |  |  | 5\% | 930-up |
| R274 | 315-153 | 15 k | $1 / 4 w$ |  |  | 5\% |  |
| R275 | 315-752 | 7.5 k | $1 / 4 w$ |  |  | 5\% |  |
| R276 | 316-104 | 100 k | 1/4w |  |  |  |  |
| R280 | 316-183 | 18k | $1 / 4 w$ |  |  |  |  |
| R281 | 316-682 | 6.8 k | 1/4w |  |  |  |  |
| R282 | 316-105 | 1 meg | $1 / 4 w$ |  |  |  |  |
| R283 | 316.151 | $150 \Omega$ | 1/4w |  |  |  |  |
| R284 | 316.150 | $15 \Omega$ | 1/4w |  |  |  |  |
| R285 | 315-104 | 100 k | 1/4w |  |  | 5\% | 100-4479 |
| R285 | 321-0385-00 | 100 k | 1/0w |  | Prec | 1\% | 4480-up |
| R286 | 315-104 | 100 k | 1/4w |  |  | 5\% | 100-4479 |
| R286 | 321-0385-00 | 100 k | 1/w w |  | Prec | 1\% | 4480-up |
| R287 | 315-273 | 27 k | 1/4w |  |  | 5\% | 100-4479 |
| R287 | 321-0328-00 | 25.5 k | 1/8w |  | Prec | 1\% | 4480-up |

${ }^{6}$ Furnished as a unit with SW240.

Resistors (cont)

Ckt. No Tektronix


Resistors (cont)


Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R471 | 316.563 | 56 k | 1/4w |  |  | 100-2996X |
| R472 | Use 316.0334-00 | 330 k | 1/4w |  |  | X2997-up |
| R473 | 316.0563-00 | 56 k | 1/4w |  |  | X2997-up |
| R474 | *310.614 | 41.5 k | 8 w | Prec | 1\% |  |
| R475 | 316.105 | 1 meg | 1/4w |  |  |  |
| R476 | 316.393 | 39 k | 1/4w |  |  |  |
| R477 | 302.273 | 27 k | 1/2w |  |  |  |
| R478 | 316-103 | 10 k | 1/4w |  |  |  |
| R481 | 321-409 | 178 k | 1/8w | Prec | 1\% |  |
| R482 | 321-350 | 43.2 k | 1/0w | Prec | 1\% |  |
| R 483 | 321-397 | 133 k | 1/6 w | Prec | 1\% |  |
| R484 | 321.379 | 86.6k | 1/8w | Prec | 1\% |  |
| R486 | 316.475 | 4.7 meg | 1/4w |  |  | 100.1718 |
| R486 | 316-0334-00 | 330 k | 1/4w |  | 10\% | 1719-up |
| R487 | 316-224 | 220 k | 1/4w |  |  |  |
| R488 | 316-103 | 10k | 1/4w |  |  |  |
| R489 | 304-183 | 18 k | 1 w |  |  |  |
| R491 | 301-752 | 7.5 k | 1/2w |  | 5\% |  |
| R492 | 321-329 | 26.1 k | 1/6w | Prec | 1\% |  |
| R493 | 323-0346-00 | 39.2 k | $1 / 2 w$ | Prec | 1\% | X2997-up |
| R501 | 323-498 | 1.5 meg | 1/2w | Prec | 1\% | 100.786 |
| R501 | 323-0496-00 | 1.43 meg | 1/2w | Prec | 1\% | 787-up |
| R502 | 321-440 | 374 k | 1/0 w | Prec | 1\% | 100.786 |
| R502 | 321-0450-00 | 475 k | 1/8w | Prec | 1\% | 787-up |
| R504 | 323-481 | 1 meg | 1/2w | Prec | 1\% | 100-786 |
| R504 | 323-0468-00 | 732 k | 1/2w | Prec | 1\% | 787-up |
| R509 | 323-481 | 1 meg | 1/2w | Prec | 1\% |  |
| R510 | 316-101 | $100 \Omega$ | 1/4w |  |  |  |
| R514 | 302-223 | 22 k | 1/2w |  |  |  |
| R516 | 321-368 | 66.5 k | 1/0w | Prec | 1\% |  |
| R517 | 321-339 | 33.2 k | 1/8w | Prec | 1\% | 100-786 |
| R517 | 321-0351-00 | 44.2 k | 1/8w | Prec | 1\% | 787-up |
| R520 | 323-377 | 82.5 k | 1/2w | Prec | 1\% |  |
| R521 | 321-249 | 3.83 k | 1/4w | Prec | 1\% |  |
| R522 | 321.318 | 20 k | 1/8w | Prec | 1\% | 100.1605 |
| R522 | 321-0317-00 | 19.6 k | 1/8w | Prec | 1\% | 1606-up |
| R523 | 321-389 | 110k | 1/8w | Prec | 1\% | 100-1605 |
| R523 | 321-0386-00 | 102 k | 1/6 w | Prec | 1\% | 1606-up |
| R525 | 323-373 | 75 k | 1/2w | Prec | 1\% |  |
| R533 | 316-224 | 220 k | 1/4w |  |  |  |
| R534 | 315-222 | 2.2 k | 1/4w |  | 5\% |  |
| R535 | 315-273 | 27 k | $1 / 4{ }^{1}$ |  | 5\% |  |
| R544 | 315.393 | 39 k | 1/4w |  | 5\% | 100-1605 |
| R544 | 316-0274-00 | 270 k | 1/4w |  |  | 1606-up |
| R551 | 316.101 | $100 \Omega$ | $1 / 4$ w |  |  |  |
| R552 | 315-0104-00 | 100 k | $1 / 4$ w |  | 5\% | X1606-up |
| R553 | 315-0474-00 | 470 k | 1/4w |  | 5\% | X1606-1718 |
| R553 | 316-0102-00 | 1 k | 1/4w |  |  | 1719-up |
| R554 | *310.614 | 41.5 k | 8 w | Prec | 1\% |  |
| R556 | 315.682 | 6.8 k | 1/4w |  | 5\% | 100-1605 |

Resistors (cont)

| Ckt. No. | Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R556 | 321.0269 .00 | 6.19 k | 1/8 w |  | Prec | 1606-up |
| R558 | Use 322-0123-00 | $187 \Omega$ | $1 / 4 w$ |  | Prec | 1\% |
| R561 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |
| R564 | *310-614 | 41.5 k | $8 w$ |  | Prec | 1\% |
| R566 | 315-682 | 6.8 k | $1 / 4 w$ |  |  | 5\% 100-1605 |
| R566 | 321-0269-00 | 6.19 k | $1 / 8 w$ | Var | Prec | 1\% 1606-up |
| R568 | 311-178 | $200 \Omega$ |  |  |  | HORIZ GAIN |
| R571 | 316-0473-00 | 47 k | $1 / 4 w$ |  |  | X1606-up |
| R574 | 315.393 | 39 k | $1 / 4 w$ |  |  | 5\% 100-1605 |
| R574 | 316-0273-00 | 27 k | 1/4w |  |  | 1606-up |
| R575 | 311-178 | $200 \Omega$ |  | Var |  | SWP/MAG REGIS |
| R576 | 316-0392-00 | 3.9 k | $1 / 4 w$ |  |  | X1606-up |
| $R 579$ | 311-360 | 5 k |  | Var Var | WW | POSITION (HORIZ) |
| R605 | 311-377 | 25 ת |  |  |  | SCALE ILLUM |
| R614 | 315-242 | 2.4 k | $1 / 4 w$ |  |  | 5\% |
| R616 | 315-184 | 180 k | 1/4w |  |  | 5\% |
| R617 | 316-471 | 470 ת | $1 / 4 w$ |  |  |  |
| R618 | 315-183 | 18 k | $1 / 4 \mathrm{w}$ | Var |  | -25 VOLTS CAL AMPL |
| R620 | 311-147 | 10 k |  |  |  |  |  |
| R621 | 302-122 | 1.2 k | $1 / 2 w$ |  |  |  |
| R624 | 321-206 | 1.37 k | 1/8 $w$ |  | Prec | 1\% |
| R625 | 315-103 | 10 k | $1 / 4 w$ |  |  | 5\% |
| R626 | 321-233 | 2.61 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |
| R634 | 304-223 | 22 k | 1 w |  |  |  |
| R640 | 307-007 | 2.7 ת | 1 w |  |  |  |
| R641 | 323-335 | 30.1 k | $1 / 2 w$ |  | Prec | 1\% |
| R642 | 321-277 | 7.5 k | $1 / 8 w$ |  | Prec | 1\% |
| R643 | 316-104 | 100 k | $1 / 4 w$ |  |  |  |
| R644 | 316-102 | 1 k | $1 / 4 w$ |  |  |  |
| R645 | 302-0103-00 | 10 k | $1 / 2 w$ |  |  | X787-up |
| R646 | 316-221 | $220 \Omega$ | $1 / 4 w$ |  |  |  |
| R647 | 304-120 | $12 \Omega$ | 1 w |  |  |  |
| R648 | 302-103 | 10 k | $1 / 2 w$ |  |  |  |
| R649 | 316-0221-00 | $220 \Omega$ | $1 / 4 w$ |  |  | X5179-up |
| R650 | 307-009 | $4.7 \Omega$ | 1 w |  |  |  |
| R652 | 302-0102-00 | 1 k | $1 / 2 w$ | Var |  | X787-up |
| R655 | 311.317 | $2 \times 1 \mathrm{k}$ |  |  |  | CRT BEAM ROTATOR |
| R800 | 302-101 | $100 \Omega$ | $1 / 2 \mathrm{w}$ |  |  |  |
| R801 | 302-0100-00 | $10 \Omega$ | $1 / 2 w$ |  |  | X1600-up |
| R802 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |
| R809 | 316-105 | 1 meg | 1/4w |  |  |  |
| R810 | 316-101 | $100 \Omega$ | 1/4w |  |  |  |
| R814 | 311-184 | 1 meg |  | Var |  | VERTICAL GAIN |
| R815 | 316-335 | 3.3 meg | 1/4w |  |  |  |
| R834 | 316-684 | 680 k | 1/4w |  |  |  |
| R835 | 311-183 | 500 k |  | Vor |  | HIGH VOLTAGE$5 \%$$5 \%$$5 \%$$5 \%$ |
| R837 | 305-565 | 5.6 meg | 2 w |  |  |  |
| R838 | 305-685 | 6.8 meg | 2 w |  |  |  |
| R839 | 305-565 | 5.6 meg | 2 w |  |  |  |
| R841 | 305-685 | 6.8 meg | 2 w |  |  |  |

Resistors (cont)

Tektronix
Ckt. No. Part No

| R842 | 305-565 | 5.6 meg | $2 w$ |  |  | 5\% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R843 | 305-685 | 6.8 meg | 2 w |  |  | 5\% |  |
| R844 | 311-505 | 10 meg |  | Var |  | FOCUS |  |
| R845 | 305-685 | 6.8 meg | $2 w$ |  |  | 5\% |  |
| R846 | 311-043 | 2 meg |  | Var |  | INTENSITY |  |
| R847 | 315-184 | 180 k | 1/4w |  |  | 5\% |  |
| R848 | 315-155 | 1.5 meg | 1/4w |  |  | 5\% |  |
| R849 | 302-155 | 1.5 meg | 1/2w |  |  |  |  |
| R855 | 311.0183-00 | 500 k |  | Var |  |  | X5420-up |
| R856 | 315-0114-00 | 110 k | $1 / 4 w$ |  |  | 5\% | X5420-up |
| R857 | 315-0223-00 | 22 k | $1 / 4 w$ |  |  | 5\% | X5420-up |
| R864 | 311-184 | 1 meg |  | Var |  | ASTIG |  |
| R865 | 316-334 | 330 k | 1/4w |  |  |  | 100-149 |
| R865 | 302-824 | 820 k | 1/2w |  |  |  | 150-619X |
| R866 | 316-336 | 33 meg | $1 / 4 w$ |  |  |  | 100-149 |
| R866 | 302.684 | 680 k | 1/2w |  |  |  | 150-up |
| R867 | 316-0184-00 | 180 k | 1/4w |  |  |  | X620-up |
| R874 | 304-273 | 27 k | 1 w |  |  |  |  |
| R875 | 316-393 | 39 k | 1/4w |  |  |  |  |
| R876 | 316-471 | $470 \Omega$ | 1/4w |  |  |  | 100-859 |
| R876 | 316-0152-00 | 1.5 k | 1/4w |  |  |  | 860-up |
| R881 | 321-327 | 24.9 k | 1/8w |  | Prec | 1\% |  |
| R882 | 321-146 | $324 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R883 | 321-191 | $953 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R885 | 321-141 | $287 \Omega$ | 1/8w |  | Prec | 1\% |  |
| R886 | 321-179 | $715 \Omega$ | 1/8w |  | Prec | 1\% |  |

## Switches

| VERTICAL INPUT |  |
| :--- | ---: |
| VOLTS FULL SCALE |  |
| VERTICAL RESPONSE |  |
|  |  |
| DC RESTORER |  |
| SYNC |  |
| FIELD SHIFT | $100-2996$ |
| HORIZONTAL DISPLAY | $2997-u p$ |
| HORIZONTAL DISPLAY | X2997-up |
| LINE SELECTOR | $100-1605$ |
| HORIZONTAL MAG | $1606-1718$ |
| HORIZONTAL MAG | $1719-\mathrm{up}$ |
| HORIZONTAL MAG |  |
| POWER |  |
| CALIBRATOR |  |

## Transformers

| T135 | 120.362 | RF 3.58 MC | Center frequency |  |
| :--- | :--- | :--- | :--- | :--- |
| T280 | $* 120-365$ | Toroid | 4 windings |  |
| T420 | $* 120-366$ | Toroid | 2 windings | $100-1909 X$ |
| T601 | $* 120.363$ | Power |  |  |
| T801 | $* 120-364$ | High Voltage |  |  |

'Furnished as a unit with R240.

## Electron Tubes

| Ckt No. | Tektronix Part No. |  | Description | S/N Range |
| :---: | :---: | :---: | :---: | :---: |
| V113 | 154-0039-01 | 12AT7 |  | 100-4909 |
| V113 | *157-0010-00 | 12AT7 | Checked | 4910-up |
| V164 | 154-420 | 7788 |  |  |
| V264 | 154-420 | 7788 |  |  |
| V293 | 154-039 | 12AT7 |  |  |
| V514 | 154-0022-03 | 6AU6 |  | 100-4019 |
| V514 | 154-0022-00 | 6AU6 |  | 4020-up |
| V554 | 154-187 | 6DJ8 |  |  |
| V800 | 154-468 | 6GV8 |  |  |
| V822 | 154-051 | 5642 |  |  |
| V832 | 154-051 | 5642 |  |  |
| V859 | *154-473 | T5290-31 | Crt Standard Phosphor | 100-5419 |
| V859 | *154-0507-00 | T5290-31 | Crt Standard Phosphor | 5420-up |

## SECTION 8

## PARTS LIST and DIAGRAMS

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix Field Office.
Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number including any suffix, instrument type, serial number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix Field Office will contact you concerning any change in part number.

ABBREVIATIONS AND SYMBOLS

| a or amp | amperes | mm | millimeter |
| :---: | :---: | :---: | :---: |
| BHS | binding head steel | meg or M | megohms or mega (10) |
| C | carbon | met. | metal |
| cer | ceramic | $\mu$ | micro, or $10^{-6}$ |
| cm | centimeter | n | nano, or $10^{-9}$ |
| comp | composition | $\Omega$ | ohm |
| cps | cycles per second | OD | outside diameter |
| crt | cathode-ray tube | OHS | oval head steel |
| CSK | counter sunk | p | pico, or $10^{-12}$ |
| dia | diameter | PHS | pan head steel |
| div | division | piv | peak inverse voltage |
| EMC | electrolytic, metal cased | plste | plastic |
| EMT | electroyltic, metal tubular | PMC | paper, metal cased |
| ext | external | poly | polystyrene |
| $f$ | farad | Prec | precision |
| F \& 1 | focus and intensity | PT | paper tubular |
| FHS | flat head steel | PTM | paper or plastic, tubular, molded |
| Fil HS | fillister head steel | RHS | round head steel |
| g. or G | giga, or $10^{9}$ | rms | root mean square |
| Ge | germanium | sec | second |
| GMV | guaranteed minimum value | Si | silicon |
| h | henry | S/N | serial number |
| hex | hexagonal | t or T | tera, or $10^{12}$ |
| HHS | hex head steel | TD | toroid |
| HSS | hex socket steel | THS | truss head steel |
| HV | high voltage | tub. | tubular |
| ID | inside diameter | $\checkmark$ or $V$ | volt |
| incd | incandescent | Var | variable |
| int | internal | w | watt |
| $k$ or K | kilohms or kilo ( $10^{3}$ ) | w/ | with |
| kc | kilocycle | w/o | without |
| m | milli, or $10^{-3}$ | WW | wire-wound |
| mc | megacycle |  |  |

## SPECIAL NOTES AND SYMBOLS

Part first added at this serial number.
000 X Part removed after this serial number.
*000-000 Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, or reworked or checked components.

Use 000-000
Part number indicated is direct replacement.
(1) Internal screwdriver adjustment.

Front-panel adjustment or connector.


FRONT

| REF. | PART NO. |  | ODEL NO. | O <br> r | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. | PART NO. | EFF. | Disc. | Y. |  |
| 1 | 333-0863-00 | $\begin{aligned} & 100 \\ & 400 \\ & 2997 \end{aligned}$ | $\begin{aligned} & 399 \\ & 2996 \end{aligned}$ | 1 | PANEL, front |
|  | 333-0863-01 |  |  | 1 | PANEL, front |
|  | 333-0863-02 |  |  | 1 | PANEL, front |
| 2 | 367-0022-00 |  |  | 2 | HANDLE, brass rod |
|  | - --. - |  |  | 2 | mounting hardware for each: (not included w/handle) |
| 3 | 213-0090-00 |  |  | 2 | SCREW, $10.32 \times 1 / 2$ inch, HHS |
| 4 | $\begin{aligned} & 366-0109-00 \\ & 213-0005-00 \end{aligned}$ |  |  | 2 | KNOB, plug-in securing |
|  |  |  |  | - | each knob includes: |
|  |  |  |  | 1 | SCREW, set, $8.32 \times 1 / 2$ inch, HSS |
| 5 | 366-0173-00 |  |  | 1 | KNOB, charcoal-VERTICAL INPUT |
|  | - --- |  |  | , | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch HSS |
| 6 | 262-0685-00 |  |  | 1 | SWITCH, wired-VERTICAL INPUT (See Ref. \#7) |
|  | - - - - - |  |  | 1 | switch includes: |
|  | 260-0658-00 |  |  | 1 | SWITCH, unwired-VERTICAL INPUT |
| 7 | - - .- |  |  | , | mounting hardware: (not included w/switch) |
|  | $\begin{aligned} & 210-0840-00 \\ & 210-0413.00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | WASHER, .390 ID $\times 9 / 16$ inch OD NUT, hex, $3 / 2-32 \times 1 / 2$ inch |
|  | $210-0413.00$ |  |  |  | NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
| 8 | 407-0079-00 |  |  | 1 | BRACKET, switch |
|  | -. - . - |  |  | - | mounting hardware: (not included w/bracket) |
|  | 211-0507-00 |  |  | 1 | SCREW, $6.32 \times 5 / 16$ inch, BHS |
|  | $211-0538-00$ |  |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, FHS phillips |
|  | 210-0803-00 |  |  | 1 | WASHER, $6 \mathrm{~L} \times 3 / 8$ inch |
|  | 210-0457-00 |  |  | 3 | NUT, keps, $6-32 \times 5 / 16$ inch |
| 9 | $\begin{aligned} & 376-0011-00 \\ & 213-0048-00 \\ & 384-0342-00 \\ & 214-0425-00 \\ & \hdashline \cdots-\cdots \\ & 210-0004-00 \\ & 210-0406-00 \end{aligned}$ |  |  | 2 | COUPLING, insulating |
|  |  |  |  | 2 | each coupling includes: |
|  |  |  |  | 2 | SCREW, set, $4-40 \times 1 / 8$ inch, HSS |
| $\begin{aligned} & 10 \\ & 11 \end{aligned}$ |  |  |  | 1 | ROD, extension |
|  |  |  |  | 1 | FASTENER, left |
|  |  |  |  | 2 | mounting hardware: (not included w/fastener) LOCKWASHER, internal, \#4 |
|  |  |  |  | 2 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 12 | $\begin{aligned} & 366-0173-00 \\ & --0 \\ & 213-0004-00 \\ & 366-0173-00 \\ & 213-0004-00 \end{aligned}$ |  |  | 1 | KNOB, charcoal-VERTICAL POSITION |
|  |  |  |  | $i$ | knob includes: <br> SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| 13 |  |  |  | 1 | KNOB, charcoal-VERTICAL RESPONSE |
|  |  |  |  | $i$ | knob includes: <br> SCREW, set, $6.32 \times 3 / 16$ inch HSS |

FRONT (Cont'd)


FRONT (Cont'd)

| \|REF.NO. | PART NO. | SERIAL/MODEL NO. |  | $\begin{aligned} & \mathbf{a} \\ & \mathbf{r} \\ & \mathbf{r} \end{aligned}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 27 | $\begin{aligned} & 407-0078-00 \\ & 211-0507-00 \\ & 210-0803-00 \\ & 210-0457-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & - \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | BRACKET, switch mounting hardware: (not included w/bracket) SCREW, $6-32 \times 5 / 16$ inch, BHS WASHER, $6 L \times 3 / 8$ inch NUT, keps, $6-32 \times 5 / 16$ inch |
| 28 | $\begin{aligned} & 386-0112-00 \\ & 352-0067-00 \\ & 211-0109-00 \\ & 210-0406-00 \end{aligned}$ |  |  | $\begin{gathered} 1 \\ 2 \\ - \\ 1 \\ 2 \end{gathered}$ | PLATE, front sub-panel HOLDER, neon, single mounting hardware for each: (not included w/holder) SCREW, $4-40 \times 7 / 8$ inch, FHS NUT, hex, $4.40 \times 3 / 16$ inch |
| 30 | $\begin{aligned} & 210-0012-00 \\ & 220-0420-00 \\ & 358-0054-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & - \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | POT <br> mounting hardware: (not included w/pot) LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch NUT, adapter, hex BUSHING, banana jack |
| 33 | $\begin{aligned} & 200-0272-00 \\ & 210-0434-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 4 \end{aligned}$ | COVER, graticule mounting hardware: (not included w/cover) NUT, graticule |
| 35 | $\begin{aligned} & 366-0215-00 \\ & 366-0215-01 \\ & 260-0490-00 \\ & 220-0413-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 890 \end{aligned}$ | 889 | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 2 \\ & 2 \end{aligned}$ | KNOB, lever-CALIBRATOR KNOB, lever-CALIBRATOR SWITCH, lever-CALIBRATOR mounting hardware: (not includedw/switch) NUT, hex, rod, $4-40 \times 3 / 16 \times .500$ inch |
| 37 | $\begin{aligned} & 260-0199-00 \\ & 210-0414-00 \\ & 354-0055-00 \\ & 210-0902-00 \\ & 210-0473-00 \\ & 378-0541-00 \\ & 136-0112-00 \\ & 211-0534-00 \\ & 210-0803-00 \\ & 210-0457-00 \end{aligned}$ |  |  | 1 $i$ 1 1 1 | SWITCH, toggle-POWER ON <br> mounting hardware: (not included $\mathrm{w} / \mathrm{switch}$ ) <br> NUT, hex, $15 / 32 \times 9 / 16$ inch <br> RING, locking, switch <br> WASHER, 470 ID $\times{ }^{21} / 32$ inch OD <br> NUT, switch, $15 / 32-32 \times 5 / 64$ inch, 12 sided <br> FILTER, lens, neon light SOCKET, graticule lamp mounting hardware for each: (not included w/socket) SCREW, $6-32 \times 5 / 16$ inch, PHS w/lockwasher WASHER, $6 L \times 3 / 8$ inch <br> NUT, keps, $6.32 \times 5 / 16$ inch |

FRONT (Cont'd)


FRONT (Cont'd)

| REF. <br> NO. | PART NO. | SERIAL/MODEL NO. |  | $\mathbf{9}$ <br> $\mathbf{1}$ <br> $\mathbf{y}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 52 | 366-0215-00 | 100 | 889 | 1 | KNOB, lever-SYNC |
|  | 366-0215-01 | 890 |  | 1 | KNOB, lever-SYNC |
| 53 | 260-0473-00 |  |  | 1 | SWITCH, lever-SYNC |
|  | - $20-0$ |  |  | 2 | mounting hardware: (not included w/switch) |
| 54 | 220-0413-00 |  |  | 2 | NUT, hex, rod, $4-40 \times 3 / 16 \times .500$ inch |
| 55 | 214-0424-00 |  |  | 1 | FASTENER, right |
|  | . . . . . - |  |  | - | mounting hardware: (not included w/fastener) |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 56 | - |  |  | 2 | POT |
|  | -....- |  |  | - | mounting hardware for each: (not included w/pot) |
|  | 210-0013-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \times 1 / 16$ inch |
|  | 210-0840-00 |  |  | 1 | WASHER, .390 ID $\times 9 / 16$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
| 5758 | 200-0269-00 |  |  | 2 | COVER, pot |
|  | 384-0030-00 |  |  | 1 | ROD, extension |
| 59 | -•••- - |  |  | 1 | POT |
|  | … |  |  | - | mounting hardware: (not included w/pot) |
|  | 210-0207-00 | X150 |  | 1 | LUG, solder, $3 / 8$ inch |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch |
|  | 210-0840-00 |  |  | 1 | WASHER, 390 ID $\times 9 / 16$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
| 60 | 366-0153-00 | X2997 |  | 1 | KNOB, charcoal_-VARIABLE |
|  | …-. |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6.32 \times 3 / 16$ inch, HSS |
| 61 | 262-0773-00 | X2997 |  | 1 | SWITCH, wired-LINE SELECTOR |
|  |  |  |  | 1 | switch includes: |
|  | 260-0793-00 |  |  | 1 | SWITCH, unwired-LINE SELECTOR |
| 63 | 384-0408-00 |  |  | 1 | ROD, extension |
|  | 426-0289-00 |  |  | 1 | MOUNT, plastic |
|  | $210-0801-00$ |  |  | 2 | mounting hardware: (not included w/mount) WASHER, flat, $5 \mathrm{~s} \times 9 / 32$ inch |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 64 | -••••• |  |  | 1 | RESISTOR, variable |
|  | - . - |  |  | * | mounting hardware: (not included w/resistor) |
|  | 210.0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0840-00 |  |  | 1 | WASHER, flat, 0.390 ID $\times 9 / 16$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| 65 | - - - |  |  | i | mounting hardware: (not included $\mathrm{w} / \mathrm{switch}$ ) |
|  | $\begin{aligned} & 210-0012-00 \\ & 210-0413-00 \end{aligned}$ |  |  | 1 | LOCKWASHER, internal, $3 / 81 D \times 1 / 2$ inch OD NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
|  | $210-0413-00$ |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| 66 | - . . - - |  |  | 1 | RESISTOR, variable |
|  | - - - |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210.0590 .00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 16$ inch |
|  | 210.0012 .00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch |
|  | 210.0840 .00 |  |  | 1 | WASHER, flat, $0.39010 \times 9 / 16$ inch OD |
|  | 210-0413.00 |  |  | 1 | NUT, hex., $/ 8-32 \times 1 / 2$ inch |



CHASSIS


CHASSIS (Cont'd)


CHASSIS (Cont'd)

| $\begin{array}{\|l\|} \hline \text { REF. } \\ \text { NO. } \end{array}$ | PART NO. | SERIAL/MODEL NO. |  | $\begin{aligned} & 0 \\ & \mathbf{1} \\ & \mathbf{Y} \\ & \hline \end{aligned}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC |  |  |
| 28 | $\begin{aligned} & 136-0015-00 \\ & 213-0044-00 \end{aligned}$ |  |  | $\begin{aligned} & 4 \\ & 2 \\ & 2 \end{aligned}$ | SOCKET, STM9G mounting hardware for each: (not included w/socket) SCREW, thread cutting, $5-32 \times 3 / 16$ inch PHS phillips |
| 29 | $\begin{aligned} & 131-0183-00 \\ & 358-0136-00 \end{aligned}$ |  |  | 2 <br> - | CONNECTOR, terminal feed-through mounting hardware for each: (not included w/connector) BUSHING, teflon |
| 30 31 | $\begin{aligned} & 348-0056-00 \\ & \cdots \\ & 210-0840-00 \\ & 210-0413-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 6 \\ & i \\ & 1 \end{aligned}$ | GROMMET, plastic, $3 / 8$ inch POT <br> mounting hardware for each: (not included w/pot) WASHER, 390 ID $\times 9 / 16$ inch OD NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
| 32 | $\cdots \cdots$ $211-0544-00$ $211-0553-00$ $210-0601-00$ $210-0478-00$ $211-0507-00$ | $\begin{aligned} & 100 \\ & 620 \\ & \times 620 \end{aligned}$ | 619 | $\begin{aligned} & 1 \\ & - \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | RESISTOR <br> mounting hardware: (not included w/resistor) SCREW, $6-32 \times 3 / 4$ inch THS phillips SCREW, $6-32 \times 1 \frac{1}{2}$ inches RHS phillips EYELET, brass NUT, hex, resistor mounting SCREW, $6-32 \times 5 / 16$ inch BHS |
| $\begin{aligned} & 33 \\ & 34 \end{aligned}$ | $\begin{gathered} 348-0031-00 \\ \cdots \cdots \\ 210-0046-00 \\ 210-0940-00 \\ 210-0583-00 \end{gathered}$ |  |  | $\begin{aligned} & 5 \\ & 2 \\ & - \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | GROMMET, snap-in POT mounting hardware for each: (not included w/pot) LOCKWASHER, internal, . 400 OD $\times .261$ inch ID WASHER, $1 / 4$ ID $\times 3 / 8$ inch OD NUT, hex, $1 / 4-32 \times 3 / 16$ inch |
| 35 | 200-0247-00 | 100 | 149X | 3 | CAP, pot |
| 36 | $\begin{gathered} \cdots \cdots \\ 210-0207-00 \\ 210-0012-00 \\ 210-0840-00 \\ 210-0413-00 \end{gathered}$ |  |  | 2 - 1 1 1 | POT <br> mounting hardware for each: (not included w/pot) LUG, solder, $3 / 8$ inch <br> LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch WASHER, 390 ID $\times 9 / 16$ inch OD NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
| 37 | 348-0055-00 |  |  | 1 | GROMMET, plastic, $1 / 4$ inch |
| 38 | 200-0385-00 | X150 | 4849X | 1 | COVER, transistor |
| 39 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 150 \end{aligned}$ | 149 | 5 5 $i$ | SOCKET, 3 pin transistor SOCKET, 4 pin transistor mounting hardware for each: (not included w/socket) RING, locking, transistor socket |

CHASSIS (Cont'd)

| $\begin{aligned} & \text { REF. } \\ & \text { NO. } \end{aligned}$ | PART NO. | SERIAL/MODEL NO. |  | $\begin{aligned} & \hline \mathbf{a} \\ & \mathbf{r} \\ & \mathbf{Y} \end{aligned}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 40 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & \hdashline- \\ & 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 560 \end{aligned}$ | 559 | $\begin{aligned} & 1 \\ & 1 \\ & i \end{aligned}$ | SOCKET, 3 pin transistor SOCKET, 4 pin transistor mounting hardware: (not included w/sockel) RING, locking, transistor socket |
| 41 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & 136-0181-00 \\ & 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 560 \\ & 1606 \end{aligned}$ | $\begin{aligned} & 559 \\ & 1605 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | SOCKET, 3 pin transistor <br> SOCKET, 4 pin transistor SOCKET, 3 pin transistor mounting hardware: (not included w/socket) RING, locking, transistor socket |
| 42 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & 136-0181-00 \\ & \hdashline- \\ & 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 150 \\ & 1606 \end{aligned}$ | $\begin{aligned} & 149 \\ & 1605 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | SOCKET, 3 pin transistor <br> SOCKET, 4 pin transistor SOCKET, 3 pin transistor mounting hardware: (not included w/socket) RING, locking, transistor socket |
| 43 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 1910 \end{aligned}$ | 1909 | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | SOCKET, 3 pin transistor SOCKET, 4 pin transistor mounting hardware: (not included w/socket) RING, locking, transistor socket |
| 44 | $\begin{aligned} & 426-0121-00 \\ & 361-0007-00 \end{aligned}$ | 100 | 1909X | $\begin{aligned} & 1 \\ & i \end{aligned}$ | MOUNT, toroid mounting hardware: (not included w/mount) SPACER, nylon, 0.063 inch |
| 45 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & 136-0181-00 \\ & \hdashline-\cdots \\ & 354-0234-00 \end{aligned}$ | $\begin{array}{\|l} 100 \\ 150 \\ 1910 \end{array}$ | $\begin{aligned} & 149 \\ & 1909 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \\ & 2 \\ & - \\ & \hline \end{aligned}$ | SOCKET, 3 pin transistor <br> SOCKET, 4 pin transistor <br> SOCKET, 3 pin transistor mounting hardware for each: (not included w/socket) RING, locking, transistor socket |
| 46 | $\begin{aligned} & 136-0181-00 \\ & 136-0182-00 \\ & \hdashline 354-0234-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 4026 \end{aligned}$ | 4025 | 2 2 - 1 | SOCKET, 3 pin transistor SOCKET, 4 pin transistor mounting hardware for each: (not included w/socket) RING, locking, transistor socket |



REAR


REAR (Cont'd)

| REF. | PART NO. | SERIAL/MODEL NO. |  | $\stackrel{9}{1}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Part NO. | EFF. | DISC. | Y. |  |
| 12 | 385-0018-00 |  |  | 2 | ROD, nylon |
| 13 | 392-0166-00 |  |  | 1 | BOARD, rectifier |
|  | - - - - - |  |  | - | mounting hardware: (not included w/board) |
|  | 211-0558-00 |  |  | 6 | SCREW, $6.32 \times 1 / 4$ inch BH nylon |
| 14 | 346-0001-00 |  |  | 1 | STRAP, mounting, high voltage transformer |
|  | - - . . - |  |  | - | mounting hardware: (not included w/strap) |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210.0406-00 |  |  | 2 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 15 | 210-0201-00 |  |  | 1 | LUG, solder, SE \#4 |
|  | - . . - |  |  |  | mounting hardware: (not included w/lug) |
|  | 213-0044-00 |  |  | 1 | SCREW, thread cutting, 5-32 $\times 3 / 16$ inch PHS phillips |
| 16 | 386-0111-00 |  |  | 1 | PLATE, right side |
|  | - . - - |  |  | - | mounting hardware: (not included w/plate) |
|  | 212-0004-00 |  |  | 3 | SCREW, 8-32 $\times 5 / 16$ inch BHS |
|  | 212-0070-00 |  |  | 6 | SCREW, $8.32 \times 5 / 16$ inch FHS phillips |
|  | 210-0458-00 |  |  | 9 | NUT, keps, $8-32 \times 11 / 32$ inch |
| 17 | $\cdots$ |  |  | 2 | SEE STANDARD ACCESSORIES |
| 18 | 351-0040-00 | 100 | 1729 | 1 | SLIDE, chassis track, slide \& guide, 1 pair (w/mounting hardware) |
|  | $351-0040-01$ | 1730 |  | 1 | TRACK, guide, 1 pair ( $w /$ mounting hardware) |
| 19 | 214-0538-00 |  |  | 1 | SPRING, ground wire |
| 20 | 214-0539-00 |  |  | 1 | SPRING, retainer wire |
| 21 | 136-0215-00 |  |  | 1 | SOCKET, relay |
|  | … . . |  |  | - | mounting hardware: (not included $w /$ socket) |
|  | 211-0008-00 |  |  | 1 | SCREW, $4-40 \times 1 / 4$ inch BHS |
|  | 210-0004-00 |  |  | 1 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 1 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 222324 | 348-0056-00 |  |  | 4 | GROMMET, plastic, $3 / 8$ inch |
|  | 200-0247-00 | 100 | 149X | 1 | CAP, pot |
|  | 352-0044-00 |  |  | 1 | HOLDER, crt coil form |
|  | - . . - - |  |  | - | mounting hardware: (not included w/holder) |
|  | $211-0011-00$ |  |  | 1 | SCREW, $4-40 \times 5 / 16$ inch BHS |
|  | 210-0004-00 |  |  | 1 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 1 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 25 | 124-0167-00 |  |  | 1 | STRIP, crt shield |
|  | 337-0725-00 |  |  | 1 | SHIELD, crt |
|  | - - - - |  |  | - | mounting hardware: (not included w/shield) |
|  | 211-0534-00 |  |  | 7 | SCREW, 6-32 $\times 5 / 16$ inch PHS w/lockwasher |
|  | 210.0803-00 |  |  | 7 | WASHER, $6 \mathrm{~L} \times 3 / 8$ inch |
|  | 210-0457-00 |  |  | 7 | NUT, keps, $6-32 \times 5 / 16$ inch |
| 27 | 175-0585-00 |  |  | 1 | WIRE, crt lead, .290 foot, striped brown, w/connector |
|  | 175-0588-00 | 100 | 149X | 1 | WIRE, crt lead, 833 foot, striped orange, w/connector |
|  | 175-0592-00 |  |  | 1 | WIRE, crt lead, . 960 foot, striped green, w/connector |
|  | 175-0593-00 |  |  | 1 | WIRE, crt lead, .333 foot, striped blue, w/connector |
|  | 175-0595-00 |  |  | 1 | WIRE, crt lead, 960 foot, striped red, w/connector |

REAR (Cont'd)

| $\left.\begin{array}{\|l\|} \hline \text { REF. } \\ \text { NO. } \end{array} \right\rvert\,$ | PART NO. | SERIAL/MODEL NO. |  | 9 1 | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | Disc. | Y. |  |
| 28 | 131-0081-00 |  |  | 5 | CONNECTOR, coaxial, 1 contact, UHF |
| 29 | 131-0064-00 |  |  | 4 | CONNECTOR, coaxial, 1 contact, UHF |
|  | - - - - |  |  | - | mounting hardware for each: (not included w/connector) |
|  | 211-0025-00 |  |  | 2 | SCREW, $4.40 \times 3 / 8$ inch, FHS |
|  | 210-0224-00 |  |  | 1 | LUG, solder, \#10 |
|  | 210-0812-00 |  |  | 2 | WASHER, fiber, \#10 |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 30 | 406-0244-00 |  |  | 1 | BRACKET, coaxial insulator |
| 31 | 136-0089-00 |  |  | 1 | SOCKET, 9 pin w/female insert |
|  | - . - - |  |  |  | mounting hardware: (not included w/socket) |
|  | 211-0011-00 |  |  | 4 | SCREW, 4-40 $\times 5 / 16$ inch, BHS |
|  | 210-0004-00 |  |  | 3 | LOCKWASHER, internal, \#4 |
|  | 210-0201-00 |  |  | 1 | LUG, solder, SE \#4. |
|  | 210-0406-00 |  |  | 4 | NUT, hex, $4-40 \times 3 / 16$ inch |
| 32 | 214-0210-00 |  |  | 1 | SPOOL, solder, assembly |
|  | - $-0 \cdot 0$ |  |  | - | spool assembly includes: |
|  | 214-0209-00 |  |  | 1 | mounting hardware: (not included w/spool) |
|  | 361-0007-00 |  |  | 1 | SPACER, nylon, 063 inch |
| 33 | 352-0025-00 |  |  | 1 | HOLDER, fuse, dual |
|  | - - - - |  |  | - | mounting hardware: (not included w/holder) |
|  | 211-0510-00 |  |  | 2 | SCREW, $6-32 \times 3 / 8$ inch, BHS |
|  | 210.0006-00 |  |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210-0407-00 |  |  | 2 | NUT, hex, $6-32 \times 1 / 4$ inch |
| 34 | 214-0517-00 |  |  | 1 | HEAT SINK |
|  | - . -- - |  |  | - | mounting hardware: (not included w/heat sink) |
|  | 212-0033-00 |  |  | 4 | SCREW, $8-32 \times 3 / 4$ inch, BHS |
|  | 210-0458-00 |  |  | 4 | NUT, keps, $8-32 \times 11 / 32$ inch |
| 35 | - - |  |  | 2 | TRANSISTOR |
|  | $211-0504-00$ |  |  | 2 | mounting hardware for each: (not included w/transistor) SCREW, $6.32 \times 1 / 4$ inch, BHS |
|  |  |  |  |  |  |
| 36 | 352-0002-00 |  |  | 1 | HOLDER, fuse, assembly |
|  | - . . . - |  |  | - | holder assembly includes: |
| 3738 | 352-0010-00 |  |  | 1 | HOLDER, fuse |
|  | 210-0873-00 |  |  | 1 | WASHER, rubber |
|  | … - |  |  | 1 | NUT, fuse holder |
| 39 | 200-0582-00 |  |  | 1 | CAP, fuse |
|  | 179-0954-00 |  |  | 1 | CABLE HARNESS, crt, assembly cable harness includes: |
| 41 | 136-0216-00 |  |  | $i$ | SOCKET, crt, assembly |
|  | - . - |  |  | - | socket assembly includes: |
| 4243 | 136-0202-01 | X150 |  | 1 | SOCKET, crt |
|  | 214-0464-00 |  |  | 14 | Socket includes: |
|  | 200-0616-00 | $\times 150$ |  | 1 | COVER, crt socket |

REAR (Cont'd)

| REF. <br> No | PART NO. | SERIAL/MODEL NO. |  | $\begin{aligned} & \hline \mathbf{O} \\ & \mathbf{T} \\ & \mathbf{Y} \\ & \hline \end{aligned}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC |  |  |
| 44 | 354-0249-00 |  |  | 1 | RING, crt clamping, assembly |
|  | - - . |  |  | - | ring includes: |
| 45 | 124-0171-00 |  |  | 1 | STRIP, liner, crt clamp |
|  | $\cdots$ |  |  |  | mounting hardware: (not included w/ring) |
| 46 | $211.0576-00$ |  |  | 2 | SCREW, $6-32 \times 7 / 8$ inch, socket head cap |
|  | 210-0949-00 |  |  | 2 | WASHER, $9 / 64$ ID $\times 1 / 2$ inch OD |
| 47 | 214.0207-00 |  |  | 1 | NUT, adjustment, securing |
| 48 | 406-0730-00 |  |  | 1 | BRACKET, adjustment |
|  | $\cdots$ |  |  | - | mounting hardware: (not included w/bracket) |
|  | 211-0534-00 |  |  | 4 | SCREW, $6-32 \times 5 / 16$ inch, PHS w/lockwasher |
|  | 210-0803-00 |  |  | 4 | WASHER, $6 \mathrm{~L} \times 3 / 8$ inch |
|  | 210-0006-00 |  |  | 4 | LOCKWASHER, internal, \#6 |
|  | 210.0407-00 |  |  | 4 | NUT, hex, $6.32 \times 1 / 4$ inch |
| 49 | 211-0560-00 |  |  | 1 | SCREW, $6.32 \times 1$ inch, RHS |
| 50 | 220-0419-00 |  |  | 1 | NUT, square, $6-32 \times 5 / 16$ inch |
| 51 | 386-0107-00 |  |  | 1 | PLATE, bulkhead |
| 52 | 334-0904-00 |  |  | 1 | TAG, voltage rating |
|  | 213-0088-00 |  |  | 2 | mounting hardware: (not included w/tag) SCREW, thread forming, $4-40 \times 1 / 4$ inch, PHS phillips |
| 53 | 161-0017-00 |  |  | 1 | CORD, power |
| 54 | 358-0025-00 |  |  | 1 | BUSHING, strain relief |
| 55 | 386-0110-00 |  |  | 1 | PLATE, rear |
| 56 | 348-0067-00 | 100 | 589 | 1 | GROMMET, delrin, 5/16 inch |
|  | 358-0215-00 | 590 |  | 1 | BUSHING, plastic, black |
| 57 | $348-0063-00$ | 100 | 786 | 1 |  |
|  | 348-0064-00 | 787 |  | 1 | GROMMET, delrin, $5 / 8$ inch |
| 58 | 337-0830-00 | X2997 |  | 1 | SHIELD, high voltage mounting hardware: (not included w/shield) |
|  | 211-0507-00 |  |  | 2 | SCREW, $6.32 \times 5 / 16$ inch, PHS |
|  | 211-0538-00 |  |  | 2 | SCREW, $6.32 \times 5 / 16$ inch, FHS |
|  | 210-0803-00 |  |  | 2 | WASHER, flat, $0.150 \mathrm{ID} \times 3 / 8$ inch OD |
|  | 210-0457-00 |  |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| 59 | - - - - | X2997 |  | 1 | RESISTOR, variable |
|  | $210-0207-00$ |  |  | 1 | mounting hardware: (not included w/resistor) LUG, solder, $3 / 8 \mathrm{ID} \times 5 / 8$ inch OD, SE |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0840-00 |  |  | 1 | WASHER, flat, $0.390 \mathrm{ID} \times 9 / 16$ inch $O D$ |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| 60 | 386-0108-00 | 100 | 3798 | 1 | PLATE, dust cover, top |
|  | $\begin{aligned} & 386-1097-00 \\ & \hdashline-- \\ & 211-0504-00 \end{aligned}$ | 3799 |  | $\begin{aligned} & 1 \\ & 6 \end{aligned}$ | PLATE, dust cover, top mounting hardware: (not included w/plate) SCREW, $6-32 \times 1 / 4$ inch BHS |

## CABLE HARNESS \& CERAMIC STRIP DETAIL



CABLE HARNESS \& CERAMIC STRIP DETAIL




IMPORTANT

## VOLTAGE AND WAVEFORM CONDITIONS

Circuit voltages measured with a $20,000 \Omega /$ volt VOM. All readings in volts. Voltages are measured with respect to chassis ground unless otherwise noted.

Waveforms shown are actual waveform photographs taken with a Tektronix Oscilloscope Camera System and Projected Graticule.

Voltages and waveforms on the schematics (shown in blue) are not absolute and may vary between instruments.

The test oscilloscope used had the following characteristics: Minimum deflection factor, 0.02 volts/division using a 10 X probe; frequency response, de to 30 MHz ; sweep rates, 5 ms to $20 \mu \mathrm{~s}$; sweep magnification, $\mathrm{X} 1, \mathrm{X} 20$ and X 100 . AC input coupling was used.

To indicate true time relationship between signals and to obtain stable displays, the test oscilloscope was externally triggered through X1 probe form:

1. Collector of Q325 (-H signal) for all waveforms except those at the junctions of C198 and R198, C364 and R365, C417 and the Collector of Q415.
2. Collector of Q344 for waveforms at the junctions of C198 and R198, C364 and R365, C417 and the collector of Q415.

Voltage readings and waveforms were obtained using the following control settings, unless otherwise noted on the individual diagrams.

For waveforms, 1 -volt of modulated staircase was connected to the left VIDEO INPUTS A connector. The right VIDEO INPUTS A connector was terminated into 75 ohms.

For voltage readings, no input signal or termination was connected to the instrument.

POWER and SCALE ILLUM
FOCUS
INTENSITY
GAIN
VERTICAL Controls

## RESPONSE

DC RESTORER
INPUT
VOLTS FULL SCALE
VARIABLE (VOLTS FULL SCALE)
CAL
POSITION
HORIZ Controls
POSITION
SYNC
MAG
DISPLAY
LINE SELECTOR (SWITCH)
FIELD
VARIABLE (LINE SELECTOR)

## 2/3 clockwise

Midrange
Adjusted for normal display brightness
As is

FLAT
ON
A
1.0

CALIB
.714 F.S.
Midrange

Midrange
INT
X 1
LINE SELECTOR . $25 \mathrm{H} / \mathrm{cm}$
Variable
TWO
Fully clockwise





REFERENCE DIAGRAMS
(1) vertical amplifier
3) dC RESTORER
5. Field selector
6. LINE SELECTOR
(7) Sweep generator

SEE PARTS LIST FOR
SEMICONDUCOR TYPES






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(1) VERTICAL AMPLIFIER
(3) DC RESTORER
4) SYNC SEPARATOR


## SECTION 10

## RACKMOUNTING

## Mounting Method (Figs. 10-1 and 10-2)

This instrument will fit most commercial consoles and most 19 -inch wide racks whose dimensions conform to EIA specifications.

Fig. 10-1 shows the instrument installed in a cabinet type rack with slideout tracks. The instrument is locked into the rack by means of pawl fasteners. When the RELEASE knobs on the front panel are turned to release the instrument, the instrument can be pulled out of the rack like a drawer to its fully extended position (see Fig. 10-2) and then tilted up about $100^{\circ}$. This position permits many routine maintenance functions to be performed without completely removing the instrument from the rack. The slideout tracks easily mount to the cabinet or relay type rack front and rear vertical mounting rails if the inside distance between front and rear rails is within $10 \% / 16$ inches to $243 / 8$ inches.

Some means of support (for example, make extensions for the rear mounting brackets) is needed to support the rear ends of the slideout tracks if the tracks are going to be installed in a cabinet rack whose inside dimension between front and rear rails is not the proper distance $10 \% / 16$ inches to $243 / 8$ inches).

## Instrument Dimensions and Weight

The last pullout page in this section shows dimensional drawings exclusive of the power cord and hables.

## Rack Dimensions

Width-A standard 19 inch rack may be used. The dimension of opening between the front rails of the rack must be at lease $175 / 8$ inches for a cabinet type rack in which the front lip of the stationary section is mounted behind the front rail as shown in Fig. 10-5B. This dimension allows room on each side of the instrument for the slideout tracks to operate so the instrument can move freely in and out of he rack.

Depth—For proper circulaion of cooling air, allow at least 2 inches clearance behind the rear of the instrument and any enclosure on the rack (see dimensional drawings). At least that much space is also needed for the coaxial cables (unless $90^{\circ}$ adapters are used) so they are not bent too sharply. If it is sometimes necessary or desirable to operate the Type RM529 in the fully extended position, use cables that are long enough to reach from the signal source to the instrument.

## Rackmounting in a Cabinet Rack (Fig. 10-2)

## General Information

The slideout tracks for the instrument consist of two assemblies, one each for the right and left sides. Each assembly consists of three sections as illustrated in Fig. 10-3. The stafionary section attaches to the fron and rear rails of he rack with inside dimensions as shown in Fig. 10-2, the chassis sec-
tion attaches to the instrument, and the intermediate section to allow the instrument to fully extend out of the rack.

The small hardware components included with the slideout track assemblies are shown in Fig. 10-4. The hardware shown in Fig. 10-4 is used to mount the slideout tracks to the rack rails having this compatibility; from and rear rail holes must be large enough to allow inserting a \#10-32 screw; rail holes must be located on EIA/RETMA/Western Electric or Universal spacing. Because of the above compatibility, there will be some parts left over.

## Stationary and Intermediate Sections Installation

The stationary and intermediate sections for both sides of the rack are shipped as a matched set and should not be separated. The matched sets for both sides are marked 351-0042-02 on the packabe. Use the following procedure to mount both sets. See Fig. 10-5 for installation details.

## NOTE

If $\mathbf{i}$ is desired to mount the rear of the stationary sildeout track sections without the bar nuts, then one hole must be drilled and tapped for a \#10-32 screw in each rear rail. To locate the desired hole: mount the front of the stationary slideout track section; level the stationary section and mark the required hole location.

1. If the instrument is to be mounted directly above or below another instrument in the cabinet rack, select the appropriate holes in the front rack rails for the stationary sections using Fig. 10-5C as a guide.
2. Mount the stationary slideout track sections to the front rack rails using Fig. 10-5B as a guide.
3. If the rear rack rail holes have been drilled and tapped as described above for \#10-32 machine screws, mount the left stationary section with hardware provided as shown in Fig. 10-5A. Using Fig. 10-5A as a guide, mount the right stationary section in the same manner.
4. If the rear rack rail holes are not drilled and tapped as described above to accept 10-32 machine screws, mount the left stationary section with hardware provided as shown in Fig. $10-5 B$. Using Fig. $10-5 B$ as a guide, mount the right stationary section in the same manner.

## Adjustments

To adjust the slideout tracks for smooth operation, proceed as follows:

1. Insert the instrument into the rack as shown in Fig. 10-6.
2. Adjust the slideout tracks for proper spacing as shown in Fig. 10-7.

## Maintenance

The slideout tracks require no lubrication. The special gray finish on the sliding parts is a permanent lubrication.


Fig. 10-3. Illustration showing the slideout track assembly for the right side.


Fig. 10-2. The Type RM529 supported by slideout tra cks mounted between front and rear cabinet rack rails.

Fig. 10-1. The Type RM529 installed in cabinet type rack.


Fig. 10-4. Small hardware components for mounting the stationary sections to the rack rails.


Fig. 10-5. Mounting the left stationary section with its matched intermediate section (not shown) to rack rails.


Fig. 10-6. Installing and removing the instrument.


Fig. 10-7. Adjusting the slideout tracks for smooth sliding action


REAR VIEW



NOTES

1. ALL DIMENSIONS ARE REFERENCE DIMENSIONS EXCEPT AS NOTED
2. SUBJECT TO APPROXIMATELY $\pm 0.047$ DEVIATION

TYPE RM529


## MANUAL CHANGE INFORMATION

At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested.

Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages. If it does not, your manual is correct as printed.

## PARTS LIST \& SCHEMATIC CORRECTION

CHANGE TO:

| R478 | $315-0183-00$ | 18 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| R847 | $315-0124-00$ | 120 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |
|  |  |  |  |  |
| V859 | $154-0514-00$ | CRT, T5291-31 | 6.4 KV |  |

## TEXT CORRECTION

Section 3 Circuit Description
Page 3-17
Sub-Title: CRT Circuit and Calibrator
ADD: After paragraph two;
The bias network consisting of R855, R856 and R857 insures wiform intensity of the CRT horizontal trace. This is accomplished by varying the voltage applied to the fixed unblanking plate.

Section 6
Calibration
Page 6-9
ADD: After atep 6, Adjust CRT BEAM ROTATOR R655
6A. Adjust UNBLANKING PLATE BIAS (R855)
a. Set the INPUT switch to A (no aigal applied to VIDEO INPUT A conmector).
b. Adjust the INTENSITY control so the CRT trace is barely visible.
c. Check for uniform intenaity along the horizontal axis.
d. Adjust the UNBLANKING PLATE BIAS (R855) for uniform intensity along the horizontal axis.

PARTS LIST CORRECTION

CHANGE TO:
Q544 151-0190-00 Silicon $2 N 3904$

ADD:
D555
152-0185-00
Silicon
6185

SCHEMATIC CORRECTION


PARTIAL
HORIZONTAL AMPLIFIER

TYPE 529
TYPE RM529

TENT SN 2680
TENT SN 5700

PARTS LIST CORRECTION

CHANGE TO:
Q533
151-0188-00
2N3906

TYPE 529
TYPE RM529

TENT SN 2740
TENT SN 5800

## PARTS LIST CORRECTION

CHANGE TO:
Q474
151-0150-00
Silicon
2N3440

TYPE RM529 -- TENT SN 6110

## PARTS LIST CORRECTION

CHANGE TO:

| Unwired |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SW520 260-0656-01 | Rotary |  |  |  |  |


[^0]:    ${ }^{3}$ An optional method of checking high-frequency response of the vertical amplifier will be found in step 33.

